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Institut für Neutronenphysik und Reaktortechnik
Projekt Schneller Brüter

MIGRØS-3:

**A Code for the Generation of Group Constants for
Reactor Calculations from Neutron Nuclear Data
in KEDAK Format**

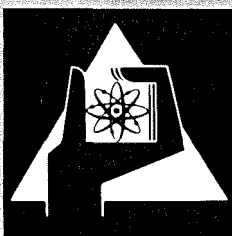
Compiled by:

I. Broeders, B. Krieg

with Contributions from:

C. H. M. Broeders, I. Broeders, F. H. Fröhner

B. Krieg, E. Stein, H. W. Wiese



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Abstract:

The code MIGRØS-3 was developed from MIGRØS-2. The main advantage of MIGRØS-3 is its compatibility with the new conventions of the latest version of the Karlsruhe nuclear data library, KEDAK-3. Moreover, to some extent refined physical models were used and numerical methods were improved.

MIGRØS-3 allows the calculation of microscopic group cross sections of the ABBN type from isotopic neutron data given in KEDAK-format. All group constants, necessary for diffusion-, consistent P_1 - and S_N -calculations can be generated. Anisotropy of elastic scattering can be taken into account up to P_5 .

A description of the code and the underlying theory is given. The input and output description, a sample problem and the program lists are provided.

MIGRØS-3: Ein Code zur Erzeugung von Gruppenkonstanten für Reaktorrechnungen
aus Neutronen-Kerndaten im KEDAK-Format

Zusammenfassung:

Der Code MIGRØS-3 ist eine Weiterentwicklung von MIGRØS-2. Der Hauptvorteil von MIGRØS-3 gegenüber MIGRØS-2 ist, daß in MIGRØS-3 die in der letzten Version der Karlsruher Kerndatenbibliothek KEDAK-3 eingeführten neuen Konventionen berücksichtigt werden. Darüber hinaus wurden teilweise verfeinerte physikalische Modelle und verbesserte numerische Methoden benutzt.

MIGRØS-3 erlaubt die Berechnung von mikroskopischen Gruppenwirkungsquerschnitten vom ABBN Typ für isotoneweise gegebene Neutronendaten im KEDAK-Format. Alle für Diffusions-, konsistente P_1 - und S_N -Rechnungen benötigten Gruppenkonstanten können erzeugt werden. Dabei kann die Anisotropie der elastischen Streuung bis P_5 berücksichtigt werden.

Der Code und die zugrunde liegende Theorie werden beschrieben. Es werden die Eingabe- und Ausgabebeschreibung, ein Rechenbeispiel und die Programmlisten bereitgestellt.

Table of contents

Introduction

1. The organization of MIGRØS-3
2. Description of the input and the output
3. The calculation of weighted group averages for infinite dilution.
Module 4.
B. Krieg
4. The calculation of average group cross sections for infinite dilution and of energy resonance self-shielding factors from resolved-resonance parameters. Module 1.
F. Fröhner
(H. Huschke, B. Krieg)⁺
5. The calculation of average group cross sections for infinite dilution and of energy resonance self shielding factors from statistical resonance parameters. Module 2.
I. Broeders
(H. Huschke, B. Krieg)⁺
6. The calculation of the normalized transfer matrices for inelastic scattering, (n,2n)- and (n,3n)-reactions. Module 5.
I. Broeders
7. The calculation of normalized elastic-scattering matrices and of elastic and total group cross sections. Module 6.
H.W. Wiese
8. The calculation of the interval cross sections and the zero'th and higher moments of the normalized elastic transfer elements for the REMO-correction. Module 9.
C.H.M. Broeders
(P. Vertes)⁺

⁺) The authors given in parentheses are the authors of the original modules as described in /1/.

9. The calculation of average group cross sections for infinite dilution and of energy resonance self-shielding factors from energy pointwise data. Module 3.
E. Stein
10. The calculation of group constants in the thermal group. Module 10.
B. Krieg
11. The calculation of weighted $1/v$ -average group values. Module 8.
B. Krieg
12. The calculation of fission spectra. Module 7.
B. Krieg

Appendix A Sample problem

Appendix B Program listing

Listing of the tables, given in chapters 1 and 2:

- Table I : Computational modules of MIGRØS-3, their tasks and their subroutines and functions.
- Table II : Overlay structure of MIGRØS-3.
- Table III : Structure of the central data array XL.
- Table IV : Structure of the unlabeled COMMON array.
- Table V : Symbols used in the printed output of MIGRØS-3.
- Table VI : Arrangement of the unformatted output.

INTRODUCTION

The code MIGRØS-3 has been further developed from MIGRØS-2, described in /1/. MIGRØS-3 is compatible with the latest version of the Karlsruhe nuclear data file KEDAK-3, /2/. That means the formal differences between KEDAK-2 and KEDAK-3 have been taken account of in MIGRØS-3. These main formal differences are

1. Introduction of an individual energy grid for each data type of each isotope, within which the data can be obtained by linear interpolation. (On KEDAK-2 the same energy grid was used for all data types of one isotope.)
2. Introduction of new data types.

Moreover the physical and numerical approaches have been improved in many of the modules.

A more detailed description of the changes in each module is given in the corresponding chapters (chapters 4 - 12).

MIGRØS-3 calculates microscopic group constants for isotopes given in KEDAK format. These can be used for the production of macroscopic group cross sections for diffusion-, consistent P_1 - and S_n -calculations. Anisotropy of elastic scattering can be taken into account up to P_5 in S_{N-P_L} - or S_{N-T_L} -approximations (higher order transport approximations /6/). Microscopic elastic scattering transfer matrices can be calculated with fine-structure weighting functions generated for special material mixtures (specified by the input; module 6) and as basic data for the REMO-correction, where mixture-dependent fine-structure weighting is performed in GRUCAL, /5/, during the computation of macroscopic cross sections, /4/, (module 9). Resonance self shielding is treated according to the method developed by ABBN, /3/.

In the following a brief description is given of the calculation of the different types of group constants in modules 1 to 10 of MIGRØS-3.

The calculation of weighted average group constants from pointwise data on KEDAK. (Chapter 3, module 4)

Weighted average group cross sections for infinite dilution are calculated from pointwise tabulated data for all reaction types given on KEDAK. Besides this weighted group values are provided for the average elastic scattering cosine, $\bar{\mu}$, for the number of secondary neutrons per fission, ν , for the ratio of capture to fission cross section, α , and for the number of fission neutrons per neutron absorption, η .

Integrations are carried out by a trapezoidal rule. In the case of an energy pointwise weighting spectrum the energy points of KEDAK and of the weighting function are used as integration grid. If the weighting spectrum is given as analytic function, an automatic interval subdivision is used, starting with the KEDAK points as integration grid.

The calculation of energy resonance self-shielding factors and group cross sections for infinite dilution from resolved resonance parameters and from statistical resonance parameters. (Chapters 4 and 5, modules 1 and 2)

For capture, fission and elastic scattering flux-weighted ($w(E) \sim \frac{1}{\sigma_t(E) + \sigma_0}$) resonance self-shielding factors and for elastic scattering and the total neutron reaction current-weighted ($w(E) \sim \left\{ \frac{1}{\sigma_t(E) + \sigma_0} \right\}^2$) self-shielding factors dependent on temperature and on the background cross section σ_0 and the average group cross sections are calculated from resonance parameters.

In the resolved-resonance region Breit-Wigner single level parameters and Doppler-broadened line shape functions are used. Interference between potential and resonance scattering and the overlapping of resonances is taken into account exactly. Integrations are carried out by a trapezoidal rule with automatic interval subdivision. The integration starts with the resonance energies and the group boundaries as interval limits.

In the unresolved resonance region an analytical model, based on average resonance parameters and χ^2 -distributions for the parameters, is used. Interference between potential and resonance scattering is partly taken into account. Overlapping of resonances is considered approximately. For the calculation of the statistical averages an approximate procedure of numerical integration is used.

The calculation of average group cross sections for infinite dilution and of energy resonance self-shielding factors from energy pointwise data.

(Chapter 9, module 3)

The module calculates flux weighted average group cross sections for infinite dilution and σ_0 -dependant (also flux weighted) energy resonance self-shielding factors for the cross section types σ_c (capture) resp. σ_a (absorption), σ_f (fission), σ_e (elastic scattering), and the product $\sigma_e \cdot \bar{\mu}_e$. For the total reaction and the product $\sigma_e \cdot \bar{\mu}_e$ additionally current weighted quantities are produced.

Both the flux weighted and the current weighted quantities can only be calculated for the temperature for which the cross sections are stored on the KEDAK library.

The grid, which is used as integration base, is composed out of the grids of all participating cross sections (and eventually the grid of the weighting function). Within an integration interval, which is defined by two adjacent energy points of the composed grid, the numerical Romberg integration method is used to compute the various integrals. If the expression of the weighting function is known, these integrals can also be solved analytically.

The calculation of normalized elastic-scattering matrices up to the fifth Legendre-order, of total elastic flux-weighted and of total group cross sections with moment-dependent weighting. (Chapter 7, module 6)

Group-to-group transfer elements are calculated from the Legendre-moments of the elastic scattering kernel for $l = 0, 1, \dots, 5$. Different options for the approximation of the moments of neutron flux density to be used as weighting functions are built in. Weighting dependent on l with $\psi_l(E) = F(E) / |\Sigma_t(E)|^{l+1}$ is recommended, $F(E) =$ total collision density, $\Sigma_t(E) =$ total macroscopic cross section of the reactor subzone under consideration. Required data are: tabulated elastic angular distributions in the c.m.-system with a unique angular grid for each isotope, total elastic, total reaction cross sections, and mean elastic scattering cosines in the laboratory system. For one isotope the energy grids for the elastic distributions, the cross sections and the scattering cosines may be different. Different isotopes may have different distribution cosine grids. Energy and angle interpolation of the scattering distributions (after transformation into the laboratory system) is achieved with polynomials up to degree three. Integration over the in-scattering group is performed as integration over the corresponding angular interval with use of Simpson's rule, the weighted integration over the out-scattering group is

done with an improved trapezoid technique. Special account is taken of strongly fluctuating integrands in case of higher l -values as well as in resonance regions of Σ_t . Total flux weighted elastic and ψ_l -weighted total reaction group cross sections (the latter for higher transport approximations) are computed with the modified trapezoid technique.

The calculation of the interval cross sections and the zero'th and higher moments of the normalized elastic transfer elements for the REMO correction. (Chapter 8, module 9)

The REMO correction, described in chapter 3.5 of /4/, improves the treatment of the elastic downscattering in a coarse energy group system (≈ 26 energy groups). For a material mixture the coarse group scattering matrix is calculated with the help of the mixture weighting spectrum in a narrow resonance approximation, e.g. with the program GRUCAL /5/. The coarse-group system is subdivided into a number of fine groups with intervals. (Usually 14 fine groups with 6 intervals each.)

MIGRØS calculates the following input for the REMO correction:

- weighted scalar group constants for the KEDAK reaction types SGT, SGN and MUEL. For the integration the trapezoidal rule is applied with the energy mesh points from KEDAK.
- weighted transfer probabilities from interval to in-scattering group. The required angle and energy integrations are performed with the Romberg method over the whole energy region to be calculated. If no angular distributions are available on KEDAK linear anisotropy is assumed. Generally the interpolations are linear in energy or in the cosine of the scattering angle. Only for angular distributions with a small number of angle meshpoints a cubic interpolation is applied.

The calculation of the normalized transfer matrices for inelastic scattering, $(n,2n)$ - and $(n,3n)$ -reactions. (Chapter 6, module 5)

The transfer matrix for inelastic scattering is calculated as a combination of transfer probabilities due to the excitation of discrete levels and of transfer probabilities due to the excitation of continuous levels of the residual nucleus. The energy loss of the inelastically scattered neutron is calculated from the excitation energies of the discrete levels and from evaporation models. For the calculation of the transfer matrices of $(n,2n)$ - or $(n,3n)$ -reactions evaporation models are used. The numerical integrations in connection

with the calculations of transfer probabilities due to the excitation of discrete levels are carried out by a trapezoidal rule. As integration points the combination of all energy points of the inelastic excitation cross sections and the energy points of the spectrum are used. The numerical integration in connection with the treatment of continuous excitation levels of the residual nucleus (evaporation models) are carried out by the Simpson rule.

The calculation of the fission spectra. (Chapter 12, module 7)

Fission spectra are calculated by the Watt-Cranberg formula using the fragment kinetic energy per nucleon and the Watt fragment nuclear "temperature" or by a Maxwellian distribution, using the Maxwellian fragment nuclear "temperature", depending on the information given on KEDAK.

The calculation of weighted $1/v$ -group values. (Chapter 11, module 8)

A trapezoidal rule with automatic interval subdivision is used for the integration.

Thermal cross sections

One thermal group with a Maxwellian spectrum is assumed.

As a consequence of its modular structure MIGRØS-3 is very flexible in its need of storage.

A standard input is provided internally for the production of a 26-group cross section set with the same group structure as the ABN-set, /3/, and with a $1/E$ weighting spectrum. All details of the standard input are given in the input description in chapter 2.1. If the user does not apply the standard input, he has to make sure, that his input is physically meaningful.

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- /6/ H.W. Wiese,
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1. The organization of MIGRØS-3

1.1 The logical structure of MIGRØS-3

The code MIGRØS-3 has a modular structure. It consists of a control module and of several computational modules. In the control module all the input information, except the nuclear data, is checked, the order of processing is fixed and the information for the single computational modules is prepared. A computational module is defined as a logically complete, executable computer procedure, consisting of several subroutines and functions. In a computational module a specific type of group constants is calculated. The necessary nuclear data are read from the Karlsruhe nuclear data library, KEDAK //, in the computational modules, which also produce an output of the group constants on paper and on an external storage unit. The available computational modules are given in table I.

Control is transferred from the control module to a computational module by a CALL statement, which calls the entry subroutine of the module. It is not possible to transfer control directly from one module to another. A computational module can be called by the control module several times.

All computational modules are written in FØRTRAN-IV. All arrays are variably dimensioned, when they are influenced by input information. the control module is written in FØRTRAN-IV, except for the routines GAREA and DDTEST, which are written in IBM/370 ASSEMBLER.

Since the input of nuclear data and the output of the results is performed in the computational modules, the only information that must be transferred between the control module and the computational modules is input information other than nuclear data and information necessary for the control of the program. The transfer of data is partly done by an unlabeled COMMON-array. However, most of the data transfer is accomplished by the parameter lists in the entry subroutines of the computational modules.

MIGRØS-3 is organized in an overlay structure, which is given in table II.

1.2 The control module

The control module has three tasks:

- to read all input information except the nuclear data,
- to provide a central data array and the unlabeled COMMON-array,
- to control the order of computation of the computational modules.

In the routines GAREA and MAIN a central data array is provided, whose length depends on the total region available for the program. All region not used by the program itself or for other system purposes as e.g. input/output buffers is taken as data array (see 1.3 and 2.).

In the subroutine INPUT, all input information except the nuclear data is read and checked. The central data array is prepared and the computational modules are called.

The input information is stored and the working arrays for the computational modules are provided in the central data array. It consists of two sections. One is permanent and the same for all computational modules. The other section depends on the particular module being considered and is allocated only when control is actually transferred to the module. All information of the central data array is transferred by parameter lists in the entry subroutines of the computational modules. A description is given in table III.

There is also an unlabeled COMMON-array, which is described in table IV.

1.3 The organization of the central data array XL

The ASSEMBLER routine GAREA provides a central array named XL for the subroutine MAIN. The length of XL is defined by the difference between the length given by the REGION-parameter of the JOB-card in the IBM/OS control language, the length of the MIGRØS-3 program system itself (\approx 165 K bytes) and the length of input/output buffers.

The subroutine MAIN calls the subroutine EING, which first prints an input description of the MIGRØS system. Then all the input for the first material is read and the information necessary for the variable dimensioning of the input arrays in the XL array is retained, as e.g. the number of group boundaries, the number of points of the weighting function, the number of computational modules to be used etc. The input unit is "backspaced" to the beginning and then the subroutine INPUT is called. The starting addresses of the input arrays in the XL array are arguments of INPUT. The index NFR indicates the beginning of the non-permanent section of the XL array and is also an argument of the subroutine INPUT. All input arrays are filled with the information from the input cards or the standard built-in data. The input is also checked for consistency. Then the computational modules are called in the order fixed by the input.

Before each call of a computational module the length of the non-permanent section of the XL array is checked, whether it is long enough for the working arrays of the module. The length of these working arrays depends on the input information and, in some cases, can finally be defined only in the computational module itself. In this case an iterative procedure is used to determine the proper length. As a first step, a minimum length of such a working array is assumed. If it turns out to be too small, control is given back to the control module and the size of the array is increased. When the required size of all working arrays for the computational module in question is so large that it can not be accommodated by the XL array this module is bypassed and a message to the user is given.

After all the required computational modules for one material have been called, a RETURN-statement to the subroutine MAIN is given. If there are more materials, a new arrangement of the XL-array is made etc.

1.4 Auxiliary subroutines

1.4.1 Reading program for the Karlsruhe nuclear data library KEDAK

For reading KEDAK, the subroutine NDF is necessary. A description is given in /3/.

1.4.2 Weighting functions

In case no weighting functions are specified for the group cross sections and matrices in the input, the following two FUNCTIØNs are used:

FUNCTIØN PHI(E)	respectively the	REAL FUNCTIØN DPHI*8(E)
PHI = 1./E	double precision	REAL*8 E
RETURN	version used by	DPHI = 1.0D+0/E
END	module 3 (FSTRUK)	RETURN
		END

E is the energy in eV.

This weighting function is used for all group constants except the first and higher Legendre moments for elastic scattering.

The following tables are given in chapter 1:

- Table I : Computational modules of MIGRØS-3, their tasks and their subroutines and functions.
- Table II : Overlay structure of MIGRØS-3.
- Table III : Structure of the central data array XL.
- Table IV : Structure of the unlabeled COMMON array.

Table I Computational modules of MIGRØS-3, their tasks and their subroutines and functions

number of the module	described in	content	names of the subroutine and functions	entry subroutine
1	chapter 4	average group cross sections for infinite dilution and energy resonance selfshielding factors from resolved Breit-Wigner resonance parameters	DØPW, FGEM, NDF, PHI, PSIXI(with entry EXPPX), STOSS, WIRQ, WIRQU	FGEM
2	chapter 5	average group cross sections for infinite dilution and energy resonance selfshielding factors from statistical Breit-Wigner resonance parameters	DELTA, DMIT, DØPW, EPSI, EZZ, FSTAT, GAFM, GAMG, GAMN, NDF, PHASE, PHI, PØL, QUER, SIGC, SUCH, TAB	FSTAT
3	chapter 9	average group cross sections for infinite dilution and energy resonance self-shielding factors from energy pointwise neutron cross section data	DPHI, FSANO2, FSANO3, FSANO4, FSANO5, FSANO6, FSANO7, FSANO8, FSANO9, FSEXIN, FSGRAL, FSGRA1, FSGRA2, FSGRA3, FSLOMQ, FSNUO1, FSNUO2, FSNUO3, FSNUO4, FSNUO5, FSNUO6, FSNUO7, FSNUO8, FSNUO9, FSQUER, FSROMB, FSSNGL, FSTOLE, FSTRUK, FSTRUO, FSTRU1, FSTRU2, FSTRU3, FSTRU4, FSTRU5, FSXINT, FSWRS1, FSWRS2, FSWRS3, FSWRS9, FSWROO, NDF	FSTRUK
4	chapter 3	average group cross sections, for infinite dilution (without resonance self-shielding) from point data and average group values of $\bar{\nu}$, η , α , ν	DØPW, FL, GRUP, NDF, PHI, SUND,	SUND
5	chapter 6	normalized transfer matrices for inelastic scattering (calculated from discrete level excitation cross sections and from evaporation models) and normalized transfer matrices for (n,2n)- and (n,3n)-reactions (calculated from evaporation models	AKED, CUTS, DAØRG, DNFAK, DØPW, ENØRG, EXD, FINT, FIPØLA, FIPØLD, NDF, NDREAD, ØRDNEN, ØRD1, PHI, PRØB, RENUA, REPRØB, SCAT, SCATC, SCATD, SGINT, SIMPSI, SINPØL, SIØRG, SPECT, TEMP, THETA, TRA, XINPØL	SCAT

Table I, continued

number of the module	described in	content	names of the subroutines and functions	entry subroutine
6	chapter 7	normalized elastic-scattering matrices up to the fifth Legendre order, elastic and total group cross sections	ADD, FLUMMI, GRUPIN, G, INFØRM, IPØLA, IPØLIN, LECAL, LEGANS, LEGINT, LEGIST, LEGPØL, LØØKO, LØØK1, LØØK2, LØØK3, MAKRØ, MIXSGT, MUKØN, NDF, PHI, PRINT, PUNK, PUSUM, SPRAL, SUM, TRAFØ.	FLUMMI
7	chapter 12	fission spectra	CHIINM, DØPW, NDF, SPALT	SPALT
8	chapter 11	1/V-average group values	EDV, PHI	EDV
9	chapter 8	zero'th and higher moments of elastic scattering for the "REMO"-correction	AKØR, AMESH, ANG, ANINT, AUSGL, BCM, EGRENZ, ENERØ, FIPØL, FXINT, HIDR, ICSØP, INTEN, IPØL, ISØFAL, IWØ, IWØ, KEDDAT, LININT, LMI, MASSIN, NDF, NØRM, ORDN1, PHI, REMØ, REMP, SEARCH, SINT, SMØRN, SUCHM, WAHRS, WINK, ZWIN	REMØ
10	chapter 10	group cross sections in the thermal group	DØPW, NDF, THERM	THERM
control module	chapter 2		DDTEST, DØPW, EING, FREEFØ, FSTAE, GAREA, INPUT, MAIN, NDF	

Table II:
Overlay Structure of MGRS-3

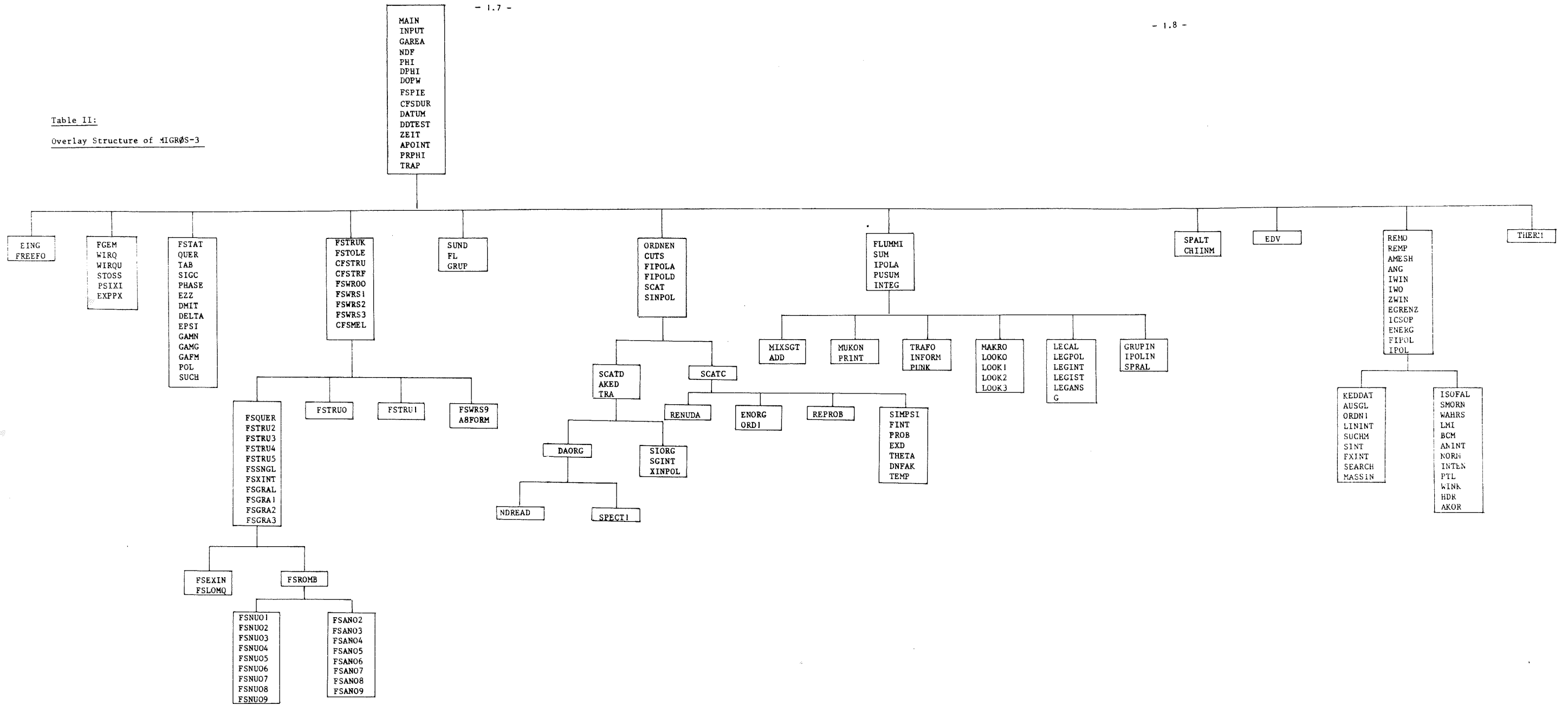


Table III

Structure of the central data array XL in the subroutine MAIN

a) The permanent section

The symbols of the input description in chapter 2 are used

length of the subarray	type	content of the subarray	see card n of the input description
NTYP	REAL*8	ITYP(I), I=1, NTYP	13
NMAT	REAL*8	NAME(I), I=1, NMAT	33
NMAT	REAL*4	TZ(I), I=1, NMAT	33
NE	REAL*4	ENG(I), I=1, NE	3
NFE+NE	REAL*4	EF(I), I=1, NFE and ENG(I), I=1, NE in increasing succession	3, 5
(NFE+NE)+ NSPEC	REAL*4	(F(I, J), I=1, (NFE+NE)), J=1, NSPEC	5
3*NA	INTEGER*4	(NR(I, J), I=1, 3), J=1, NA	7
NT	REAL*4	TEMP(I), I=1, NT	9
MI+1	REAL*4	SIGO(I), I=1, MI	11
NA	INTEGER*4	NGRE(I), I=1, NA	7, 44, 41
NA*NE	INTEGER*4	(N1(I, J), I=1, NA) J=1, NE	3, 7, 44, 41
NA*NE	INTEGER*4	(N2(I, J), I=1, NA), J=1, NE	3, 7, 44, 41
NA*NE	INTEGER*4	(NFG(I, J), I=1, NA), J=1, NE	3, 7, 44, 41
NA*NE	INTEGER*4	(NFI(I, J), I=1, NA), J=1, NE	3, 7, 44, 41
2*NE	INTEGER*4	this subarray is defined, but information is actually only stored if module 9 is called	-

Table III, cont.

b) The non-permanent section

Besides the permanent section a non-permanent section is defined when a computational module is called. This non-permanent part exists only during the execution of a computational module. The non-permanent section starts with the index NFR, defined in the subroutine MAIN. The names of the auxiliary arrays are the same as those used in the formal parameters of the entry subroutines of the computational modules. All other symbols are the same as in the input description of chapter 2. (NE: see card 3 of the input description, MI: see card 11 of the input description. Some symbols used in b3) module 3 are also explained in 2.1.2.)

b1) Module 1

length of the subarray	type	name of the subarray
MI x 7	Real*4	SUM
NE x 3	Real*4	SUØ
max (300,r)	Real*4	ER
max (300,r)	Integer*4	L
max (300,r)	Real*4	GJ
max (300,r)	Real*4	GAT
max (300,r)	Real*4	GAN
max (300,r)	Real*4	GAG
max (300,r)	Real*4	GAF
5 x max (400,i)	Real*4	STE
max (400,i)	Real*4	STE1

r = number of resonances on the KEDAK-library for the isotope in question.

i = number of integration points for the integration of the effective group cross section in one energy group.

Table III, cont.

b2) Module 2

length of the subarray	type	name of the subarray
3 x 5 x MI	Real*4	SE
3 x 5 x MI	Real*4	SM
5 x MI	Real*4	XEUGZ

b3) Module 3

length of the subarray	type	name of the subarray
MIBER	Real*4	GIBER
MIBER	Integer*4	IIBER
MIBER	Real*4	GIBER
MI*6	Real*4	FFAKT
MABWF*4	Real*4	ABWF
MXINT	Real*4	XINT
MABQ1*4	Real*4	ABQ1
MABQ2*4	Real*4	ABQ2
MABQ3*4	Real*4	ABQ3
KMROM	Real*8	AUXROM
MI*MRF	Real*4	RF
MI*MRF	Real*4	RFL

Table III, cont.

- MIBER = maximum number of ranges with different weighting functions or different integration methods. MIBER is set equal to 5 in the subroutine INPUT.
- MABWF = maximum number of energy points in one group of the pointwise given weighting function.
- MXINT = maximum number of energy points in one group summed over all participating cross sections (and eventually the pointwise given weighting function).
- MABQ1 = maximum number of energy points in one group for the cross section types σ_t , σ_a , σ_e and - if existent - σ_f .
- MABQ2 = maximum number of energy points in one group for the cross section type $\bar{\mu}_e$.
- MABQ3 = maximum number of energy points in one group for the cross section type σ_t .
- KMROM : KMROM-1 = maximum number of bisections in the Romberg integration routine FSROMB.
- MRF = 7 for nonfissionable material
8 for fissionable material

b4) Module 4

length of the subarray	type	name of the subarray
NE	Real*4	SGC
NE	Real*4	DUE
NE	Real*4	XINTE
NE	Real*4	ZINT
NE	Real*4	XNEN
NE	Real*4	STREU
max (1500,i)	Real*4	SE
max (1500,i)	Real*4	FSE

i = number of $\bar{\mu}_e$ values or v_f values for one isotope in the KEDAK library.

Table III, cont.

b5) Module 5

In the organizing subroutine INPUT the XL-array minus the permanent section is transferred to the entry subroutine of module 5, SCAT. In SCAT this array, X(MMAxx), is subdivided into fields of different lengths, which are described in more detail in the following tables (and in chapter 6).

1. Fields used in SCATD and its subroutines:

length of the subarray	type	name of the subarray
NE*NE	Real*4	WEIN
NE	Real*4	QUOT
NE	Real*8	WAHR
NE	Real*8	VW
NE27	Real*8	E
max(30,j)	Real*8	AE
NE	Real*4	SU
NE	Real*4	LBA
max(200,i)	Real*4	SGIT
max(30,j)	Real*4	IANF
max(6000,i*j)	Real*4	SGIP
max(200,i)	Real*4	WERT
max(400,k)	Real*8	EZ

NE27: = NE, if the energy groups given on card 3 of the input contain the thermal group,
= NE+1 otherwise

i : maximum number of energy points that are needed during the calculation for any of the outscattering energy groups, specified in the input. These energy points are the joint set of the energy points of all SGIZ on KEDAK and the energy points of the weighting function.

Table III, cont.

- j : maximum number of excited levels of one isotope that contribute in any outscattering energy group specified in the input.
- k : i + maximum number of energy points of any SGIZ (for one isotope) on KEDAK in any of the (outscattering) energy groups specified in the input.

b5) 2. Fields used in SCATC and its subroutines

length of the subarray	type	name of the subarray
NE*NE	Real*4	WEINC
NE	Real*4	QUOTC
NE27	Real*4	ENG
max(200,i)	Real*4	EZ
max(200,i)	Real*4	SGIZC
max(300,j)	Real*4	EI
max(30,k)	Real*4	EP
max(150,k*1)	Real*4	F1
max(150,k*1)	Real*4	F2
max(150,k*1)	Real*4	F3
max(150,k*1)	Real*4	F4

NE27: = NE, if the energy groups, given on card 3 of the input contain the thermal group
 = NE+1 otherwise

i : maximum number of energy points of SGIZC (SGI,SG2N,SG3N) on KEDAK in any of the outscattering energy groups specified in the input.

j : maximum number of energy points, that are obtained by combination of the energy points on KEDAK for type SGIZC (SGI,SG2N,SG3N) and the energy points of the weighting function in any of the outscattering groups specified in the input.

Table III, cont.

- k: number of incident neutron energies, given in KEDAK-type SEDIC(SED2N, SED3N).
- l: number of different analytical spectra - as given in KEDAK-type SEDIC(SED2N, SED3N) - from which the total spectrum has to be combined.

b6) Module 6

length of the subarray	type	name of the subarray
max (i,400)	Real*4	A
max (i,400)	Real*4	B
max (i,400)	Real*4	EA
max (i,400)	Real*4	EB
max (i,400)	Real*4	E
max (j,1000)	Real*4	EN
max (j,1000)	Real*4	SGN
max (j,1000)	Real*4	ECØ
max (j,1000)	Real*4	SCØ
max (j,1000)	Real*4	V
max (j,1000)	Real*4	W
max (j,1000)	Real*4	F
k	Real*4	AR
k	Real*4	FU
NE + 1	Real*4	ABN
NE + 1	Integer*4	INT
NE + 1	Real*4	GR
NE + 1	Real*4	FEKØE
NE	Real*4	R
6 x NE	Real*4	RSP
k x i	Real*4	SGNC
l x i	Real*4	FEKØ
6 x l x NE	Real*4	ELSIG
2 x NE	Real*4	ELTØT
max (m,3000)	Real*4	ET
max (m,3000)	Real*4	ST
max (j,1000)	Real*4	GE
max (j,1000)	Real*4	SG
6 x NE	Real*4	SGTØT

Table III, cont.

- i : 300 + maximum number of energy points for the data type SGNC on KEDAK in one energy group.
- j : i + maximum number of energy points for the data types SGN or MUEL or SGT on KEDAK in one energy group.
- k : number of cosine mesh points for the data type SGNC on KEDAK.
- l : maximum energy degradation
- m : maximum number of energy points for the data type SGT on KEDAK in one group for the given mixture of isotopes.

b7) Module 7

length of the subarray	type	name of the subarray
NE	Real*4	X

b8) Module 8

length of the subarray	type	name of the subarray
NE	Real*4	V
max (200,m)	Real*4	ST
max (200,m)	Real*4	FI

- m : maximum number of integration points in one energy group.

b9) Module 9

length of the subarray	type	name of the subarray
XL-array minus the permanent section	Real*4	WØRK

Table III, cont.

b10) Module 10

This module uses only the permanent section of the XL-array.

Table IV: Structure of the unlabeled COMMON array

length of the subarray	type	content of the subarray	see card n of the input description
1	Real*8	MAT	1
1	Integer*4	ISTRUK	1
1	Integer*4	ISPA ^{+))}	-
1	Integer*4	unit number for print output	-
1	Integer*4	external storage number for the output of the results	-
2	Integer*4	NR(2,J), NR(3,J) J is the index of the module actually called	7
1	Integer*4	KL at the end of each module KL must be enlarged by one	7

^{+))} In MIGRØS-3 ISPA is only used internally. ISPA = 1 for fissile isotopes, ISPA = 0 for non-fissile isotopes.

References

/1/ J.J. Schmidt

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/3/ B. Krieg

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File KEDAK

Part I: Management and Retrieval Programs

KFK 1725, 1972

see also chapter II of the KEDAK Program Compendium

(KFK 2387, II 2.9)

2. Input and output of MIGRØS-3

2.1 Description of the input

On the following pages the computer output of the input description of MIGRØS-3 is given.

INPUT DESCRIPTION FOR THE PROGRAM SYSTEM MIGROS-3

INTRODUCTION

THE PROGRAM SYSTEM MIGROS CALCULATES MICROSCOPIC GROUP CONSTANTS FROM NUCLEAR CROSS SECTION DATA STORED IN THE NUCLEAR DATA LIBRARY KEDAK. THE SYSTEM CONSISTS OF THE FOLLOWING MODULES:

MODULE NO.	PURPOSE
1	CALCULATION OF GROUP CROSS SECTIONS FOR INFINITE DILUTION AND OF RESONANCE SELF SHIELDING FACTORS FROM RESOLVED RESONANCE PARAMETERS.
2	CALCULATION OF GROUP CROSS SECTIONS FOR INFINITE DILUTION AND OF RESONANCE SELF SHIELDING FACTORS FROM STATISTICAL RESONANCE PARAMETERS.
3	CALCULATION OF GROUP CROSS SECTIONS FOR INFINITE DILUTION AND OF RESONANCE SELF SHIELDING FACTORS FROM POINT CROSS SECTION DATA.
4	CALCULATION OF WEIGHTED GROUP AVERAGES FOR INFINITE DILUTION.
5	CALCULATION OF NORMALIZED TRANSFER MATRICES FOR INELASTIC SCATTERING, (N,2N) AND (N,3N) PROCESSES.
6	CALCULATION OF NORMALIZED ELASTIC SCATTERING MATRICES UP TO 5-TH ORDER (LEGENDRE REPRESENTATION), OF ELASTIC GROUP CROSS SECTIONS, OF THE AVERAGE ELASTIC SCATTERING COSINE AND OF TOTAL GROUP CROSS SECTIONS WITH ORDER-DEPENDENT WEIGHTING.
7	CALCULATION OF FISSION SPECTRA.
8	CALCULATION OF WEIGHTED 1/V GROUP AVERAGES.
9	CALCULATION OF NORMALIZED ELASTIC SCATTERING MATRICES UP TO 5-TH ORDER (LEGENDRE REPRESENTATION), OF WEIGHTED TOTAL AND ELASTIC SCATTERING GROUP CROSS SECTIONS AND OF GROUP-AVERAGED SCATTERING COSINES FOR THE REMO CORRECTION.
10	CALCULATION OF THERMAL CROSS SECTIONS.

THE FOLLOWING INPUT MUST BE PROVIDED. IF GROUP CONSTANTS ARE TO BE CALCULATED FOR SEVERAL MATERIALS THE COMPLETE INPUT MUST BE REPEATED FOR EACH ONE. THE INPUT IS FORMAT-FREE FOLLOWING THE FREEFC CONVENTIONS: EACH DATA RECORD STARTS IN COLUMN 1 OF A DATA CARD. IF IT IS NOT POSSIBLE TO PLACE ALL THE DATA OF ONE DATA RECORD ON ONE CARD, A SECOND, THIRD, ETC. CARD MAY BE USED, WHICH MUST HAVE A BLANK IN COLUMN 1. OR: A NON BLANK COLUMN 1 IN THE INPUT CARD IS AN INDICATION FOR A NEW INPUT RECORD. ONE HAS TO DISTINGUISH BETWEEN AN ALPHAMERIC WORD OF THE LENGTH REAL*4 AND OF THE LENGTH REAL*8. A REAL*4 WORD MUST BE ENCLOSED IN APOSTROPHIES AND IS STORED LEFT-ADJUSTED IN THE COMPUTER AND FILLED UP WITH BLANKS IF NOT ALL 4 BYTES ARE OCCUPIED. EXAMPLE: 'ARG' OR 'ABCD'. A REAL*8 WORD MAY BE ENCLOSED IN APOSTROPHIES COMPRISING AT LEAST 5 CHARACTERS AND AT MOST 8 CHARACTERS, WHICH ARE STORED LEFT-ADJUSTED IN THE COMPUTER IF NOT ALL 8 BYTES ARE OCCUPIED. A SPECIAL CASE ARE REAL*8 WORDS WITH A NUMBER OF OCCUPIED BYTES LESS THAN OR EQUAL TO 5. THESE WORDS MAY BE ALSO ENCLOSED IN @-SIGNS. THEY ARE ALSO STORED LEFT-ADJUSTED IN THE COMPUTER AND FILLED UP WITH BLANKS. EXAMPLES: 'PU239'='PU239 '=@PU239@; 'RES'=@RES@. FIXED POINT AND FLOATING POINT NUMBERS ARE WRITTEN IN THE USUAL MANNER, E. G: FIXED POINT NUMBERS: 1 10 875 AND FLOATING POINT NUMBERS: 10. 5.E3 0.7E-3 0.01 . THE INPUT DATA ITEMS ARE SEPARATED BY ONE OR MORE BLANKS.

CARD 1

MAT MATERIAL NAME IN KEDAK NOMENCLATURE
(8-BYTE ALPHAMERIC REPRESENTATION).
ISTRUK =0 : DOPPLER BROADENING IS NEGLIGIBLE AS IS TYPICAL
FOR S-WAVE RESONANCES OF STRUCTURAL MATERIALS,
=1 : DOPPLER BROADENING MUST BE ACCOUNTED FOR AS IS
TYPICAL FOR HEAVY NUCLIDES.

MORE SPECIFICALLY: IF MODULES 1 AND 2 ARE
UTILIZED, INFINITE DILUTION GROUP CROSS SEC-
TIONS AND RESONANCE SELF SHIELDING FACTORS ARE
CALCULATED FROM RESONANCE PARAMETERS FOR THE
FOLLOWING STANDARD TEMPERATURES :
T=0 K IF ISTRUK=0,
T=300, 900, 2100 K IF ISTRUK=1.
IF MODULE 3 IS UTILIZED THE SAME QUANTITIES ARE
CALCULATED FROM POINT DATA FOR THAT TEMPERATURE
FOR WHICH THE POINT DATA ARE STORED (T=0 K IN
THE PRESENT VERSION, KEDAK-3), REGARDLESS OF
THE ISTRUK VALUE.
IF TEMPERATURES DIFFERING FROM THE STANDARD
TEMPERATURES ARE TO BE USED, THIS MUST BE SPE-
CIFIED ON CARD 9 BELOW.

IF GROUP BOUNDARIES DIFFERING FROM THOSE OF THE 26-GROUP ABBN
SET ARE TO BE USED (VIZ. 0.215EV, 0.465EV, 1EV, 2.15EV, 4.65EV,
10EV, 21.5EV, 46.5EV, 100EV, 215EV, 465EV, 1KEV, 2.15KEV,
4.65KEV, 10KEV, 21.5KEV, 46.5KEV, 100KEV, 200KEV, 400KEV,
800KEV, 1.4MEV, 2.5MEV, 4MEV, 6.5MEV, 10.5MEV) TWO MORE CARDS
FOLLOW:

CARD 2

ABLCCA 1 INVARIANT

CARD 3

NE NUMBER OF ENERGY GROUP BOUNDARIES
(ARBITRARY),
(ENG(I), I=1, NE) ENERGY GROUP BOUNDARIES IN UNITS OF EV
IN ASCENDING ORDER.

NOTE THAT THE NUMBER OF ENERGY GROUPS THAT MIGRCS CAN TREAT
IS NOT RESTRICTED TO 26.

THE STANDARD WEIGHTING FUNCTION IS THE COLLISION DENSITY
 $F(I,1)=\Phi(E(I))=1./E(I)$. ALTERNATIVELY ONE CAN EMPLOY OTHER
WEIGHTING FUNCTIONS AFTER LINKAGE OF AN APPROPRIATE FUNCTION
 $\Phi(E)$ WITH MIGRCS. IF IN THIS CASE MODULE 3 IS USED ONE MUST
LINK AN ADDITIONAL FUNCTION $D\Phi(E)$ YIELDING BASICALLY THE
SAME RESULT AS Φ BUT WITH DOUBLE PRECISION. A THIRD ALTERNA-
TIVE IS UTILIZATION OF A POINTWISE GIVEN COLLISION DENSITY FOR
WHICH ONE NEEDS THE FOLLOWING CARDS:

CARD 4
 @BLDCC@ 2 INVARIANT

CARD 5
 NSPEC NUMBER OF SPECTRA,
 NFE NUMBER OF ENERGY GRID POINTS,
 ((F(I), I=1, NFE), ((F(I, J), I=1, NFE), J=1, NSPEC) WITH
 EF: ENERGY GRID POINTS IN UNITS OF EV
 IN ASCENDING ORDER,
 F: COLLISION DENSITY VALUES.

IF THE NUMBER OF SPECTRA (COLLISION DENSITY FUNCTIONS) IS GREATER THAN 1 THE SPECTRA 2, 3, ... ARE INTERPRETED ONLY IN MODULE 6 WHERE THEY ARE TAKEN AS THE WEIGHTING FUNCTIONS FOR THE 1ST, 2ND, ... MOMENT OF THE ELASTIC SCATTERING MATRIX (MW=1 ON CARD 35). MAKE SURE THAT THE NUMBER OF SPECTRA IS CONSISTENT WITH THE NUMBER OF MOMENTS CALCULATED. IF ONLY ONE SPECTRUM IS SPECIFIED IT WILL BE EMPLOYED FOR ALL REQUIRED MOMENTS OF THE ELASTIC SCATTERING MATRIX. A SPECIAL MODIFICATION, HOWEVER, ALLOWS AN IMPROVED TREATMENT OF FINE-STRUCTURE WEIGHTING (SEE CARDS 32-35). THE NUMBER OF GRID POINTS IS ARBITRARY BUT CARE SHOULD BE TAKEN THAT THE SPECTRA COVER THE WHOLE ENERGY RANGE OF INTEREST.

CARD 6
 @BLDCC@ 3 INVARIANT

CARD 7
 NA NUMBER OF MODULES UTILIZED,
 ((NR(I, J), I=1, 3), J=1, NA) WITH
 NR(1, J) NUMBER OF MODULE,
 NR(2, J) NUMBER OF ENERGY GROUP WHERE CALCULATION WITH MODULE NR(1, J) IS TO BEGIN,
 NR(3, J) NUMBER OF ENERGY GROUP UP TO WHICH CALCULATION WITH MODULE NR(1, J) IS TO BE EXTENDED.
 THE LIMITS NR(2, J), NR(3, J) ARE TO BE GIVEN IN THE USUAL SENSE OF ASCENDING ENERGY. NOTE THAT THEN NR(3, J) <= NR(2, J), SINCE GROUPS ARE CONVENTIONALLY LABELED IN THE REVERSE SENSE, I. E. GROUP NUMBER 1 IS ASSIGNED TO THE GROUP BETWEEN THE HIGHEST TWO ENERGY VALUES ON CARD 3.

COMMENT:
 MODULES CAN BE CALLED MORE THAN ONCE. THIS IS NECESSARY IF SEVERAL UNCONNECTED RANGES OF ENERGY GROUPS MUST BE TREATED. FOR EACH RANGE ONE CALL MUST BE MADE.
 NR(2, J) AND NR(3, J) ARE INTERPRETED AS REFERRING TO OUT-SCATTERING GROUPS IN THE CASE OF ELASTIC AND INELASTIC SCATTERING

MATRICES. THE CALCULATION IS PERFORMED FOR ALL IN-SCATTERING GROUPS, I. E. ALL GROUPS LISTED IN @BLOC@ 1 INTO WHICH A NEUTRON CAN GET IN THE COURSE OF SCATTERING PROCESSES. THE THERMAL GROUP IS INCLUDED AS IN-SCATTERING GROUP.

IF MODULE 1 AND 2 FOR CALCULATION OF SELF-SHIELDING FACTORS FROM RESOLVED AND STATISTICAL RESONANCE PARAMETERS ARE CALLED, AND TEMPERATURES OTHER THAN THE STANDARD TEMPERATURES (0 KELVIN FOR STRUCTURAL MATERIALS, ISTRUK=0, 300, 900 AND 2100 KELVIN FOR HEAVY NUCLEI, ISTRUK=1) ARE NEEDED, TWO MORE CARDS MUST FOLLOW:

CARD 8
@BLOC@ 4 INVARIANT
CARD 9
NT NUMBER OF TEMPERATURES (ARBITRARY),
(TEMP(I), I=1, NT) TEMPERATURES IN KELVIN.

IF SELF-SHIELDING FACTORS ARE TO BE CALCULATED (WITH MODULE 1, 2 OR 3) FOR DILUTION CROSS SECTIONS SIGMAO (SIGC(I)) DIFFERING FROM THOSE OF THE ABBN GROUP CONSTANT SET (VIZ. 0, 10, 100, 1000, 10000, 100000 AND 1000000 BARN) THE FOLLOWING CARDS ARE NEEDED:

CARD 10
@BLOC@ 5 INVARIANT
CARD 11
MI NUMBER OF DILUTION CROSS SECTIONS
(ARBITRARY),
(SIGC(I), I=1, MI) DILUTION CROSS SECTION VALUES (SIGMAO-
VALUES) IN BARN.

IF WEIGHTED GROUP AVERAGES FOR INFINITE DILUTION ARE TO BE CALCULATED (WITH MODULES 4 AND 10) FOR DATA TYPES OTHER THAN THE 8 STANDARD TYPES MUEL, NUF, SGA, SGF, SGI, SGN, SG2N, AND SGT THE FOLLOWING CARDS ARE NEEDED:

CARD 12
@BLOC@ 6 INVARIANT
CARD 13
NTYP NUMBER OF DATA TYPES (ARBITRARY),
(ITYP(I), I=1, NTYP) DATA TYPES (KEDAK NOMENCLATURE).

COMMENT:

WEIGHTED GROUP AVERAGES CAN BE CALCULATED FOR ALL DATA TYPES WHICH CAN BE REPRESENTED AS ONE-VALUED FUNCTIONS OF A SINGLE ARGUMENT (INCIDENT NEUTRON ENERGY). THE POSSIBLE TYPES ARE LISTED IN KFK 1725 OR KFK 2234. SPECIAL DEFINITIONS OF GROUP AVERAGES ARE USED FOR COMPOSITE QUANTITIES SUCH AS ALPHA, ETA, MUEL OR NUE (CF. KFK 1784). IF THE CROSS SECTION TYPES SGF AND SGA (SFE KFK 2234) ARE TREATED THE CROSS SECTION TYPE SGC=SGA-SGF IS AUTOMATICALLY TREATED, TOO.

IF RESONANCE SELF-SHIELDING FACTORS ARE TO BE CALCULATED FROM INDIVIDUAL RESONANCE PARAMETERS (MODULE 1), BUT ONLY WITH A LIMITED NUMBER OF RESONANCES ON EITHER SIDE OF EACH ENERGY GRID POINT, TWO MORE CARDS FOLLOW:

CARD 14

@BLOC@ 11 INVARIANT

CARD 15

NRES NUMBER OF RESONANCES TO BE CONSIDERED ON EITHER SIDE OF A GIVEN ENERGY.

IF MODULE 1 IS TO BE EMPLOYED, BUT NOT WITH THE STANDARD VALUE 0.01 OF THE MAXIMUM ADMISSIBLE RELATIVE ERROR FOR THE INTEGRATION, ONE NEEDS THE FOLLOWING TWO CARDS:

CARD 16

@BLOC@ 12 INVARIANT

CARD 17

ERROR MAXIMUM ADMISSIBLE RELATIVE INTEGRATION ERROR.

IF GROUP CROSS SECTIONS AND SELF-SHIELDING FACTORS ARE TO BE CALCULATED FROM POINT DATA (MODULE 3) BUT NOT WITH THE STANDARD VALUES EPSROM=5.0E-05, DRINWA=5.0, (EXPLAINED BELOW) ONE NEEDS THE FOLLOWING TWO CARDS:

CARD 18

@BLOC@ 31 INVARIANT

CARD 19

EPSROM RELATIVE ACCURACY FOR THE ROMBERG INTEGRATION. THE ITERATION STOPS IF THE RELATIVE DIFFERENCE BETWEEN TWO SUCCESSIVE APPROXIMATIONS IS NOT GREATER THAN EPSROM,

DRINWA

CONTROL OF ERROR PRINTING IN THE RCMBERG
ITERATION SUBROUTINE. IF THE ITERATION IS
STOPPED (E. G. BY ROUND-OFF ERRORS) BEFORE
THE EPSROM CRITERION IS FULFILLED, AN ERROR
MESSAGE IS PRINTED ONLY IF THE CRITERION IS
NOT EVEN FULFILLED WITH DRINWA TIMES EPSROM.

IF MODULE 3 IS TO BE EMPLOYED BUT NOT WITH THE DEFAULT VALUES
ITEST=0, IZPUMS=-1 AND ITUMS=0 (CF. CARD 21), THE FOLLOWING
TWO CARDS ARE NEEDED:

CARD 20
@BLOC@ 22

INVARIANT

CARD 21
ITEST

CONTROL OF ERROR MESSAGES AND WARNINGS
=0: NORMAL PRINT-OUT FOR PRODUCTION RUNS,
=1: EXTENDED PRINT-OUT FOR PROGRAM
DEBUGGING,
=2: AS ITEST=1 WITH ADDITIONAL PRINT-OUT,
=3: AS ITEST=2 WITH FURTHER EXTENDED PRINT-
OUT,
=4, 5, ..9: AS ITEST=3,
=10, 11, 12, 13: AS ITEST=0, 1, 2, 3 WITH
ADDITIONAL ERROR MESSAGES FOR EACH
SIGO VALUE,
>13: AS ITEST=13.

IZPUMS

CONTROL OF ITEST FOR DIFFERENT GROUPS
<=-1: ITEST IS UNCHANGED,
=IGR: BEGINNING WITH THE IGR-TH GROUP UP TO
THE NR(3,J)-TH GROUP (CF. CARD 7)
ITEST HAS THE NEW VALUE ITUMS (SEE
BELOW). IGR MUST BE LESS THAN OR
EQUAL TO NR(2,J) (CF. CARD 7). THIS
IS VALID FOR ALL J WITH NR(1,J)=3,
I. E. WHENEVER MODULE 3 IS CALLED.

ITUMS

NEW VALUE OF ITEST.

IF MODULE 3 IS TO BE UTILIZED BUT NOT WITH THE DEFAULT VALUES
NENBER=1, ENBER(1)=-1.0, CONWFU(1)=1.0, OR NOT WITH NWFUN(1)=0
IN CASE OF A CALCULATED COLLISION DENSITY, OR NOT WITH
NWFUN(1)=-1 IN CASE OF A POINTWISE GIVEN COLLISION DENSITY
(CF. CARD 23) ONE NEEDS THE NEXT TWO CARDS:

CARD 22
@BLOC@ 23

INVARIANT

CARD 23
NENBER

NUMBER OF ENERGY INTERVALS WITH DIFFERENT
WEIGHTING FUNCTIONS AND/OR DIFFERENT INT-
GRATION METHODS,

(ENBER(I),NWFUN(I),CONWFU(I),I=1,NENBER) WITH
ENBER(I): UPPER LIMIT OF I-TH ENERGY INTER-
VAL, EQUAL TO LOWER LIMIT OF (I+1)-TH
ENERGY INTERVAL, SO THAT
ENBER(I) < ENBER(I+1).
THE LOWER LIMIT FOR THE FIRST ENERGY INTER-
VAL IS TAKEN AS EQUAL TO THE BEGINNING OF
THE CURRENT ENERGY GROUP RANGE (SMALLEST
ENERGY VALUE) AS SPECIFIED ON CARD 3 (CR IN
THE PROGRAM AND IN CARD 7 IN CASE OF SEVE-
RAL DISCONNECTED ENERGY GROUP RANGES).
ENBER(NENBER) MUST BE AT LEAST AS GREAT AS
THE LARGEST ENERGY OF THE CURRENT ENERGY
GROUP RANGE.
SPECIAL CASE FOR NENBER=1:
ENBER(1)=-1.0. THIS MEANS THE WHOLE SPECI-
FIED ENERGY GROUP RANGE.
NWFUN(I): TYPE OF WEIGHTING FUNCTION AND
METHOD OF INTEGRATION USED IN INTERVAL I.
METHOD OF INTEGRATION:
NWFUN(I) <= 0: NUMERICAL INTEGRATION WITH
THE ROMBERG METHOD,
NWFUN(I) > 0: ANALYTICAL INTEGRATION.
TYPE OF WEIGHTING FUNCTION:
|NWFUN(I)| = 0: ARBITRARY FUNCTION WITH THE
NAME DPHI. (DPHI=1./E BY DE-
FAULT IF NOT GIVEN BY THE
USER AS A FUNCTION SUBROUTINE
TO THE PROGRAM),
|NWFUN(I)| = 1: POINTWISE WEIGHTING FUNCTION,
|NWFUN(I)| = 2: DPHI=CONWFU(I)/E (FOR CONWFU
SEE NEXT INPUT VARIABLE).
CAUTION: BECAUSE IN SOME
CASES ROUNDING ERRORS APPEAR
WHEN THE ANALYTICAL INTEGRA-
TION IS CHOSEN, WE RECOMMEND
TO USE ONLY NWFUN(I) <= 0.
THERE IS NO DIFFERENCE IN THE
CPU TIMES BETWEEN ROMBERG AND
ANALYTICAL INTEGRATION.
CONWFU(I): FACTOR IN THE WEIGHTING FUNC-
TION DPHI=CONWFU(I)/E. ONLY
USED IF |NWFUN(I)| = 2.

THREE DIFFERENT OPTIONS ARE AVAILABLE FOR THE TRANSFER PROBA-
BILITIES NEEDED FOR THE CALCULATION (WITH MODULE 5) OF NORMA-
LIZED TRANSFER MATRICES FOR INELASTIC SCATTERING WITH EXCITA-
TION OF DISCRETE LEVELS AT EXCITATION ENERGIES E_j :

- (1) $F(E_p \rightarrow E) = \Delta(E_p - E - E_j)$ IF $KINEM=0$,
WHERE Δ DENOTES DIRAC'S DELTA FUNCTION. THIS FORM
WAS USED IN THE ORIGINAL VERSION OF MIGROS-2 (KFK 1784).

(2) $F(E_P \rightarrow E) = \Delta(F_P - F - E_J * (A + 1.) / A)$ IF KINEM=1
THIS FORM WAS USED IN THE REVISED VERSION OF MIGROS-2
(TRANSFORMATION OF E_J FROM CMS TO LAB COORDINATES).

(3) $F(E_P \rightarrow E) = \Delta(E - E_P * (A ** 2 + 1.) / (A + 1.) ** 2$
 $+ E_J * A / (A + 1.))$ IF KINEM=2
THIS APPROXIMATION WAS RECOMMENDED BY SEGEV (SEGEV,
NSE 45 (1971) 269 AND VERTES, NSE 52 (1973) 485) AND IS
ALSO PROPOSED FOR THE PROCESSING OF ENDF/B DATA (DRAKE,
BNL 5C274 (T-601) ENDF 102, VOL.1).

FORM (2), I. E. KINEM=1, IS THE DEFAULT OPTION IN MODULE 5. IF
EITHER FORM (1) OR (3) IS TO BE USED ONE NEEDS THE FOLLOWING
ADDITIONAL INPUT:

CARD 24

@BLOC@ 51 INVARIANT

CARD 25

KINEM TAG FOR TREATMENT OF DISCRETE LEVELS
(SEE ABOVE).

IF FOR THE MATERIAL OF INTEREST THE NUCLEAR DATA LIBRARY DCFS
DO NOT CONTAIN ANY INFORMATION ON THE ENERGY DISTRIBUTION OF
SECONDARY NEUTRONS (SEDIC, SED2N, SED3N) IN THE ENERGY REGION
OF CONTINUOUS LEVEL EXCITATION OF THE RESIDUAL NUCLEUS AN
EVAPORATION MODEL IS EMPLOYED IN MODULE 5. THE PARAMETER XNUE
FOR THE CALCULATION OF THE NUCLEAR TEMPERATURE,
 $\Theta(F_P) = \text{SQRT}(E_P / (XNUE * A))$, IS SET EQUAL TO XNUE=0.16/MEV BY
DEFAULT. (A= ATOMIC WEIGHT OF THE TARGET NUCLEUS.) IF OTHER
XNUE VALUES ARE TO BE USED ONE NEEDS THE FOLLOWING ADDITIONAL
INPUT:

CARD 26

@BLOC@ 52 INVARIANT

CARD 27

XNUE EVAPORATION MODEL PARAMETER
(IN UNITS OF 1/MEV).

IF MODULE 5 IS CALLED THE TRANSFER MATRICES FOR INELASTIC
SCATTERING AND FOR (N,2N) ARE CALCULATED BY DEFAULT. IF OTHER
REACTION TYPES ARE WANTED ONE NEEDS THE FOLLOWING ADDITIONAL
INPUT:

CARD 28

@BLOC@ 53 INVARIANT

CARD 29

NIN NUMBER OF REACTION TYPES,
(INTYP(I), I=1, NIN) REACTION TYPE INDICATORS:
INTYP=1 FOR INELASTIC SCATTERING,
INTYP=2 FOR (N,2N) PROCESSES,
INTYP=3 FOR (N,3N) PROCESSES.

IF MODULE 6 IS TO BE USED BUT NOT WITH THE STANDARD VALUES
ISEL=2, NLE=5 ONE NEEDS THE FOLLOWING CARDS:

CARD 30
@BLOC@ 61 INVARIANT

CARD 31
ISEL TAG FOR POSSIBLE CROSS SECTION MODIFICATION
AND ADDITIONAL PRINT-OUT (DEFAULT VALUE: 2)
|ISEL|=2: NO CROSS SECTION MODIFICATION;
|ISEL|=1: BELOW 10KEV, IN THE RESOLVED
RESONANCE RANGE, THE ELASTIC
SCATTERING AND TOTAL CROSS SEC-
TIONS ARE SET EQUAL TO 1 BARN
(MAINLY TO SIMPLIFY THE CALCULA-
TION OF APPROXIMATE SCATTERING
PROBABILITIES AND AVERAGE ELASTIC
SCATTERING COSINES FOR HEAVY ELE-
MENTS, AND TO SAVE CORE MEMORY
SPACE).

ISEL<0: ADDITIONAL PRINT-CUT OF INTERME-
DIATE INFORMATION.

NLE HIGHEST ORDER IN LEGENDRE EXPANSION (MAX 5)
THE ACTUAL VALUE USED IS MAX(1,NLE) BECAUSE
OF THE NORMALIZATION OF THE AVERAGE SCATTE-
RING COSINES TO THE KEDAK MUEL VALUES. THE
MODULE ALWAYS CALCULATES SCATTERING
MATRICES FROM MOMENT ZERO TO MOMENT NLE.

IF MODULE 6 IS CALLED AND FINE-STRUCTURE WEIGHTING WITH
1./SGT**(L+1) IS TO BE EMPLOYED FOR THE L-TH MOMENT ADD THE
CARDS 32 UP TO 35:

ADD THE FOLLOWING CARDS:

CARD 32
@BLOC@ 62 INVARIANT

CARD 33
NMAT NUMBER OF MATERIALS IN THE MIXTURE WHOSE
MACROSCOPIC TOTAL CROSS SECTION IS TO BE
USED FOR FINE-STRUCTURE WEIGHTING;
(NAME(I),TZ(I),I=1,NMAT) WITH
NAME: MATERIAL NAME (8-BYTE ALPHAMERIC
REPRESENTATION),
TZ : NUCLEAR DENSITY (NUCLEI PER CM**3)
TIMES 1.E-24.

IF MODULE 6 IS CALLED AND NOT ALL MOMENTS ARE TO BE WEIGHTED
BY THE COLLISION DENSITY F(I,1) (CF. CARD 5) OF THE 0-TH MO-
MENT, THE FOLLOWING CARDS ARE NEEDED:

CARD 34
@BLOC@ 63 INVARIANT

CARD 35
MW TAG FOR WEIGHTING,
MW=1: WEIGHT F(I,L+1) FOR L-TH MOMENT,
NSPEC=NLE+1 MUST OCCUR ON CARD 5 WITH
NLE GIVEN ON CARD 31 OR BY DEFAULT;

MW=2: WEIGHT $F(I,1)/SGT^{*(L+1)}$ FOR L-TH
MOMENT (CARD 33 MUST PRECEDE).

IF MODULE 6 IS USED BUT NOT WITH THE STANDARD GRID POINT
NUMBERS PER GROUP (NK=70, NR=16, SEE BELOW) ONE NEEDS THE
FOLLOWING CARDS:

CARD 36
@BLOC@ 64 INVARIANT
CARD 37
NK $NK * \min(1, \text{ALOG}(\text{ENG}(I)/\text{ENG}(I-1))/$
 $\text{ALOG}(1/\text{ALFA}))$ IS THE NUMBER OF BASIC GRID
POINTS IN THAT ENERGY REGION WITHIN GROUP I
FROM WHICH ELASTIC SCATTERING INTO ADJACENT
GROUPS IS POSSIBLE, $\text{ALFA} = ((A-1)/(A+1))^{**2}$,
A= ATOMIC WEIGHT IN NEUTRON MASS UNITS;
NR NR IS THE NUMBER OF BASIC GRID POINTS IN
THAT ENERGY REGION OF EACH GROUP FROM WHICH
ELASTIC SCATTERING INTO ADJACENT GROUPS IS
IMPOSSIBLE. (THIS REGION POSSIBLY MAY NOT
EXIST, THEN NR HAS NO MEANING.)

IF 1/V AVERAGES ARE TO BE CALCULATED (WITH MODULE 8), BUT NOT
WITH THE MAXIMUM ADMISSIBLE RELATIVE INTEGRATION ERROR
EPS=0.01, ONE NEEDS THE FOLLOWING CARDS:

CARD 38
@BLOC@ 81 INVARIANT
CARD 39
EPS MAXIMUM ADMISSIBLE RELATIVE INTEGRATION
ERROR.

IF REMC DATA ARE TO BE CALCULATED (WITH MODULE 9) BUT NOT WITH
THE STANDARD VALUES (SEE BELOW) ERR=0.01, NJM=10, NUJM=10,
ONE NEEDS THE FOLLOWING TWO CARDS:

CARD 40
@BLOC@ 91 INVARIANT
CARD 41
ERR MAXIMUM ADMISSIBLE RELATIVE INTEGRATION
ERROR;
NJM $2^{*}NJM+1$ IS THE MAXIMUM NUMBER OF GRID
POINTS FOR THE ANGULAR INTEGRATION;
NUJM $2^{*}NUJM+1$ IS THE MAXIMUM NUMBER OF GRID
POINTS FOR THE ENERGY INTEGRATION.

IF MODULE 9 IS TO BE USED BUT NOT WITH THE DEFAULT VALUES (EXPLAINED BELOW) ISELR=1 FOR ISTRUK=0, ISELR=0 FOR ISTRUK=1, NLRA=0, NLRE=5, NCALL=0, NFG=14, NFI=5, ONE NEEDS THE FOLLOWING CARDS:

CARD 42
@BLOC@ 92 INVARIANT

CARD 43
ISELR =1: SCATTERING PROBABILITIES ARE CALCULATED ACCORDING TO EQ. 8.3 OF KFK 1784 WITH THE KEDAK VALUES FOR THE SCATTERING CROSS SECTION $\sigma_{sc}(F)$,
=0: IN EQ. 8.3 OF KFK 1784 THE SCATTERING CROSS SECTION $\sigma_{sc}(E)$ IS TAKEN AS 1 BARN;
NLRA LOWEST LEGENDRE ORDER;
NLRF HIGHEST LEGENDRE ORDER;
NCALL =0: EACH TIME MODULE 9 IS CALLED ALL ENERGY GROUPS ARE SUBDIVIDED INTO 14 SUBGROUPS WITH 5 ENERGY INTERVALS EACH,
>0 NUMBER OF CALLS FOR MODULE 9 (MUST BE CONSISTENT WITH CARD 7).

IN CASE NCALL>0 THE FOLLOWING CARD IS NEEDED NCALL TIMES:

CARD 44
NGRE NUMBER OF ENERGY GROUP RANGES WITH DIFFERENT ENERGY GRIDS;
(N1(I),N2(I),NFG(I),NFI(I),I=1,NGRE) WITH
N1 : NUMBER OF FIRST GROUP IN RANGE,
N2 : NUMBER OF LAST GROUP IN RANGE,
NFG: NUMBER OF SUBGROUPS PER GROUP,
NFI: NUMBER OF ENERGY INTERVALS PER SUBGROUP.

THE LAST CARD FOR A GIVEN MATERIAL IS AS FOLLOWS:

CARD 45
@ENDE@ 111 INVARIANT

CARDS 1 TO 45 HAVE TO BE REPEATED FOR EACH MATERIAL WANTED AND/OR EACH WEIGHTING SPECTRUM TO BE USED. THE LAST CARD FOR THE ENTIRE JCB IS:

CARD 46
@ENDE@ 112 INVARIANT

PRINTING OF THE PRESENT INPUT DESCRIPTION CAN BE SUPPRESSED BY PLACING THE FOLLOWING CARD (WITH THE M PUNCHED IN COLUMN 1) IN FRONT OF THE FIRST INPUT CARD:

CARD C
MIGR INVARIANT

THIS CARD DOES NOT APPEAR IN THE FREEFC DISPLAY OF INPUT DATA.

THE PROGRAM SYSTEM MIGROS REQUIRES DD-CARDS FOR THE FOLLOWING EXTERNAL STORAGE DEVICES:

8 UNIT ON WHICH THE DECODED INPUT IS WRITTEN BY FREEFC,
1 UNIT FROM WHICH THE NUCLEAR DATA LIBRARY IS AVAILABLE,
3 UNIT ON WHICH ALL MODULES WRITE RESULTS,
10 TEMPORARY INTERMEDIATE LIBRARY NEEDED ONLY BY MODULE 6.

THE REQUIRED ARRAY LENGTHS DEPEND ON THE INPUT AND ON THE CALLED MODULES. THE NOTATION OF THE INPUT DESCRIPTION IS USED IN WHAT FOLLOWS. ALL ARRAY LENGTHS ARE GIVEN IN TERMS OF 4-BYTE WORDS UNLESS STATED OTHERWISE.

THE CONTROL PHASE NEEDS

$2*NTYP+3*NMAT+NFE*(NSPEC+1)+NT+MI+1+3*NE+4*NA*(1+NE)$ WORDS,
WHERE THE DEFAULT VALUES ARE USED FOR QUANTITIES NOT SPECIFIED IN THE INPUT, VIZ. $NTYP=7$, $NFE=1$, $NSPEC=1$, $NT=3$, $MI=7$, $NMAT=1$, AND $NE=26$.

TO THIS ONE MUST ADD THE MEMORY SPACE OCCUPIED BY THE UTILIZED MODULE WITH THE LARGEST STORAGE REQUIREMENT. THE STORAGE REQUIREMENTS OF THE VARIOUS MODULES ARE AS FOLLOWS:

MODULE NO. STORAGE REQUIREMENT (4-BYTE WORDS)

1 $7*MI+3*NE+7*MAX(300, \text{NUMBER OF RESONANCES ON KEDAK})+6*MAX(400, \text{MAXIMUM NUMBER OF GRID ENERGIES FOR INTEGRATION OVER ONE ENERGY GROUP})$ WORDS
 COMMENT: THE USER CANNOT DETERMINE THE NUMBER OF GRID ENERGIES IN ADVANCE. IF 400 WORDS ARE NOT SUFFICIENT THE SPACE FOR DATA STORAGE IS ENLARGED PROVIDED THE AVAILABLE REGION ADMITS THIS. IF THE REGION IS NOT LARGE ENOUGH THE MODULE IS BY-PASSED. IT IS RECOMMENDED IN THIS CASE TO ENLARGE THE REGION BY AT LEAST 2K BYTES.

2 $35*MI$ WORDS.

3 $3*MIBER+6*MI+MXINT+4*(MABWF+MABQ1+MABQ2+MABQ3)+2*KMROM+4*MRF*MI$ WORDS.

MIBER: MAXIMUM NUMBER OF RANGES WITH DIFFERENT WEIGHTING FUNCTIONS OR DIFFERENT INTEGRATION METHODS. MIBER IS SET EQUAL TO 5 IN THE SUBROUTINE INPUT.

MABWF: MAXIMUM NUMBER OF ENERGY POINTS IN ONE GROUP OF THE POINTWISE GIVEN WEIGHTING FUNCTION. MABWF HAS THE VALUE 0 IF NO POINTWISE GIVEN WEIGHTING FUNCTION IS PROVIDED IN THE INPUT. OTHERWISE IT HAS THE MINIMUM VALUE 50.

MXINT: MAXIMUM NUMBER OF ENERGY POINTS IN ONE GROUP SUMMED OVER ALL PARTICIPATING CROSS SECTIONS (AND EVENTUALLY THE POINTWISE GIVEN WEIGHTING FUNCTION), MINIMUM VALUE = 200.

MABQ1: MAXIMUM NUMBER OF ENERGY POINTS IN ONE GROUP FOR THE CROSS SECTION TYPES SGT, SGA, SGN AND, IF EXISTENT, SGF, MINIMUM VALUE = 200.

MABQ2: MAXIMUM NUMBER OF ENERGY POINTS IN ONE GROUP FOR THE CROSS SECTION TYPE MUEL, MINIMUM VALUE = 200.

MABQ3: MAXIMUM NUMBER OF ENERGY POINTS IN ONE GROUP FOR THE CROSS SECTION TYPE SGT, MINIMUM VALUE = 200.

KMROM: KMROM-1 = MAXIMUM NUMBER OF BISECTIONS IN THE ROMBERG INTEGRATION ROUTINE FSROMB, MINIMUM VALUE = 20.

MRF : 7 FOR NON-FISSIONABLE MATERIAL,
8 FOR FISSIONABLE MATERIAL.

WITH THE MINIMUM VALUES A MINIMUM MEMORY DEMAND OF 3121 4-BYTE WORDS (POINTWISE WEIGHTING SPECTRUM GIVEN, FISSIONABLE MATERIAL) IS NECESSARY TO RUN MODULE 3 (FSTRUK). BUT WE RECOMMEND TO USE ABOUT 10000 4-BYTE WORDS, BECAUSE SOME OR ALL OF THE MINIMUM VALUES MUST BE INCREASED DURING THE CALCULATIONS.

4 6*NE+2*MAX(1500,NUMBER OF SGN VALUES, NUMBER OF
SGF VALUES ON KEDAK IN THE ENERGY INTERVAL
CONSIDERED) WORDS

5 MAX(7+NE*NE+7*NE+2*NE27+4*NAE+3*ISG+2*NISGD,
4+2*NE*NE+3*NE+NE27+2*NISGC+NISGI+NFP+4*NEP*
NF) WORDS

NE27: NUMBER OF ENERGY GROUP BOUNDARIES OF IN-SCATTERING GROUPS. STANDARD ESTIMATE: 27 (THE STANDARD ESTIMATES ARE USED AS STARTING VALUES IN THE PROGRAM BUT MAY BE MODIFIED AUTOMATICALLY DEPENDING ON THE ACTUAL JOB CHARACTERISTICS).

NAE: MAXIMUM NUMBER OF EXCITED LEVELS THAT CONTRIBUTE IN A GIVEN OUT-SCATTERING GROUP. STANDARD ESTIMATE: 30.

ISG : MAXIMUM NUMBER OF ENERGY GRID POINTS IN ONE OF THE CONSIDERED OUT-SCATTERING GROUPS. THIS NUMBER IS DETERMINED BY THE COMBINATION OF THE ENERGY GRID POINTS OF ALL EXCITED LEVELS WHICH MUST BE USED IN THE OUT-SCATTERING GROUP AND OF THOSE GRID POINTS OF THE SPECTRUM THAT LIE IN THE OUT-SCATTERING GROUP. STANDARD ESTIMATE: 200

NISGD: ISG+MAXIMUM NUMBER OF ENERGY GRID POINTS OF ANY EXCITED LEVEL (SGIZ) WHICH CONTRIBUTE IN THE OUT-SCATTERING GROUP. STANDARD ESTIMATE: 400.

NISGC: MAXIMUM NUMBER OF ENERGY GRID POINTS OF SGI (SG2N, SG3N) ON KEDAK IN ONE OF THE OUT-SCATTERING GROUPS. STANDARD ESTIMATE: 200.

NISGI: MAXIMUM NUMBER OF ENERGY POINTS AS OBTAINED BY COMBINING THE KEDAK POINTS OF SGI (SG2N, SG3N) AND THE MESH POINTS OF THE SPECTRUM IN ANY OUT-SCATTERING GROUP. STANDARD ESTIMATE: 300.

NEP : NUMBER OF INCIDENT-NEUTRON ENERGIES, FOR WHICH THE DISTRIBUTIONS SEDIC (SED2N, SED3N) ARE GIVEN ON KEDAK. STANDARD ESTIMATE: 30.

NF : NUMBER OF DIFFERENT ANALYTICAL DISTRIBUTIONS GIVEN ON KEDAK FOR SEDIC (SED2N, SED3N) FROM WHICH THE TOTAL DISTRIBUTION MUST BE COMPOSED. STANDARD ESTIMATE: 5

6 APPROXIMATELY 30000 (STANDARD) TO 200000 (MANY GROUPS, LARGE ENERGY DEGRADATION) WORDS. THE EXACT STORAGE REQUIREMENT DEPENDS ON THE MOSTLY UNKNOWN DISTRIBUTION OF THE KEDAK DATA OVER THE ENERGY GROUPS. IT IS RECOMMENDED TO BEGIN WITH THE STANDARD VALUE AND TO INCREASE THE STORAGE SPACE ONLY IF THIS DOES NOT WORK. THE PROGRAM TRIES IN ANY CASE TO ORGANIZE THE CALCULATIONS IN ACCORDANCE WITH THE AVAILABLE MEMORY SPACE.

7 NE WORDS.

8 $NE+2*NFE$ WORDS.

9 $45+NM1*IMAX*(3+NUJM)+ICOS*(4+NIV)+IMAX+2*NJM+NF+15*NMAX+NZM*(2+IZV)+BUF$ WORDS.

NM1 : $NLRE+1$.

IMAX: MAXIMUM ENERGY DEGRADATION IN TERMS OF ENERGY GROUPS (=2 FOR SIMPLE SCATTERING INTO THE ADJACENT GROUP).

ICOS: NUMBER OF ANGULAR GRID POINTS OF THE SENC DATA ON KEDAK.

NIV : NUMBER OF ENERGY GRID POINTS OF THE SENC DATA ON KEDAK.

NMAX: MAXIMUM NUMBER OF ENERGY GRID POINTS WITHIN ONE ENERGY GROUP FOR THE DATA TYPES SGT, SGN OR MUEL ON KEDAK.

NZM : MAXIMUM NUMBER OF ENERGY INTERVALS IN ONE
SUBGROUP TIMES MAXIMUM NUMBER OF SUBGROUPS
PER GROUP.

IZV : MAX(4, IMAX*NMI).

BUF : MAX(2+IMAX*NZM, NTOT), WHERE NTOT IS THE
MAXIMUM NUMBER OF DATA POINTS WITHIN ONE
GROUP FOR THE TYPES SGT, SGN AND MUEL (ALL
THREE CONSIDERED AS A JOINT POINT SET) ON
KEDAK.

10 NO SPACE FOR DATA ARRAYS REQUIRED.

THE REGION PARAMETER ON THE JOB CARD IS THE SUM OF
-MAXIMUM LENGTH OF DATA ARRAYS,
-17CK BYTES FOR THE MIGROS PROGRAM,
-BUFFER LENGTH.

2.2 Description of the output

2.2.1 Printed output

Each computational module prints the results. An explanation of the symbols is given in table V.

2.2.2 Unformatted output

Besides the printed output an unformatted output on unit 3 is provided. The arrangement of this output is described in table VI. The unformatted output of MIGRØS serves as input for the program MITRA, /3/. MITRA checks the results of MIGRØS and transforms them into an input of GRUMA, /4/, the management program for the group constant library GRUBA, /4/.

The following tables are given in chapter 2:

Table V : Symbols used in the printed output of MIGRØS-3.

Table VI : Arrangement of the unformatted output.

Table V Symbols used in the printed output of MIGRØS-3

Module 1

Symbol	content	defined by formula	required KEDAK-types	
SIGMA G	average group cross section for infinite dilution, radiative capture	(4.6)	} ISØT1 ISØT2 RES	
SIGMA N	average group cross section for infinite dilution, elastic scattering	(4.6)		
SIGMA F	average group cross section for infinite dilution, fission	(4.6)		
SIGMANI	identical with SIGMA N	-		
SIGMATI	SIGM G + SIGMA N + SIGMA F	-		
SIGMA O	background cross section σ_o	(4.1)		
FG	flux-weighted resonance self shielding factors for	(4.1)		
FN				} radiative capture elastic scattering fission
FF				
FN1	current weighted resonance self shielding factors for	(4.3)		
FT1			} elastic scattering total	

Temperatures are given in K, the group boundaries in eV, cross sections in barns.

Table V, cont.

Module 2

Symbol	content	defined by formula	required KEDAK-types
SIGMA G	average group cross sections for infinite dilution	radiative capture (5.32)	ISØT1
SIGMA N		elastic scattering (5.33)	
SIGMA F		fission (5.32)	
SIGMAN1	identical with SIGMA N	-	ISØT1
SIGMAT1	SIGMA G + SIGMA N + SIGMA F	-	ISØT2
SIGMA O	background cross section σ_o	(5.1)	ST
FG	flux-weighted resonance self shielding factors	radiative capture	STGF
FN		elastic scattering	
FF		fission	
FN1	current-weighted resonance self shielding factors	elastic scattering	(5.8)
FT1		total	
Temperatures are given in K, group boundaries in eV, cross sections in barns			

Table V, cont.

Module 3

Symbol	content	defined by formula	required KEDAK-types	
SIGMA A ⁺	average group cross sections for infinite dilution,	absorption capture elastic scattering	SGA SGN SGF SGT MUEL	
SIGMA C ⁺				(9.7)
SIGMA N				
SIGMA F		fission		
SIGMA NO1		$\sigma_e \cdot \bar{\mu}_e$		(9.8)
SIGMA T1 SIGMA N1		identical to SIGMA NO1		(9.13)
FA	flux-weighted resonance self-shielding factors,	absorption		
FC		capture		
FN		elastic scattering		
FF		fission		
FN01	flux-weighted resonance self-shielding factor for $\sigma_e \cdot \bar{\mu}_e$	(9.5)		
FN1	current-weighted resonance self-shielding factor for $\sigma_e \cdot \mu_e$	(9.10)		
FT1	current-weighted total resonance self-shielding factor	(9.9)		
SIGO	background cross section σ_0			
Group boundaries are given in eV, cross sections in barns				

⁺ To calculate SIGMA A the KEDAK type SGA (see /5/) is used. In the case of fissionable materials SIGMA C is produced, which is defined by the formula SIGMA C = SIGMA A - SIGMA F.

Table V, cont.

Module 4

Symbol	content	defined by formula	required KEDAK-types
SGN	average group cross section for	(3.1)	SGN
SGA ^{+))}			SGA
SGF			SGF
SGI			SGI
SGC			SGA,SGF
SG2N			SG2N
MUEL	average cosine of elastic scattering	(3.2)	SGN,MUEL
NUE	average number of secondaries per fission	(3.3)	SGF,NUE
ALPHA	average α -value	(3.4)	SGG,SGF
ETA	average η -value	(3.5)	NUE,SGG,SGF

If group averages of other types of cross sections available on KEDAK are calculated, averages in the sense of formula (3.1) are calculated. The names are the same as the names of the underlying KEDAK-types. Cross sections are given in barns.
 If SGN for the material Hbb01 is calculated, also a type STR is calculated, which corresponds to formula (3.6).

^{+))} Definition of the absorption cross section (KEDAK-type SGA; compare /5/):

$$\sigma_{ab} = \sigma(n,\gamma) + \sigma(n,f) + \sigma(n,p) + \sigma(n,d) + \sigma(n,\alpha)$$

Table V, cont.

Module 5

Symbol	content	defined by formula	underlying KEDAK-type
PRØBSGI	transfer probabilities for inelastic scattering	(6.21.1) together with (6.21.2), (6.14) and (6.20.1) with (6.20) and (6.20.2)	ISØT1, SGIZ, SGIZC, SGI, SEDIC
PRØBSG2N	transfer probabilities for (n,2n)-reactions	(6.23)	SG2N, SED2N, ISØT1
PRØBSG3N	transfer probabilities for (n,3n)-reactions	(6.23), where (n,2n) has to be replaced by (n,3n)	SG3N, SED3N, ISØT1
<p>In the first column the numbers of the outscattering groups are printed. The numbers above the values of PRØBSGI(PRØBSG2N, PRØBSG3N) are the inscattering groups.</p>			

Table V, cont.

Module 6

Symbol	content	defined by formula	underlying KEDAK-type
SGNC0	zero'th moment	(7.2)	} SGNC SGN MUEL SGT
SGNC1	1 st moment		
SGNC2	2 nd moment		
SGNC3	3 rd moment		
SGNC4	4 th moment		
SGNC5	5 th moment		
	} of the elastic scattering matrix normalized to the total elastic cross section		
SGN	total elastic group cross section	(7.1)	SGN
MUEL	group-averaged mean elastic-scattering cosine	(7.3)	SGNC SGN MUEL
SGT	total group cross section with moment-dependent weighting	(7.1')	SGT

Table V, cont.

Module 7

Symbol	content	defined by formula	required KEDAK-types
CHI	fission spectrum	(12.1), (12.2), (12.4), (12.6)	CHICR SEDF

Module 8

Symbol	content	defined by formula	required KEDAK-types
1/V	1/v-group averages in [sec/cm]	(11.1)	-

Module 9

Symbol	content	defined by formula	required KEDAK-types
SGT	average total cross section	(8.1)	SGT
SGN	average elastic-scattering cross section	(8.1)	SGN
MUEL	average cosine of elastic scattering	(8.2)	MUEL
FLUX	average flux (weighting function)	-	-
SGNCn	the n-th legendre moment for elastic scattering	(8.3)	SGN, SGNC

Cross sections are given in barns, the legendre moments are normalized to the total elastic cross section. The interval averages within one group are arranged with increasing energy.

Table V, cont.

Module 10

In this module the group constants for the thermal group are calculated. The same types as in module 4 are possible. The group constants are defined by the formulas (10.1) to (10.6).

Table VI: Arrangement of the unformatted output

(The symbols of table V are used)

Module 1

1st record: o , 'MIGR----'
2nd record: n , material name, temperature in /K/, number of the
energy group, lower group boundary in /eV/, upper
group boundary in /eV/
3rd record: n , SIGMA G, SIGMA N, SIGMA F, SIGMA NI, SIGMATI
4th record: n , SIGMA O, FG, FN, FF, FNI, FTI
. .
. .
. .
. for all SIGMA O-values

n is an Integer $I \times 4$ and gives the number of succeeding 4-byte words in the record. The material names are 8-byte alphanumerical words. All other words are REAL*4. The 8-byte alphanumeric words are counted as two words in n. These conventions are the same for all other modules. Exceptions are mentioned. "-" in the label names must be interpreted as blank.

Module 2

1st record: o , 'FSTAT---'
2nd record: n , material name, temperature in /K/, number of the
energy group, lower group boundary in /eV/, upper
group boundary in /eV/.
3rd record: n , SIGMA G, SIGMA N, SIGMA F, SIGMANI, SIGMATI
4th record: n , SIGMA O, FG, FN, FF, FNI, FTI
. .
. .
. for all SIGMA-O values

Table VI, cont.

Module 3

1st record: 0, 'STRK----'

The following records are repeated for each energy group.

2nd record: 5, material name (8 Byte), number of the energy group⁺
lower group boundary measured in eV, upper group boundary
measured in eV.

3rd record: for non-fissionable materials
5, SIGMA A, SIGMA N, SIGMA NO1, SIGMA N1, SIGMA T1
for fissionable materials
6, SIGMA C, SIGMA N, SIGMA F, SIGMA NO1, SIGMA N1, SIGMA T1

4th record: for non-fissionable materials
6, SIGO, FA, FN, FNO1, FN1, FT1
for fissionable materials
7, SIGO, FC, FN, FF, FNO1, FN1, FT1
record 4 is repeated for all SIGO values.

⁺) An internal numeration is used. The group with the greatest number has the highest energy boundaries.

Module 4

1st record: 0, 'SGKE----'

2nd record: n, highest energy group (lowest number), lowest
energy group

3rd record: n, material name, name of reaction type (8-byte,
alphanumeric)

4th record: n, group constant of the type defined by the 3rd
word in the 3rd record, for all energy groups,
specified by the 2nd record. The values are
ordered with increasing energy and decreasing
group numbers.

The records 2 to 4 are repeated for all reaction types, specified by the input.

Table VI, cont.

Module 5

Module 5 produces separately labelled output on unit 3 for inelastic-scattering transfer matrices, for $(n,2n)$ -matrices and for $(n,3n)$ -matrices. In the following the output produced for inelastic-scattering transfer matrices is given first. The output produced for $(n,2n)$ - or $(n,3n)$ -matrices is added in parentheses.

1st record o , 'SMTØT---'('SMTØT2N-' ; 'SMTØT3N-')

2nd record n , material name, total number of outscattering groups

3rd record n , number of the outscattering rroup, elements of
the matrix PRØBSGI (PRØBSG2N; PRØBSG3N) in the sense,
that the first element describes scattering within the
group, the second element describes scattering into
the neighbouring group etc.
repeated for all outscattering groups.

Module 6

1st record: o , 'FLUM----'

2nd record: n , material name, number of outscattering groups, number
of Legendre moments.

3rd record: n , number of the outscattering groups, group averaged
total elastic cross section, group averaged cosine
for elastic scattering, group averaged ψ_l -weighted
total cross sections, $l = 0$, number of Legendre
moments.
repeated for all outscattering groups.

4th record: n , number of the Legendre moment, number of the outscattering
group, matrix elements SGNCi (i = number of the moment)
arranged in the sense that the first word describes
scattering within the group, the next one scattering
into the neighbouring group etc.
repeated for all outscattering groups (for a certain
Legendre moment)
repeated for all Legendre moments.

Table VI, cont.

Module 7

- 1st record: o , 'SPALT---'
2nd record: n , material name, energy of the fission-inducing neutron in eV, number of the lowest energy group, number of the highest energy group.
3rd record: n , CHI for all groups specified in the 2nd record, arranged with increasing energy.

Module 8

- 1st record: o , 'S1/V----'
2nd record: n , 1/V-values for all energy groups defined by the group boundaries in the input, arranged with increasing energy and decreasing group numbers.

Module 9

- 1st record: o , 'REMØ----'
2nd record: n , material name, total number of outscattering groups, total number of Legendre moments.
3rd record: n , number of the outscattering group, number of subgroups in the outscattering group, number of intervals in one subgroup (the same for all subgroups in one outscattering group), SGT for all intervals in one group (product of the number of subgroups and the number of intervals in one subgroup) arranged with increasing energy, SGN for all intervals in one group, MUEL for all intervals in one group, FLUX for all intervals in one group.
repeated for all outscattering groups.
4th record: n , number of the Legendre moment, number of the outscattering group, SGNCi (i = Legendre moment) for all intervals in one group arranged in the sense that first the elements describing scattering within the group, then the elements describing scattering into the neighbouring group etc. are stored.
repeated for all outscattering groups (for a fixed Legendre moment)
repeated for all Legendre moments.

Table VI, cont.

Module 10

1st record: o , 'THERM---'

2nd record: n , material name, name of the reaction type, number
of the thermal group.

3rd record: n , value of the group constant specified in the 2nd record.

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see also chapter II of the KEDAK Program Compendium (KFK 2387, II 2.9)

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Status of the Nuclear Data Library KEDAK-3

October 1975

KFK 2234, NEANDC(E) 171 "U", 1975

3. The calculation of weighted group averages for infinite dilution (from tabulated neutron data). Module 4

3.1 The difference between module 4 in MIGROS-2 and in MIGROS-3 is a more exact method of integration. Again the integration in the averages is done by a trapezoidal rule but the integration points are as well the energy points at which the nuclear data used in the numerator or eventually denominator integral are tabulated on the KEDAK library as the group boundaries as the energy points at which the weighting function is tabulated. The values of the weighting function are linearly interpolated at the energy points of the nuclear data from KEDAK and at the energy group boundaries, and the nuclear data are also linearly interpolated at the energy points of the weighting function and at the energy group boundaries. In the case of a weighting function given as analytical function the integration intervals are given by the energy points of all used nuclear data on KEDAK and the group boundaries. Each interval is divided into three equal parts and the integration is done. Then the integration is repeated once more in the interval now divided into six equal parts. If the results of these two subsequent integrations have a relative deviation greater than 1 %, the interval is now divided into twelve equal parts, the integration is done and the precision is tested once more and so on. If the relative error is less than or equal to 1 % the result of the last integration is taken and the next interval is regarded.

3.2 The average group cross sections are defined by

$${}^k_{\sigma_{x,g}} = \frac{\int_{(g)} {}^k_{\sigma_x}(E) \cdot F(E) dE}{\int_{(g)} F(E) dE} \quad (3.1)$$

k = isotope

x = neutron reaction (n,x)

g = energy group

F(E) is a weighting function given by the input. Normally a slowly varying collision density is used, so that formula (3.1) defines the average group cross section for infinite dilution. The average group cross sections for all types of neutron reactions are calculated by formula (3.1) except:

- the average cosine of the elastic scattering

$$k_{\mu_e, g}^- = \frac{\int_{(g)} k_{\mu_e}^-(E) \cdot k_{\sigma_e}(E) \cdot F(E) dE}{\int_{(g)} k_{\sigma_e}(E) \cdot F(E) dE} \quad (3.2)$$

- the average number of secondaries per fission

$$k_{\nu, g} = \frac{\int_{(g)} k_{\nu}(E) \cdot k_{\sigma_f}(E) \cdot F(E) dE}{\int_{(g)} k_{\sigma_f}(E) \cdot F(E) dE} \quad (3.3)$$

- the average α -value

$$k_{\alpha, g} = \frac{\int_{(g)} k_{\sigma_\gamma}(E) \cdot F(E) dE}{\int_{(g)} k_{\sigma_f}(E) \cdot F(E) dE} \quad (3.4)$$

γ = radiative capture

- the average η -value

$$k_{\eta, g} = \frac{k_{\nu, g}}{1 + k_{\alpha, g}} \quad (3.5)$$

For which type of neutron reaction an average cross section shall be calculated can be chosen by input. There must be information available on the KEDAK library. If the reaction types σ_a^{+} and σ_f are given in the input, the type $\sigma_c = \sigma_a - \sigma_f$ is automatically calculated.

Besides that, the following group average

$$\sigma_{\text{beH}}^{(g)} = \frac{\int \frac{\sigma_e(E)}{E} \cdot F(E) dE}{\int F(E) dE} \quad (3.6)$$

is calculated for hydrogen. This group average can be used for the production of the elastic scattering matrix.

3.3 The following subroutines are necessary

SUBROUTINE SUND (MM, ENG, NFE, REFE, EFE, ITYP, ITNAM, SGC, DUE, XINTE, ZINT, XNEN, STREU, LDIM, LDIMP, SE, FSE)

The following parameters are defined by the control program:

MM	Number of energy group boundaries,
ENG(MM)	one-dimensional field containing the energy group boundaries in [eV],
NFE	number of points of the neutron flux density, = 1, if the function PHI(E) is used,
REFE(NFE)	one-dimensional field containing the energy points of the weighting function in eV ,
EFE(NFE)	one-dimensional field containing the weighting function,
ITYP	number of cross section types,
ITNAM(ITYP)	one-dimensional field containing the names of the reaction types for which the weighted group averages shall be calculated,
LDIM	dimension of the following fields SE and FSE which is max (1500, number of $\sigma_e(E)$ values on KEDAK, number of $\sigma_f(E)$ values on KEDAK in all regarded energy groups).

^{*)}The absorption cross section σ_a (KEDAK-type SGA) is defined on KEDAK in the following way:

$$\sigma_a = \sigma(n,\gamma) + \sigma(n,f) + \sigma(n,p) + \sigma(n,d) + \sigma(n,\alpha) \quad //$$

The following parameters are working fields used by the subroutine SUND

SGC, DUE, XINTE, ZINT, XNEN, STREU one-dimensional fields of
the length MM,

SE, FSE one-dimensional fields of the length LDIM which are
used for the calculation of $k_{\mu_{e,g}}^-$ and k_{ν_g} containing
the energies and $k_{\sigma_e}(E)$ or the $k_{\sigma_f}(E)$ respectively.

The following parameter is calculated in SUND

LDIMP: 0, if the length of the working fields dimensioned
with LDIM is sufficient,
n, number by which LDIM should be increased.

The subroutine SUND calls GRUP and FL.

SUBROUTINE GRUP (I, II, M, ENG, SE, FSE, SF, MOD)

The subroutine GRUP is used only for the calculation of k_{ν_g} . Because on
KEDAK the σ_f -values start to be greater zero at a higher energy than
the ν -values, it is not possible to calculate ν_g with formula (3.3)
in the lower energy region. A way out of this is to set σ_f internally
in this module equal to a positive value (1.E20) for all energies with
 $\sigma_f = 0$ on KEDAK. The task of subroutine GRUP is to reset σ_f from
1.E20 to 0, if σ_f was not set in the entire actual energy group equal
to 1.E20, that means, if σ_f is not zero on KEDAK in the entire energy group.

The following parameters are defined by SUND or by the control program.

I Index of the lower energy group boundary in field ENG,
II beginning index in the field SE for the actual energy group,
M length of the field SE,
ENG one-dimensional field containing the energy group boundaries,
SE(M) one-dimensional field containing the energy points of
 k_{σ_f} from KEDAK,
FSE(M) one-dimensional field containing the k_{σ_f} values from KEDAK,
SF lower integration interval boundary in the actual energy group,

MOD = 0 field SE contains the original σ_f values from KEDAK,
 = 1 field SE contains the modified σ_f values (zero modified
 to 1.E20).

SUBROUTINE FL (EFE1, EFE2, REFE1, REFE2, E, ERG)

The task of FL is to realize the linear interpolation of the weighting function and the cross sections from KEDAK to the boundaries of the integration interval.

The following parameters are defined by SUND.

EFE1 Value of the lower interpolation base,
EFE2 value of the higher interpolation base,
REFE1 energy point of EFE1,
REFE2 energy point of EFE2,
E energy point of the value to be calculated.

The following parameter is filled by FL.

ERG Interpolated value to energy E.

/1/ B. Goel, B. Krieg,

Status of the Nuclear Data Library KEDAK-3

October 1975

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4. The calculation of weighted average group cross sections for infinite dilution and of energy resonance self shielding factors from resolved resonance parameters. Module 1.

4.1 Flux-weighted energy resonance self shielding factors are calculated for capture, fission and elastic scattering. They are defined as

$${}^k f_{x,g}(\sigma_o, T) = \frac{{}^k \tilde{\sigma}_{x,g}(\sigma_o, T)}{{}^k \tilde{\sigma}_{x,g}(\sigma_o \rightarrow \infty, T)} \quad (4.1)$$

k = isotope

x = neutron reaction (n,x)

g = energy group

T = temperature in K

σ_o = background cross section in barns

where

$${}^k \tilde{\sigma}_{x,g}(\sigma_o, T) = \frac{\left\langle \frac{{}^k \tilde{\sigma}_x(T, E) F(E)}{{}^k \tilde{\sigma}_t(T, E) + \sigma_o} \right\rangle}{\left\langle \frac{F(E)}{{}^k \tilde{\sigma}_t(T, E) + \sigma_o} \right\rangle} \quad (4.2)$$

is the microscopic effective cross section.

The weighting function $F(E)$ is the collision density and is assumed to have no resonance structure in the NR-approximation.

$F(E)$ is the weighting function defined by the input.

(See Card 4 of the input description.)

The average is defined as

$$\langle y(E) \rangle = \frac{1}{\Delta E_g} \int_{\Delta E_g} y(E) dE$$

where ΔE_g is the group width of group g .

The current-weighted resonance self-shielding factors are calculated for elastic scattering and for the total neutron reaction

$$k_{f,x,g}^k(\sigma_o, T) = \frac{k_{\tilde{\sigma}_{x,g}}^k(\sigma_o, T)}{k_{\tilde{\sigma}_{x,g}}^k(\sigma_o \rightarrow \infty, T)} \quad (4.3)$$

where

$$k_{\tilde{\sigma}_{x,g}}^k(\sigma_o, T) = \frac{\left\langle \frac{k_{\tilde{\sigma}_x}^k(T, E) F(E)}{\{k_{\tilde{\sigma}_t}^k(T, E) + \sigma_o\}^2} \right\rangle}{\left\langle \frac{F(E)}{\{k_{\tilde{\sigma}_t}^k(T, E) + \sigma_o\}^2} \right\rangle} \quad (4.4)$$

is the current weighted microscopic effective cross section. For infinite dilution

$$\lim_{\sigma_o \rightarrow \infty} k_{\tilde{\sigma}_{x,g}}^k(\sigma_o, T) = \lim_{\sigma_o \rightarrow \infty} k_{\tilde{\sigma}_{x,g}}^k(\sigma_o, T) = k_{\tilde{\sigma}_{x,g}}^k \infty \quad (4.5)$$

and

$${}^k\sigma_{x,g}^{\infty}(T) = \frac{\langle {}^k\tilde{\sigma}_x(E, T) F(E) \rangle}{\langle F(E) \rangle} \quad (4.6)$$

Therefore the denominators of (4.1) and (4.3) may be replaced by (4.6).

Normally ${}^k\sigma_{x,g}^{\infty}$ is independent of temperature, but in cases when only few resonances are within an energy group, and the group boundary cuts the wings of an important resonance, ${}^k\sigma_{x,g}^{\infty}$ may be temperature dependent.

The averages of (4.2), (4.4) and (4.6) are calculated by numerical integration. The microscopic cross sections $\sigma_x(E)$ are calculated from resonance parameters by a Breit-Wigner single level formula.*

$$\tilde{\sigma}_x(E, T) = \sum_{r=1}^R \tilde{\sigma}_x(E, E_r, T) \quad (4.7)$$

r = resonance

R = number of resonances taken into account

E_r = resonance energy

$$\tilde{\sigma}_x(E, E_r, T) = {}_r\tilde{\sigma}_{ox} \cdot \Psi_r(\theta, x) \quad (4.8a)$$

for radiative capture and fission,

* (the index for the isotope will be neglected)

$$\tilde{\sigma}_t(E, E_r, T) = \tilde{\sigma}_p + r_{oc} \tilde{\sigma} \cdot \{ \Psi_r \cdot \cos 2\delta_L + \chi_r \cdot \sin 2\delta_L \} \quad (4.8b)$$

and for elastic scattering

$$\tilde{\sigma}_e(E, E_r, T) = \tilde{\sigma}'_t(E, E_r, T) - \sum_x \tilde{\sigma}_x(E, E_r, T) \quad (4.8c)$$

x = radiative capture, fission, where

$$\tilde{\sigma}_{ox} = 4\pi \lambda^2(E) \cdot g \cdot \frac{\Gamma_n(E) \Gamma_x(E_r)}{\Gamma^2(E)} \quad (4.9)$$

$$\tilde{\sigma}_{oc} = 4\pi \lambda^2(E) \cdot g \cdot \frac{\Gamma_n(E)}{\Gamma(E)} \quad (4.10)$$

$$\Psi(\theta, x) = \frac{\theta}{2\sqrt{\pi}} \int_{-\infty}^{+\infty} \frac{\exp\left\{-\frac{\theta^2}{4} \cdot (x-y)^2\right\}}{1+y^2} dy \quad (4.11)$$

$$\chi(\theta, x) = \frac{\theta}{2\sqrt{\Gamma}} \int_{-\infty}^{+\infty} \frac{y \cdot \exp\left\{-\frac{\theta^2}{4} \cdot (x-y)^2\right\}}{1+y^2} dy \quad (4.12)$$

$$\theta = \frac{\Gamma}{\Delta}, \quad x = \frac{2(E-E_r)}{\Gamma(E)}, \quad y = \frac{2(E'-E_r)}{\Gamma(E)} \quad (4.13)$$

$$\Delta = \left(\frac{4kTE}{A}\right)^{1/2} : \text{Doppler width}$$

$$\Gamma(E) = \Gamma_n(E) + \sum_{x \neq n} \Gamma_x : \text{total width}$$

$$\delta_\ell = \frac{R'}{\lambda} - \arctg \frac{R'}{\lambda} \cdot \ell \text{ for } \ell = 0, 1$$

R' : effective radius of the nucleus

λ : reduced neutron length

$$\Gamma_n(E) = \Gamma_n(E_r) \left(\frac{E}{E_r}\right)^{1/2} \left[\frac{(R'/\lambda)^2}{1+(R'/\lambda)^2}\right]^\ell \text{ for } \ell = 0, 1 : \text{neutron width}$$

For resonances at negative resonance energies the KEDAK file contains the reduced width Γ_n^ℓ in place of the neutron width $\Gamma_n(E_r)$ and $\Gamma_n(E)$ is calculated as

$$\Gamma_n(E) = \Gamma_n^\ell \sqrt{\frac{E}{1\text{eV}}} \left[\frac{(R'/\lambda)^2}{1+(R'/\lambda)^2}\right]^\ell$$

Γ_x : fission or radiative capture width

$$\sigma_P = 4\pi\lambda^2 \sum_{\ell=0}^1 (2\ell+1) \sin^2 \delta_\ell : \text{potential cross section}$$

For $\Gamma \rightarrow 0$, that means $\Theta \rightarrow \infty$, one obtains the unbroadened resonance profiles

$$\psi(\Theta \rightarrow \infty, x) = \frac{1}{1 + x^2}$$

$$\chi(\Theta \rightarrow \infty, x) = \frac{x}{1 + x^2}$$

It should be pointed out that eqs. (4.9) - (4.13) and some of the definitions below eq. (4.13) supersede those given in the original description of MIGROS-2 (H. Huschke, B. Krieg, KFK 1784).

Corresponding changes have been made in the subprograms WIRQ and WIRQU in order to improve the accuracy of cross section calculations between resonances and in the thermal region. These changes refer to the energy dependences of Γ_n (hence Γ), Δ and σ_p , which are now fully taken into account.

4.2 The method of integration for the averages in (4.2), (4.4) and (4.6)

The expressions (4.2), (4.4) and (4.6) are calculated by numerical integration. The trapezoidal rule is used. To keep the number of integration points as small as possible the integration points are not taken as equidistant. This is necessary, because the calculation of the function values is very time consuming. To be sure that the resonances are not lost during the integration, the resonance energies are chosen as integration points. Let X_i be the integration points and Y_i the corresponding function values. Then the integration algorithm can be described in the following way:

First step: Initial abscissa and ordinate vectors are defined as

$$X^0 = (X_1^0, X_2^0, X_3^0, \dots, X_{n-1}^0, X_n^0) = (E_{g+1}, E_{r,1}, E_{r,2}, \dots, E_{r,n-2}, E_g)$$

$$Y^0 = (Y_1^0, Y_2^0, Y_3^0, \dots, Y_{n-1}^0, Y_n^0)$$

with

$$\begin{aligned} E_{g+1} &: \text{lower group limit,} \\ E_g &: \text{upper group limit,} \\ E_{r,i} &: \text{resonance energy of } i\text{-th resonance in} \\ &\quad \text{energy group } g, \end{aligned}$$

and $Y_i^0 = F(X_i^0)$, where $Y = F(E)$ is the integrand function.

Second step: The center of the first interval is added to the grid points, and new abscissa and ordinate vectors are defined accordingly,

$$X^1 = (X_1^1, X_2^1, X_3^1, \dots, X_{n+1}^1) = (X_1^0, \frac{1}{2}(X_1^0 + X_2^0), X_2^0, \dots, X_n^0),$$

$$Y^1 = (Y_1^1, Y_2^1, Y_3^1, \dots, Y_{n+1}^1) = (Y_1^0, F(X_2^1), Y_2^0, \dots, Y_n^0).$$

Furthermore one calculates the contributions from the interval $[X_1^1, X_2^1]$ to the trapezoidal-rule integral with and without the newly-inserted grid point,

$$a = \frac{1}{2}(Y_2^1 + Y_1^1) (X_2^1 - X_1^1),$$

$$b = \frac{1}{2}(\tilde{Y}_2^1 + Y_1^1) (X_2^1 - X_1^1)$$

with $\tilde{Y}_2^1 = \frac{1}{2}(Y_3^1 + Y_1^1)$.

This second step is repeated until the criterion

$$\left| \frac{b - a}{a} \right| < \epsilon \quad (4.18)$$

is fulfilled twice in succession. To be specific let the condition (4.18) be fulfilled after $m-1$ and again after m applications of the second step, the last application yielding

$$X^m = (X_1^m, X_2^m, X_3^m, \dots, X_{n+m}^m) = (X_1^{m-1}, \frac{1}{2}(X_1^{m-1} + X_2^{m-1}), X_2^{m-1}, \dots, X_{n+m-1}^{m-1}),$$

$$Y^m = (Y_1^m, Y_2^m, Y_3^m, \dots, Y_{n+m}^m) = (Y_1^{m-1}, F(X_2^m), Y_2^{m-1}, \dots, Y_{n+m-1}^{m-1}).$$

The calculation proceeds then to the interval $[X_2^m, X_3^m]$:

Third step: One calculates the contributions with and without the last inserted grid point from the interval $[X_2^m, X_3^m]$,

$$a = \frac{1}{2}(Y_3^m + Y_2^m) (X_3^m - X_2^m),$$

$$b = \frac{1}{2}(Y_3^m + \tilde{Y}_2^m) (X_3^m - X_2^m)$$

with
$$\tilde{Y}_2^m = \frac{1}{2}(Y_3^m + Y_1^m).$$

If the condition

$$\left| \frac{b - a}{a} \right| < \epsilon \tag{4.19}$$

is fulfilled the integral over the interval $[X_1^m, X_3^m]$ is taken as

$$I_1 = \frac{1}{2}(Y_3^m + Y_1^m) (X_3^m - X_1^m)$$

and the whole algorithm is now applied to the remaining interval $[X_3^m, X_{n+m}^m]$ starting with the ordinate vector

$$X^o = (X_1^o, X_2^o, \dots, X_{n+m-2}^o) = (X_3^m, X_4^m, \dots, X_{n+m}^m).$$

If the criterion (4.10) is not satisfied the integral over the interval $[X_1^m, X_2^m]$ is taken as

$$I_1 = \frac{1}{2}(Y_2^m + Y_1^m) (X_2^m - X_1^m)$$

and the algorithm is repeated in the remaining interval $[X_2^m, X_{n+m}^m]$ starting with the ordinate vector

$$X^0 = (X_1^0, X_2^0, \dots, X_{n+m-1}^0) = (X_2^m, X_3^m, \dots, X_{n+m}^m)$$

The algorithm is repeated until the integration over the total energy width is performed. The integral over the energy group is given by the sum.

$$I = \sum_{i=1}^{N+1} I_i, \text{ where } N \text{ is the number of repetitions of the algorithm.}$$

4.3 For the calculation of energy resonance self shielding factors and average weighted group constants from resolved resonance parameters the following subroutine are used:

FGEM (NS, SIGO, NE, ENG, NEF, ES, F, NT, TEMP, PR, NMR, NFST, SUM, SUO, IRE, IREP, ER, L, GJ, GAT, GAN, GAG, GAF, ISTE, ISTEP, STE, STE1)

In this subroutine the input of the nuclear data from the Karlsruhe nuclear data library KEDAK and the output of the f-factors and the average cross sections is organized. Also the integration algorithm is performed in this subroutine. The following parameters must be defined:

NS : number of σ_0 -values.
SIGO(NS) : one-dimensional field containing the σ_0 -values [barn].
NE : number of the group boundaries.
ENG(NE) : one-dimensional field containing the group boundaries [eV].
NEF : number of energy points of the weighting spectrum.
ES(NEF) : one-dimensional field containing the energy points of the weighting spectrum [eV].
F(NEF) : one-dimensional field containing the weighting function at the energy points of field ES.

NT : number of temperatures.
TEMP(NT) : one-dimensional field containing the temperatures
[K].
PR : error limit ϵ , as defined in (4.18).
NMR : R/2 as defined in (4.7).
IRE : length of working fields, should be longer than
the number of resonances for one isotope.
ISTE : length of a working field for integration, should
be longer than the number of integration points
necessary for the integration of effective group
cross sections within one group.

Working fields:

SUM(NS,7), SUO (NE,3), ER (IRE), GJ (IRE), GAT (IRE), GAN (IRE),
GAG (IRE), GAF (IRE), STE (5, ISTE), STE1(ISTE)

The following parameters are calculated in the subroutine:

NFST : number of the first energy group, for which f-factors
can be calculated only from statistical resonance
parameters. This parameter is important only, if the
f-factors are calculated for an energy range,
covering both, the range of resolved and the range
of unresolved resonances.
IREP : 0, if the length of the working fields dimensioned
with IRE is sufficient.
: n number, by which IRE should be increased.
ISTEP : 0, if the length of the working field dimensioned
with ISTE is sufficient.
: n number, by which ISTE should be increased.

Information is also transferred by the unlabeled COMMON. It is
described in chapter 1.

A description of the output is given in chapter 1.

WIRQ (INR, E, SF, SG, ST, IRE, ER, GJ, GAN, GAT, GAF, L, GAG, T, A, R,
RLA)

In this subroutine the contribution of one resonance to the energy dependent cross section at a given energy is calculated by a Breit-Wigner single level formula.

The following parameters must be defined:

INR : number of the resonance (all resonances of an isotope are numbered with increasing resonance energies).

E : energy, [eV].

ER(IRE) : one-dimensional field containing the resonance energies for one isotope, [eV].

IRE : must be greater or equal to the number of resonances for one isotope.

GJ(IRE) : one dimensional field containing the statistical parameters g_j for all resonances of one isotope.

GAN(IRE) : one dimensional field containing the neutron half widths for all resonances of one isotope, [eV].

GAT(IRE) : one dimensional field containing the total half widths for all resonances of one isotope, [eV].

GAF(IRE) : one dimensional field containing the fission widths for all resonances of one isotope, [eV].

L(IRE) : one dimensional field containing the neutron angular momentum for all resonances of one isotope.

GAG(IRE) : one dimensional field containing the capture widths for all resonances of one isotope, [eV].

T : temperature in K.

A : atomic weight.

R : radius of the nucleus, [$\sqrt{\text{barn}}$].

RLA : reduced neutron wave length, [$\sqrt{\text{barn}} \cdot \sqrt{\text{eV}}$].

The following parameters are calculated in the subroutine:

SF : contribution to the fission cross section at the energy E from the resonance with number INR, [barn].
SG : contribution to the capture cross sections at the energy E from the resonance with number INR [barn].
ST : contribution to the total resonance cross section at the energy E from the resonance with number INR, [barn].

WIRQU (NR1, E, SIFG, SIGG, SIGT, NR, IRE, ER, GJ, GAN, GAT, GAF, L, GAG, T, A, R, RLA, NMIN)

In this subroutine the sum of the contribution to the cross section at the energy E from all resonances, that are taken into account, is performed.

The following parameters must be defined:

NR1 : the number of the resonance belonging to the first resonance energy that is greater than the higher energy limit of the actual energy group. All resonances of an isotope are numbered with increasing resonance energies).
E : energy [eV].
NR : maximum number of resonances for one isotope.
IRE : must be greater or equal to NR.
ER(IRE) : one-dimensional field containing the resonance energies for one isotope.
GJ(IRE) : one-dimensional field containing the statistical parameters g_j for all resonances of one isotope.
GAN(IRE) : one-dimensional field containing the neutron half widths for all resonances of one isotope [eV].
GAT(IRE) : one-dimensional field containing the total half widths for all resonances of one isotope. [eV].
GAF(IRE) : one-dimensional field containing the fission half widths for all resonances of one isotope. [eV].

L(IRE) : one-dimensional field containing the neutron angular momentum for resonances of one isotope.
GAG(IRE) : one dimensional field containing the capture widths for all resonances of one isotope. [eV].
T : temperature in K.
A : atomic weight.
R : radius of the nucleus in [$\sqrt{\text{barn}}$]
RLA : reduced neutron wave length, [$\sqrt{\text{barn}} \cdot \sqrt{\text{eV}}$].
NMIN : the number of resonances at higher and at lower resonance energies than the energy E, that are taken into account for the calculation of the cross sections at the energy E.

The following parameters are calculated in the subroutine:

SIFG : fission cross section at the energy E, [barn].
SIGG : radiative-capture cross section at the energy E, [barn].
SIGT : total cross section at the energy E, [barn].

STOSS (E1, E2, E3, F1, F2, F3, NFE, ES, F)

In this subroutine the macroscopic weighting function (collision density) at the energies E1, E2, E3 is calculated either from an energy point wise given weighting function by interpolation or from a function PHI(E). As standard PHI(E) = 1/E is used.

The following parameters must be defined:

E1, E2, E3 : energies in [eV].
NFE : number of energy points of the weighting spectrum.
If NFE = 0,1, the standard PHI(E) = 1/E is used.
ES(NFE) : one-dimensional field containing the energy points of the weighting spectrum [eV].
F(NFE) : one-dimensional field containing the weighting spectrum.

The following parameters are calculated in this subroutine:

F1, F2, F3 : weighting spectrum at the energies E1, E2, E3.

PSIXI(X, T, U, V) /1/, /2/.

In this subroutine the functions (4.11) and (4.12) are calculated.

The following parameters must be defined:

X : defined as (4.13)

T : is defined as $\left\{\frac{1}{\theta}\right\}^2$, where θ is given in (4.13).

The following parameters are calculated in the subroutine:

U : defined by (4.11)

V : defined by (4.12)

References

/1/ H. Späth, INR-Arbeitsbericht, private Communication.

/2/ C. Chiarella, A. Reichel

On the Evaluation of Integrals Related to the Error Function
Math. of Computation 22, 1968, p. 137 - 143.

5. The calculation of average group cross sections for infinite dilution and of energy resonance self shielding factors from statistical resonance parameters. Module 2

The main change in module 2 compared to the description given in /3/ concerns the calculation of the statistical mean values $\overline{s\Gamma_x J(s\beta, s\theta)}$ and $\overline{s\Gamma J(s\beta, s\theta)}$. In the former version of the programme analytic approximations were used for the integrals under conditions depending on the Doppler width Δ and on the background cross-section σ_0 , namely for

$$\frac{\overline{sD}}{\sqrt{2\pi} \cdot \Delta} \cdot \frac{\langle s\tilde{\sigma}_r \rangle}{s\tilde{\sigma}_{p,eff}} \cdot sE_r < 0.1$$

(compare formulas (5.28) to (5.32) of /3/). In the new version of the module $\overline{s\Gamma_x J(s\theta, s\beta)}$ and $\overline{s\Gamma J(s\Gamma, s\beta)}$ are in all cases calculated by numerical integration. Although this procedure is more time consuming it was preferred, as the results of the original programme showed deviations from the expected trend of the resonance self shielding factors as function of the temperature, which were removed by use of the modified programme.

5.1 The flux weighted resonance self shielding factors are calculated for radiative capture, fission and elastic scattering. They are defined as

$$k_{f,x,g}^r(\tilde{\sigma}_0, T) = \frac{k_{x,g}^r(\tilde{\sigma}_0, T)}{k_{x,g}^r(\tilde{\sigma}_0 \rightarrow \infty, T)} \quad (5.1)$$

$k_{\sigma_{x,g}}^r$ = microscopic effective group cross section (group cross section for a certain background cross section σ_0 and a certain temperature T)

k = isotope

x = neutron reaction (n,x)

g = energy group

T = temperature in K

σ_0 = background cross section in barns.

The following approximation is used:

$$k_{x,g}^r(\tilde{\sigma}_0 \rightarrow \infty, T) \cong k_{x,g}^r(\tilde{\sigma}_{0,max}, T) \quad (5.2)$$

with

$$\tilde{\sigma}_{0,max} = \max(10^6, \text{highest } \sigma_0 \text{ value given by the input}) \quad (5.3)$$

The microscopic effective group cross section may be represented by

$$\bar{\sigma}_{x,g}(\bar{\sigma}_o, T) = \frac{\sum_j \phi_j \cdot \sigma_{x,g}(\bar{\sigma}_o, T, E_j) \cdot \Delta E_j}{\sum_j \phi_j \cdot \Delta E_j} \quad (5.4)$$

ϕ_j is a slowly varying, resonance free flux density at the energy E_j , normally approximated by a collision density (The weighting function defined by the input is used. See card 4 of the input description.)

ΔE_j = energy interval around E_j

$\sigma_{x,g}(E_j)$ is the effective cross section in the energy interval ($=\sigma_{x,g}(\bar{\sigma}_o, T, E_j)$) ΔE_j around E_j belonging to energy group g) for the temperature T and the background cross section $\bar{\sigma}_o$.

The $\sigma_{x,g}(E_j)$ are slowly varying with energy when calculated from statistical resonance parameters. The group average of (5.4) is therefore performed in the following approximate way

$$\bar{\sigma}_{x,g}(\bar{\sigma}_o, T) \simeq \frac{\sum_j \phi_j \cdot \sigma_{x,g}(E_j)}{\sum_j \phi_j} \quad (5.5)$$

where for the E_j are chosen: the upper and the lower group boundary of group g , E_g and E_{g+1} , and $(E_g + E_{g+1})/2$.

$\sigma_{x,g}(E_j)$ is composed of the contributions of all resonance series s .

$$\tilde{\sigma}_{x,g}(E_j) = \sum_s \tilde{\sigma}_{x,g}^s(E_j) \quad (5.6)$$

for radiative capture and fission, and

$$\tilde{\sigma}_{e,g}(E_j) = \sum_s \{ \tilde{\sigma}_{r,g}^s(E_j) - \tilde{\sigma}_{c,g}^s(E_j) - \tilde{\sigma}_{f,g}^s(E_j) \} + \tilde{\sigma}_p \quad (5.7)$$

$\sigma_{r,g}^s(E_j)$ is the total resonance cross section, (c = radiative capture, f = fission).

The current weighted resonance self shielding factors are calculated for the total neutron reaction and for elastic scattering. They are defined as :

$$k_{rx}(\tilde{\sigma}_o, T) = \frac{k_{1\tilde{\sigma}_{x,g}}(\tilde{\sigma}_o, T)}{k_{1\tilde{\sigma}_{x,g}}(\tilde{\sigma}_o \rightarrow \infty, T)} \quad (5.8)$$

where

$$k_{1\tilde{\sigma}_{x,g}}(\tilde{\sigma}_o \rightarrow \infty, T) \cong k_{1\tilde{\sigma}_{x,g}}(\tilde{\sigma}_{o,max}, T) \quad (5.9)$$

$\sigma_{o,max}$ is given by (5.3).

The microscopic effective cross section for the neutron reaction (n,x) in the energy group g may be written as :

$${}^1\tilde{\sigma}_{x,g} = \frac{\sum_j {}^1\phi_j \cdot {}^1\tilde{\sigma}_{x,g}(E_j) \cdot \Delta E_j}{\sum_j {}^1\phi_j \cdot \Delta E_j} \quad (5.10)$$

${}^1\phi_j$ is a slowly varying, resonance free current density, normally approximated by a collision density. (In the programme the weighting function defined by the input is used; card 4 of the input description.)

For (5.10) the same approximation for averaging as for (5.5) is used.

${}^1\sigma_{x,g}(E_j)$ is composed of the contributions of the single resonance series s.

$${}^1\tilde{\sigma}_{e,g}(E) = \sum_s \left\{ {}^s\tilde{\sigma}_{r,g}(E_j) - {}^s\tilde{\sigma}_{c,g}(E_j) - {}^s\tilde{\sigma}_{f,g}(E_j) \right\} + \tilde{\sigma}_p \quad (5.11)$$

$${}^1\tilde{\sigma}_{t,g}(E) = \sum_s {}^s\tilde{\sigma}_{r,g} + \tilde{\sigma}_p \quad (5.12)$$

The effective resonance cross section at the energy E_j and the series s is calculated by a theory, first developed by R. Froelich /1/, /2/ and modified by H. Huschke. This modified theory is given in appendix I of /3/.

$${}^s\tilde{\sigma}_{x,g}(E) = {}^s\tilde{\sigma}_{p,eff} \frac{\left[1 + \frac{\langle {}^s\tilde{\sigma}_r \rangle}{\langle {}^s\tilde{\sigma}_t \rangle} \right] \frac{{}^s\Gamma_x \cdot J(\beta, \theta)}{{}^sD \cdot \cos 2\delta_L} - \frac{{}^sD \langle {}^s\tilde{\sigma}_x \rangle \langle {}^s\tilde{\sigma}_r \rangle}{\Delta \sqrt{2\pi} \langle {}^s\tilde{\sigma}_t \rangle^2} \cdot E}{1 - \left[1 + \frac{\langle {}^s\tilde{\sigma}_r \rangle}{\langle {}^s\tilde{\sigma}_t \rangle} \right] \frac{{}^s\Gamma_x \cdot J(\beta, \theta)}{{}^sD} + \frac{{}^sD \langle {}^s\tilde{\sigma}_r \rangle^2}{\Delta \sqrt{2\pi} \langle {}^s\tilde{\sigma}_t \rangle^2} \cdot E} \quad (5.13)$$

for fission and capture

and

$${}^s\tilde{\sigma}_{r,g}(E) = {}^s\tilde{\sigma}_{p,eff} \frac{\left[1 + \frac{\langle \tilde{\sigma}_r \rangle}{\langle \tilde{\sigma}_t \rangle} \frac{{}^s\Gamma \cdot J({}^s\beta, {}^s\theta)}{{}^sD} - \frac{{}^sD \langle \tilde{\sigma}_r \rangle^2}{\Delta \sqrt{2\pi} \langle \tilde{\sigma}_t \rangle^2} \cdot \varepsilon \right]}{1 - \left[1 + \frac{\langle \tilde{\sigma}_r \rangle}{\langle \tilde{\sigma}_t \rangle} \frac{{}^s\Gamma \cdot J({}^s\beta, {}^s\theta)}{{}^sD} + \frac{{}^sD \langle \tilde{\sigma}_r \rangle^2}{\Delta \sqrt{2\pi} \langle \tilde{\sigma}_t \rangle^2} \cdot \varepsilon \right]} \quad (5.14)$$

for the total resonance cross section.

${}^s\Gamma_x$ width for the neutron reaction (n,x) and the resonance series s

${}^s\Gamma$ total width for the resonance series s.

$$J(\beta, \theta) = \int_0^{\infty} \frac{\psi(\theta, x)}{\psi(\theta, x) + \beta} dx \quad (5.15)$$

$$\psi(\theta, x) = \frac{\theta}{2\sqrt{\pi}} \int_{-\infty}^{+\infty} \frac{\exp\left\{-\frac{\theta^2}{4} \cdot (x-y)^2\right\}}{1+y^2} dy \quad (5.16)$$

$$\theta = \frac{\Gamma}{\Delta} \quad , \quad \Delta = \sqrt{\frac{4kTE}{A}} \quad (5.17)$$

k = Boltzmann constant

E = energy

A = mass number

T = temperature

$$\delta_l = \frac{R}{\lambda} - \arctg \frac{R}{\lambda} \cdot l \quad \text{for } l = 0, 1; \quad \delta_2 = \frac{R}{\lambda} - \arctg \left(\frac{3\frac{R}{\lambda}}{3 - (\frac{R}{\lambda})^2} \right)$$

R = effective radius of the nucleus

λ = reduced neutron wave length

$\overline{s_D}$ = average level distance for the resonance series s.

$$\overline{\Gamma \cdot \Gamma} \equiv \int_0^{\infty} \Gamma_n \cdot \Gamma_f \cdot {}^s F_n(\Gamma_n) \cdot {}^s F_f(\Gamma_f) d\Gamma_n d\Gamma_f \quad (5.18)$$

where ${}^s F_n(\Gamma_n)$ is the distribution of the neutron width of the resonance series s and ${}^s F_f(\Gamma_f)$ is the distribution of the fission width of the resonance series s.

$\langle \tilde{\sigma}_x \rangle$ *) average cross section of the neutron reaction (n,x) for the series s (See formula (5.28))

$\langle \tilde{\sigma}_r \rangle$ average resonance cross section of the series s. (See formula (5.33))

$$\langle \tilde{\sigma}_t \rangle \equiv \tilde{\sigma}_o + \tilde{\sigma}_p + \sum_s \langle \tilde{\sigma}_r \rangle, \quad (5.19)$$

with

$$\tilde{\sigma}_o = \frac{1}{N} \left\{ \langle \Sigma_t \rangle - N \cdot (\tilde{\sigma}_p + \sum_s \langle \tilde{\sigma}_r \rangle) \right\} \quad (5.20)$$

*) $\langle y(E) \rangle = \frac{1}{\Delta E} \int_{\Delta E} y(E) dE$

the average background cross section.

Σ_t is the total cross section of the mixture.

$${}^s\tilde{\sigma}_{p,eff} = \langle \tilde{\sigma}_t \rangle - \langle {}^s\tilde{\sigma}_r \rangle \quad (5.21)$$

$$s\beta = \frac{\langle \tilde{\sigma}_t \rangle}{{}^s\tilde{\sigma}_{oc}} \quad (5.22)$$

$${}^s\tilde{\sigma}_{oc} = 4\pi \lambda^2 \cdot g \cdot \frac{{}^s\Gamma_n}{s\Gamma} \cdot \cos 2\delta_l \quad (5.23)$$

$$\varepsilon = 2 \cdot \int_0^{\infty} \exp\left\{-\frac{D^2}{2\Delta^2}\right\} \cdot \Omega(D) dD \quad (5.24)$$

There must be noted that the expression (5.24) for the correction is only correct for Doppler broadened resonances, so that $\Gamma/\Delta \ll 1$. The formalism cannot be used for the natural line shape of the resonances.

$$\Omega(D) = \frac{1}{D} \int_{\mathcal{R}=1}^{\nu/2} \cos\left\{\frac{4\pi}{\nu} \mathcal{R} + \frac{\nu \cdot D}{2D} \sin \frac{4\pi}{\nu} \mathcal{R}\right\} \exp\left\{\frac{\nu D}{2D} \left(\cos \frac{4\pi}{\nu} \mathcal{R} - 1\right)\right\} (5.25)$$

with $\nu = 10$.

To calculate the current weighted effective cross sections for the resonance series s , an approximation of H. Huschke* is used. That means, that the current weighted effective cross section can be calculated by the formulas (5.13) to (5.25), when $\langle \sigma_t \rangle$ is replaced by $\langle \sigma_t \rangle / 2$. This also means, that ${}^s\sigma_{p,eff}$ is replaced by $\{ {}^s\sigma_{p,eff} - \langle \sigma_r \rangle \} / 2$.

The average level distance \overline{sD} for the resonance series s at the energy E is given by

$$\overline{sD} = \overline{{}^osD} \cdot \frac{\{ {}^sE_B + E \}^2}{\{ {}^sE_B \}^2} \cdot \exp \left\{ -\sqrt{89,72({}^sE_B + E)} + \sqrt{89,72{}^sE_B} \right\} \quad (5.26)$$

$\overline{{}^osD}$ average level distance of resonance series s for low energies, $E \ll E_B$.

E_B binding energy of the last neutron in the compound nucleus in MeV.

E energy in MeV.

The statistical mean values of $\overline{{}^s\Gamma_x \cdot J({}^s\beta, {}^s\theta)}$ are calculated by numerical integration. For the distribution of the neutron half widths $F_n(\Gamma_n)$ and the fission half widths $F_f(\Gamma_f)$ χ^2 -distribution are used.

$$F(\Gamma) d\Gamma = \frac{\nu}{2\Gamma \cdot G(\frac{\nu}{2})} \left(\frac{\nu \cdot \Gamma}{2\Gamma} \right)^{\frac{\nu}{2} - 1} \cdot \exp \left\{ -\frac{\nu}{2} \frac{\Gamma}{\Gamma} \right\} d\Gamma \quad (5.27)$$

ν degree of freedom

G here is the Γ -function

* see appendix II of /3/.

The average cross sections of the neutron reaction (n,x) for the resonance series s are given by

$$\langle \sigma_x^s \rangle = \frac{2\pi^2}{s_D} \cdot \lambda^2 \cdot g \cdot \overline{s\Gamma_n} \cdot sS_x \quad (5.28)$$

with

$$sS_x = \frac{\left[\frac{s\Gamma_n \cdot s\Gamma_x}{s\Gamma} \right]}{\overline{s\Gamma_n}} \quad (5.29)$$

and

$$\langle \sigma_r^s \rangle = \frac{2\pi^2}{s_D} \cdot \lambda^2 \cdot g \cdot \overline{s\Gamma_n} \cdot \cos 2\delta_l \quad (5.30)$$

with

$$\delta_l = \frac{R}{\lambda} - \arctan \left(\frac{R}{\lambda} \cdot l \right) \quad \text{for } l = 0, 1 \text{ and}$$

$$\delta_2 = \frac{R}{\lambda} - \arctan \left(\frac{3 \frac{R}{\lambda}}{3 - \left(\frac{R}{\lambda}\right)^2} \right)$$

The sS_x are calculated by numerical integration with the χ^2 -distributions defined in (5.27)

The average neutron half widths are calculated from the reduced average neutron half widths

$$\overline{{}^s\Gamma}_n = \overline{{}^{os}\Gamma}_n \cdot \sqrt{E} \cdot v_l \quad (5.31)$$

with

$$v_l = \frac{R^2 + (1+l)\lambda^2}{R^2 + \lambda^2} \quad \text{for } l = 0, 1 \text{ and}$$

$$v_2 = \frac{(R/\lambda)^4}{(R/\lambda)^4 + 3(R/\lambda)^2 + 9}$$

The average group cross sections for infinite dilution are calculated in the following way:

$$\tilde{\sigma}_{x,g}^\infty = \frac{\sum_j \phi_j \left\{ \sum_s \langle {}^s\sigma_x \rangle \right\}}{\sum_j \phi_j} \quad (5.32)$$

for capture and fission,

$$\tilde{\sigma}_{e,g}^\infty = \frac{\sum_j \phi_j \left\{ \sum_s (\langle {}^s\sigma_r \rangle - \langle {}^s\sigma_c \rangle - \langle {}^s\sigma_f \rangle) + \sigma_p \right\}}{\sum_j \phi_j} \quad (5.33)$$

for elastic scattering, where ϕ_j is the weighting function (provided by the input) at the group boundaries and in the middle of the group.

5.2 The numerical procedure in calculating the statistical averages.

Statistical averages of the following type have to be calculated:

$$\overline{f(\Gamma)} = \int_0^{\infty} f(\Gamma) F(\Gamma) d\Gamma \quad (5.34)$$

where $f(\Gamma)$ is a function, which depends on Γ , $F(\Gamma)$ is a probability distribution. $F(\Gamma)$ is a χ^2 -distribution of the degree of freedom ν .

The procedure of integration is the following. The whole range of integration is divided into n intervals so that

$$\int_{\Gamma_i}^{\Gamma_{i+1}} F(\Gamma) d\Gamma = \frac{1}{n} \quad \text{for all intervals } i=1, n \quad (5.35)$$

In the interval i the average $\overline{\Gamma}_i$ is calculated

$$\overline{\Gamma}_i = \frac{\int_{\Gamma_i}^{\Gamma_{i+1}} \Gamma \cdot F(\Gamma) d\Gamma}{\int_{\Gamma_i}^{\Gamma_{i+1}} F(\Gamma) d\Gamma} = n \cdot \int_{\Gamma_i}^{\Gamma_{i+1}} \Gamma \cdot F(\Gamma) d\Gamma \quad (5.36)$$

For χ^2 -distributions for several degrees of freedom

$$\chi_i = \frac{\overline{\Gamma}_i}{\Gamma} \quad ; \quad i = 1, n \quad (5.37)$$

are tabulated.

$$\bar{\Gamma} \equiv \int_0^{\infty} \Gamma \cdot F(\Gamma) d\Gamma \quad (5.38)$$

The integral (5.34) then is approximated by

$$\overline{f(\Gamma)} = \sum_{i=1}^n f(\bar{\Gamma} \cdot \chi_i) \cdot \int_{\bar{\Gamma}_i}^{\bar{\Gamma}_{i+1}} F(\Gamma) d\Gamma = \frac{1}{n} \sum_{i=1}^n f(\bar{\Gamma} \cdot \chi_i) \quad (5.39)$$

This approximation reproduces $\bar{\Gamma}$ exactly

$$\bar{\Gamma} = \frac{1}{n} \sum_{i=1}^n \bar{\Gamma} \cdot \chi_i = \frac{1}{n} \sum_{i=1}^n \bar{\Gamma}_i$$

Using equation (5.36) one gets

$$\bar{\Gamma} = \sum_{i=1}^n \int_{\bar{\Gamma}_i}^{\bar{\Gamma}_{i+1}} \Gamma \cdot F(\Gamma) d\Gamma = \int_0^{\infty} \Gamma \cdot F(\Gamma) d\Gamma$$

In the same way the statistical averages of the type

$$\overline{f(\Gamma_1, \Gamma_2)} = \int_0^{\infty} d\Gamma_1 \int_0^{\infty} d\Gamma_2 f(\Gamma_1, \Gamma_2) \cdot F_1(\Gamma_1) \cdot F_2(\Gamma_2) \quad (5.40)$$

are approximated by

$$\overline{f(\Gamma_1, \Gamma_2)} = \frac{1}{n_1 \cdot n_2} \sum_{i=1}^{n_1} \sum_{j=1}^{n_2} f(\bar{\Gamma}_1 \cdot \chi_{1,i}, \bar{\Gamma}_2 \cdot \chi_{2,j}) \quad (5.41)$$

with

$$\chi_{1,i} = \frac{\overline{\Gamma_{1,i}}}{\Gamma_1} \quad , \quad \chi_{2,j} = \frac{\overline{\Gamma_{2,j}}}{\Gamma_2} \quad . \quad (5.42)$$

5.3 For the calculation of energy resonance self shielding factors and average group constants from statistical resonance parameters the following subroutines are used:

FSTAT (MI, SIGO, J, ENG, NFE, REFE, EFE, MT, TEMP, SE, SM, XEUGZ)

In this subroutine the average group cross sections and the energy resonance self shielding factors are calculated from statistical parameters residing on the KEDAK-file. After the subroutine QUER has calculated the microscopic average cross sections and the effective microscopic cross sections at three energy points E numerical integration is performed and the average group cross sections and the self shielding factors are printed on paper and are stored on an external unit.

MI : number of values of the background cross section σ_0
SIGO(MI) : one-dimensional field containing the background cross sections [barns].
J : number of energy group limits .
ENG(J) : one-dimensional field containing the energy group limits in [eV].
NFE : number of points of the collision density,
0 or 1, if the function $\text{PHI}(E) = 1/E$ is used .
REFE(NFE) : one-dimensional field containing the energy points of the collision density in [eV].
EFE(NFE) : one-dimensional field containing the flux density for all energy points in REFE .
MT : number of temperatures .

TEMP(MT) : one-dimensional field containing the temperatures
in [K].

SE(3,5,MI) : three-dimensional field which is calculated in
the subroutine QUER .

SM(3,5,MI) : three-dimensional field which is calculated in
the subroutine QUER .

XEUG(5,MI) : two-dimensional field containing the resonance
self shielding factors for all σ_0 -values .
The first index indicates the reaction type

- 1: radiative capture, flux-weighted
- 2: elastic scattering, flux-weighted
- 3: fission, flux-weighted
- 4: elastic scattering, current-weighted
- 5: total, current-weighted

A description of the COMMON and of the output is given in chapters 1
and 2.

QUER (E, TT, N, SE, SM, XNYN, FXNY, DEL, RQU, CHI, DN, EBI, XA, XL,
GN, GG, NEY, EY, GFA, GI, IT, MI, SIGO, NEXTGR, ENEXT, INEXT, SSSSNE)

In this subroutine the effective microscopic cross sections for the
resonance series s at the energy E as defined by equation (5.13)
and (5.14) are calculated. Also the effective microscopic cross
sections at the energy E including the contributions of all
resonance series s as defined by the equations (5.6), (5.7), (5.11) and
(5.12) are calculated in this subroutine. The following parameters
must be defined:

E : energy in [eV], at which the effective cross
section should be calculated

TT : temperature in [K].

N : n-th energy point within an energy group at which
the microscopic effective cross sections are
calculated for the evaluation of the effective
group cross sections.

- XNYN(10) : one-dimensional field containing the ν_n , the degree of freedom of the χ^2 -distributions for the neutron width, for all resonance series s ($s \leq 10$).
- FXNY(10) : one-dimensional field containing the ν_f , the degree of freedom of the χ^2 -distribution for the fission width, for all resonance series.
- DEL : $(4k/A) \cdot 10^6$, k = Boltzmann constant in $[eV/K]$, A = mass number.
- RQU : R^2 [barn], R = effective radius of the nucleus.
- CHI(25,4) : 2-dimensional field, containing the χ_i as defined in equation (5.37) for several degrees of freedom for the χ^2 -distribution ($n = 25$, $\nu = 1, 2, 3, 4$).
- DN(10) : one-dimensional field containing the average level distance at low energies $\overline{0s_D}$ for all resonance series s ($s \leq 10$) [meV].
- EBI : binding energy of the last neutron in the compound nucleus [eV].
- XA : $\Lambda_0^2 = E \cdot \kappa^2$ [eV barn].
- XL(10) : one-dimensional field containing the quantum numbers l for the angular momentum in all resonance series.
- GN(10) : one-dimensional field containing the average reduced neutron widths $\overline{\Gamma}_n^0 \cdot 10^3$ for all resonance series. $\overline{\Gamma}_n^0$ in $[eV^{1/2}]$.
- GG(10) : one-dimensional field containing the average capture widths for all resonance series in [meV].
- NEY : number of energy points, for which the fission widths are tabulated on the KEDAK-library.
- EY(199) : one-dimensional field containing the energy points, for which the fission widths are read from the nuclear data library [eV]; maximum number of points is 199.
- GFA(10, 199) : two dimensional field containing the average fission widths at the energies EY for all resonance series in [meV], first parameter for the series, second parameter for the energy points.

GI(10) : one-dimensional field containing the statistical parameter $\frac{2J+1}{2(2I+1)}$ for all resonance series. (J=spin of the compound nucleus. I=spin of the target nucleus.)
IT : number of resonance series
MI : number of values of the background cross section σ_0 .
SIGO(MI) : one-dimensional field containing the values of the background cross sections.

The following parameters are calculated in the subroutine

SE(3,5,MI) : three-dimensional field containing the microscopic effective group cross section in / barn /, first index for energy, second index for the reaction type.
1: capture, see formula (5.6)
2: elastic scattering, see formula (5.7)
3: fission, see formula (5.6)
4: elastic scattering, see formula (5.11)
5: total, see formula (5.12)
third index for the background cross section σ_0 .
SM(3,5,MI) : three-dimensional field containing the microscopic average group cross sections in [barn], as given by formulas (5.19), (5.28) and (5.30)
First index for energy,
second index for the reaction type as for SE,
third index for the background cross section σ_0 ,
(not significant, because the average cross section does not depend on σ_0).

Only local variables are: NEXTGR, ENEXT, INEXT, SSSSNE

EZZ (E, NS, EZG, EZC, EZF, DRSG, DRFS, CHI, XNYN, FXNYN, GN, RQU, XL, XA, GG, NEY, EY, GF)

In this subroutine the statistical mean values, defined by equation (5.29) are calculated.

The following parameters must be defined:

- E : energy [eV].
- NS : number of the resonance series to be calculated.
- CH1(25,4) : two-dimensional field containing the χ_i as defined in equation (5.37) for several degrees of freedom for the χ^2 -distribution ($n = 25$, $\nu = 1, 2, 3, 4$).
- XNYN(10) : one-dimensional field containing the ν_n , the degree of freedom of the χ^2 -distribution for the neutron half width, for all resonance series s ($s \leq 10$).
- FXNYN(10) : one-dimensional field containing the ν_f , the degree of freedom of the χ^2 -distribution for the fission width, for all resonances.
- GN(10) : one-dimensional field containing the average reduced neutron widths $\bar{\Gamma}_n^0 \cdot 10^3$ for all resonance series. $\bar{\Gamma}_n^0$ in [$\sqrt{\text{eV}}$].
- RQU : R^2 [barn], $R =$ **effective radius of the nucleus.**
- XL(10) : one-dimensional field containing the quantum numbers l for the angular momentum for all resonance series.
- XA : $\Lambda_0^2 = E \cdot k^2$ [eV barn].
- GG(10) : one-dimensional field containing the average capture widths for all resonance series [meV].
- EY(99) : one-dimensional field containing the energy points, for which the fission widths are read from the nuclear data library [eV]; maximum number of points is 199.
- GF(10,199) : two-dimensional field containing the average fission widths at the energies EY for all resonance series in [meV],
first index for the series,
second index for the energy points.

The following parameters are calculated in the subroutine:

- EZG : defined by equation (5.32) of /3/, for capture, not used in the present version of the programme.
- EZC : defined by equation (5.31) of /3/; not used in the present version of the programme.

EZF : defined by equation (5.32) of /3/, for fission; not used
in the present version of the programme.
DRSG : defined by equation (5.29), for capture.
DRFS : defined by equation (5.29), for fission

TAB(XT, XK, LG, DSJ, XABCJ, DJK)

In this subroutine the $J(\beta, \theta)$ -function and the derivatives $\frac{\partial J}{\partial \beta}$ and $\frac{\partial J}{\partial \theta}$ are calculated.

The following parameters must be defined:

XT : $\theta = \frac{\Gamma}{\Delta}$, Γ and Δ in [eV], (5.17).
XK : k, where k is defined by $\beta = 2^k \cdot 10^{-5}$, β is defined
by (5.22).
LG : 1, if XABCJ is calculated
2, if DJK is calculated
0, if DSJ is calculated
negative, if XABCJ, DJK and DSJ are calculated

The following parameters are calculated by the subroutine:

XABCJ : $J(\beta, \theta)$ -function as defined by (5.15).
DSJ : $\frac{\partial J(\beta, \theta)}{\partial \theta}$
DJK : $\frac{\partial J(\beta, \theta)}{\partial k}$, with $\beta = 2^k \cdot 10^{-5}$.

SUCH (E, NSU, NEY, EY)

This is an auxiliary subroutine

Besides the subroutines the following functions are necessary:

DMIT (E, NS, DN, EBI)

In this function the average level distance at the energy E is calculated by formula (5.26).

E : energy in [eV].
NS : number of the resonance series .
DN(1o) : one-dimensional-field containing the $\overline{\sigma}_D^{OS}$ for all resonance series s [meV].
EBI : binding energy E_B of the last neutron in the compound nucleus [eV].
DMIT : $\overline{\sigma}_D^S$ at the energy E for the resonance series NS in [meV].

GAMN (E, NS, GN, RQU, XL, XA)

In this function the average neutron width at the energy E is calculated by the formula (5.31).

E : energy in [eV].
NS : number of the resonance series.
GN(1o) : one-dimensional field containing the reduced average neutron half widths $\overline{\Gamma}_n^0$ for all resonance series in [meV].
RQU : R^2 in [barn], R = effective radius of the nucleus
XL(1o) : one-dimensional field containing the quantum numbers for the angular momentum for all resonance series.
XA : $\lambda^2 \cdot E$ in [eV · barn], λ is the neutron wave length.
GAMN : $\overline{\Gamma}_n$, the average neutron half width at the energy E for the resonance series NS [meV].

GAMG (E, NS, GG)

In this subroutine the average capture half width at the energy E is provided.

E : energy in [eV].
NS : number of the resonance series.
GG(10) : one-dimensional field containing the average capture half widths for all resonance series in [meV].
GAMG : average capture half widths at the energy E for the resonance series NS in [meV].

GAFM (E, NS, NEY, EY, GF)

In this subroutine the average fission half width at the energy E is interpolated from the tabulated values.

E : energy [eV].
NS : number of the resonance series.
EY(199) : one-dimensional field, containing the energies, at which the average fission widths are tabulated [eV].
GF(10,199) : one-dimensional field, containing the tabulated average fission widths in [meV].
GAFM : average fission width at the energy E for the resonance series NS in [meV].

POL (X, X1, FX1)

Auxiliary function for a linear interpolation

X : argument, for which an arbitrary function should be interpolated.
X1(2) : one-dimensional field, containing two arguments of the function.
FX1(2) : one-dimensional field, containing the values of the function at the arguments X1.
POL : value of the function at X.

EPSI (E, T, NS, DN, EBI, DEL)

In this function the overlapping correction ϵ , defined by formula (5.24) is calculated.

E : energy in [eV].
T : temperature in [K].
NS : number of resonance series.
DN(10) : one-dimensional field containing the $\overline{\sigma}_D^s$ for all resonance series s [meV].
EBI : binding energy E_B of the last neutron in the compound nucleus [eV].
DEL : $(4k/A) \cdot 10^6$, k = Boltzmann constant in [eV/ K],
A = mass number.

DELTA (E, T, NS, DEL)

In this function the Doppler width, formula (5.17), is calculated.

E : energy in [eV].
T : temperature in [K],
NS : number of resonance series.
DEL : $\frac{4k}{A} \cdot 10^6$; k = Boltzmann constant in [eV/ K],
A = mass number.

PHASE (E, NS, XA, RQU, XL)

In this function $\cos 2\delta_1$ is calculated, where $\delta_1 = R/\lambda - \arctg \frac{R}{\lambda} \cdot 1$.
R is the effective radius of the nucleus, λ is the reduced neutron wave length.

E : energy in [eV].
NS : number of resonance series.

XA : $\Lambda_0^2 = E \cdot \lambda^2$ [eV·barn].
XL(10) : one-dimensional field containing the quantum numbers l for the angular momentum in all resonance series .

SIGC(E, NS, XA, GI, DN, EBI, GN, RQU, XL)

In this function the average radiative capture cross section at the energy E for a single resonance series is calculated

E : energy in [eV].
NS : number of resonance series .
XA : $\Lambda_0^2 = E \cdot \lambda^2$ [eV·barn].
GI(10) : one-dimensional field containing the statistical parameter $\frac{2J+1}{2(2I+1)}$ for all resonance series.
DN(10) : one-dimensional field containing the average level distance at low energies $\overline{\sigma}_D$ for all resonance series in [meV].
EBI : binding energy of the last neutron in the compound nucleus in [eV]
GN(10) : one-dimensional field containing the average reduced neutron widths $\overline{\Gamma}_n^0 \cdot 10^3$ for all resonance series, $\overline{\Gamma}_n^0$ in [eV^{1/2}].
RQU : R^2 in [barn], R = effective radius of the nucleus.
XL(10) : one-dimensional field containing the quantum number l of the angular momentum for all resonance series.

5.4 Description of the (not selfexplaining) warnings, produced by module 2

*** WARNING 2.04

Comment: To get a correct overlapping correction, Γ/Δ should be much smaller than one. Normally it is assumed, that $\Gamma/\Delta < 0.5$ is small enough. See the discussion following formula (5.24).

*** WARNING 2.05

Comment: For the calculation of the current weighted resonance self shielding factors an approximation is used, which in some cases is not valid for small σ_0 -values. (See also Appendix II, formula (25) of /3/). In these cases a warning is produced and the smallest σ_0 -value, for which the applied approximation is valid, is printed out.

*** WARNING 2.06

Comment: The reason for this warning might be the same as in *** WARNING 2.04. If not, the formalisme for approximating the overlapping correction is insufficient. The warning is given, when the denominator in formula (5.14) becomes negative. If the resulting ${}^s\sigma_{r,g}$ in (5.14) is small against the contribution of all other resonance series, this warning may be ignored.

References

/1/ R. Froelich

Theorie der Dopplerkoeffizienten schneller Reaktoren unter Berücksichtigung der gegenseitigen Abschirmung der Resonanzen.
KFK 367 (1965)

/2/ H. Huschke

Gruppenkonstanten für dampf- und natriumgekühlte Reaktoren in einer 26-Gruppendarstellung.
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/3/ H. Huschke, B. Krieg

MIGRØS-2: A Program Written in FORTRAN for the Calculation of Microscopic Group Constants from Nuclear Data.
KFK 1784 (1973)

6. The calculation of normalized transfer matrices for inelastic scattering, (n,2n)- and (n,3n)-reactions. Module 5.
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6.1 Changes with respect to module 5 in MIGRØS-2

Module 5 has been nearly completely rewritten for MIGRØS-3. The reasons for this were partly connected with the introduction of KEDAK 3,/1/. In addition to the KEDAK-3-materials evaluated at Karlsruhe those materials have to be processed by the new module, that have been transferred from ENDF/B,/2/, by the code BRIGITTE,/3/.

Information about new cross-section types (SGIZC, SEDIC, SED2N, SED3N) is available on KEDAK 3 and is used in the new module 5. At the time, when the first version of module 5, /4/, was written, these types did not contain information and therefore were not taken account of in that first version of the module.

Moreover the physical, numerical and code-procedures have been refined in the MIGRØS-3-version.

The following points give the main differences in detail:

- 1.) The convention of KEDAK-2, /5/, that for one material the energy points, at which the cross-sections are stored, are the same for all cross-section types has been given up on KEDAK-3 in order to save storage on the nuclear data library. Especially for the calculation of transfer matrices for inelastic scattering this means, that the excitation cross-sections for the different discrete levels (SGIZ(E_j ,E)) are no longer stored at the same energy points E.
- 2.) On KEDAK-2 there were two clearly separated energy regions in connection with inelastic scattering: one region of low neutron incident energies, by which discrete levels of the residual nucleus are excited and an adjacent region of higher neutron incident energies, by which continuous levels of the residual nucleus are excited. On KEDAK-3 the energy regions (regions of primary neutron energy), which are connected with excitation of discrete or continuous levels of the residual nucleus may overlap.

- 3.) In contrary to KEDAK-2 the nuclear library KEDAK-3 provides energy distributions for the secondary neutrons produced in inelastic scattering processes, by (n,2n)-reactions and by (n,3n)-reactions (types SEDIC, SED2N, SED3N). Therefore the corresponding transfer matrices can now be calculated with the information taken from the nuclear data library.
- 4.) Three different options are given to choose the physical approximation by which the partial transfer matrix connected with the excitation of discrete levels of the residual nucleus is calculated.
- 5.) The method of numerical integration over the outscattering energy group has been refined for the calculation of transfer probabilities, that are in connection with discrete excitation levels of the residual nucleus and for those, that are connected with the excitation of continuous levels of the residual nucleus.
- 6.) The nuclear data are no longer kept in core storage for the entire energy region given on KEDAK but are kept in core storage only for the outscattering group just treated.

6.2 Formulas used

In correspondence with /4/ the general formula for the calculation of the inelastic scattering transfer probability from energy group g to energy group h is given by

$$k_{\sigma_{i,g \rightarrow h}} = \frac{\int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' k_{\sigma_i}^k(E') \phi(E') P(E' \rightarrow E)}{\int_{E_{g+1}}^E \phi(E') dE'} \quad (6.1)$$

Again E' is the energy of the incident neutron and E the energy of the scattered neutron. $k_{\sigma_i}^k(E')$ is the inelastic cross section of material $k^{+)}$ at energy E' , $\phi(E')$ is the energy dependent neutron flux and $P(E' \rightarrow E)$ the probability

^{+) The index k will be omitted in the following.}

that an incident neutron of energy E' produces a secondary neutron of energy E by inelastic scattering. (6.1) is valid for (n,2n)- and (n,3n)- processes as well.

In the programme to be described for $\phi(E')$ the weighting function given by the input (see BLØC2 in the input description, chapter 2) is inserted. This weighting function (given by input) may be chosen by the user. In general it will be a collision density ($F(E') = \Sigma_t(E') \cdot \phi(E')$), where $\Sigma_t(E')$ is the total cross-section of the material composition under consideration and $\phi(E')$ the neutron flux. Weighting by $F(E')$ instead of weighting by $\phi(E')$ means that most of the energy dependent structure in the weighting function is neglected. It has to be considered however, that for all materials the threshold for inelastic scattering lies above the resonance region of the heavy materials. (In the (200 - 300) energy group representation, /6/, the full energy dependence of the total cross-section of the material composition is taken into account in the weighting flux $\phi(E') = \frac{F(E')}{\Sigma_t(E')}$.)

To make quite clear, that the weighting function supplied by the input, $w(E')$, is used for the calculation of the transfer probabilities formula (6.1) is rewritten as

$$k_{\sigma_i, g \rightarrow h} = \frac{\int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sigma_i(E') w(E') P(E' \rightarrow E)}{\int_{E_{g+1}}^E dE' w(E')} \quad (6.1.1)$$

6.2.1 Calculation of the partial inelastic transfer matrices connected with the excitation of discrete levels of the residual nucleus

For our calculations we have to start from formula (6.1.1). The inelastic cross-section for the excitation of discrete levels of the residual nucleus is given separately for each excitation level E_j as $\sigma_i^{E_j}(E')$. The total inelastic cross-section for excitation of discrete levels of the residual nucleus is $\sum_j \sigma_i^{E_j}(E')$ (\sum_j means summation over j). The

probability, that an incident neutron of energy E' by excitation of the level E_j produces a scattered neutron of energy E is $\sigma_i^{E_j}(E') P_j(E' \rightarrow E)$. For an exact calculation of the neutron energy loss in inelastic processes, the scattering angle-energy correlation has to be taken fully into account, /7/, /8/, /9/. In module 5 three different approximations to this exact treatment are applied:

$$1.) P_j(E' \rightarrow E) = \delta(E' - E - E_j) \quad (6.2)$$

δ is the Dirac δ -function.

This approximation corresponds to the one applied in MIGRØS-2, /4/. Here the excitation energy E_j of the residual nucleus is used as it is given on the nuclear library, that means in the center of mass system. If the transformation of E_j into the laboratory system is carried out the second possibility to calculate the transfer probability in the new version of module 5 is given.

$$2.) P_j(E' \rightarrow E) = \delta\left(E' - E - \frac{AT+AN}{AT} E_j\right), \quad (6.3)$$

where AT is the atomic mass of the target nucleus and AN that of the neutron. The atomic weights given on KEDAK (type ISØT1) are referred to the atomic mass of $C12 = 12$ AMU. In this system the mass of the neutron is 1.008665 AMU, so that

$$P_j(E' \rightarrow E) = \delta\left(E' - E - \frac{AT+1.008665}{AT} E_j\right) \quad (6.3.1)$$

The third approximation used in module 5 has been recommended by Segev, /7/, /9/. This is the approximation used on ENDF/B, /2/.

$$3.) P_j(E' \rightarrow E) = \delta\left(E - \frac{(AT)^2 + 1.008665^2}{(AT+1.008665)^2} E' + \frac{AT}{AT+1.008665} E_j\right) \quad (6.4)$$

To obtain the inelastic transfer probabilities from outscattering group g to inscattering group h the relations 1.) to 3.) have to be inserted into formula (6.1.1). The integration using the transfer probability given in relation 1.) (formula (6.2)) has been carried out in /4/. Here we shall insert relations 2.) and 3.) into the general formula (6.1.1). First the relation 2.).

$$\sigma_{i,g \rightarrow h} = \frac{\int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j} (E') w(E') \delta(E' - E - \frac{AT+AN}{AT} E_j)}{\int_{E_{g+1}}^E dE' w(E')} \quad (6.5)$$

First the double integration in the numerator is carried out starting with the integration over E' using the relationship /10/:

$$\left. \begin{aligned} &\text{if } f_2(x_0) = 0, \\ &\int_{x_1}^{x_2} f_1(x) \delta[f_2(x)] dx = \frac{f_1(x_0)}{\left| \frac{df_2}{dx} \right|_{x=x_0}}, \\ &\text{if } x_1 \leq x_0 \leq x_2 \end{aligned} \right\} \quad (6.6)$$

This results in

$$\begin{aligned} &\int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j} (E') w(E') \delta(E' - E - \frac{AT+AN}{AT} E_j) \\ &= \int_{E_{h+1}}^{E_h} dE \sum_j \sigma_i^{E_j} (E + \frac{AT+AN}{AT} E_j) w(E + \frac{AT+AN}{AT} E_j) \cdot \chi(E_{g+1} \leq E + \frac{AT+AN}{AT} E_j \leq E_g) \end{aligned} \quad (6.7)$$

with

$$\chi(E_{g+1} \leq E + \frac{AT+AN}{AT} E_j \leq E_g) = \begin{cases} 1, & \text{if the inequality in the argument} \\ & \text{is valid} \\ 0, & \text{if the inequality in the argument} \\ & \text{is not valid} \end{cases}$$

Transformation of the integration over E in (6.7) to an integration over $E'_0 = E + \frac{AT+AN}{AT} E_j$ results in

$$\left. \begin{aligned}
 & \int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j} (E') w(E') \delta(E' - E - \frac{AT+AN}{AT} E_j) \\
 & = \int_{E_{h+1} + \frac{AT+AN}{AT} E_j}^{E_h + \frac{AT+AN}{AT} E_j} dE'_0 \sum_j \sigma_i^{E_j} (E'_0) w(E'_0) \chi(E_{g+1} \leq E'_0 \leq E_g)
 \end{aligned} \right\} (6.8)$$

The function $\chi(E_{g+1} \leq E'_0 \leq E_g)$ may be replaced by a modification of the integration region, so that the numerator of (6.5) is finally given by

$$\left. \begin{aligned}
 & \int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j} (E') w(E') \delta(E' - E - \frac{AT+AN}{AT} E_j) \\
 & = \int_{E_u}^{E_o} dE'_0 \sum_j \sigma_i^{E_j} (E'_0) w(E'_0)
 \end{aligned} \right\} (6.9)$$

with

$$\left. \begin{aligned}
 E_u &= \text{Max}(E_{g+1}, E_{h+1} + \frac{AT+AN}{AT} E_j) \\
 E_o &= \text{Min}(E_g, E_h + \frac{AT+AN}{AT} E_j)
 \end{aligned} \right\} (6.9.1)$$

In (6.9.1) the function Max means the maximum value of the two numbers in the argument. Correspondingly the function Min means the minimum value of the two numbers in the argument.

If instead of relation 2.) relation 1.) (formula (6.2)) for $P_j(E' \rightarrow E)$ is inserted into the numerator of (6.11) the result of the integration corresponds to the one given in formulas (6.9), (6.9.1), if the constant $\frac{AT+AN}{AT}$ is replaced by 1 in these formulas. (See /4/, (6.4) and (6.5).)

If the option 3.) for $P_j(E' \rightarrow E)$ (formula (6.4)) is chosen the formula (6.1.1) for the inelastic transition probability becomes:

$$\sigma_{i,g \rightarrow h} = \frac{\int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j} (E') w(E') \delta(E - \frac{AT^2 + AN^2}{(AT+AN)^2} E' + \frac{AT}{AT+AN} E_j)}{\int_{E_{g+1}}^E dE' w(E')} \quad (6.10)$$

The double integral in the numerator is reduced to a single integral by the δ -function. Using (6.6) the result of the integration over E' is

$$\left. \begin{aligned} & \int_{E_{g+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j} (E') w(E') \delta(E - \frac{AT^2 + AN^2}{(AT+AN)^2} E' + \frac{AT}{AT+AN} E_j) \\ &= \frac{(AT+AN)^2}{AT^2 + AN^2} \int_{E_{h+1}}^{E_h} dE \sum_j \sigma_i^{E_j} (E_0') w(E_0') \cdot \chi(E_{g+1} \leq E_0' \leq E_g) \end{aligned} \right\} \quad (6.11)$$

with

$$E_0' = \frac{(AT+AN)^2}{AT^2 + AN^2} (E + \frac{AT}{AT+AN} E_j) \quad (6.11.1)$$

To carry out the integration over the inscattering group $h = (E_{h+1}, E_h)$, the integration over E is transformed into an integration over E_0' , so that the right hand side of (6.11) becomes:

$$\frac{(AT+AN)^2}{AT^2 + AN^2} (E_h + \frac{AT}{AT+AN} E_j) \int dE_0' \sum_j \sigma_i^{E_j} (E_0') w(E_0') \cdot \chi(E_{g+1} \leq E_0' \leq E_g) \quad (6.11.2)$$

$$\frac{(AT+AN)^2}{AT^2 + AN^2} (E_{h+1} + \frac{AT}{AT+AN} E_j)$$

The restriction given by the function χ may be taken into account by modification of the integration limits, so that for the application of option 3.) (6.4) in the numerator of formula (6.1.1) the following result is obtained:

$$\left. \begin{aligned} & \int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j} (E') w(E') \delta\left(E - \frac{AT^2 + AN^2}{(AT+AN)^2} E' + \frac{AT}{AT+AN} E_j\right) \\ & = \int_{E_u}^{E_o} dE' \sum_j \sigma_i^{E_j} (E') w(E') \end{aligned} \right\} \quad (6.12)$$

with

$$\left. \begin{aligned} E_u &= \text{Max}\left(E_{g+1}, \frac{(AT+AN)^2}{AT^2+AN^2} \left(E_{h+1} + \frac{AT}{AT+AN} E_j\right)\right) \\ E_o &= \text{Min}\left(E_g, \frac{(AT+AN)^2}{AT^2+AN^2} \left(E_h + \frac{AT}{AT+AN} E_j\right)\right) \end{aligned} \right\} \quad (6.12.1)$$

In formulas (6.9) and (6.12) the integration over E'_o is carried out by a trapezoidal rule. Integration points are the combination of all energy points of the KEDAK-type SGIZ(E_j, E'_o) for all E_j contributing between E_u and E_o and the energy points of the weighting function. If $w(E')$ is not given energy-pointwise, an energy grid is constructed for the weighting function $\text{PHI}(E')$, so that all points between the grid points can be obtained by linear interpolation with a relative error of less than 10^{-6} . For the trapezoidal integration this energy grid is combined with the energies of KEDAK.

6.2.2 Short summary of formulas derived for the calculation of partial inelastic transfer matrices connected with the excitation of discrete levels of the residual nucleus

Given are the results for the normalized partial inelastic transfer probabilities $P_{i,g \rightarrow h}^d$, when options 1.), 2.) or 3.) are inserted into (6.1.1). The superscript d refers to discrete levels. The general

formula for $P_{i,g \rightarrow h}^d$ is:

$$P_{i,g \rightarrow h}^d = \frac{\sigma_{i,g \rightarrow h}^d}{\sigma_{i,g}^d} \quad (6.13)$$

with

$$\sigma_{i,g}^d = \frac{\int_{E_{g+1}}^E \sum_j \sigma_i^{E_j}(E') w(E') dE'}{\int_{E_{g+1}}^E w(E') dE'} \quad (6.13.1)$$

For the three options 1.) (6.2), 2.) (6.3) and 3.) (6.4) the transfer probability $P_{i,g \rightarrow h}^d$ is given by

$$P_{i,g \rightarrow h}^d = \frac{\int_{E_u}^E dE'_0 \sum_j \sigma_i^{E_j}(E'_0) w(E'_0)}{\int_{E_{g+1}}^E \sum_j \sigma_i^{E_j}(E') w(E') dE'} \quad (6.14)$$

The different approximations used for the inelastic energy transfer (options 1.), 2.), 3.)) are expressed in the result (6.14) by different integration limits E_u and E_0 .

If approximation 1.) (6.2) is applied the integration limits are given by:

$$\left. \begin{aligned} E_u^{(1)} &= \text{Max}(E_{g+1}, E_{h+1} + E_j) \\ E_0^{(1)} &= \text{Min}(E_g, E_h + E_j) \end{aligned} \right\} \quad (6.15)$$

The superscript on E_u , E_0 refers to options 1.), 2.) or 3.)

$$\left. \begin{aligned} E_u^{(2)} &= \text{Max}(E_{g+1}, E_{h+1} + \frac{AT+AN}{AT} E_j) \\ E_o^{(2)} &= \text{Min}(E_g, E_h + \frac{AT+AN}{AT} E_j) \end{aligned} \right\} \quad (6.16)$$

and finally

$$\left. \begin{aligned} E_u^{(3)} &= \text{Max}(E_{g+1}, \frac{(AT+AN)^2}{AT^2+AN^2} (E_{h+1} + \frac{AT}{AT+AN} E_j)) \\ E_o^{(3)} &= \text{Min}(E_g, \frac{(AT+AN)^2}{AT^2+AN^2} (E_h + \frac{AT}{AT+AN} E_j)) \end{aligned} \right\} \quad (6.17)$$

6.2.3 Calculation of partial inelastic transfer matrices connected with the excitation of continuous levels of the residual nucleus

Again formula (6.1.1) has to be evaluated inserting now the nuclear data that describe the excitation of continuous levels. In the following formulas the superscript c refers to "continuous" level excitation.

$$\sigma_{i,g \rightarrow h}^c = \frac{\int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sigma_i^c(E') P_i^c(E' \rightarrow E) w(E')}{\int_{E_{g+1}}^E dE' w(E')} \quad (6.18)$$

The continuous level inelastic scattering cross-section, $\sigma_i^c(E')$, is given by the type SGIZC on KEDAK. For some materials this type is not filled. In these cases $\sigma_i^c(E')$ is equal to the total inelastic cross-section (KEDAK-type SGI) above the last energy point of the type SGIZ and is set equal to zero in the energy region where excitation cross-sections for discrete levels, SGIZ, are given. $P_i^c(E' \rightarrow E)$ may be analytic or tabulated functions of E and E'. In the present version of MIGRØS-3 (summer 1976) only evaporation distributions can be processed. Additional subroutines are being worked on, to enable module 5, to process secondary neutron energy distributions, that are given by tabulated functions.

The evaporation distribution is given by

$$P_i^c(E' \rightarrow E) \left\{ \begin{array}{l} = \frac{E}{I} e^{-E/\theta(E')}, \text{ if } 0 \leq E \leq E' - U \\ = 0, \text{ else} \end{array} \right. \quad (6.19)$$

U is the threshold energy of the inelastic scattering process and θ the nuclear temperature, which on KEDAK is given as a tabulated function of E'. The normalization constant I depends on the nuclear temperature and the threshold energy U of the inelastic scattering process.

$$I = \theta^2(E') \left[1 - e^{-(E'-U)/\theta(E')} \left(1 + \frac{E'-U}{\theta(E')} \right) \right] \quad (6.19.1)$$

θ and U are given in the KEDAK-type SEDIC. If SEDIC is not filled an evaporation model with a nuclear temperature $\theta(E') = \sqrt{\frac{E}{v \cdot A}} \text{ [MeV]}$, //11/, is used by module 5. A is the atomic weight of the target nucleus, read from KEDAK, and v an adjustable parameter, that is set equal to 0.16 MeV^{-1} in the standard case but may be modified by input. If SEDIC is not filled U is read from KEDAK as the threshold of SGI.

P_i^c in (6.19) is a continuous function of E and E'. In (6.18), (6.19) the integration over E may be carried out first with the result

$$\sigma_{i,g \rightarrow h}^c = \frac{\int_{E_{g+1}}^E dE' \sigma_i^c(E') w(E') P_i^c(E' \rightarrow h)}{\int_{E_{g+1}}^E w(E') dE'} = \frac{\int_{E_{g+1}}^E dE' \frac{1}{I} \sigma_i^c(E') w(E') \theta^2(E') \left[\exp\left(-\frac{E_{h+1}}{\theta(E')}\right) \left(\frac{E_{h+1}}{\theta(E')} + 1\right) - \exp\left(-\frac{E_h}{\theta(E')}\right) \left(\frac{E_h}{\theta(E')} + 1\right) \right]}{\int_{E_{g+1}}^E w(E') dE'} \quad (6.20)$$

The normalized transfer probability is

$$P_{i,g \rightarrow h}^c = \frac{\sigma_{i,g \rightarrow h}^c}{\sigma_{i,g}^c} \quad (6.20.1)$$

$$\sigma_{i,g}^c = \frac{\int_{E_{g+1}}^E \sigma_i^c(E') w(E') dE'}{\int_{E_{g+1}}^E dE' w(E')} \quad (6.20.2)$$

The integrations over E' in (6.20) and (6.20.2) is done by Simpson's rule. The energy grid, with which the integration is started is the combination of the energy points of $\sigma_i^c(E')$ on KEDAK and the energy points of the weighting function, if $w(E')$ is given energy-pointwise. If $w(E')$ is given as a function the integration starts with the energy points of $\sigma_i^c(E')$.

6.2.4 Total inelastic scattering transfer matrix

The group constant sets need the total inelastic transfer-matrix, which is the combination of the inelastic transfer matrix for discrete level excitation, $P_{i,g \rightarrow h}^d$ and the inelastic transfer matrix for continuous level excitation $P_{i,g \rightarrow h}^c$. Combination of formulas (6.13) and (6.20.1) gives the total inelastic scattering transfer matrix:

$$P_{i,g \rightarrow h} = \frac{\sigma_{i,g}^d P_{i,g \rightarrow h}^d + \sigma_{i,g}^c P_{i,g \rightarrow h}^c}{\sigma_{i,g}^d + \sigma_{i,g}^c} \quad (6.21)$$

or, written in a slightly modified manner:

$$P_{i,g \rightarrow h} = \frac{R_{i,g}^d P_{i,g \rightarrow h}^d + R_{i,g}^c P_{i,g \rightarrow h}^c}{R_{i,g}^d + R_{i,g}^c} \quad (6.21.1)$$

$$R_{i,g}^d = \int_{E_{g+1}}^E \sigma_i^d(E') w(E') dE' \quad R_{i,g}^c = \int_{E_{g+1}}^E \sigma_i^c(E') w(E') dE' \quad (6.21.2)$$

6.2.5 Calculation of transfer probabilities for (n,2n)- and (n,3n)-reactions

The transfer probabilities for (n,2n)- and (n,3n)-reactions are calculated with formulas corresponding to those used in chapter 6.2.3 for the calculation of inelastic transfer matrices in connection with excitation of continuous levels of the residual nucleus. In correspondence with (6.18) we have:

$$\sigma_{(n,2n)g \rightarrow h} = \frac{\int_{E_{h+1}}^{E_h} dE \int_{E_{g+1}}^E dE' \sigma_{(n,2n)}(E') w(E') P_{(n,2n)}(E' \rightarrow E)}{\int dE' w(E')} \quad (6.22)$$

The same formula is valid for (n,3n)-reactions, if (n,2n) is replaced by (n,3n).

For $P_{(n,2n)}(E' \rightarrow E)$ and $P_{(n,3n)}(E' \rightarrow E)$ the information of the KEDAK type SED2N and SED3N is used. In the present version of KEDAK evaporation distributions are given, which from (6.19), (6.19.1) differ by the values of θ and U . Again, if no information is contained in SED2N, SED3N the nuclear temperature is taken as an analytic function of E' with an adjustable parameter ν , which may be chosen by input.

After integration over the inscattering group the normalized element of the transfermatrix is

$$P_{(n,2n)g \rightarrow h} = \frac{\int_{E_{g+1}}^E dE' \frac{1}{I} \sigma_{(n,2n)}(E') w(E') \theta^2(E') \left[\exp\left(-\frac{E_{h+1}}{\theta(E')}\right) \left(\frac{E_{h+1}}{\theta(E')} + 1\right) - \exp\left(-\frac{E_h}{\theta(E')}\right) \left(\frac{E_h}{\theta(E')} + 1\right) \right]}{\int_{E_{g+1}}^E dE' \sigma_{(n,2n)}(E') w(E')} \quad (6.23)$$

again the integration over E' is carried out by Simpson's rule.

6.3 Description of the code

The main subroutine of module 5, SCAT, is a subroutine of the organizing subroutine of MIGRØS-3, INPUT. SCAT itself calls two subroutines, SCATD, that provides the transition probabilities for inelastic scattering reactions, that occur by excitation of discrete levels of the residual nucleus and SCATC, which provides transfer probabilities for inelastic scattering processes, that excite continuous energy levels of the residual nucleus. SCATC also calculates the transfer matrices of (n,2n)- and (n,3n)-processes.

6.3.1 Description of the subroutine SCATD and its subprogrammes

SCATD has been developed from the former subroutine SCAT^{+) (see /4/). The main differences are, that now the KEDAK-data are read for each outscattering group separately and that instead of formula (6.2) only formulas (6.2), (6.3) or (6.4) may be used for the calculation of the energy transfer by inelastic scattering. The subroutine SCATD calculates the integration limits E_u and E_o given in equations (6.15), (6.16) or (6.17) and carries out the numerical integration over the outscattering group in formulas (6.9) and (6.12). The integration is done in a threefold nested doloop, in which the inner index treats the excitation levels, the second index treats the inscattering groups and the outer index treats the outscattering groups.}

Subroutine SCATD(NX,EG,NFE,EF,FI,NE27,WEIN,QUØT,WAHR,VW,E,AE,SU,LBA,
SGIT,IANF,SGIP,WERT,EZ,NISG,NISGP,NAE,NAEP,ISG,ISGP,
KINEM,NEA,NAB)

Arguments, that have to be defined, when SCATD is called:

EG(NX) provided by the input, energy group boundaries of the outscattering groups. Internally in the programme the energy group limits are numbered starting with 1 for the lowest energy (internal energy group count). EG(NX) may or may not contain the thermal group.

NX number of energy group boundaries of outscattering groups.

EF(NFE) provided by the input: energy grid of the weighting spectrum

^{+) SCAT (/4/) was originally developed by B. Schatz}

FI(NFE) points of the weighting spectrum
 NFE number of energy points of the weighting spectrum
 (NFE is set equal to 1 internally, if the weighting
 spectrum is given by an analytical function)
 NE27 number of energy group boundaries of the in-
 scattering groups. The inscattering groups
 contain the thermal group.
 NISG } estimations of needed lengths of fields, that
 NAE } are used in SCATD and related subroutines
 ISG }
 KINEM provided by the input: decides, whether approximation
 (6.2), (6.3) or (6.4) is chosen, to describe the
 energy transfer connected with the excitation
 of discrete levels of the residual nucleus

Arguments, that are transferred by SCATD to the calling subroutine SCAT.

NEA number of energy group of lowest energy (internal
 group count), for which transfer matrices are calculated
 in SCATD (provided by DAØRG).

NAB number of energy group of highest energy (internal
 group count), for which transfer matrices are calculated
 in SCATD (provided by DAØRG).

WEIN(NX,NX) transfer probabilities for inelastic scattering with
 excitation of discrete levels of the residual nucleus
 (corresponding to formula (6.14)). The first index
 gives the group number of the outscattering group
 (1 being the number of the energy group with lowest
 energy), the second index refers to the inscattering
 group. Second index 1 means inscattering group is
 equal to outscattering group, second index 2 means
 the inscattering group is the energetically next
 lower group, second index I means inscattering group
 is the energy group, that energetically lies (I-1)
 groups below the outscattering group.

QUØT(NX)
$$\int_{E_{g+1}}^E dE' \sum_j \sigma_i^{E_j}(E') w(E')$$
 (internal group count)

(calculated in AKED)

= $R_{i,g}^d$ given by formula (6.21.2)

NISGP } numbers, that have to be added to NISG,NAE,ISG to get
 NAEP } sufficient field lengths for the tasks to be carried
 ISGP } out by SCATD and its subprogrammes. NISGP,NAEP and ISGP
 are provided by the subroutine DAØRG.

The following arguments are working fields in SCATD:

local working fields: WAHR(NX), VW(NX), E(NE27) (E(NE27) = energy group boundaries , containing thermal group , LBA(NX).

Working fields, supplied by subroutine AKED:

AE(NAE),SU(NX),SGIT(ISG),IANF(NAE),SGIP(ISG,NAE),WERT(ISG),EZ(NISG)

The subroutine AKED, called by SCATD is a modified version of the subroutine AKED⁺⁾ described in /4/. AKED calculates

$$\int_{E_{g+1}}^E \sum_j \sigma_i^j(E') w(E') dE' \quad \text{and}$$

$$\int_{E_{g+1}}^E w(E') dE'$$

Subroutine AKED(I,E,EZ,SGIP,JMAT,LMAX,SU,QUØT,WERT,AE,IA,NAB,IE,INF,NFE,EF,FI,NE,NX,SGIT,NAE,NAEP,ISG,ISGP,IANF,NISG,NISGP,EJMAX)

Arguments, that have to be defined, when AKED is called:

I	group number of outscattering group (internal energy group count).
E(NE)	energy group boundaries (containing thermal group)
IE	number of energy group of lowest energy required by input
INF	number of energy group of highest energy required by input
NFE,EF(NFE),FI(NFE)	see arguments of SCATD
NE	number of energy boundaries, including thermal group
NX	number of energy boundaries given by input
NAE	} needed field lengths, provided by DAØRG
ISG	
NISG	

Arguments, that are supplied by AKED to calling subroutine SCATD.

EZ(ISG) energy field, containing combination of energy points of the excitation cross-sections $\sigma_i^j(E')$, contributing in energy group I together with the energy points of the

⁺⁾ AKED(/4/) was originally developed by B. Schatz.

weighting function, energy points of the weighting function given energy-pointwise by input or energy points constructed by the subroutine SPECT1 for the representation of an analytic weighting spectrum given by a function subprogramme. (provided by DAØRG)

SGIP(ISG,NAE) level excitation cross-sections from KEDAK $\sigma_i^{E_j}$ (KEDAK-type SGIZ(E.,E')). First index refers to the energy E_i point E' in the E_j field EZ, the second index gives the number of the excitation level (provided by SIØRG)

JMAT number of excitation levels, contributing in energy group I (provided by DAØRG)

LMAX actual length of energy field EZ, needed to store cross-section and spectrum points for energy group I (provided by DAØRG)

SU(NX) energy group integral of the weighting function:

$$\int_{E_{g+1}}^E w(E') dE'$$

QUØT(NX) energy group integral of discrete level inelastic cross-section* weighting function

$$\int_{E_{g+1}}^E \sum_j \sigma_i^{E_j}(E') w(E') dE'$$

WERT(ISG) contains values of the weighting function w at energy points EZ(1)... EZ(LMAX)

AE(NAE) excitation energies of discrete levels contributing in energy group I (provided by SIØRG)

SGIT(ISG) $\sum_j \sigma_i^{E_j}(E')$. SGIT(II) is the total discrete level inelastic cross-section at the energy point EZ(II). (provided by SIØRG)

IANF(NAE) IANF(J) : number of first energy point of field EZ, for which an excitation cross-section of level J, $\sigma_i^{E_j}(E')$, is given on KEDAK. This first cross-section value is stored in SGIP(1,J), the corresponding energy is stored in EZ(IANF(J)):

$$\begin{array}{ll} \text{EZ(IANF(J))} & \dots \text{SGIP(1,J)} \\ \text{EZ(IANF(J)+1)} & \dots \text{SGIP(2,J)} \end{array}$$

$$\begin{array}{c} \vdots \\ \vdots \\ \vdots \end{array}$$

$$\text{EZ(LMAX)} \quad \dots \quad \text{SGIP(LMAX-IANF(J)+1)}$$

(provided by SIØRG)

EJMAX energy of excitation level of the highest energy, contributing in energy group I (provided by DAØRG)

local variables: NAEP,ISGP,NISGP,IA,NAB.

The subroutine DAØRG has two tasks. The first time DAØRG is called (by the subroutine SCATD for all energy groups required by input) its task is to find out

1. The common range of outscattering energies, that is required by the input and for which inelastic scattering reactions to excited levels occur, that means the range of energy groups, for which the calculation of inelastic scattering matrices to discrete levels is actually performed (IA,NAB).
2. The maximum values of the fieldlengths NISG,ISG and NAE, that are needed in any of the energy groups to be treated. If the values, of NISG, ISG NAE, estimated by the organizing subroutine SCAT are not sufficient, numbers NISGP,ISGP and NAEP are provided, that have to be added to NISG,ISG,NAE, to get sufficient field lengths.

The second call (subroutine DAØRG called by subroutine AKED) provides the energy field EZ.

Subroutine DAØRG(I,KEN,EZ,E,AE,EF,FI,J,KMAX,NISG,NISGF,NISGP,NE27,NAE, NAEF,NAEP,ISG,ISGF,ISGP,IA,NAB)

Arguments, that have to be defined, before DAØRG is called:

I	number of energy group
KEN=NFE	number of energy points of the weighting spectrum
EF(KEN)	energy points of the weighting spectrum
FI(KEN)	weighting spectrum
NE27	number of energy boundaries including thermal group
E(NE27)	energy group boundaries including thermal group
NISG,NAE, ISG	} field lengths estimated by subroutine SCAT

Quantities, that are supplied by DAØRG to the calling programme:

EZ(KMAX)	energy field, that contains all energy points of the partial inelastic excitation cross-section within energy group I and the energy points of the weighting spectrum.
KMAX	actual dimension of energy field described above.

AE(J) excitation energies, that may be excited by primary neutron energies belonging to energy group I

J actual length of field AE

NISGP } if $\neq 0$, they give the numbers, that have to be added to NISG,
NAEP } NAE, ISG, to get sufficient field lengths.
ISGP }

IA number of energy group of lowest energy, from which discrete levels can be excited and which is lying within the energy-group-range required by input.
IA = 0, if nuclear data are available for lowest energy group required by input

NAB number of energy group of highest energy, from which discrete levels can be excited, and which is lying within the energy-group range, required by input.
NAB = NE27-1, if nuclear data are available for highest energy group required by input.

If no excitation levels for discrete levels are available on the nuclear data library for the material in question, a return is made to the calling programme.

NISGF, NAEF, ISGF not used in the calling programme in the present version of the module.

The subroutine NDREAD reads from KEDAK the energy points, for which excitation cross-sections of the excitation level next higher to a given excitation level XLEVEL are stored within given energy limits.

NDREAD is called by DAØRG.

Subroutine NDREAD(I, EZ, E, AE, XLEVEL, J, KMAX, NENRE, NISG, NISGF, NISGP, NE27, NAE, NAEF, NAEP, NETMAX, IL, IB, IH, *)

Variables, that have to be defined, when NDREAD is called:

I number of energy-group, for which data are to be read.

NE27 see DAØRG

E(NE27) see DAØRG

XLEVEL Real*8-number, that is set equal to 0.0 by the calling programme, when the first excited level is to be found on KEDAK and that has to be slightly higher than the excitation energy of the level just below the one, that has to be read next /13/.

NISG maximum possible length of field EZ

NAE maximum possible length of field AE

KMAX EZ(1)...EZ(KMAX) is already filled with energy points of excitation cross-sections belonging to preceding levels.

Arguments, that are results of NDREAD:

KMAX After the return to the calling subroutine KMAX gives the number of energy points EZ, stored before calling NDREAD plus the number of energy points of the excitation cross-section of the energy level treated by the latest call of NDREAD.

EZ(KMAX) after returning to the calling programme EZ(KMAX) contains the energy points of the excitation cross-sections of the first J excitation levels. The energy points of the first (J-1) excitation levels are ordered according to ascending energies, following in the field EZ are the energypoints of the excitation cross-section of level number J.

AE(J) energy levels, whose excitation cross-sections have already been treated.

XLEVEL after return to the calling programme, XLEVEL contains the excitation energy of the excitation level, that has been read during the latest run of NDREAD.

J number of excitation levels, already treated by NDREAD.

NENRE NENRE = 2: The excitation level read during the latest run of NDREAD cannot be excited by neutrons with primary energies belonging to energy group I.

NISGF
NAEF
NISGP
NAEP } quantities needed for the calculation of the field lengths
 NISG,NAE

NETMAX maximum number of energy points within group I, at which the excitation cross-sections of any excitation level are stored (maximum needed length of NISG = maximum needed length of ISG+NETMAX).

IL,IB,IH local variables of the calling subroutine, that are commented on in the FORTRAN-programmes (NDREAD,DAØRG)

The subroutine ØRDNEN arranges the numbers, contained in the double precision array FELD(NTT), according to increasing quantities. ØRDNEN is called by DAØRG and SPECTI.

Subroutine ØRDNEN(KMAX,EMIN,EMAX,FELD,NTT,EPS)

Arguments, that have to be known, before the subroutine ØRDNEN is called:

KMAX used length of array FELD

FELD(1)...FELD(KMAX) array, that has to be ordered according to increasing numbers

NTT available length of array FELD
EPS if the relative deviation between any two members of FELD(KMAX)
 is less or equal EPS:

$$\left| \frac{\text{FELD}(I+1) - \text{FELD}(I)}{\text{FELD}(I+1)} \right| \leq \text{EPS},$$

FELD(I) is set equal to FELD(I+1). In the present version
of the module EPS = 0

Arguments, that are supplied by the subroutine ØRDNEN:

EMIN value of lowest number of FELD
EMAX value of highest number of FELD
KMAX number of members of FELD after eliminating equal numbers.

The subroutine CUTS cuts array FELD (that is ordered according to increasing quantities) at lower energy limit UGG and at upper energy limit ØGG. CUTS is called by DAØRG and by ENØRG.

Subroutine CUTS(UGG,ØGG,FELD,NFE,KA,KE,KMAX1)

Arguments, that have to be defined, before CUTS is called:

UGG lowest energy value, that shall be contained in FELD
 after cutting
ØGG highest energy value, that shall be contained in FELD
 after cutting
NFE length of array FELD
FELD(NFE) array (ordered according to increasing quantities), that
 has to be cut

Arguments, that are supplied by CUTS:

KA FELD(KA) = lowest value to be kept in array FELD after cutting
KE FELD(KE) = highest value to be kept in array FELD after cutting
KMAX1 KMAX1 = KE-KA+1 = number of values left in FELD after cutting
 low and high values

The subroutine SPECT1 checks, whether the energy field EZ(KMAX) contains enough points, to represent the analytical weighting function in such a way, that all points of the spectrum may be obtained by linear interpolation with a deviation of less than EPSI from the exact value. Actually it is checked, whether the midpoints between two given energy points may be obtained

by linear interpolation with sufficient accuracy. If not, the corresponding midpoints are added to the field EZ and the procedure is repeated until the condition

$$\left| \frac{\text{PHI}_{\text{interpolated}} - \text{PHI}_{\text{exact}}}{\text{PHI}_{\text{exact}}} \right| < \text{EPSI}$$

is fulfilled. SPECT1 is called by DAØRG.

Subroutine SPECT1(KMAX,EZ,NISG,NISGF,NISGP,EPSI,EPS)

Arguments, that have to be defined, before SPECT1 is called:

KMAX actual length of energy field EZ
NISG available length of energy field EZ
EZ(KMAX) field containing energy points (constructed from the energy points of the excitation cross-sections of all levels, that may be excited by neutrons of energy group I).
EPSI required accuracy of linear interpolation. In the present version EPSI is set equal to 0.001
EPS argument for the subroutine ØRDNEN (called by SPECT1)

Arguments, that are results of SPECT1:

KMAX actual length of array EZ after adding energy points of the analytic weighting function.
EZ(KMAX) energy points of EZ after adding analytic weighting spectrum
NISGF } if ≠ 0, the field length NISG of EZ is not sufficient.
NISGP } NISGF,NISGP give information about necessary field length

The subroutine TRA corresponds to the subroutine of the same name in /4/. TRA supplies the values FIS of the (tabulated or analytic) weighting function at energy points EFI. TRA is called by AKED and SCATD.

Subroutine TRA(EFI,FIS,NF,EF,FI)

Arguments, that have to be defined, before TRA is called:

EFI energy point, at which the weighting function has to
 be calculated

NF field length of tabulated weighting function

EF(NF) }
FI(NF) } tabulated weighting function

supplied by TRA is FIS

FIS value of the weighting function at energy EFI

The subroutine SIØRG organizes the interpolation of the excitation cross-sections read from KEDAK into the energy grid EZ(KMAX) provided by DAØRG. Moreover it calculates at each point of the energy grid the sum of the excitation cross-sections over all excitation levels: $\sum_j \sigma_i^{E_j}(E')$.

The reading of the cross-sections from the KEDAK-library is done by SGINT, the interpolation is performed by XINPØL. The subroutine SIØRG is called by AKED.

Subroutine SIØRG(I,EZ,AE,SGIP,SGIT,IANF,JMAX,KMAX,NISG,ISG,NAE)

Arguments, that have to be known, before calling SIØRG:

I number of energy group

KMAX length of energy grid EZ, established by DAØRG and its
 subroutines

EZ(KMAX) energy grid, established by DAØRG and its subroutines

NISG }
ISG } available lengths of arrays, given in the dimension statement
NAE }

Arguments, that are supplied by SIØRG:

JMAX number of excitation levels, that may be excited by
 neutrons with primary energies of energy-group I

AE(JMAX) excitation levels

SGIP(KMAX,JMAX) excitation cross-sections at KMAX energy points and
 for JMAX levels

SGIT(KMAX) $\sum_j \sigma_i^{E_j}(E')$: total discrete level excitation inelastic cross section

IANF(JMAX) IANF(J): pointer, that gives the number of the energy point of the field EZ, at which the excitation cross-section for level AE(J) starts (pointer for the threshold of the excitation cross-section of AE(J))

The subroutine SGINT reads for level XLEVEL excitation cross-sections from KEDAK, that lie within the energy limits EZ(1)...EZ(KMAX). SGINT is very similar to the subroutine NDREAD, however SGINT reads energy-points and cross-section-points. SGINT is called by SIØRG.

Subroutine SGINT(EZ,AE,SGIT,KMAX,KMAX1,XLEVEL,J,NISG,NAE,ISG,NENRE,IH)

Arguments, that have to be defined, before SGINT is called:

KMAX the energy field EZ is already in use until EZ(KMAX): EZ(KMAX+1) may be used, to store the first energy point read from KEDAK

XLEVEL the following excitation energy to be read from KEDAK has to be higher than XLEVEL /13/.

NISG } available lengths of arrays
NAE }
ISG }

quantities, that are supplied by SGINT:

KMAX1 KMAX1-KMAX: number of energy points of excitation cross-section of level AE(J), that are stored on the nuclear library within the energy region EZ(1)...EZ(KMAX)

EZ(KMAX+1)... EZ(KMAX1): energy points of excitation cross-section of AE(J) on KEDAK (within the energy limits EZ(1)...EZ(KMAX)).

AE(J) excitation energy, that was treated in the latest call of SGINT

J number of energy level, that was the latest one, that was read from the library

SGIT(ISG) SGIT(1)...SGIT(KMAX1-KMAX): excitation cross-section of level AE(J) read from KEDAK

XLEVEL AE(J), when SGINT returns to SIØRG.

quantities, that are of local significance in SIØRG: NENRE,IH.

The subroutine XINPØL performs the following task: The cross-sections SGIT(1) ... SGIT(NETACT) with the corresponding energy-points EZ(KMAX+1)...EZ(KMAX+NETACT) are to be interpolated (linear interpolation) into the energy field EZ(1)...EZ(KMAX). The subroutine XINPØL is called by SIØRG.

Subroutine XINPØL(EZ,SGIT,SGP,NISG,NETACT,KMAX,KANF,KEND)

Arguments, that have to be defined, when XINPØL is called:

EZ(1)...EZ(KMAX)	energy field, into which the cross-sections are to be interpolated
EZ(KMAX+1)...EZ(KMAX+NETACT)	energy points of the cross-section
SGIT(NETACT)	cross-sections
NISG	available length of field EZ
NETACT	number of energy points of the cross-section
KMAX	length of the energy field, into which the cross-section are to be interpolated

Arguments, that are results of the subroutine XINPØL:

SGP(KMAX)	values of cross-sections, interpolated into energy-field EZ(1)...EZ(KMAX)
KANF	pointer, that gives the number of the first energy point of EZ, for which a value of SGP is given: EZ(KANF)...SGP(1) EZ(KANF+1)...SGP(2)
KEND	pointer, that gives the number of the last energy point of EZ, for which a value of SGP is given. EZ(KEND)...SGP(NETACT)

The function FIPØLA performs linear interpolation to one point lying between two given points

FIPØLA is called by TRA,SPECTI,RENUDA,SINPØL.

Function FIPØLA(XA,XB,XC,YA,YC)

XA	abscissa of first given point
YA	ordinate of first given point
XC	abscissa of second given point
YC	ordinate of second given point
XB	abscissa of point, to which the interpolation has to be carried out.

All arguments are REAL*4-variables.

When returning to the calling programme, FIPØLA contains the ordinate corresponding to XB.

The function FIPØLD corresponds to the function FIPØLA, however the arguments, containing the given and required abscissa are REAL*8-variables.

The function FIPØLD is called by SCATD,AKED,XINPØL.

Function FIPØLD(XAD,XBD,XCD,YA,YC)

XAD	abscissa of first given point (REAL*8)
YA	ordinate of first given point (REAL*4)
XCD	abscissa of second given point (REAL*8)
YC	ordinate of second given point (REAL*4)
XBD	abscissa of point, to which the interpolation has to be carried out (REAL*8)

6.3.2 Description of the subroutine SCATC and its subprogrammes

The subroutine SCATC together with its subprogrammes calculates transfer probabilities for inelastic scattering with excitation of continuous levels of the residual nucleus according to formulas (6.20), (6.20.1) and (6.20.2). Moreover transfer matrices for (n,2n)- and (n,3n)-reactions are calculated according to formula (6.23). For the calculation of the total inelastic scattering transfer matrices in the programme SCAT $R_{i,g}^c$ (formula 6.21.2) is provided by SCATC. SCATC organizes for the outscattering groups required by input (and for which continuous level inelastic scattering occurs) and for all inscattering groups the calculation of the transfer matrices and of the reaction rates.

Subroutine SCATC(NX,EG,XNUE,NFE,EF,FI,NE27,INTYP,WEINC,QUOTC,ENG,EZ,SGIZC, EI,EP,F1,F2,F3,F4,NISG,NISGP,NISGI,NISGIP,NEP,NEPP,NF,NFP, IA,NAB)

Arguments, that have to be defined, when the subroutine SCATC is called

NX	number of energy group boundaries of outscattering groups (may or may not contain thermal group)
EG(NX)	energy boundaries of outscattering groups (internal energy group count: EG(1) refers to the lowest energy value)
XNUE	parameter of the evaporation model; used only, if type SEDIC(SED2N,SED3N) is not given on KEDAK for the material in question
NFE	number of points of the weighting function given by the input
EF(NFE)	energy points of the weighting function
FI(NFE)	values of the weighting function
NE27	number of energy boundaries of inscattering groups (contains thermal group)
INTYP	gives type of reaction, for which the transfer probabilities have to be calculated: $\left. \begin{array}{l} 1: \text{inelastic scattering with excitation of} \\ \text{continuous levels of the residual nucleus} \\ 2: \text{(n,2n)-reactions} \\ 3: \text{(n,3n)-reactions} \end{array} \right\} \text{INTYP}$

NISG,NISGI,NEP,NF : estimated lengths of arrays, used as working fields by SCAT and its subroutines.

Arguments, that are results of SCATC and its subroutines:

- WEINC(NX,NX) normalized transfer probabilities for the reaction type given by INTYP. The first index refers to the outscattering group (internal energy-group count). The second index refers to the inscattering group in the following manner:
second index = 1: inscattering group = outscattering group;
second index = 2: inscattering group lies energetically one group lower than the outscattering group; second index = 3: inscattering group lies energetically two groups lower than the outscattering group and so on.
- QUØTC(NX) $R_{i,g}^c$, given in formula (6.21.2). The reaction rate is calculated for the reaction, defined by INTYP
- IA number of outscattering group of lowest energy, for which transfer probabilities are provided by SCATC
- NAB number of outscattering group of highest energy, for which transfer probabilities are provided by SCATC

The following arguments are working fields:

- ENG(NE27) energy group boundaries containing thermal group; given in internal energy-group count
- EZ(NISG) energy points of SGIZC (SG2N,SG3N), read from KEDAK
- SGIZC(NISG) array, that contains continuous level inelastic cross-sections (or (n,2n)-cross-sections or (n,3n)-cross-sections), read from KEDAK
- NISGP if $\neq 0$, NISGP has to be added to NISG, to obtain sufficient field lengths
- EI(NISGI) array, in which the combination of EZ and EF is stored
- NISGIP if $\neq 0$, NISGIP has to be added to NISGI, to obtain sufficient field length
- EP(NEP),
F1(NF,NEP),
F2(NF,NEP),
F3(NF,NEP),
F4(NF,NEP) } filled by subroutine RENUA
(see below)with information of
KEDAK-type SEDIC (or SED2N or SED3N)
- NEPP } if $\neq 0$, NEPP(NFP) has to be added to
- NFP } NEP(NF), to obtain sufficient array lengths

Subroutine RENUDA reads from the nuclear data library continuous level inelastic cross-sections (SGIZC) (or (n,2n)-cross-sections (SG2N), or (n,3n)-cross-sections (SG3N)) within given energy limits. If the type SGIZC is not available on KEDAK (for the material in question) the points of type SGI, lying above the energy region of discrete level inelastic scattering, (above the highest energy point of SGIZ) are interpreted as points of SGIZC.

RENUDA is called by SCATC.

Subroutine RENUDA(TYP,KONT,SGIZC,EZ,EU,EØ,NACT,NISG,NISGP)

Arguments, that have to be defined, before RENUDA is called:

TYP	type of cross-section, that has to be read from the nuclear data library
EU	lower limit of energy region, within which the cross-section has to be read from KEDAK
EØ	upper limit of energy region, within which the cross-section has to be read from KEDAK
NISG	length of array EZ, available to store energy points read from KEDAK

Arguments, that are results of RENUDA

KONT	{	= 0: the required cross-section type is not available on the nuclear data library	
		= 1: the required cross-section type is available on the nuclear data library	
NISGP		see description of SCATC	
NACT		contains actual length of fields EZ and SGIZC, if $NACT \leq NISG$	
EZ(NACT)	}	energy points	} read from KEDAK
SGIZC(NACT)		cross-sections of type TYP	

The subroutine ENØRG constructs the energy field EI(KMAX), that consists of the energy points EZ(NACT) (energy points of the cross-sections read from KEDAK) and the energy points of the weighting functions EF(NFE) in case the weighting function is given energy pointwise by the input). If the weighting function is given by an analytical function, ENØRG is not called. The

resulting energy field EI(KMAX) has the lower energy limit EU and the upper energy limit EØ and is ordered according to growing energy values.

The subroutine ENØRG is called by SCATC.

Subroutine ENØRG(EU,EØ,EI,EF,NACT,KMAX,KEN,NISGI,NISGIP)

Arguments, that have to be defined, when ENØRG is called:

EU	lower energy limit for the resulting energy field EI
EØ	upper energy limit for the resulting energy field EI
EI(NACT)	when ENØRG is called EI contains the energy field EZ(NACT)
EF(KEN)	energy points of the weighting function given by the input
NACT	length of the field EI, that is to be combined with the energy points EF, that lie within the energy limits EU, EØ
KEN	total number of energy points of the weighting function, given by the input (=NFE)
NISGI	available length of field EI

Arguments, that are results of the subroutine ENØRG.

KMAX	gives length of energy field, that is the combination of EI(NACT) and EF(NFE)
EI(KMAX)	resulting combined energy field
NISGIP	if ≠ 0, NISGIP gives number, that has to be added to NISGI, to get sufficient field length for EI

The subroutine CUTS, called by ENØRG is described in the preceding chapter 6.3.1.

The subroutine ØRD1, called by ENØRG has the same task as the subroutine ØRDNEN described in chapter 6.3.1. However, the field FELD(NTT), to be ordered according to increasing values is a REAL*4 variable in ØRD1 and a REAL*8 variable in ØRDNEN.

The subroutine REPROB reads from KEDAK the energy distribution of secondary neutrons for continuous level inelastic scattering or (n,2n)-processes or (n,3n)-processes respectively. The corresponding KEDAK-types are SEDIC, SED2N and SED3N. In the present status the programme can handle an evaporation model only. The nuclear temperature may be given as tabulated function of the incident neutron energy or as analytic function of the incident neutron energy. An extension to secondary energy distributions given by tables (types CHII, CHI2N, CHI3N on KEDAK) is being worked on.

If the KEDAK-types SEDIC (or SED2N or SED3N respectively) do not contain information, an evaporation model is used with the nuclear temperature given by $\Theta = \sqrt{\frac{E^*}{v \cdot A}}$ (compare chapter 6.2.3). The atomic weight A is obtained by reading the KEDAK-type ISOT1 /13/. The threshold U for the wanted reaction type is obtained by reading from KEDAK the respective cross-section (SGI,SG2N,SG3N) and finding the energy point, where the cross-section starts to be greater than zero.

The subroutine REPROB is called by SCATC.

Subroutine REPROB(INTYP,KONT,EP,F1,F2,F3,F4,NEP,NEPP,NF,NFP)

Arguments, that have to be known, before REPROB is called

INTYP gives reaction type, for which the energy distribution of secondary neutrons has to be read from KEDAK.

INTYP = $\left\{ \begin{array}{l} 1: \text{ type SEDIC has to be read} \\ \quad \text{(or A from ISOT1 and U from SGI)} \\ 2: \text{ type SED2N (or A from ISOT1} \\ \quad \text{and U from SG2N)} \\ 3: \text{ type SED3N (or A from ISOT1} \\ \quad \text{and U from SG3N)} \end{array} \right.$

NEP available length of array EP and of second index of F1, F2, F3, F4

NF available length of first index of F1, F2, F3, F4

Arguments, that are results of REPRØB:

KØNT { 1: required type (SEDIC,SED2N,SED3N)
available on KEDAK
0: required type not available on KEDAK, an
evaporation model with $\theta = \sqrt{\frac{E'}{v \cdot A}}$ has to be used

EP(NEP) primary neutron energies, obtained from KEDAK as
further name from types SEDIC,SED2N,SED3N (see /13/)

F1(NF,NEP): K }
F2(NF,NEP): P } from types SEDIC,SED2N,
F3(NF,NEP): Ø } SED3N (see /13/)
F4(NF,NEP): U }

If there is no information stored in types SEDIC or SED2N or SED3N
respectively two quantities from KEDAK are stored in the field F4:

F4(1,1) is filled with A, the atomic weight of the material
considered

F4(1,2) is filled with U, the threshold energy of the reaction

NEPP if $\neq 0$, NEPP gives number, which has to be added to NEP,
to obtain sufficient lengths of arrays

NFP if $\neq 0$, NFP gives number, which has to be added to NF,
to obtain sufficient lengths of arrays

The labelled COMMON APØINT contains the information about the actual lengths
of fields EP,F1,F2,F3,F4, in case NEP and NF were sufficient.

COMMON/APØINT/INEP,INF

INEP actual value of NEP
INF actual value of NF

The subroutine SIMP SI performs the integration in numerator and denomi-
nator of formulas (6.20) and (6.20.2) and (6.23) using the Simpson-rule /12/.

SIMP SI is called by SCATC

Subroutine SIMPSI (NUGRE,U,AW,XNUE,A,B,EPS,NMAXX,RESINT,N,EZ,SGIZC,
 EF,FI,ENG,NACT,NFE,NE,NN,EP,F1,F2,F3,F4,NEP,NF,
 KØNT,ERR)

Arguments, that have to be defined, when SIMPSI is called:

NUGRE group number of inscattering group in internal energy
 group count (NUGRE is used only, if NN=1)

U threshold energy for reaction under consideration

AW atomic weight as given by the KEDAK-type ISØT1

XNUE parameter of the evaporation model (ν), used if no
 information is given in the KEDAK-type SEDIC (SED2N,SED3N)

A lower energy limit of integration

B upper energy limit of integration

the values of A and B are the energy points of the field EI, constructed
 by ENØRG. If the weighting spectrum is given as an analytic function, A
 and B are given by the array EI, that contains the energy points of the
 corresponding cross-section on KEDAK and the energy group boundaries.

EPS required accuracy of the integration (1 % in the present
 version). EPS means the relative deviation of two sub-
 sequent integrations

NMAXX maximum number of integration intervals during Simpson integration.
 (NMAXX = 100 000 in the present version; see the
 discussion of the warning printed out by SIMPSI)

EZ (NACT)	}	quantities, described before in connection with subroutines RENUA, REPRØB and SCATC
SGIZC (NACT)		
EF (NFE)		
FI (NFE)		
ENG (NE)		
EP (NEP)		
F1 (NF,NEP)		
F2 (NF,NEP)		
F3 (NF,NEP)		
F4 (NF,NEP)		
NACT		
NFE		
NE		
NEP		
NF		

KØNT	}	if = 0, the nuclear temperature has to be calculated from $\theta = \sqrt{\frac{E^i}{\nu \cdot A}}$ (no information in types SEDIC (SED2N,SED3N) on KEDAK)
		if = 1, the nuclear temperature is given on KEDAK (SEDIC,SED2N,SED3N)

NN characterizes function, that has to be integrated by SIMPSI

NN = 0: $\int_A^B \sigma_i^c(E')w(E')dE'$ has to be calculated (formula (6.21.2))

NN = 2: $\int_A^B w(E')dE'$ has to be calculated (denominator of (6.20))

NN = 1: $\int_A^B \sigma_i^c(E')w(E')P_i^c(E' \rightarrow h)dE'$

(see numerator of formula (6.20))

Arguments, that are results of SIMPSI:

RESINT result of integration
N number of integration intervals, actually used
ERR accuracy of integration, actually obtained (relative deviation between the two last subsequent integrations)

Warning printed out by SIMPSI

In case the required integration accuracy, EPS, is not obtained after using NMAXX integration points in the energy region (A,B), a message is printed out by SIMPSI. It contains information about

N number of integration intervals, actually used
NMAX maximum number of integration intervals (which is 100 000 in the present version, but may be reduced, if A and B are very close to each other; see below)
RESINT result of integration
ERR integration accuracy, actually obtained
NN type of function, that has to be integrated
A lower integration limit
B upper integration limit
INUGRE number of inscattering group in external energy group count (group number one refers to energy group of highest energy)

This message is often produced for the case NN=1, when the integration limits lie within an outscattering group, that contains the threshold of the considered reaction. To get an impression of the error, that may be

introduced into the final result, the integral (NN=1) over the entire outscattering group into group INUGRE is printed out by SCATC. This write-statement gives number of outscattering group, number of in-scattering group (both in external group count) and the integral (NN=1) over the entire outscattering group

$$\int_{E_{g+1}}^{E_g} \sigma_i^c(E') w(E') P_i^c(E' \rightarrow h) dE'$$

In some cases the maximum number of intervals, that may be generated during the Simpson-integration is restricted, in order to save computer time: If the integration interval (A,B) is very small, ($\frac{B-A}{B}$ less or equal $1.1E-5$) the integration is carried out by the trapezoidal rule. For $\frac{B-A}{B}$ less or equal $5.E-5$ the maximum number of integration intervals, NMAX, is restricted to 20. (The integration interval (A,B) becomes small, if energy points on KEDAK are very close to each other, or if one of the KEDAK energy points lies very close to one of the energy points of the weighting function.)

If the threshold of the reaction lies within the outscattering group and the upper energy boundary of the in-scattering group is less or equal 101 eV, the number of integration intervals is restricted to 100.

If during the integration the interval H becomes small compared to the lower integration limit A, $\frac{H}{A}$ less or equal $0.5E-6$, and the number of integration intervals is already greater than 100, the Simpson-integration is stopped and the message explained above is printed out.

The function, that has to be integrated by SIMPSI is provided by the function FINT. This may be $\sigma_i^c(E') w(E')$ (6.21.2)

$w(E')$

$\sigma_i^c(E') w(E') P_i^c(E' \rightarrow h)$ (numerator of (6.20))

FINT is called by SIMPSI.

Function FINT(E,NUGRE,U,AW,XNUE,EZ,SGIZC,EF,FI,ENG,NACT,NFE,NE,NN,EP,F1,F2,F3,F4,NEP,NF,KONT)

Arguments of function FINT:

E energy point of outscattering group, at which the function is to be calculated. This corresponds to E' in formulas (6.20), (6.21.2)

NUGRE
U
AW
XNUE

} same meaning as in SIMPSI

EZ(NACT)
SGIZC(NACT)
EF(NFE)
FI(NFE)
ENG(NE)
EP(NEP)
F1(NF,NEP)
F2(NF,NEP)
F3(NF,NEP)
F4(NF,NEP)

} quantities, described before in connection with subroutines RENUA, REPRØB and SCATC

NACT
NFE
NE
NEP
NF

} described in connection with RENUA, REPRØB, SCATC

NN characterization of function, that has to be calculated (see discussion of argument list of SIMPSI)

KØNT see description of argument list of SIMPSI

The function SINPØL performs linear interpolation to a given abscissa, starting from a tabulated function. SINPØL calls the function FIPØLA. SINPØL is called by FINT, to interpolate the cross-section and the weighting function.

Function SINPØL(EINT,EFELD,FELD,NFELD)

discussion of the arguments of the function SINPØL:

EINT energy point, at which the value of the tabulated function has to be obtained by linear interpolation

NFELD number of tabulated values

EFELD(NFELD) abscissa of tabulated function (energy points)

FELD(NFELD) function value FELD(I) corresponds to energy EFELD(I)

The function PRØB calculates the transfer probabilities $P_i^c(E' \rightarrow h)$ (see formula (6.20)) for inelastic scattering, (n,2n) or (n,3n)-reactions.

PRØB is called by FINT

Function PRØB(E,NUGR,U,A,XNUE,ENG,NE,EP,F1,F2,F3,F4,NEP,NF,KØNT)

E energy point of outscattering group, for which the transfer probability has to be calculated (corresponds to E' in formulas)

NUGR group number of inscattering group (internal group count)

U threshold of reaction

A atomic weight as given by KEDAK-type ISØT1

XNUE parameter for the calculation of the nuclear temperature

KØNT { = 0, if nuclear temperature is not given on KEDAK
= 1, if nuclear temperature is given on KEDAK

NE,NEP,NF
ENG(NE)
EP(NEP)
F1(NF,NEP),F2(NF,NEP)
F3(NF,NEP),F4(NF,NEP)

} described in connection with SCATC and REPRØB

The double precision function EXD(X) calculates (with double precision) the series $(\exp(x)-1)$, which is needed for a good numerical evaluation of $P_i^c(E' \rightarrow h)$ in the numerator of formula (6.20) for inscattering groups of small energy, (see /4/, chapter 6, page 6.8)

The function EXD is called by PRØB.

The double precision function DNFAK(NN) calculates (with double precision) NN!

DNFAK is called by EXD.

The function TEMP calculates the nuclear temperature used for the evaporation model by linear interpolation of the data given by the KEDAK types SEDIC, SED2N, SED3N.

TEMP is called by PRØB.

Function TEMP(EFS,EP,F3,NEP,NF)

description of the arguments:

EFS energy point of outscattering group, at which the
 nuclear temperature has to be calculated

EP(NEP) energy points (energies of incident neutron)
 given on KEDAK (KEDAK types SEDIC, SED2N, SED3N)
 /13/

F3(NF,NEP) nuclear temperatures given on KEDAK. If the energy
 distribution of secondary neutrons is given by a
 linear combination of different analytic functions
 on KEDAK, the first index of F3 refers to the number
 of the analytic function. In most cases the distri-
 bution is described by one analytic function only.
 The second index refers to the primary energy given
 in EP.

NEP,NF available field lengths

The actual field lengths of EP and F3 given by the KEDAK data are transferred by the common |APØINT|

INEP actual value of NEP

INF actual value of NF

The function THETA calculates the nuclear temperature for the evaporation model, in case no information is contained in SEDIC (or SED2N or SED3N respectively).

THETA is called by PRØB.

Function THETA(E,XN)

E energy point, for which the nuclear temperature
 is to be calculated (E' in formulas)

XN XNUE*A, prepared in PRØB

6.3.3 The organizing subroutine of module 5, SCAT

One task of the subroutine SCAT is to organize the working field X(MMAXX) for the use in SCATD and SCATC. In the programme MIGRØS-2, /4/, the organizing of the working fields used in module 5 was done by the subroutine INPUT. In the new version of module 5 the inelastic scattering to discrete levels of the residual nucleus and the inelastic scattering to continuous levels of the residual nucleus are treated in completely separated sets of subroutines, SCATD and SCATC, with completely different working fields and consequently completely different storage requirements. In order to avoid too many changes in the subroutine INPUT (call and organization of two different modules (instead of one) for the calculation of inelastic transfer matrices) the organization of the working fields of SCATD and SCATC is now done in SCAT.

If the length of the working field, MMAXX, is not sufficient to carry out the calculations in SCATD or SCATC, control is returned to the calling subroutine INPUT. The subroutine INPUT checks, whether transfer matrices for further reactions ((n,2n) or (n,3n)) are required by the programme input. In that case SCAT is called again and it is tried, to calculate the (n,2n)- or (n,3n)-matrices; otherwise the module with the next module number required by the programme-input is called. The second task of SCAT is, to calculate the total inelastic scattering transfermatrix from the results of SCATD and SCATC according to formula (6.21.1) in chapter 6.2.4. $R_{i,g}^d, R_{i,g}^c$ and $P_{i,g \rightarrow h}^d, P_{i,g \rightarrow h}^c$ are given as results of SCATD and SCATC.

Finally SCAT organizes the output of module 5 on listing and produces the unformatted output.

SCAT is called by the subroutine INPUT.

Subroutine SCAT(NX,EG,XNUE,NFE,EF,FI,NE27,KINEM,NIN,NINA,INTYP,X,IX,MMAXX, MFELD)

The first eleven variables of the argument list are input quantities, that are transferred by the calling programme INPUT.

NX number of group boundaries of outscattering groups
EG(NX) energy group boundaries of outscattering groups
XNUE parameter of the evaporation model
NFE number of points of the weighting function
EF(NFE) abscissa of the weighting function
FI(NFE) ordinates of the weighting function
NE27 number of energy group boundaries of the inscattering groups (includes thermal group)
KINEM parameter, that selects, how the energy loss of the incident neutron is calculated in inelastic scattering processes with excitation of discrete levels of the residual nucleus:

KINEM=0: formula (6.2) is applied

KINEM=1: formula (6.3) is applied
(this is the standard input
in the present version)

KINEM=2: formula (6.4) is applied

NIN number of reaction types, for which transfer matrices are to be calculated. Possible are inelastic scattering, (n,2n)-processes and (n,3n)-processes
(standard input is NIN=2)

INTYP(NIN) characterization of the reaction types

INTYP(I)=1: inelastic scattering

INTYP(I)=2: (n,2n)-reactions

INTYP(I)=3: (n,3n)-reactions

(standard input is INTYP(1)=1, INTYP(2)=2)

Moreover the subroutine INPUT defines the available length of the working field:

MMAXX available length of the working field

X(MMAXX),IX(MMAXX) working field, available in SCAT

Results from SCAT, that are returned to the calling programme INPUT.

MFELD actually needed length of working field

NINA number of reactions, for which calculations in SCAT have already been carried out or had to be interrupted because of insufficient length of the working field

In the following the most important variables used in SCAT are described

1. Correspondence between the working fields in SCAT and the results of the subroutine SCATD:

$X(L1) \dots X(L1+NX*NX-1)$: corresponds to $WEIN(1,1) \dots WEIN(NX,NX)$ in SCATD and contains normalized transfer probabilities of inelastic scattering processes connected with excitations of discrete levels of the residual nucleus as given in formula (6.14)

$X(L2) \dots X(L2+NX-1)$: corresponds to $QUOT(1) \dots QUOT(NX)$ in SCATD and contains the resonance integrals $R_{i,g}^d$ as given in formula (6.21.2).

Explanation of some variables used in SCAT, to handle the results of SCATD (in the statements following "CALL SCATD").

IG	external count of group numbers (1 corresponds to energy group with highest energy)
MG	internal count of group numbers (1 corresponds to energy groups with lowest energy)
NXMH	number of downscattering (in-scattering) groups (containing outscattering group)
MH	group count for downscattering (in-scattering) groups
	MH=1: in-scattering group corresponds to outscattering group
	MH=2: in-scattering group is the energy group, energetically next lower to the out-scattering group
	MH=3: in-scattering group is the energy group, that energetically is two groups lower than the outscattering group
	MH=NXMH: in-scattering group is that energy group, that energetically is (NXMH-1) groups below the outscattering group

Detailed correspondence between $X(L1) \dots X(L1+NX*NX-1)$ and $WEIN(1,1) \dots WEIN(NX,NX)$ and $X(L2) \dots X(L2+NX-1)$ and $QUOT(1) \dots QUOT(NX)$

$X(L1)$ corresponds to $WEIN(1,1)$:

transfer probability (for inelastic scattering with excitation of discrete levels) from outscattering group of lowest energy into the same group:
(EG(1),EG(2))

$X(L1+MG-1)$ corresponds to $WEIN(MG,1)$:

transfer probability from energy group MG (internal group count) into energy group MG.

$X(L1+MG+NX-1)$ corresponds to $WEIN(MG,2)$:

transfer from energy group MG (internal count) to that inscattering group, that energetically lies one group below MG.

$X(L1+MG+2*NX-1)$ corresponds to $WEIN(MG,3)$:

transfer from group MG to that group, that energetically lies two groups below MG.

finally:

$X(L1+MG+(NXMH-1)*NX-1)$ corresponds to $WEIN(MG,NXMH)$:

transfer from group MG to that group, that energetically lies $(NXMH-1)$ groups below MG.

$X(L2)$ corresponds to $QUOT(1)$:

resonance integral (according to formula (6.21.2) for outscattering group of lowest energy (EG(1), EG(2))

$X(L2+1)$ corresponds to $QUOT(2)$:

resonance integral for outscattering group of second lowest energy

$X(L2+NX-1)$ corresponds to $QUOT(NX)$:

resonance integral for outscattering group of highest energy (EG(NX-1), EG(NX))

2. Correspondence between the working fields in SCAT and the results of the subroutine SCATC:

$X(L3)...X(L3+NX*NX-1)$ correspond to $WEINC(1,1)...WEINC(NX,NX)$, the normalized transfer probabilities for inelastic scattering with excitation of continuous levels (or for $(n,2n)$ - or $(n,3n)$ - transfer probabilities). See formulas (6.20)-(6.20.2) (or (6.23)).

$X(L4) \dots X(L4+NX-1)$ correspond to $QU\emptyset TC(1) \dots QU\emptyset TC(NX)$ and contain the resonance integrals $R_{i,g}^c$ according to formula (6.21.2)

The relations between $X(L3) \dots X(L3+NX*NX-1)$ and $WEINC(1,1) \dots WEINC(NX,NX)$ and between $X(L4) \dots X(L4+NX-1)$ and $QU\emptyset TC(1) \dots QU\emptyset TC(NX)$ correspond to the relations between the working fields in SCAT and the results of SCATD:

$X(L3)$ corresponds to $WEINC(1,1)$

$X(L3+MG-1)$ corresponds to $WEINC(MG,1)$

$X(L3+MG+NX-1)$ corresponds to $WEINC(MG,2)$

$X(L3+MG+(NXMH-1)*NX-1)$ corresponds to $WEINC(MG,NXMH)$

$X(L4)$ corresponds to $QU\emptyset TC(1)$

$X(L4+NX-1)$ corresponds to $QU\emptyset TC(NX)$

The results of SCAT, which are total inelastic scattering matrices (INTYP=1) or transfer matrices for (n,2n) - reactions (INTYP=2) or for (n,3n)-reactions (INTYP=3) are finally stored in $X(L1) \dots X(L1+NX*NX-1)$

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7. Calculation of Normalized Elastic Scattering Matrices and of Elastic and Total Group Cross Sections. Module 6.

In neutronic assemblies in which neutrons with energies above 100 keV essentially determine reaction rates, neutron leakage etc. anisotropic elastic scattering has to be taken account of. In widely used S_N -transport calculations this is achieved with a Legendre-expansion of the elastic scattering kernel in the multigroup transport equation. Especially extended transport approximations, consistent /1/ or inconsistent /2/ with the Boltzmann equation, turned out to be well suited for anisotropic calculations. The MIGROS-module to be described here provides the needed microscopic multigroup cross sections up to a Legendre-order $L = 5$. The Legendre-moments of the neutron flux density in suitably chosen subzones of the reactor under consideration, being needed as weighting-functions, are approximated by $\psi_\ell(E) = F(E) / [\Sigma_t(E)]^{\ell+1}$, $\ell = 0, 1, \dots, 5$, where $F(E)$ is the total collision density and $\Sigma_t(E)$ is the macroscopic total cross section of the subzone. Additionally, simpler weighting options may be applied. For a detailed discussion on weighting the reader is referred to /1/.

Since the first report on MIGROS-2 /3/ in 1973 this module has undergone some modifications. These are

- the additional determination of ψ_ℓ -weighted total group cross sections for S_N -calculations in extended transport approximations
- a reduction in weighting options (options for test purposes are cancelled)
- an improved calculation of hydrogen scattering matrices (transfer elements for scattering into the last group had been erroneous)
- improvements in fine-structure weighting in connection with the calculation of total group cross sections
- substitution of the non-linear interpolation procedure to smoothe interpolated values
- initial determination of the need of computer storage to save computing time in case of a restart

- cancellation of the restriction to four fine-groups per macro-group to save time in many-group calculations (more than 200 groups)
- changes in output format to compact the written output
- changes in messages (errors and warnings)

In Tab. 1 the modified and unmodified subroutines are listed separately. For the performance of each subroutine see below (chapter 7.3).

Tab. 1: Subroutines of the modified module 6

Modified	Unmodified
FLUMMI, SUM, IPØLA, PUSUM ⁺ , MAKRO, MIXSGT ⁺ , INFØRM ⁺ , PUNK, LØØKO ⁺ , LØØKI ⁺ , LØØK2 ⁺ , GRUPIN, SPRAL, TRAPEZ ⁺⁺ , MUKØN ⁺ , PRINT	ADD, TRAFØ, LØØK3, LECAL, LEGPØL, LEGINT, G, LEGIST, LEGANS, IPØLIN, PHI

⁺ only slightly modified, ⁺⁺ eliminated

Along with these modifications a change in the overlay structure was necessary (see Chapter 1, Table II).

7.1 Definition of the quantities calculated in this module

Given are the KEDAK data

$\sigma(E)$ = microscopic cross section for elastic neutron scattering at energy E
(KEDAK type SGN),

$\bar{w}(E, \bar{\mu}_0)$ = angular distribution in the c.m.-system for elastic neutron scattering with

$$2\pi \int_{-1}^{+1} d\bar{\mu}_0 \bar{w}(E, \bar{\mu}_0) = 1$$

E = energy of the incoming neutrons

$\bar{\mu}_0$ = scattering cosine in the c.m.-system
(KEDAK type SGNC),

$\sigma_t(E)$ = total microscopic neutron reactions cross section at energy E (KEDAK type SGT).

Then for energy groups (E_g, E_{g-1}) , $E_1 > E_2 > \dots > E_G$, G = number of groups, the module calculates the elastic group cross sections⁺

$$\sigma_g^E = \int_g dE \sigma(E) \psi_0(E) / \int_g dE \psi_0(E), \quad (7.1)$$

$$g = 1, 2, \dots, G,$$

the total ψ_ℓ -weighted group cross sections

$$\sigma_{t,\ell}^g = \int_g dE \sigma_t(E) \psi_\ell(E) / \int_g dE \psi_\ell(E), \quad (7.1')$$

$$\ell = 0, 1, \dots, 5; \quad g = 1, 2, \dots, G,$$

the normalized ℓ -th order matrixelements for elastic scattering from group g' to group g

$$s_\ell^{g' \rightarrow g} = \frac{1}{\sigma_{g'}^{g'}} \int_{g'} dE \sigma(E) w_\ell(E \rightarrow g) \psi_\ell(E) / \int_{g'} dE \psi_\ell(E) \quad (7.2)$$

$$\ell = 0, 1, \dots, 5; \quad g', g = 1, 2, \dots, G,$$

and the mean scattering cosine in group g

$$\bar{\mu}^g = \sum_{g' \geq g} s_1^{g \rightarrow g'}, \quad g = 1, 2, \dots, G. \quad (7.3)$$

In (7.2) the quantity $w_\ell(E \rightarrow g)$ is defined as

⁺ in the following $\int_{E_g}^{E_{g-1}} dE \dots$ is shortened by $\int_g dE \dots$

$$w_{\ell}(E \rightarrow g) = \int_g dE' w_{\ell}(E, E'), \quad (7.4)$$

where

$$w_{\ell}(E, E') = \begin{cases} \frac{d}{dE'} \int_{-1}^{\mu_0(E, E')} \mu_0(E, E') d\mu_0 \cdot 2\pi w(E, \mu_0) P_{\ell}(\mu_0) & \text{if } E' \leq E \leq E'/\alpha \\ 0 & \text{otherwise} \end{cases} \quad (7.5)$$

with $\alpha = \left(\frac{A-1}{A+1}\right)^2$, A = atomic weight of the scattering nucleus in neutron mass units.

$P_{\ell}(\mu_0)$ is the Legendre-polynomial of degree ℓ , $P_0(\mu_0) = 1$, $P_1(\mu_0) = \mu_0$ etc., and $\mu_0(E, E')$ is the scattering cosine in the laboratory system for elastic scattering from energy E to energy E' :

$$\mu_0(E, E') = \frac{A+1}{2} \sqrt{E'/E} - \frac{A-1}{2} \sqrt{E/E'}. \quad (7.6)$$

Further $w(E, \mu_0)$ is the angular distribution for elastic neutron scattering in the laboratory system, related to $\bar{w}(E, \bar{\mu}_0)$ through

$$w(E, \mu_0) = \bar{w}(E, \bar{\mu}_0) \frac{d\bar{\mu}_0(\mu_0)}{d\mu_0}, \quad (7.7)$$

where

$$\bar{\mu}_0(\mu_0) = \frac{1}{A}(\mu_0^2 - 1 + \mu_0 \sqrt{\mu_0^2 - 1 + A^2})$$

The quantity $w_0(E \rightarrow g)$ gives the probability for elastic scattering from energy E into the interval (E_g, E_{g-1}) , the energy group g .

For computation the righthand side of the defining equation (7.4) which involves a double-integration as it stands can easily be simplified.

In the case of isotropy in the s.m.-system we have $\bar{w}(E, \bar{\mu}_0) = 1/4\pi = \text{const.}$ and therefore according to (7.5) and (7.7)

$$w_\ell(E \rightarrow g) = \frac{1}{2} \frac{\hat{\mu}_0(E, E_{g-1})}{\hat{\mu}_0(E, E_g)} \int_{\hat{\mu}_0(E, E_g)}^{\hat{\mu}_0(E, E_{g-1})} d\mu_0 \frac{d\bar{\mu}_0(\mu_0)}{d\mu_0} P_\ell(\mu_0), \quad (7.8)$$

where

$$\hat{\mu}_0(E, E_g) = \begin{cases} -1 & \text{if } E \geq E_g/\alpha \text{ and } E_g > \hat{E} \\ +1 & \text{if } E \leq E_g \text{ and } E_g > \hat{E} \\ \mu_0(E, E_g) & \text{if } E_g < E < E_g/\alpha \text{ and } E_g > \hat{E} \\ -1 & \text{if } E_g = \hat{E} \end{cases} \quad (7.9)$$

Here \hat{E} is the lower limit of the considered energy region, usually $\hat{E}=0.001$ eV. (In the subroutine LECAL $\hat{E} = \text{ABN}(\text{IM}+1)$). With (7.9) scattering to energies below \hat{E} is avoided, in particular: there is no scattering out of the lowest group.

In the case of anisotropy in the c.m.-system, normally for energies above 10 keV, we have

$$w_\ell(E \rightarrow g) = 2\pi \frac{\hat{\mu}_0(E, E_{g-1})}{\hat{\mu}_0(E, E_g)} \int_{\hat{\mu}_0(E, E_g)}^{\hat{\mu}_0(E, E_{g-1})} d\mu_0 w(E, \mu_0) P_\ell(\mu_0) \quad (7.10)$$

7.2 Integration, interpolation, energy and cosine grid, weighting

The multigroup constants to be determined according to (7.1), (7.1') and (7.2) contain integrals over products of cross sections and weighting functions, these two factors generally behaving differently and being given at different grids of energy points. Additionally, in (7.2) the elastic cross section is multiplied by the transfer "probabilities", $w_\ell(E \rightarrow g)$, which are angular integrals over the product of angular distributions and the Legendre-

polynomials according to (7.8) and (7.10). Especially these $w_{\ell}(E \rightarrow g)$ are strongly fluctuating functions, a fact that requires great care during integration.

The techniques of integration, interpolation, and the choice of meshpoints applied in this module result from a comparison of the results of the totally numerical procedure with the analytical ones in special cases as well as from a comparison of different numerical methods. So

- angular integration is performed with Simpson's rule,
- energy integration is done with a modified trapezoidal rule because of the varying density of discrete cross section energies and the need for a fine mesh in the outgroup scattering region (defined below),
- interpolation of the elastic (SGN) and total cross sections (SGT) and the mean scattering cosines (MUEL) is linear, energy and angle interpolation of the elastic scattering distributions (SGNC) is performed with polynomials up the third order - a detailed description of this non-linear interpolation procedure is given in ref. 1, p. 140.

In particular, in the angular integrals (7.8) and (7.10) there is partial cancellation since the Legendre-polynomial $P_{\ell}(\mu_0)$ has ℓ zeros in $[-1, +1]$ and therefore the integrand changes sign. This effect of cancellation increases with ℓ , but can be overcome by a cosine grid with a number of meshpoints increasing with ℓ .

For the computation of the integral (7.10) - anisotropy in the c.m.-system - table 7.2 gives the number NST(L) of cosine meshpoints for the L-th moment in $[-1, +1]$.

Table 7.2: Number of cosine meshpoints in $[-1, +1]$
(scattering anisotropic)

L	0	1	2	3	4	5
NST(L)	81	81	161	161	321	321

The integration according to (7.10) is performed by LEGANS.

The integral (7.8) - isotropy in the c.m.-system - does not depend on energy. The values

$$B_{\ell}(\omega) = \frac{1}{2} \int_{-1}^{\omega} d\mu_0 \frac{d\bar{\mu}_0(\mu_0)}{d\mu_0} P_{\ell}(\mu_0) \quad (7.11)$$

$$\ell = 0, 1, \dots, 5$$

with $\bar{\mu}_0(\mu_0)$ from (7.7) need be calculated only once for all groups in the region of isotropic scattering. So we can afford to determine the $B_{\ell}(\omega)$ at 321 ω -points in $[-1, +1]$. The integration is done analytically with suitable different approximations for $A = 1$, $1 < A \leq 30$, and $A > 30$.

The $w_{\ell}(E \rightarrow g)$ according to (7.8) are calculated by LEGIST by interpolating in the table of the $B_{\ell}(\omega)$ which are determined with LEGINT.

In concern with energy integrations the choice of the energy grid is strongly influenced by the oscillatory behaviour of the transfer probabilities $w_{\ell}(E \rightarrow g)$ which is qualitatively shown in fig. 7.1 for $\ell = 5$.

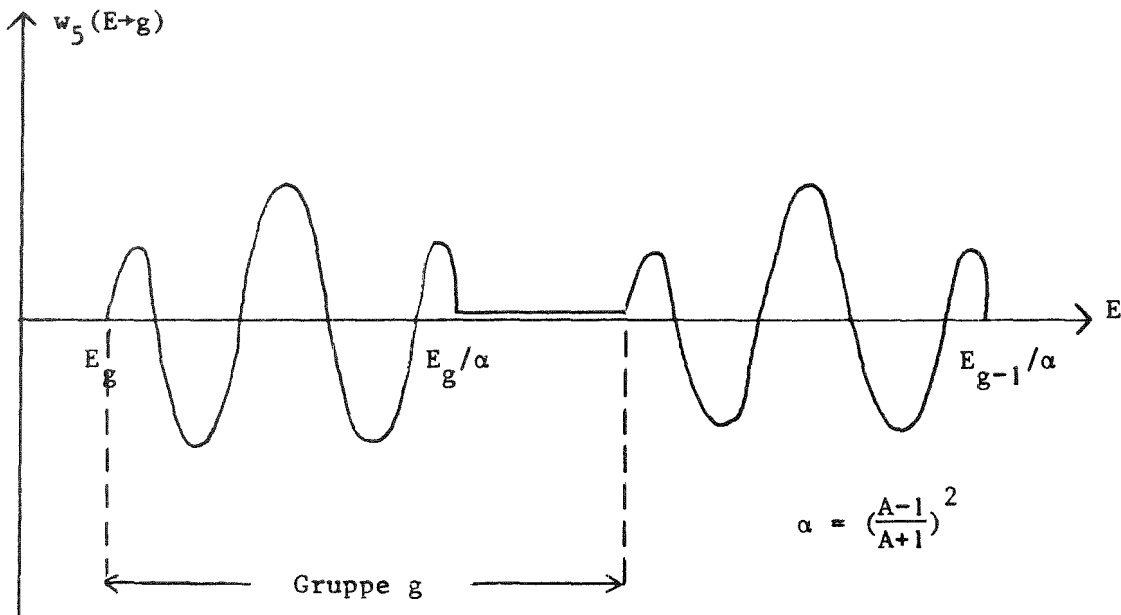


Fig. 7.1: Behaviour of the $w_{\ell}(E \rightarrow g)$ for $\ell = 5$

Thus the energy integrals that require the finest energy mesh are the numerator in (7.2), namely

$$\int_{g'} dE \sigma(E) w_{\ell}(E \rightarrow g) \psi_{\ell}(E) \quad (7.12)$$

The interval $[\bar{E}_g, E_g/\alpha]$ from which scattering to energies $E < E_g$ is possible is called outgroup scattering region; if $E_g/\alpha < E_{g-1}$, the interval $[\bar{E}_g/\alpha, E_{g-1}]$ from which scattering occurs only to energies $E \geq E_g$ within group g is called ingroup scattering region.

In the outgroup scattering region $w_{\ell}(E \rightarrow g)$ may change its sign several times due to the zeros of the Legendre-polynomials in (7.5). To describe this behaviour properly we need a sufficiently fine energy grid (independent of α). In the ingroup scattering region there is only a weak dependence on energy so that a coarse mesh will do.

Comparisons with analytical cases show that for $\ell \leq 5$ and for a group lethargy $\ln(E_{g-1}/E_g) = \Delta u_g \leq 0.7$ an appropriate choice is $NK = 70$ and $NR = 16$ where $NK(NR)$ is the number of discrete energies in the outgroup (ingroup) scattering region used for the representation of the $w_{\ell}(E \rightarrow g)$; other values can be specified by input.

NR should be large enough to guarantee a sufficiently accurate representation of an analytically given macroweighting spectrum (see below) if there are only a few discrete SGN-energies.

The whole group g is an outgroup scattering region if $E_g/\alpha \geq E_{g-1}$; in this case $NK \cdot \ln(E_{g-1}/E_g) / \ln(1/\alpha)$ - instead of NK in the first version of this module - discrete energy points are assigned to the group. In case of hydrogen 100 energy points per energy decade are taken.

These discrete energies are called basic points; they are determined in PUNK. Together with the discrete SGNC-energies found on KEDAK they form the coarse energy grid corresponding to which the $w_{\ell}(E \rightarrow g)$ we calculated in LECAL.

In GRUPIN the coarse grid, the SGN-energies and, if given, the energy points of the macroweighting spectrum are joined by means of PUSUM to form the fine energy grid. Linear interpolation of the $w_{\ell}(E \rightarrow g)$ and the elastic cross

sections $\sigma(E)$ to the fine grid yields a pointwise representation of the transfer cross sections $\sigma_{\ell}(E \rightarrow g) = \sigma(E) \cdot w_{\ell}(E \rightarrow g)$ which contains on one hand the information available from KEDAK and on the other hand the oscillatory behaviour of the $\sigma_{\ell}(E \rightarrow g)$ in the outgroup scattering region. For the representation of $\sigma_{\ell}(E)$ in (7.10) the energy points of SGT found on KEDAK are used.

For the final integration, which is performed groupwise in SPRAL, in case of a fine-structure weighting with $1/\Sigma_t^{\ell+1}$ the energy points of the macroscopic total cross section $\Sigma_t(E)$ - the sum of the energy points of the constituent σ_{ℓ} 's - are added to the fine grid, and the $\sigma_{\ell}(E \rightarrow g)$ are interpolated linearly to the resulting grid. In case of a mere macroweighting the fine grid is used.

The modified trapezoid integration procedure in SPRAL was developed from the usual trapezoid rule which treats the integrand as a whole linearly between to neighbouring points. The procedure applied here merely requires a linear behaviour of the components of the integrand. That this is a less severe restriction is clear from the fact that the product of two linear functions does not show a linear but a quadratic behaviour. For a detailed description see ref. /1/, p. 136.

The weighting function $\psi_{\ell}(E)$ is approximated by the product of a macro- and a micro-spectrum, representing the slowly varying collision density and the possibly strongly fluctuating fine-structure of the neutron flux density, respectively.

The possible weighting options are listed in the table 7.3.

Table 7.3: The fine-weighting options of module 6

Opt.	Macro-spectrum	Micro-spectrum	MW	NSPEC
1	$1/E$	1	-	-
2	$1/E$	$[1/\Sigma_t(E)]^{\ell+1}$	2	-
3	$F_o(E)$	1	-	1
4	$F_o(E)$	$[1/\Sigma_t(E)]^{\ell+1}$	2	1
5	$F_{\ell}(E)$	1	1	$\ell+1$

MW and NSPEC are the corresponding input parameters.

7.3 The routines of this module: purpose and a description of the argument lists and the commons

Subroutine:	Purpose:
FLUMMI	main control program
SUM	summation
IPØLA	interpolation with polynomials up to degree 3
PUSUM	joining of point sets
MAKRØ	construction of a macro-group structure dependent on given density of data points
MIXSGT, ADD	calculation of the total macroscopic cross section for fine-structure weighting
TRAFØ	transformation of angular distributions
INFØRM	printing of additional information
PUNK	generation of the basic energy grid
(NDF)	reading of KEDAK
LØØKO	reading of ISØT1 (atomic weight) using NDF
LØØK1	reading of SGN, MUEL, SGT using NDF
LØØK2	reading of SGNC using NDF
LØØK3	reading of SGNC-energies using NDF
LECAL	control of the calculation of the $w_g(E \rightarrow g)$ according to (7.8) and (7.10)
LEGPØL	calculation of pointwise Legendre polynomials
LEGINT	calculation of Legendre integrals according to (7.11)
G(FUNCTIØN)	$G(N, X, Y) = (X^N - Y^N) / (X - Y)$
LEGIST	calculation of partial Legendre coefficients according to (7.8)
LEGANS	calculation of partial Legendre coefficients according to (7.10)
GRUPIN	preparing of weighted energy integration
IPØLIN	linear interpolation
SPRAL	weighted energy integration
PHI(FUNCTIØN)	$PHI(E) = 1/E$
MUKØN	final determination of group constants according to (7.1), (7.1'), (7.2), (7.3)
PRINT	printing and reserving of final results

In the following a description of the argument lists and the commons of the subroutines is given. Under the heading "Arguments" those quantities are found which must be defined before computation will start. Under the heading "Results" those quantities are listed which are calculated by the routine.

SUBROUTINE FLUMMI (A,B,EA,EB,E,EN,SGN,ECØ,SCØ,V,W,F,AR,FU,ABN,INT,
GR,FEKØE,EG,R,RSP,ESP,SPEK,SGNC,FEKØ,ELSIG,ELTØT,
ET,ST,MAT,DAT,NLA,NLE,ISEL,NMAX,NX,NE27,NSPEK,
LSPEK,MAZ,NTK,KT,NTTT,NTTP,ICØS,ICØSP,NECU,NECUP,
ISM,ISMP,ISØ,ISØP,ISCØ,ISCØP,ISEC,ISECP,KIM,NS,
NK,NR,GE,SØ,SGTØT)

COMMON STØFF,ISTRUK,ISPA,NØUT,KPR,IM,IL,KL

Purpose: - Construction of macro-groups by means of MAKRØ;
 - calculation of unnormalized scattering matrices
 for each macro-group by means of LECAL and
 GRUPIN,
 - calculation of normalized scattering matrices etc.
 by means of MUKØN,
 - printing and reserving of results with PRINT

Arguments:

NX number of energy group boundaries (input or standard)
EG(NX) energy group boundaries (increasing) (input or
 standard)
NE27 NX + 1

Comment: the group boundaries will be modified and
rearranged in the following manner:

ABN(I) = EG(NX - I+1), I = 1,2,...,NX,
if ABN(NX) $\left\{ \begin{array}{l} > 10^{-3} : \text{NEGR} = \text{NE27}, \text{ABN}(\text{NEGR}) = 10^{-3} \text{ eV} \\ = 10^{-3} : \text{NEGR} = \text{NX} \\ < 10^{-3} : \text{ERRØR } 6.8 \end{array} \right.$

NGR = NEGR-1

NGR number of energy groups
NEGR number of group boundaries

ABN(NEGR) group boundaries (decreasing)

IL,IM indices of the first and last energy
group for which scattering matrices etc.
shall be calculated (input)

NMAX highest Legendre order which can be treated
(NMAX = 5 in this version)

NLA first Legendre moment to be calculated
(input or standard, but finally NLA = 0 always)

NLE last Legendre moment to be calculated (input
or standard)

NSPEK macro-weighting spectrum control parameter
(= 1: spectrum from FUNCTIØN PHI
> 1: NSPEK = number of discrete energies of the
macro-weighting spectrum)

LSPEK number of values of the macro-weighting spectrum
if NSPEK > 1, = 1 otherwise

ESP(NSPEK) discrete energies of the macro-weighting spectrum
if NSPEK > 1, no meaning otherwise (input)

SPEK(LSPEK) values of the macro-weighting spectrum (the first
NSPEK values for the 0. moment, the second NSPEK
values for the 1. moment etc. if MAZ(1) = 1,
the first NSPEK values - there will be no more in
this case - for all moments if MAZ(1) = 0)

NTK micro-weighting spectrum pointer (= 1: the fine-
structure mixture from which the micro-weighting
spectrum is to be calculated is given in the
arrays MAT and DAT; = 0: no fine-structure weighting)

KT number of different nuclei in the fine-structure
mixture (input), if NTK = 1; = 1 otherwise

MAT(KT) nuclei in KEDAK notation in the fine-structure
mixture (input)

DAT(KT) densities in particles per ccm times 10^{-24} of the
nuclei in the fine-structure mixture (input)

NTTT estimated number of discrete energies of the micro-
spectrum

MAZ(2) pointers for the weighting of the higher moments
(see SPRAL: MZ)

ISM estimated number of energy meshpoints of the coarse
mesh per macro-group

ISD estimated number of energy meshpoints of the fine
mesh per macro-group

ICØS number of angular meshpoints of the angular
 distributions (SGNC) on KEDAK

NECU scattering width

ISCØ Max (NECU·ISD, ISM·ICØS)

ISEC Max (ISD, ISM·NECU)

NS maximum number of energy groups per macro-group
 (input or standard)

NK number of basic points in the outgroup scattering
 region per group (input or standard)

NR number of basic points in the ingroup scattering
 region per group (input or standard)

STØFF nucleus in KEDAK notation for which scattering matrices
 etc. shall be calculated

NØUT printed-output unit (usually NØUT=6)

KPR unit on which the final results are stored

ISEL pointer for additional output (input or standard)

KL MIGRØS counting index

Auxiliary arrays:

A(ISM),B(ISM),EA(ISM),EB(ISM),E(ISM),EN(ISD),SGN(ISD),ECØ(ISD),SCØ(ISD),
V(ISD),W(ISD),F(ISD),AR(ICØS),FU(ICØS),ABN(NE27),INT(NE27),GR(NE27),
FEKØE(NE27),R(NX),RSP(6,NX),SGNC(ICØS,ISM),FEKØ(ISM,NECU),ELSIG(6,NECU,NX),
ELTØT(2,NX),ET(NTTT),ST(NTTT),GE(ISD),SG(ISD),SGTØT(6,NX)

Results:

NTTP increment of NTTT if NTTT is found to be for small
 during execution

ICØSP increment of ICØS if ICØS is found to be too small
 during execution

NECUP }
ISMP }
ISDP } analogous
ISCØP }
ISECP }

KIM downward extension in groups of the energy region to be calculated in order to treat outscattering in the low energy groups correctly

SUBROUTINE SUN(M,A,S)

Purpose: Summation of real numbers different in sign and magnitude with minimization of rounding errors

Arguments:

M number of summands

A(M) summands

Results:

S $\sum_{I=1}^M A(I)$

SUBROUTINE IPOLA(M,A,B,N,X,Y,T)

Purpose: Interpolation with polynomials up to degree three (for details see ref. 1, p. 140)

Arguments:

M number of given points

A(M) given abszissae

B(M) given ordinates

N number of the given new abszissae

X(N) given new abszissae with $X(1) = A(1)$, $X(N) = A(M)$, $X(I-1) < X(I)$, $I = 2, N$

Auxiliary array:

I(M)

Results:

Y(N) new ordinates corresponding with the given new abszissae

SUBROUTINE PUSUM (ISD,KA,A,KE,E,B)

Purpose: Joining of point sets

Arguments:

KA number of elements in the array A

A(KA) first point set (increasing)

KE number of elements in the array E

E(KE) second point set (increasing)

Auxiliary array:

B(KE)

Results:

KE number of different points in A and E

E(KE) different points in A and the given E (increasing)

SUBROUTINE MAKRO (ALFA,ALLN,ISO,IL,IM,NGR,ABN,R,ISD,ISM,ISDP,NS,NK,NR,
NEN,NECU,NUEB,V,W,F,LST,INTT,INT,NEGR,KSPE,NSPEK,ESP,
NTK,KT,MAT,NTTT,NTTP,NF,ISEL,ISGT)

COMMON STOFF,ISTRUK,ISPA,NOUT

Purpose: A macro-group is defined as an energy region consisting of one group or several connected groups. MAKRO subdivides the given energy region (ABN(IM + 1), ABN(IL)) into macro-groups meeting the following conditions:

each macro-group contains

- a) as many groups as possible
- b) NS groups at most
- c) ISD - ISM SGN-meshpoints at most
- d) either groups with only isotropic outscattering in the c.m.-system or groups with only anisotropic outscattering in the c.m.-system

Arguments:

ALFA $((A-1)/(A+1))^2$ where A is the atomic weight of the scattering nucleus in neutron mass units

ALLN ln ALFA

IL,IM	indices of the first and last group for which scattering matrices shall be calculated
ISØ	index of the first group with only isotropic outscattering in the c.m.-system
NUEB	scattering width
NS	maximum number of groups per macro-group
NK	number of basic points in the outgroup scattering region per group, reduced if NUEB > 2
NR	number of basic points in the ingroup scattering region
NEN	total number of SGNC-energies
NGR	number of energy groups
NEGR	number of energy group boundaries
ABN(NEGR)	energy group boundaries
R(NGR)	group lethargy widths
NECU	maximum scattering width
ISM	maximum number of basic points plus discrete SGNC-energies per macro-group
ISD	ISM plus maximum number of discrete SGN-energies per macro-group
KSPE	pointer for macro-weighting (=0: 1/E-weighting, = 1: weighting with a spectrum given pointwise)
NSPEK	number of energy points of the macro-spectrum if KSPE = 1, = 1 otherwise
ESP(NSPEK)	energy points of the macro-spectrum
NTK	pointer for micro-weighting (= 0: No micro-weighting with $1/\Sigma_t^{k+1}$)
KT	number of materials for micro-weighting if NTK = 1; = 1 if NTK = 0
MAT(KT)	materials for micro-weighting if NTK = 1; no meaning if NTK = 0
NTTT	maximum number (estimated) of energy points per group for micro-weighting
NF	unit for temporary storage purposes
ISEL	pointer for additional output

STØFF nucleus in KEDAK notation for which scattering matrices
 etc. shall be calculated

NØUT printed-output unit

Auxiliary arrays:

V(ISD), W(ISD), LST(2, NGR), F(ISD)

Results:

INTT number of macro-group boundaries

INT(INTT) macro-group boundaries given by group indices

ISDP increment of ISD if ISD is found to be too small
 during execution

NTPP increment of NTPP if NTPP is found to be too small
 during execution

ISGT interrupt indicator (= 0: no interrupt;
 = 1: an interrupt with printing of an error message
 has occurred)

comment: the determined macro-groups are as follows:

- 1. macro-group: $\boxed{ABN(INT(2)+1), ABN(IN(1))}$
- I-th macro-group: $\boxed{ABN(INT(I+1)+1), ABN(INT(I)+1)}$
- I = 2,3,...,INTT-1

SUBROUTINE MIXSGT(KT,MAT,DAT,NTT,NTP,NT,ET,ST,EA,EE,ISGT)

COMMON STØFF, ISTRUK, ISPA, NØUT

Purpose: Calculation of the total macroscopic cross section
 of a given mixture according to

$$\Sigma_t(E) = \sum_{I=1}^{KT} d_I \cdot \sigma_{t,I}(E)$$

where d_I = density in nuclei per ccm times 10^{-24}
of the I-th nucleus in the mixture and $\sigma_{t,I}$ =
total microscopic cross section of the I-th nucleus
in the mixture; KT see below. E stands for the joint
set of discrete energies for which for at least one
nucleus in the mixture a σ_t is found on KEDAK.

D density of the K-th nucleus
 E, EV energy points of the polygonal to be added
 S, SV microscopic total cross sections at E and EV
 EW ET(NU) before the last modification
 SW ST(NU) before the last modification

Results:

NT number of discrete energies of the mixture up to E
 ET(NT) discrete energies up to E
 ST(NT) total macroscopic cross sections up to E
 NU index of the highest energy up to which the K-th nucleus has been taken into account
 NTP see MIXSGT

Definition of $P(E|ET,ST)$ and $P_{I,J}(E|ET,ST)$:

Be

$$P(E|ET,ST) = P(E|ET(1), ET(2), \dots, ET(NT); ST(1), ST(2), \dots, ST(NT))$$

$$= \begin{cases} 0 & \text{if } E < ET(1) \text{ or } E > ET(NT) \\ ST(J) & \text{if } E = ET(J) \\ ST(j-1) + \frac{ST(J) - ST(J-1)}{ET(J) - ET(J-1)} (E - ET(J-1)) & \text{if } ET(J-1) < E < ET(J) \end{cases}$$

provided $ET(1) < ET(2) < \dots < ET(NT)$.

Be now

$$P_{I,J}(E|ET,ST) = \sum_{K=1}^{I-1} P_{K,NT_K}(E|ET,ST)$$

$$+ P(E|ET_I(1), ET_I(2), \dots, ET_I(J);$$

$$ST_I(1), ST_I(2), \dots, ST_I(J))$$

where the $ET_I(K)$ are the discrete σ_t -energies of the I-th nucleus and the $ST_I(K)$ are the corresponding macroscopic cross sections.

SUBROUTINE TRAFØ(IC,NE,ISM,S,XM,AL,A)

Purpose: Transformation of angular distributions for elastic neutron scattering from the c.m.-system into the laboratory system according to equ. (7.7)

Arguments:

IC number of uniformly spaced cosine meshpoints of the angular distributions in the c.m.-system

NE number of angular distributions undergoing transformation

ISM maximum number of angular distributions

S(IC,NE) angular distributions in the c.m.-system

A(IC) uniformly spaced cosine meshpoints of the angular distributions in the c.m.-system with $A(1) = -1$, $A(IC) = 1$

AL ALFA (see MAKRØ)

Results:

A(IC) cosine meshpoints in the laboratory system

S(IC,NE) angular distributions in the laboratory system

SUBROUTINE INFØRM(ALFA,NEGR,ABN,R,IL,IM,INTT,INT,NST,NSTIS,IR,ISTT,K,NTK,NTT,NØUT)

Purpose: Printing of additional information if ISEL < 0

Arguments:

ALFA,NEGR,ABN,
IL,IM,INTT,INT,
NØUT } see MAKRØ

R(NEGR-1) group lethargy widths

NST(6),NSTIS see LECAL

IR macro-group index

ISTT number of energy meshpoints in the fine-mesh in the IR-th macro-group

K number of discrete SGN-energies in the IR-th
macro-group

NTK pointer for micro-weighting

NTT number of discrete energies of the micro-weighting
spectrum in the IR-th macro-group if $NTK \neq 0$

SUBROUTINE PUNK(NGR,NEGR,ABN,NA,NE,NEN,ALFA,NK,NR,ISM,ISMP,ISN,E,R,ALLN)

Purpose: Generation of the basic energy grid uniformly spaced
in lethargy

Arguments:

NGR number of energy groups

NEGR number of energy group boundaries

ABN(NEGR) group boundaries

NA,NE first and last group in the considered macro-group

NEN number of angular distributions in the considered
macro-group

ALFA,ALLN see MAKRO

NK number of basic points in the outgroup scattering
region

NR maximum number of basic points in the ingroup scattering
region; is reduced if the whole group is ingroup sent.reg.

ISM maximum number of basic points plus discrete SGNC-energies
per macro-group

R(NGR) group lethargy widths

Results:

ISN calculated number of basic points in the macro-group
defined through NA,NE

E(ISN) calculated basic points in this macro-group

ISMP increment of ISM if ISM is too small

SUBROUTINE L00KO(XMAT,MASSE,C0M,x)

COMMON ST0FF, ISTRUK, ISPA, N0UT

Purpose: Reading the atomic weight from KEDAK and relating it to the neutron mass as mass unit, calculation of the mass number and of the mean scattering cosine in the laboratory system for isotropic scattering in the c.m.-system

Arguments:

ST0FF nucleus in KEDAK notation

Results:

XMAT atomic weight of the nucleus in ST0FF in neutron mass units

MASSE mass number

C0M $\frac{2}{3 \cdot XMAT}$

Remark: L00KO calls the Entry NDFL0C of the KEDAK routine NDF

SUBROUTINE L00KI(ISD,K,E,SGN,E0,EE,NT,ISGT)

COMMON ST0FF, ISTRUK, ISPA, N0UT

Purpose: Reading of SGN, MUEL and SGT from KEDAK

Arguments:

ST0FF nucleus in KEDAK notation for which data shall be read from KEDAK

ISD maximum number of data which may be read with a single call

E0, EE lower and upper boundary of the energy region for which data shall be read

NT data-type pointer (NT = 1: SGN are read; NT = 2: MUEL are read; NT = 3: SGT are read)

N0UT printed-output unit

Results:

K number of data (SGN, MUEL or SGT) in $[E_0, E_1]$.
E(K) discrete energies at which data are given
SGN(K) data read from KEDAK (SGN, MUEL or SGT)
ISGT interrupt indicator (see MAKRO)

Remarks: The conditions $E(1) = E_0$ and $E(K) = E_1$ are met by
linear interpolation or constant extrapolation.
L00K1 calls the Entries NDFLOC and NDFNXT of the
KEDAK routine NDF.

SUBROUTINE L00K2(NEN,EA,IC0S,IC0SP,ISM,AR,SGNC)

COMMON STOFF, ISTRUK, ISPA, NOUT

Purpose: Reading of SGNC from KEDAK

Arguments:

STOFF nucleus in KEDAK notation
NEN number of discrete energies at which SGNC are given
EA(NEN) discrete energies for which SGNC shall be read (they
have been read before with L00K3)
IC0S maximum number of SGNC cosine meshpoints
ISM maximum number of discrete SGNC-energies
NOUT printed-output unit

Results:

IC0SP increment of IC0S if IC0S has found to be too small
during reading SGNC from KEDAK
AR(IC0S) SGNC cosine meshpoints from KEDAK
SGNC(IC0S,NEN) SGNC from KEDAK corresponding to the cosine mesh AR
and the energy mesh EA

Remarks: The cosine mesh must be the same for all energies.
L00K2 calls the entries NDFLOC and NDFNCT of the KEDAK
routine NDF.

SUBROUTINE L00K3(NE,EA,IS0,NGR,ABN,ISM,ISMP,LST,NEGR,ISEL,ISGNC)

COMMON ST0FF, ISTRUK, ISPA, N0UT

Purpose: Reading from KEDAK the entire SGNC-energy mesh for one nucleus

Arguments:

ST0FF, ISM, N0UT see L00K2

NGR, NEGR, ABN see MAKR0

Results:

ISEL pointer for additional output

ISMP estimated increment of ISM if there are more than ISM angular distributions on KEDAK for the considered nucleus

NE number of angular distributions on KEDAK for the nucleus in question

EA(NE) SGNC-energy mesh on KEDAK for the considered nucleus

LST(NGR) LST(I) = number of energies EA(N) with
ABN(I+1) ≤ EA(N) < ABN(I)

IS0 see MAKR0

ISGNC interrupt indicator (compare ISGT in MAKR0)

Remark: L00K3 calls the Entry NDFL0C of the KEDAK routine NDF

SUBROUTINE LECAL(MASSE, XMAT, ALFA, IS0T, LEG, NLE, NANF, NEND, NUEB, IL, IM,
NEGR, ABN, IC0S, AR, ISN, E, SGNC, NST, NSTIS, ISM, ISD, NECU,
ITA, NF, GR, FEK0E, FU, EW, A, H, V, W, F, FEK0)

Purpose: Control of the calculation of the $w_{\lambda}(E \rightarrow g)$ according to equations (7.8) and (7.10)

Arguments:

MASSE atomic mass number of the scattering nucleus

XMAT atomic weight of the scattering nucleus in neutron mass units

ALFA $((XMAT-1)/(XMAT+1))^2$

ISØT anisotropy pointer
(ISØT=1: the considered macro-group is within the energy region of anisotropic scattering in the c.m.-system, ISØT = 0 otherwise)

LEG(6) sequence of calculated moments

NLE upper Legendre index (input)

NANF,NEND indices of the first and the last group in the macro-group for which scattering matrices etc. shall be calculated

NUEB scattering width

IL,IM indices of the first and the last group for which scattering matrices etc. shall be calculated

NEGR number of energy group boundaries

ABN(NEGR) energy group boundaries

ICØS number of cosine meshpoints of the SGNC on KEDAK

AR(ICØS) cosine meshpoints of the SGNC on KEDAK

ISM number of basic points plus discrete SGNC-energies in the macro-group to be calculated

E(ISN) basic points plus discrete SGNC-energies in the macro-group to be calculated (coarse mesh)

SGNC(ICØS,ISM) angular distributions in the laboratory system

NST(6) moment-dependent number of uniformly spaced cosine meshpoints for μ_0 -integration when ISØT = 1

NSTIS moment-independent number of uniformly spaced cosine meshpoints for μ_0 -integration when ISØT = 0

ISM maximum number of basic points and discrete SGNC-energies per macro-group

ISD ISM plus maximum number of discrete SGN-energies per macro-group

NECU maximum scattering width

ITA pointer for the calculation of Legendre integrals by means of LEGINT
(ITA = 0: Legendre integrals are calculated,
ITA = 1: Legendre integrals have already been calculated)

NF unit on which the $w_l(E \rightarrow g)$ are stored temporarily

Auxiliary arrays:

GR(NEGR), FEKØE(NEGR), FU(ICØS), EW(ISM), A(ISD), H(ISD), V(ISD),
W(ISD), F(ISD), FEKØ(ISM,NECU)

Results: $w_l(E \rightarrow g)$ on unit NF

SUBRØUTINE LEGPØL(NST,A,N,NSTIS)

CØMMØN /INTEG/ X, F, D

Purpose: Calculation of pointwise Legendre polynomials

Arguments:

NST number of uniformly spaced cosine meshpoints
N order up to which Legendre polynomials shall be calculated
NSTIS number of uniformly spaced cosine meshpoints if ISØT = 0 (here: maximum length of A)

Results:

A(NST) uniformly spaced cosine meshpoints
X(NST) uniformly spaced cosine meshpoints (double precision)
F(NST,N+1) Legendre polynomials pointwise
 $F(L,I) = P_{L-1}(A(I))$
D spacing of the A(I):
 $D = A(I) - A(I-1), I = 2, NST$

SUBRØUTINE LEGINT(N,NAK,XMAT,ITA)

CØMMØN /INTEG/ H, GRAL, D

Purpose: Calculation of Legendre integrals

$$B_n(\omega) = \frac{1}{2A} \int_{-1}^{\omega} d\mu_0 \frac{(\mu_0 + \sqrt{\mu_0^2 - 1 + A^2})^2}{\sqrt{\mu_0^2 - 1 + A^2}} P_n(\mu_0)$$

$n = 0, 1, \dots, 5$

Arguments:

N upper Legendre index (is ignored; the $B_n(w)$ are always determined for $N = 0, 1, 2, 3, 4, 5$)

NAK number of cosine meshpoints

XMAT atomic weight in neutron mass units

Results:

H(NAK) uniformly spaced cosine mesh-points, $H(1) = -1$,
 $H(NAK) = 1$

D spacing of the H(I)

GRAL(6,NAK) $GRAL(L,I) = 2 \cdot B_{L-1}(H(I))$

ITA pointer (ITA = 1 after calculation)

Remarks: For $A = 1$, $1 < A \leq 30$, $A > 30$ the above integral is treated numerically in different ways.

FUNCTION G(N, X, Y)

$$G(N, X, Y) = \frac{X^N - Y^N}{X - Y}$$

is determined according to

$$\frac{X^N - Y^N}{X - Y} = D^{N-1} + \binom{N}{1} D^{N-2} Y + \binom{N}{2} D^{N-3} Y^2 + \dots + \binom{N}{N-1} Y^{N-1}$$

where

$$D = X - Y$$

SUBROUTINE LEGIST(L,NST,IA,IB,NEGR,GR,E)

COMMON /INTEG/ X, GRAL, D

Purpose: Calculation of partial Legendre coefficients when scattering is isotropic in the c.m.-system according to equ. (7.8)-multiplication with 2π is performed in LECAL:

$$E(I) = \frac{1}{4\pi} \frac{GR(I)}{GR(I+1)} \int_{-1}^1 d\mu_o \frac{d\bar{\mu}_o}{d\mu_o} P_{L-1}(\mu_o)$$

using the previously in LEGINT determined integrals

$$GRAL(L,I) = 2 \int_{-1}^{X(I)} d\mu_o \frac{d\bar{\mu}_o}{d\mu_o} P_{L-1}(\mu_o)$$

Arguments:

L Legendre degree plus 1
 NST number of uniformly spaced cosine meshpoints
 X(NST) cosine mesh from LEGINT
 D spacing of the X(I)
 GRAL(6,NST) see above
 NEGR length of array E
 IA,IB boundary indices within which the E(I) shall be determined
 (GR(I),I=IA,IB) cosine integration boundaries

Results:

E(NEGR) (E(I), I=IA,IB-1) = partial Legendre coefficients (see above)
 E(NEGR) = total Legendre coefficient

$$= \sum_{I=IA}^{IB-1} E(I)$$

SUBROUTINE LEGANS (L,NST,F,IA,IB,NEGR,GR,E,POLY,A)

COMMON /INTEG/ X,POL,D

Purpose: Calculation of partial Legendre coefficients when scattering is anisotropic in the c.m.-system according to equ. (7.10)-multiplication with 2π is performed in LECAL:

$$E(I) = \int_{GR(I)}^{GR(I+1)} d\mu_o w(E,\mu_o) P_{L-1}(\mu_o)$$

Arguments:

L,NST,D,NEGR, see LEGIST
IA,IB,GR

X(NST) cosine mesh from LEGPOL

F(NST) pointwise angular distribution corresponding with the X(I)

POL(6,NST) Legendre polynomials pointwise from LEGPOL corresponding with the X(I)

Auxiliary arrays:

POLY(NST), A(NST)

Results:

E(NEGR) (E(I), I=IA, IB-1) = partial Legendre coefficients (s.above)
E(NEGR) = total Legendre coefficient

$$= \sum_{I=IA}^{IB-1} E(I)$$

SUBROUTINE GRUPIN(MASSE,XMAT,ALFA,COM,ISOT,PM,LEG,NLE,NANF,NEND,NUEB,IL,IM,NGR,NEGR,ABN,ISN,EH,K,H,F,M,G,EN,NTT,ET,ST,MAZ,KSPE,KSPEK,ESP,SPEK,NSPEK,LSPEK,ISM,ISD,NECU,ISCO,ISEC,NF,E,EW,GR,WA;U,V,W,ISTT,RSP,ELSIG,NGT,NGG,EG,SG,SGTOT)

Purpose: Preparing of weighted energy integration

Arguments:

MASSE,XMAT,ALFA, }
ISOT,LEG,NLE,NANF, } see LECAL
NEND,NUEB,IL,IM, }
NEGR,ABN,ISN,ISM, }
ISD,NECU,NF }

COM mean scattering cosine when scattering is isotropic in the c.m.-system = 2/(3·XMAT)

PM fraction of MUEL in the corrected first moment (normally 1.)

NGR number of energy groups

EH(ISN) basic points plus discrete SGNC-energies in the macro-group to be calculated

K number of SGN

H(K) discrete SGN-energies
 F(K) SGN corresponding with the H(I)
 M number of MUEL
 G(M) discrete MUEL-energies
 EN(M) MUEL corresponding with the G(I)
 NTT,ET(NTT),ST(NTT),
 MAZ(2),KSPE,KSPEK,NSPEK,
 LSPEK,ESP(KSPEK),SPEK(KSPEK), } see subroutine SPRAL
 NTT,ET(NTT),ST(NTT),MZ(2),
 KS,NS,NP,NL,E,S } , correspondingly
 NGT pointer for the calculation of ψ_{ℓ} -weighted total group
 cross sections (= 1: calculation, = 0: no calculation)
 NGG number of given total cross section values in the
macro-group considered
 EG(NGG) total cross section energy points
 SG(NGG) total cross sections corresponding to EG
 ISCØ dimension of WA (see below and FLUMMI)
 ISEC dimension of U (see below and FLUMMI)

Auxiliary arrays:

E(ISD), EW(ISM), GR(NEGR), WA(ISCØ), U(ISEC), V(ISD), W(ISD)

Results:

ISTT number of energy meshpoints in the fine energy grid
 consisting of the basic points (from PUNK), the discrete
 SGNC-energies, the discrete SGN- and MUEL-energies
 RSP(6,NGR) energy group integrals of the **w**eighting spectra

$$RSP(L,N) = \int_N dE \psi_{L-1}(E)$$

ELSIG(6,NUEB,NGR) elastic scattering transfer cross sections

$$ELSIG(L,I,N) = \sigma_{L-1}^{N \rightarrow II}$$

$$= \int_N dE \sigma(E) w_{L-1}(E \rightarrow II) \psi_{L-1}(E) / \int_N dE \psi_{L-1}(E)$$

where II = N + I - 1

SGTØT(6,NGR) total group cross sections (if NGT = 1)

$$\text{SGTØT}(L,N) = \sigma_{t,L-1}^N$$

$$= \int_N dE \sigma_t(E) \psi_{L-1}(E) / \int_N dE \psi_{L-1}(E)$$

SUBROUTINE IPØLIN(M,A,B,N,X,Y,HR)

Purpose: Linear interpolation

Arguments:

M number of given points

A(M),B(M) given points

N number of given new abszissae

X(N) given new abszissae where X(1) = A(1), X(N) = A(M)

Auxiliary array:

HR(M)

Results:

Y(N) new ordinates corresponding with the X(I)

SUBROUTINE SPRAL(KS,NS,MZ,E,S,NTT,ET,ST,L,IKK,EN,H,G,VAL,NP,NL,NLE)

Purpose: Calculation of integrals

$$\int_g dE H(E) \psi_\ell(E), \text{ where } H(E) = \begin{cases} \sigma(E)w_\ell(E \rightarrow h) \\ \sigma_t(E) \\ 1 \end{cases}$$

Arguments:

KS pointer for macro-weighting
(= 0 : 1/E-weighting, = 1: weighting with a pointwise spectrum)

NS number of energy points of the macro-weighting spectrum
if KS = 1; = 0 otherwise

MZ(2) pointers for the weighting of the higher moments
(MZ(1) = 0; same macro-weighting for all moments,
= 1: special macro-weighting for each moment;
MZ(2): same as MZ(1) but for micro-weighting

NP field dimension (= NS if KS = 1, = 1 otherwise)

NLE order of the last Legendre-moment to calculated
(1 ≤ NLE ≤ 5)

NL field dimension (= NS if MZ(1) = 0, = NP·(NLE+1) if
MZ(1) = 1)

E(NS) macro-spectrum energy points overlapping group g if
KS = 1, no meaning otherwise

S(NL) macro-spectrum values corresponding to E if KS = 1,
no meaning otherwise

NTT field dimension and pointer for micro-weighting (= 1:
no micro-weighting, > 1: micro-weighting with NTT
energy points)

ET(NTT) energy points for micro-weighting overlapping group g

ST(NTT) total macroscopic cross sections for micro-weighting
corresponding to ET

L Legendre-order for which cross sections shall be
calculated plus 1 (L = ℓ+1)

IKK number of energy points in the fine energy grid

EN(IKK) energy points in the fine energy grid for group g,
boundaries included

H(IKK) values of the function H in the fine energy grid (see
Purpose) corresponding to EN

Auxiliary array:

G(IKK)

Result:

VAL $\int_{\mathcal{E}} dE H(E) \psi_{\ell}(E)$, H see Purpose

Remarks: In case of fine weighting with $1/\Sigma_t^{\ell+1}$ the energy grid for
integration consists of the fine grid and the points at
which the Σ_t 's are given. The behaviour of the cross
sections to be integrated, the macro-weighting spectrum
and the $1/\Sigma_t^{\ell+1}$ -values is assumed to be linear between
adjoining points of this grid.

FUNCTION PHI(E) = 1/E

SUBROUTINE MUKON(ELSIG,ELTOT,NLE,NECU,NUEB,IL,IM,NGR,MASSE)

Purpose: Determination of σ^{NN} , S_L^{NN+II} and $\bar{\mu}^{NN}$ from σ_L^{NN+II} according to (7.1), (7.2) and (7.3):

$$\sigma^{NN} = \sum_{II \geq NN} \sigma_o^{NN+II},$$

$$S_L^{NN+II} = \sigma_L^{NN+II} / \sigma^{NN}, L = 0, 1, \dots, NLE,$$

$$\bar{\mu}^{NN} = \sum_{II \geq NN} S_1^{NN+II}$$

Arguments:

NLE Legendre degree up to which scattering matrices are calculated

NUEB scattering width

IL, IM first and last calculated energy group

ELSIG(6, NUEB, NGR) $ELSIG(L, I, NN) = \sigma_{L-1}^{NN+NN+I-1}$ (see GRUPIN)

where $NN = IL, \dots, IM$

$I = 1, \dots, NUEB$

$L = 1, 2, \dots, NLE+1$

Results:

ELSIG(6, NUEB, NGR) $ELSIG(L, I, NN) = S_{L-1}^{NN+NN+I-1}$ (see above)

ELTOT(2, NGR) $ELTOT(1, NN) = \sigma^{NN}$
 $ELTOT(2, NN) = \bar{\mu}^{NN}$ (see above)

where $NN = IL, \dots, IM$

$I = 1, \dots, NUEB,$

$L = 1, 2, \dots, NLE+1$

Remark:

Comparisons with cases which can be treated analytically (atomic weight $A > 1$) show that the matrixelements $S_{L-1}^{NN+NN+I-1}$ are calculated here with a maximum absolute error

$$\Delta S \approx 4 \cdot 10^{-4}$$

Thus quantities smaller than 10^{-5} in absolute value are ignored and set equal to zero (except for hydrogen)

```
SUBROUTINE PRINT(ELSIG,ELTØT,NLA,NLE,NECU,NUEB,ISEL,NGR,KSPEK,MAZ,NTK,  
KIM,NGT,SGTØT,RSP,MASSE,NGS)
```

```
COMMON STØFF, ISTRUK, ISPA, NØUT, KPR, NEND, NANF
```

Purpose: Printing and reserving of final results

Arguments:

ELSIG,ELTØT see MUKØN results

NGT,RSP,SGTØT, see GRUPIN

NLE,NECU,NUEB, }
NGR } see MUKØN

MAZ,NTK,KIM see FLUMMI

KSPEK corresponds to KSPE in GRUPIN

NLA first Legendre moment to be calculated
(NLA = 0 always)

NANF,NEND indices of the first and last group for which
scattering matrices have been calculated

STØFF nucleus for which scattering matrices have been
calculated

ISEL pointer for additional output

NØUT printed-output unit

KPR unit on which all MIGRØS-results are stored

MASSE mass number of the nucleus in STØFF

NGS index of the first group in which has been put
SGN = SGT = 1 (only for heavy materials in case of
/ISEL/ = 1 (input))

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8. The Calculation of the interval cross sections and the zero'th and higher moments of the normalized elastic transfer elements for the REMO-correction. Module 9.
-

8.1 Basic formulae and notations

- a) The fine interval system for the REMO-Correction //.

The I-th group of the basic broad group system is divided into NFG(I) fine-groups, equidistant in lethargy. Any of these fine groups is divided into NFI(I) fine intervals, equidistant in energy. The fine interval width is denoted by ΔE .

- b) The fine-interval averaged cross-sections are defined by:

$$\langle \sigma \rangle = \frac{\int dE \sigma(E) F(E)}{\int_{\Delta E} dE F(E)} \quad (8.1)$$

The REMO correction procedure requires the total σ_t and the elastic scattering cross-sections σ_e and the averaged cosine which is defined by

$$\langle \mu_e \rangle = \frac{\int dE \mu_e(E) \sigma_e(E) F(E)}{\int_{\Delta E} dE \sigma_e(E) F(E)} \quad (8.2)$$

- c) The elastic scattering transfer probability matrix-elements are defined by

$$\langle {}_l P(E \rightarrow n) \rangle = \frac{\int dE \sigma_e(E) \pi_l(E \rightarrow n) F(E)}{\sum_n \int_{\Delta E} dE \sigma_e(E) \pi_0(E \rightarrow n) F(E)} \quad (8.3)$$

where

$$\pi_l(E \rightarrow n) = \frac{(A+1)^2}{4A} \cdot \frac{1}{E} \cdot \int_{\max(\alpha E, E_{n+1})}^E dE' \gamma(\mu_c) P_l(t) \quad (8.4)$$

where $P_l(t)$ are the Legendre polynomials.

A is the mass of the scatterer, and

$$\alpha = \left(\frac{A-1}{A+1} \right)^2.$$

The scattering angle in the center-of-mass system

$$\mu_c = 1 - \frac{(A+1)^2}{2A} \cdot \left(1 - \frac{E'}{E} \right),$$

and that in the laboratory system,

$$t = \frac{A+1}{2} \sqrt{\frac{E'}{E}} - \frac{A-1}{2} \sqrt{\frac{E}{E'}}.$$

$\gamma(\mu_c)$ = the angular distribution of the elastic scattering in the center of mass system. It should be normalized i.e.

$$\frac{1}{2} \int_{-1}^{+1} d\mu_c \gamma(\mu_c) = 1$$

($\gamma(\mu_c) \equiv 1$, for isotropic case)

It is practical to transform the integral (8.4) into

$$\pi_\ell(E+n) = \frac{1}{2} \int_{\mu_{n+1}}^{\mu_n} d\mu_c \gamma(\mu_c) P_\ell(t(\mu_c)), \quad (8.5)$$

where

$$t(\mu_c) = 0.5 \sqrt{1 - (1-\mu_c) \frac{2A}{(A+1)^2}} \left\{ A+1 - \frac{A-1}{1 - (1-\mu_c) \frac{2A}{(A+1)^2}} \right\} \quad (8.6)$$

or after some calculations

$$t(\mu_c) = \frac{\mu_c + \frac{1}{A}}{\sqrt{\frac{1}{A^2} + \frac{2\mu_c}{A} + 1}} \quad (8.6-b)$$

Let the energy E fall into the group g . The neutron transfer may occur into the groups $g, g+1, \dots, g+k$, where $E_k > \alpha E > E_{k+1}$. As there is an unambiguous relation between the scattering angle μ_c and energy loss, a division of the angle interval $-1 \leq \mu_c \leq 1$ corresponds to the acceptor groups, i.e.

$$-1 \equiv \mu_{k+1} < \mu_k \dots < \mu_1 < 1$$

Thus the neutrons scattered with angle $1 \geq \mu \geq \mu_1$ remain in the group g , and those with the angle $\mu_j \geq \mu \geq \mu_{j+1}$ will fall into the group $g+j$.

According to our experience, the calculation and the physical interpretation are the simplest when the integration is performed over the center-of-mass scattering angle.

8.2 Method of calculation

According to the formulae (8.1), (8.2), (8.3) and (8.5) the main task is to perform numerical integrations.

For (8.1) and (8.2) a simple trapezoidal rule is used. The meshpoints for the integration are derived from the KEDAK-data. All different energy points of the datatypes SGT, SGN and MUEL and the intervalboundaries are taken. The functional values are obtained by linear interpolation in the energy. For the integral (8.3) and (8.5) the Romberg integration method (see app. III in /2/) is used. The alternating sign of the Legendre polynomial P_ℓ and the "ill-behaviour" of the $\gamma(\mu_c)$ at some energy values require special consideration which are described in app. IV. of /2/.

Before the integral (8.3) is performed, the fine interval ΔE is to be divided into subintervals with the following mesh-points:

- i All energy points for which elastic scattering cross-sections are given in the nuclear data file should be a mesh point.
- ii If an energy value E_k/α falls into the fine interval, this also should be a mesh point. The Romberg integration procedure is performed for each subinterval.

8.3 The removal of possible inconsistencies between the average cosine calculated from the angular distribution and the average cosine available on KEDAK

There may two types of the above inconsistency exist:

- a) The angular distributions of the scattered neutrons for the energy range in question are not given, but the retrieved average cosine $\overline{\mu}_{ret}$ is different from $2/3A$. In this case a linear anisotropy is assumed i.e. the following center of mass angular distribution is used

$$\gamma(\mu_c) = 1 + \left(\overline{\mu}_{ret} - \frac{2}{3A} \right) \frac{3}{1 - \frac{3}{5A^2}} \cdot \mu_c \quad (8.7)$$

Formula (8.7) is always used for the calculations.

- b) The nuclear data file gives center of mass angular distributions for the energy range in question, but the calculated average cosine differs from the retrieved one. This difference can be attributed to the uncertainties in the evaluated angular distribution as well as to the uncertainties in their interpolation. Consequently there exist only ad hoc methods for the removal of this inconsistency. We have applied the following simple treatment.

Let the Legendre expansion of the scattering probability in the labor system be.

$$w_s(\mu) = \sum_{\ell=0}^{\infty} \frac{2\ell+1}{2} \cdot b_{s,\ell} \cdot P_{\ell}(\mu), \quad b_{s,0} = 1, \quad b_{s,1} = \overline{\mu}_{ang} \quad (8.8)$$

$\overline{\mu}_{ang}$ is the labor average cosine calculated from the given mass angular distribution. The above scattering probability is corrected with the retrieved average cosine i.e.

$$\overline{w}_s(\mu) = w_s(\mu) + \frac{3}{2} \left(\overline{\mu}_{ret} - \overline{\mu}_{ang} \right) P_1(\mu) \quad (8.9)$$

and the correction to a transfer matrix element is

$$\Delta \pi_{\ell}(E \rightarrow n) = \frac{3}{2}(\bar{\mu}_{\text{ret}} - \bar{\mu}_{\text{ang}}) \int_{\mu_{n+1}}^{\mu_n} d\mu P_{\ell}(\mu) P_1(\mu) \quad (8.10)$$

where (μ_n, μ_{n+1}) is the angle interval in the laboratory system belonging to the scattering from E into the group N.

Formula (8.10) is always used for the calculations.

8.4 Strategy of the extrapolation

It may occur that for a cross-section or angular distribution the energy interval given on the KEDAK library does not cover the whole energy range of the group system. In this case a message is printed out and the functional values are taken equal to the corresponding boundary value (horizontal extrapolation).

8.5 Description of the routines

In this chapter a brief description of the purpose and the argumentlists of the programmes of module 9 of MIGROS-3 will be given. The meaning of each variable of the argumentlists is explained once: the first time they occur.

Module 9 only has one working array (WØRK, IWØRK) for storing the results and other variables dynamically. The contents of this array is described in Table VIII. All the results are transferred within the system with the help of (WØRK, IWØRK)

8.5.1 List of the programmes⁺⁾

Name	Purpose
REMØ	main control program
REMP	Control program for groupwise calculation

⁺⁾ (F) means FUNCTIØN, otherwise SUBRØUTINE

Name	Purpose
KEDDAT	Data retrieval from the KEDAK Library
DATNUM	
KEDLEC	
NIVNUM	
AUSGL	Correction of a groupwise energy mesh
MASSIN	Initialisation of mass dependent quantities
ENERG	Calculation of groupwise energy intervals
ØRDN1	Sorting the members of an array in increasing order
SEARCH	Organisation of the output of scalar group constants
SUCHM	Organisation of the output of transfer matrices
SINT	Calculation of scalar group constants
FXINT	Integration by trapezoidal rule
ISOFAL	Organisation of the groupwise calculation of elastic transfer probabilities
WAHRS	Organisation of the subdivision of an energy interval according to the principle in chapter 8.2
LMI	Calculation of the transferprobabilities
ANINT(F)	Calculation of the integral (8.5)
AMESH	Subdivision of an angle interval
IRDMES	
INTEN	Interpolation of angular distributions
AKØR	Calculation of the average cosine correction for (8.9)
BCM(F)	Cosine of scattering angle in centre of mass system
PTL(F)	Calculation of Legendre polynomials
WINK(F)	Calculation of $\gamma(\mu)\sigma_s$
IPOL	Interpolation of angular distributions of elastically scattered neutrons
HIDR	Calculation of integral (8.5) for the hydrogen case
LININT	array-wise linear interpolation
FIPOL(F)	point-wise linear interpolation
NØRM	Normalisation of angular distribution
SMØRN	Normalisation of transfer probabilities

Name	Purpose
ZWIN	Determination of the boundaries of an energy range
ICSOP(F)	Determination of the groupnumber of an energy point
IWØ(F)	Getting integer from an array
IWIN	Storing integer in an array
EGRENZ	Dummy routine
ANG	Calculation of formula (8.6-b)

8.5.1 Purpose and argumentlists of the routines

+ Module 9 is entered at the SUBROUTINE REMO (NG,ABN,NSP,F,E,ERR,NLA,NLE,NGRE,NFG,NFI,NJM,NUJM,ISEL,IWORK,WORK,L)

with

NG	The number of energy boundaries
ABN(I),I=1, NG	The energy group boundaries /eV/
NSP	The number of energy points for the neutron spectrum
F(I),I=1, NSP	The neutron spectrum
E(I),I=1, NSP	Energy points for the neutron spectrum
ERR	The error limit for the Romberg integration
NLA,NLE	The first and the last moment to be calculated
NGRE	The number of groups to be calculated
NFG(I),I=1,NGRE	The number of finegroups
NFI(I),I=1,NGRE	The number of fine-intervals per fine-group
NJM	The maximum number of mesh points for angle integration is 2**NJM+1
NUJM	The maximum number of mesh points for energy integration is 2**NUJM+1
ISEL	= 1: The formula (8.3) will be computed 0: The fomula to be obtained from (8.3), when $\sigma_s(E) = 1$, will be computed
IWORK(I),WORK(I)I=1,L	Work-array. IWØRK and WØRK must be the same array in the calling program
L	The length of the work-array

The routine REMO performs the following tasks:

- to determine and to store the control information of TABLE VIII in the array WØRK. For this purpose the KEDDAT entries NIVNUM and DATNUM and the routine MASSIN are called.
- to retrieve the angular distributions in the energy range to be calculated from the KEDAK library with the KEDDAT entry KEDLEC.
- to determine the needed length and compare with the available length of the array WØRK.
- to call the subroutine REMP for the groupwise calculations.

+ SUBROUTINE REMP (ABN, IGR, NFI, FLUX, EFLUX, WØRK, IWØK, IS)

ABN and NFI are defined in REMØ.

IGR	is identical with NFG	} in REMØ
FLUX	is identical with F	
EFLUX	is identical with E	

IS is the lowest energy group for which angular distributions are available

In REMP the calculations are organised groupwise. The following tasks are carried out:

- to establish the energy group- and intervalstructure with the routine ENERØ
- to retrieve the nuclear data from the nuclear library KEDAK for the data types SGT, SGN and MUEL with the routine KEDDAT.
- to determine the final energy meshpoints for the calculations from the available data for SGT, SGN and MUEL. All different energy points and the groupboundaries are taken. These points are sorted by the routine ØRDNI.

- to interpolate the datatypes SGT, SGN and MUEL for the final energy array with the routine LININT.
 - to calculate the group averaged quantities of formula (8.1) and (8.2) with the routine SINT
 - to call the organisation program for the transfer matrices ISOFAL
 - to call the output organisation routines SEARCH and SUCHM
- + The retrieval of the data from the KEDAK library is organised by the routine KEDDAT with the special entries DATNUM, NIVNUM and KEDLEC

SUBROUTINE KEDDAT (NAMIZ,NAMTYP,NW,NW1,FNW,NDAT,FA,FF,EP,*,*,*)

NAMIZ /8-bytes/ name of the material
NAMTYP /8-bytes/ data type name
NW if there is a further name the sequential number of the required namecombination, otherwise without meaning.
NW1 if there is a further name then the number of retrieved name combination, otherwise without meaning.
FNW if there is a further name then its value, otherwise without meaning.
NDAT the number of retrieved data pairs.
FA(I), I=1,NDAT argument values
FF(I), I=1,NDAT function values
EP,EM upper and lower energy boundary [eV], for which the cross-section values are to be retrieved.

ENTRY DATNUM (NAMIZ,NAMTYP,NDAT,NW,EP,EM,*,*,*)

This entry is used when only NDAT is to be determined.

ENTRY KEDLEC (NAMIZ,NAMTYP,NW1,EA,IAE,EPW,EMW,FA,FF,FAW,FFW,EP,EM,*,*,*)

This entry is used to retrieve angular distributions in the energy interval $[\overline{EPW}, \overline{EMW}]$ [eV].

In this case EP, EM are not energy but cosine of the scattering angle.

EA(I), I=1, NW1 the energy points
IEA(I), I=1, NW1 the number of angle points per angular distribution
FAW(I), I=1, NW1xNDAT the angle points of angular distributions
FFW(I), I=1, NW1xNDAT the angular distributions (in one field, one by one)

ENTRY NIVNUM (NAMIZ, NAMTYP, NW1, EPW, EMW, EFR, *, *, *)

EFR is the energy for the first angular distribution. This entry is used for the determination of NW1 and EFR.

The data retrieval from the KEDAK library is performed with the standard retrieval package NDF. If no KEDAK data is available for a material or a data type the RETURN 1 statement is carried out.

In the present version RETURN 2 and RETURN 3 are defined in the argument-lists, but are not used in the program.

Further the subroutine AUSGL is called by KEDDAT in order to correct the retrieved energy meshpoints.

+ SUBROUTINE AUSGL(NDAT, EM, EP, FA, FF)

The arguments are explained in KEDDAT.

The input of AUSGL are NDAT datapoints with argument values FA and function values FF and the following properties:

$$FA(1) \leq EM$$

$$FA(NDAT) \geq EP$$

In AUSGL

$$FA(1) = EM$$

$$FA(NDAT) = EP$$

with corresponding interpolation of FF is carried out. In the case that

$$\left| \frac{FA(2) - FA(1)}{FA(1)} \right| \leq 10^{-6}, \quad \text{the point } FA(2)$$

and

$$\left| \frac{FA(NDAT) - FA(NDAT-1)}{FA(NDAT)} \right| \leq 10^{-6}, \text{ the point } FA(NDAT-1)$$

are omitted to avoid difficulties during the RØMBERG integration.

+ SUBRØUTINE MASSIN(WØRK,ABN)

WORK and ABN are defined in REMØ.

The routine MASSIN gets the mass of the desired material from KEDAK and calculates often used mass dependent quantities and stores them into the array WØRK (see TABLE VIII).

Moreover in MASSIN a transformation of the roots of the Legendre polynomials is performed and the results are transferred to the subroutine AMESH with the help of the entry IRDMES.

+ SUBRØUTINE ENERG(NFG,NFI,EM,EP,E)

NFG and NFI are defined in REMØ

EM and EP are defined in KEDDAT

E REAL*8 array with results

ENERG is the centralized subroutine for the groupwise calculation of the group- and interval boundaries. The result has double precision.

+ SUBRØUTINE ØRDNI(KMAX,FELD)

KMAX number of values to be sorted

FELD(KMAX) array with input values

The routine ØRDNI sorts the first KMAX members of the array FELD in increasing order .

+ SUBRØUTINE SEARCH(NFG,NFI,WØRK,IWØRK,FLUX,EFLUX,ENERG)

NFG,NFI,WØRK,IWØRK are defined in REMØ

FLUX is identical with F } in REMØ

EFLUX is identical with E }

ENERG REAL*8 array with group- and interval boundaries

In the routine SEARCH the output of the scalar groupconstants $\langle \sigma_t \rangle$, $\langle \sigma_s \rangle$ and $\langle \mu_s \rangle$ is organized and performed groupwise.

+ SUBROUTINE SUCHM(NFG,NFI,IWORK,WORK,MOM,ABN)

NFG,NFI,WORK,IWORK and ABN are defined in REMØ

MOM Moment of the Legendre Polynomials, used for the storing formats.

The routine SUCHM organizes the output of the transfer probability matrices.

+ SUBROUTINE SINT(NG,NI,FLUX,EFLUX,WORK,N,N4,ENERG)

NG	is identical with NFG	} in REMØ
NI	is identical with NFI	
FLUX	is identical with F	
EFLUX	is identical with E	
WORK	is defined in REMØ	
ENERG	is defined in SEARCH	
N4	Index of WORK of the actual energy mesh	
/N/	Index of WORK of the functional values to be integrated by the trapezoidal rule.	
	if N > 0 Formula (8.1) is calculated	
	N < 0 Formula (8.2) is calculated	

+ FUNCTION FXINT(EP,EM,SGN,ES,FLUX,EFLUX,NSP,NDAT)

EP	Upper integration boundary	
EM	lower integration boundary	
SGN(I)	functional values of the integration	
ES(I)	energy mesh points of the integration	
FLUX	is identical with F	} in REMØ
EFLUX	is identical with E	
NSP	is defined in REMØ	
NDAT	total number of datapoints in ES,SGN	

The function FXINT calculates the integral

$$\int_{EM}^{EP} dE \sigma(E) F(E)$$

by the trapezoidal rule.

+ SUBROUTINE ISOFAL(ABN,IGR2,NFII,FLUX,EFLUX,WORK,ENERG)

ABN and WORK	are defined in REMØ	
IGR2	is identical with NFG(I)	} in REMØ
NFII	is identical with NFI(I)	
FLUX	is identical with F	
EFLUX	is identical with E	
ENERG	is defined in SEARCH	

The routine ISOFAL organises the calculation of the transfer probability matrices.

+ SUBROUTINE WAHRS(EP,EM,IMAX,PI,ABN,NMI,NUJM,FLUX,EFLUX,TE,WORK,EZ)

ABN,NUJM,WORK	are defined in REMØ	
EP,EM	are defined in KEDDAT	
FLUX	is identical with F	} in REMØ
EFLUX	is identical with E	
IMAX	maximum group change + 1	
NMI NLE+1	(NLE defined in REMØ)	
PI(NMI,IMAX)	} auxiliary arrays	
TE(NMI,IMAX,NUJM)		
EZ	array with energy meshpoints	

The routine WAHRS subdivides the energy interval (EM,EP) for the calculation of the integral (8.3) by the RØMBERG method.

Partial results are calculated and stored.

+ SUBROUTINE LMI(EP,EM,E1,E2,SG1,SG2,AMU1,AMU2,IMAX,ABN,TE,NM1,NUJ,NUJM,
FLUX,EFLUX,WORK,PER,IMAM,PL)

ABN,NUJ,NUJM,WORK are defined in REMØ
 FLUX is identical with F } in REMØ
 EFLUX is identical with E }
 TE,NM1 are defined in WAHRS
 EP upper energy boundary } E2 ≤ EM < EP ≤ E1
 EM lower energy boundary }
 E1 upper meshpoint with
 SG1 elastic scattering cross section at anergy E1
 AMU1 average cosine at energy E1
 E2 }
 SG2 } as above for the lower meshpoint
 AMU2 }
 IMAX the maximum group change by a scattering in the
 interval (EM,EP)
 IMAM is identical with IMAX in WAHRS
 PER(NM1,IMAM) } auxiliary arrays
 PL(NM1,IMAM) REAL*8 }

The routine LMI calculates transfer probabilities from the energy interval (EM,EP).

+ DOUBLE PRECISION FUNCTION ANINT(BU,BL,K,SG,XL,AZ,ICØS,WØRK,T,NJM)

The function ANINT calculates the integral (8.5) by the RØMBERG method.

BU corresponds with μ_n
 BL " " μ_{n+1}
 K " " k
 XL(I) " " μ_c
 SG(I) " " $\gamma(\mu_c)$
 ICØS number of meshpoints of XL and SG
 AZ is calculated in LMI $(\bar{\mu}_{ret} - \frac{2}{3A}) \frac{3}{(1 - \frac{3}{5A^2})}$ Part of formula (8.7)
 WØRK, NJM are defined in REMØ
 T(NJM) auxiliary array

+ SUBROUTINE AMESH(B1,B2,Z,J2,NX,NL)

B1	is identical with BU	} in ANINT
B2	is identical with BL	
Z	array with the zeros of Legendre polynomials	
J2	starting index of the zeros of the NL Legendre polynomial	
NX	starting index for the zeros of the (NL+1) Legendre polynomial	
NL	moment of the Legendre polynomial	

The subroutine AMESH prepares the division of the angle interval (B1,B2) according to the roots of Legendre polynomial of the order NL. The entry IRDMES(AC) initialises the array AC with preprocessed data from the roots of the first five Legendre polynomials. These initialisation takes place in the routine MASSIN.

+ SUBROUTINE INTEN(E,SG,SGNC,EA,ICØS)

E	Energy for which the angular distribution is to be interpolated
SG	array with results
SGNC(ICØS,1)	angular distributions
EA	energy mesh points of the distributions
ICØS	number of angles

The routine INTEN performs a linear interpolation of the angular distributions at the energy E.

+ FUNCTION AKØR(B1,BL,K,AM)

The function AKØR calculates analytically the integral of formula (8.10).

$$AKØR = \frac{3}{2} \int_{\mu_{n+1}}^{\mu_n} d\mu P_l(\mu) P_l(\mu)$$

B1	corresponds with μ_n
BL	" " μ_{n+1}
K	" " l
AM	is the mass of the scatterer.

+ FUNCTION BCM(EI,EO,WØRK)

EI the energy of the neutron before scattering
EO the energy of the neutron after scattering
WØRK is defined in REMØ
BCM gives the cosine of the scattering angle in the
 center of mass system

+ DOUBLE PRECISION FUNCTION PTL(N,XX)

N Order of the Legendre polynomial
XX REAL*8 Argument of the Legendre polynomial
PTL REAL*8 Value of the Legendre polynomial

+ FUNCTION WINK(XL,SG,KJ,ICØS,AZ,AM)

XL,SG,ICØS,AZ are defined in ANINT
KJ control number for the anisotropy
 identical with IWØRK(23) see TABLE VIII

 KJ = 0 no angular distributions on KEDAK in
 the actual energy group
 KJ ≠ 0 angular distributions from KEDAK
AM is identical with μ
WINK $\gamma(\mu)$ of formula (8.5)

+ SUBROUTINE IPØL(M,A,B,X,Y,T)

M number of datapoints
A(M) array with angles
B(M) array with functional values
X angle for which the interpolation is to be done
Y result of the interpolation
T(M) auxiliary array

The routine IPØL is a slightly modified version of the SUBROUTINE IPOLIN by H. Wiese in chapter 7 of /2/. IPØL performs the pointwise interpolation of angular distributions of elastically scattered neutrons.

+ SUBROUTINE HIDR(BU,BL,K,A,+)

BU,BL,K are defined in ANINT
A result of the integral (8.5) for the material hydrogen
Only a RETURN 1 is performed in the program.

The integral (8.5) is calculated analytically in the case of hydrogen.

+ SUBROUTINE LININT(N,X1,Y1,M,X2,Y2)

N	number of datapoints	}	input
X1(N)	arguments		
Y1(N)	functional values		
M	number of datapoints	}	output
X2(M)	arguments		
Y2(M)	functional values		

Starting from the input N,X1,Y1 for the M arguments of array X2 the functional values are calculated by linear interpolation and stored into the array Y2.

+ FUNCTION FIPØL (XA,XB,XC,YA,YC)

$$FIPØL = \frac{YA (XC-CB) + YB(XB-XA)}{(XC-XA)}$$

FIPØL is the centralized function for pointwise linear interpolation.

+ SUBROUTINE NØRM(J2,J1,SC,WØRK)

WØRK is defined in REMØ
SC array with angular distributions
J2 first angular distribution to be normalized
J1 last angular distribution to be normalized

The routine NØRM normalizes angular distributions in the array SC. If the normalisation integral cannot be calculated with the desired accuracy and the allowed number of points, the control number for anisotropy KJ=IWØRK (23) is set equal two. In this case in ANINT the angle meshpoints from KEDAK instead from AMESH are taken.

+ SUBROUTINE SMØRN(PI,N,IM,WØRK)

WØRK is defined in REMØ
PI(N,IM) array with transfer matrix elements, when SMØRN is
 entered.
N NLE+1 (NLE defined in REMØ)
IM maximum group change + 1

In the routine SMØRN the calculated transfer matrices are normalized in order to get the transfer probabilities.

+ SUBROUTINE ZWIN(KL,EP,EM,ES,J2,J1)

EP upper energy
EM lower energy
KL number of energy meshpoints
ES(KL) array with energy meshpoints
J2 largest index of the array ES fulfilling
 the condition $ES(J2) \leq EM$
J1 smallest index of the array ES fulfilling
 the condition $ES(J1) \geq EP$

+ FUNCTION ICSØP(E,ABN)

ABN is defined in REMØ
E energy point
ICSØP groupnumber of the system ABN for the energy E

+ FUNCTION IWØ(L,IWØRK)

IWØRK is defined in REMØ
L index
IWØ IWØRK(L)

+ SUBROUTINE IWIN(L,N,IWØRK)

IWØRK is defined in REMØ
L index
N number

The routine IWIN performs the statement $IWØRK(L) = N$.

+ SUBROUTINE EGRENZ(E,ABN,IK,IV,WORK)

This subroutine was intended for the inelastic scattering case. In the module 9 for the REM correction EGRENZ is a dummy routine.

+ DOUBLE PRECISION FUNCTION ANG(XX,GAM)

XX	Corresponds with μ_c
GAM	Corresponds with $\frac{1}{A}$
ANG	the result of equation (8.6-b)

TABLE VIII

Control information in the array (WØRK,IWØRK)

Word	Content	Comment
1	Address of EA/1/	Energy meshpoints for angular distribution
2	Address of XL/1/	Angle mesh points
3	Address of SGNC/1/	Angular distributions
4	I	The number of the actual calculated group
5	Address of SGN/1/	Elastic scattering or total cross-section
6	Address of AMU/1/	Retrieved average cosine
7	Address of ES/1/	Energy mesh points for cross-sections
8	ISEL	See input description
9	Address of SG/1/	Auxiliary array defined in ANINT
10	Address of TE/1/	Auxiliary array defined in WAHRS
11	Address of PER/1/	Auxiliary array defined in LMI
12	Address of SP/1/	Array for the storage of results
13	Address of BUF/1/	Buffer-array for output
14	NG	See input description
15	NSP	" " "
16	NLA	" " "
17	NLE	" " "
18	IMAX	Maximum group change+1
19	NJM	See input description
20	NUJM	" " "
21	ICOS	Number of angle mesh points
22	Address of the actual first free word of SP	
23	KJ	Control number of the anisotropy (see routine WINK)
24	NJ	2**NJ+1 number of mesh points to be required for angular integration
25	NDAT	Number of cross section points
26	NIV	Number of energy points for angular distribution
27	ERR	Error for RØMBERG integration procedure
28	A	
29	$((A+1)/(A-1))^2$	

TABLE VIII (cont.)

Word	Content	Comment
30	$(A+1)^2/2A$	
31	$\log \left(\left(\frac{A+1}{A-1} \right)^2 \right)$	
32	Q =-0.1	
33	Address of T/1/	REAL*8 Auxiliary array defined in ANINT
34	Address of PL/1/	REAL*8 Auxiliary array defined in LMI
35	Address of E/1/	REAL*8 array with groupwise energy boundaries defined in ENERG
36	NMAX	The maximum number of datapoints of one of the datatypes SGT,SGN or MUEL within an energy group

References

/1/ H Huschke

Gruppenkonstanten für dampf- und natriumgekühlte Schnelle Reaktoren
in einer 26-Gruppendarstellung (Chapter 3.5)

KFK 770 (1968)

/2/ H. Huschke, B. Krieg et al.

MIGROS-2. A Program written in FORTRAN for the Calculation of
Microscopic Group Constants from Nuclear Data.

KFK 1784 (1973)

9. The calculation of average group cross sections for infinite dilution and of energy resonance self-shielding factors from energy pointwise data. Module 3 (FSTRUK).⁺⁾
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9.1 Introduction

The calculation of the group constants defined in the following has originally done by a module written by B. Krieg and described in /1/. The results of this module showed in general good agreement with results obtained from other sources. But in some cases discrepancies (about 10 %) occurred. The reason for this effect was a not sufficient dense storage of the energy points of the cross sections on the used library.

By this presupposition of a sufficient dense energy grid, it was possible, that the structure of a pointwise given weighting function has been overlooked by the program, or that by using the trapezoidal rule, the numerical value of an integral has been calculated with insufficient accuracy.

Number and largeness of the discrepancies increased, when due to limited storage the use of a common energy grid on KEDAK (/2/ and /3/) for all cross sections types of the form $Q = F(E)$, could not longer be hold. Because the program has relied upon this assumption, only the energy points of a specified cross section type have been used as integration base. This can induce big errors, if another cross section type, which is participating in the function to be integrated, has - within the integration range - a different energy grid with great fluctuations of the cross section values.

Due to the reasons given in the preceding we have decided to revise this module 3. Attempts in this direction showed, that it would be more effective to reprogram this module and by doing this also to use new methods in solving the problems.

⁺⁾ This chapter has been written completely new, because the program, described by this chapter, has also been rewritten. Compared with the old program the program described here is using other methods in solving the problem. Yet the formulaes defining the physical quantities, are identical to those given by B. Krieg, H. Huschke in /1/.

In the following, first the physical quantities to be calculated are defined. Afterwards a description of the program is given.

9.2 Definition of the quantities calculated by the program

Starting with pointwise data the program FSTRUK calculates energetic self shielding factors and average group cross sections for infinite dilution. Flux and current weighting is used.

For simplification of the formulaes the following definitions are used. If E_ℓ and E_h are two energy group boundaries with $E_\ell < E_h$, then we define

$$\langle y(E) \rangle \equiv \frac{1}{E_h - E_\ell} \int_{E_\ell}^{E_h} y(E) dE \quad (1)$$

We also define

$$\begin{aligned} x &= \text{type of neutron reaction (n,x)} \\ g &= \text{number of the energy group} \\ \sigma_o &= \text{background cross section} \end{aligned} \quad (2)$$

All these definitions are related to a specified isotope. But for simplification we have neglected the corresponding index.

Flux weighted resonance self shielding factor are calculated for

capture (reaction (n,c) = total absorption-fission, type name FC⁺)
for fissionable resp. FA for non fissionable materials),

elastic scattering (reaction (n,e), type name FN)

and

fission (reaction (n,f), type name FF):

⁺) These type names FC, FA, FN, ... are used in the print output of the program and in the general parts of this report.

$$f_{x,g}(\sigma_0) = \frac{\sigma_{x,g}(\sigma_0)}{\sigma_{x,g}(\sigma_0 \rightarrow \infty)} \quad (3)$$

with

$$\sigma_{x,g}(\sigma_0) = \frac{\left\langle \frac{\sigma_x(E) \cdot F(E)}{\sigma_t(E) + \sigma_0} \right\rangle}{\left\langle \frac{F(E)}{\sigma_t(E) + \sigma_0} \right\rangle} \quad (4)$$

$F(E)$ means the weighting function, $\sigma_t(E)$ the total microscopic cross section and $\sigma_x(E)$ - according to the desired self shielding factor - the microscopic capture cross section σ_c (resp. σ_a), the microscopic elastic scattering cross section σ_e , or the microscopic fission cross section σ_f . If the term σ_x in the formulae (3) and (4) is replaced by $\sigma_e(E) \cdot \bar{\mu}_e(E)$, then the flux weighted self shielding factor $FNOI^{+}$ is produced with

$$I_{e,g}(\sigma_0) = \frac{\{\sigma_e \bar{\mu}_e\}(\sigma_0)}{\{\sigma_e \bar{\mu}_e\}(\sigma_0 \rightarrow \infty)} \quad (5)$$

with

$$\{\sigma_e \bar{\mu}_e\}(\sigma_0) = \frac{\left\langle \frac{\sigma_e(E) \cdot \bar{\mu}_e(E) \cdot F(E)}{\sigma_t(E) + \sigma_0} \right\rangle}{\left\langle \frac{F(E)}{\sigma_t(E) + \sigma_0} \right\rangle} \quad (6)$$

⁺) See footnote on page 9.5

$\bar{\mu}_e(E)$ means the average cosine for elastic scattering.

The terms in the denominator in formulae (3) and (5) are the group cross sections for infinite dilution. For σ_0 toward infinity in the formulae (4) and (6) - with respect to formulae (1) - we get

$$\lim_{\sigma_0 \rightarrow \infty} \sigma_{x,g}(\sigma_0) = \sigma_{x,g}^{\infty} = \frac{\langle \sigma_x(E) \cdot F(E) \rangle}{\langle F(E) \rangle} \quad (7)$$

and

$$\lim_{\sigma_0 \rightarrow \infty} \{\sigma_{e\bar{\mu}_e}\}_g(\sigma_0) = \{\sigma_{e\bar{\mu}_e}\}_g^{\infty} = \frac{\langle \sigma_e(E) \bar{\mu}_e(E) \cdot F(E) \rangle}{\langle F(E) \rangle} \quad (8)$$

Replacing x in formulae (7) by c, e or f we get the following quantities:

x = c (capture) SIGMA A for non fissionable materials
 SIGMA C for fissionable materials

x = e (elastic scattering) SIGMA N

x = f (fission) SIGMA F

The denomination of the quantity calculated in formulae (8) is SIGMA N01.

All self shielding factors defined until now have been flux weighted. For the elastic scattering and the total reactions additionally the following current weighted quantities are calculated:

$$I_{t,g}^f(\sigma_0) = \frac{I_{t,g}^{\sigma}(\sigma_0)}{I_{t,g}^{\sigma}(\sigma_0 \rightarrow \infty)} \quad (9)$$

and

$$I_{e,g}^f(\sigma_0) = \frac{I_{e\bar{\mu}_e}^{\sigma}(\sigma_0)}{I_{e\bar{\mu}_e}^{\sigma}(\sigma_0 \rightarrow \infty)} \quad (10)$$

+) See footnote on page 9.5

The terms ${}_1\sigma_{t,g}(\sigma_0)$ and ${}_1\{\sigma_e\bar{\mu}_e\}(\sigma_0)$ are defined by the following expressions:

$${}_1\sigma_{t,g}(\sigma_0) = \frac{\left\langle \frac{\sigma_t(E) \cdot F(E)}{(\sigma_t(E) + \sigma_0)^2} \right\rangle}{\left\langle \frac{F(E)}{(\sigma_t(E) + \sigma_0)^2} \right\rangle} \quad (11)$$

and

$${}_1\{\sigma_e\bar{\mu}_e\}_g(\sigma_0) = \frac{\left\langle \frac{\sigma_e(E) \cdot \bar{\mu}_e(E) \cdot F(E)}{(\sigma_t(E) + \sigma_0)^2} \right\rangle}{\left\langle \frac{F(E)}{(\sigma_t(E) + \sigma_0)^2} \right\rangle} \quad (12)$$

The quantity defined in formulae (9) will be found in the program output headed with FT1, whereas the quantity defined in formulae (10) will be found under the heading FN1. Doing the limit for σ_0 toward infinity in the formulae (11) respectively (12) we get expressions similar to those in formulae (7) and (8).

$${}_1\sigma_{t,g}^\infty = \lim_{\sigma_0 \rightarrow \infty} {}_1\sigma_{t,g}(\sigma_0) = \frac{\langle \sigma_t(E) \cdot F(E) \rangle}{\langle F(E) \rangle} \quad (13)$$

and

$${}_1\{\sigma_e\bar{\mu}_e\}_g^\infty = \lim_{\sigma_0 \rightarrow \infty} {}_1\{\sigma_e\bar{\mu}_e\}_g = \frac{\langle \sigma_e(E) \cdot \bar{\mu}_e(E) \cdot F(E) \rangle}{\langle F(E) \rangle} \quad (14)$$

+) The quantities in formulae (5) and (8) respectively (10) and (14) are used, together with other quantities, to determine the transport cross section. For consistent transport and diffusion calculations the current weighting (see formulae 10 and 14) should be used. But remember that for average cross sections for infinite dilution there is no difference between flux or current weighting. The quantities in formulae (9) and (13) are used to calculate the total current weighted cross section.

This current weighted average group cross sections for infinite dilution are named in the program with SIGMA T1 ($\int_1 \sigma_{t,g}^{\infty}$) respectively SIGMA N1 ($\int_1 \{\sigma_e \bar{\mu}_e\}_g^{\infty}$). If we compare formulae (13) with formulae (7), and formulae (14) with formulae (8), we see, that there is no difference for the average cross sections for infinite dilution between flux and current weighting. Therefore the following statement is valid:

$$\text{SIGMA N1} = \int_1 \{\sigma_e \bar{\mu}_e\}_g^{\infty} = \int_1 \{\sigma_e \bar{\mu}_e\}_g^{\infty} = \text{SIGMA N01} \quad (15)$$

9.3 Numerical calculation of the integrals

A central task of FSTRUK is to calculate the integral defined in formulae (1). Therefore we will describe in this section, how we have solved the problem to determine the numerical value of

$$\int_{E_l}^{E_h} y(E) dE \quad (16)$$

One can see in the preceding section 9.2 that $y(E)$ is normally composed out of several functions. For example $y(E)$ may be $\sigma_e(E) \cdot \bar{\mu}_e(E) \cdot F(E)$ or $\frac{\sigma_t(E) \cdot F(E)}{(\sigma_t(E) + \sigma_o)^2}$ or simply $F(E)$. The cross sections ($\sigma_e(E)$, $\sigma_t(E)$, ...) are given pointwise (see KEDAK /2/ and /3/), whereas $F(E)$ may be given as an analytical expression or also pointwise. The cross sections can - according to KEDAK conventions - predicted by linear interpolation between two adjacent energy values. We assume that this is also the case for the pointwise given weighting function.

If we take a specific cross sections (or the pointwise weighting function), then it follows that this quantity can be represented in the interval $[E_\ell, E_h]$ by a set of straight line equations $y = a_i \cdot E + b_i$ with a_i and b_i defined in the interval $[E_i, E_{i+1}]$. E_i and E_{i+1} are adjacent energy points at which the specific cross sections (or the pointwise weighting function) are stored resp. given. The formation of the composite function $y(E)$ out of the partial functions is best shown in an example. Assuming $E_\ell = 1$ eV, $E_h = 2.15$ eV (group 23 in the ABN-group set) and $y(E) = \sigma^1(E) \cdot \sigma^2(E)$. The two cross section types σ^1 and σ^2 are given at the following energy points:

$$\sigma^1: E_i^1 = 1.0 \text{ eV}, 1.2 \text{ eV}, 1.5 \text{ eV}, 2.0 \text{ eV}, 2.5 \text{ eV}.$$

$$\sigma^2: E_i^2 = 0.8 \text{ eV}, 1.2 \text{ eV}, 1.4 \text{ eV}, 1.6 \text{ eV}, 1.8 \text{ eV}, 2.0 \text{ eV}, 2.2 \text{ eV}.$$

We calculate for both cross section types the a_i and b_i :

cross section type: σ^1		
Interval [eV]	i	a, b
1.0-1.2	1	a_1^1, b_1^1
1.2-1.5	2	a_2^1, b_2^1
1.5-2.0	3	a_3^1, b_3^1
2.0-2.15	4	a_4^1, b_4^1

cross section type: σ^2		
Interval [eV]	i	a, b
1.0-1.2	1	a_1^2, b_1^2
1.2-1.4	2	a_2^2, b_2^2
1.4-1.6	3	a_3^2, b_3^2
1.6-1.8	4	a_4^2, b_4^2
1.8-2.0	5	a_5^2, b_5^2
2.0-2.15	6	a_6^2, b_6^2

If there are no energy points stored corresponding to the lower or upper group boundary, the next point near the boundary (next means less at the beginning and greater at the end) is taken to calculate the a_i and b_i . It is evident that this a_i and b_i are also valid in the minor interval until the group boundary.

To get the function $y(E)$ all the energy values of the various participating cross sections are taken and a new energy grid is composed. Equal or nearly equal⁺⁾ values are taken only once. In the case of nearly equal values the minor one is taken.

In the new energy grid we can now define the function $y(E)$. In our example it is a quadratical polynomial, as shown in the following table:

Interval [eV]	$y(E)$
1.0 - 1.2	$(a_1^1 \cdot E + b_1^1) \cdot (a_1^2 \cdot E + b_1^2)$
1.2 - 1.4	$(a_2^1 \cdot E + b_2^1) \cdot (a_2^2 \cdot E + b_2^2)$
1.4 - 1.5	$(a_2^1 \cdot E + b_2^1) \cdot (a_3^2 \cdot E + b_3^2)$
1.5 - 1.6	$(a_3^1 \cdot E + b_3^1) \cdot (a_3^2 \cdot E + b_3^2)$
1.6 - 1.8	$(a_3^1 \cdot E + b_3^1) \cdot (a_4^2 \cdot E + b_4^2)$
1.8 - 2.0	$(a_3^1 \cdot E + b_3^1) \cdot (a_5^2 \cdot E + b_5^2)$
2.0 - 2.15	$(a_4^1 \cdot E + b_4^1) \cdot (a_6^2 \cdot E + b_6^2)$

If we generalize this method, we can define $y(E)$ for all cases (appearing in the preceding chapter) over an energy grid, constructed in the same manner as in the example. By this subdividing of the integration range we can transform the integral (16) as shown in the following:

⁺⁾ Nearly equal will be defined in the following.

$$\int_{E_\ell}^{E_h} y(E) dE = \int_{E_1}^{E_2} y_1(E) dE + \int_{E_2}^{E_3} y_2(E) dE + \dots + \int_{E_{n-1}}^E y_{n-1}(E) dE \quad (17)$$

with

$$E_1 = E_\ell, E_n = E_h; E_i < E_{i+1} \text{ for } i = 1, 2, \dots, n-1;$$

$$[E_\ell, E_h] = [E_1, E_2] + [E_2, E_3] + \dots + [E_{n-1}, E_n]$$

Each of this subintegrals

$$\int_{E_i}^{E_{i+1}} y_i(E) dE \quad (18)$$

can now be calculated in a very simple way, because a rule to calculate $y_i(E)$ exists for each value of E in the interval $[E_i, E_{i+1}]$. By summation of the subintegrals, we will get the total integral. The subintegrals can be calculated by numerical methods or, if the expression of the weighting function is known, also analytically. Before this will be shown in part 9.4 and 9.5, we must first define the expression "nearly equal". Due to numerical reasons it is not desirable to deal with very small intervals. Therefore points with very close energy distance are regarded as one point, and only the lower value is taken. Two points E_a and E_b are "nearly equal", if they fulfill the condition

$$\frac{|E_a - E_b|}{\max(|E_a|, |E_b|)} \leq \epsilon \quad (19)$$

max means the maximum value. The value of ϵ depends from the number representation accuracy of the specified computer. In the version running on the IBM/370 model 168 of the GfK, ϵ has the value $1.0E-6$.

9.4 Romberg integration

For the calculation of the integrals (18) we have chosen the trapezoidal rule in connection with the Romberg extrapolation method (/4/). A modified subroutine of the SSP (Scientific Subroutine Package) from IBM (/5/) has been used.

We assume, that the Romberg method is known. If not, a description can be found e.g. in /4/ or in the numerical mathematics literature. Because of our assumption we will only describe special features of the used method.

For each bisection of the integration interval an approximation of the integral is calculated. These approximations are compared. The process will stop, if the changes will be small enough. The process will also stop, if the changes, which normally become smaller, will increase, whereby one times an increase will be tolerated. By this, we avoid an endless running of the program due to rounding errors.

The tests on the desired accuracy or on the occurrence of rounding errors will be switched on normally after some bisections of the integration interval. The number of this bisections depends on the size of the interval. For very small ones all tests will start after the first bisection. By this method we avoid unnecessary calculation expense.

The results of the integration can be divided into three classes:

- class 1: desired integration error has been reached.
 Tests have been started after the first bisection.

- class 2: desired integration error has been reached.
 Tests have been started after some (defined in the
 routine) bisections. This is the normal case.

- class 3: desired integration error has not been reached because
 of rounding errors.

The Romberg integration is controlled by the values of the variables given in BLOC 31 (see input description 2.1.1). The iteration is stopped if the absolute relative difference is less or equal EPSROM. In the case of a termination of the process, before the error has reached the value EPSROM, a printout in the routine is done, if this actual error is DRINWA-times greater than EPSROM. If BLOC 31 is not given in the input, the values EPSROM = 5.0E-5 and DRINWA = 5.0 are used.

9.5 Analytical integration

If the analytical representation for the weighting function $F(E)$ is known, we can try to solve the integrals (18) by an analytic expression. This is done in the program for two weighting functions: first for the pointwise given weighting function, which can be represented as straight lines, and second for the function $F(E) = 1/E$. Regarding the equations in 9.2 we can see that the general form for $y_i(E)$ is

$$y_i(E) = \frac{h_3 E^3 + h_2 E^2 + h_1 E + h_0}{(r_1 E + r_0)^n} \quad n = 0, 1, 2 \quad (20)$$

for the pointwise given weighting function and

$$y_i(E) = \frac{h_2 E^2 + h_1 E + h_0}{E (r_1 E + r_0)^n} \quad n = 0, 1, 2 \quad (21)$$

for the $1/E$ -weighting. The terms h_3 , h_2 , h_1 , h_0 , r_1 and r_0 are determined by the a and b of the contributing functions and by σ_0

The integration of these functions is not very difficult. But it generates very extended expressions. For example, if using $y_i(E)$ from formulae (20) with $n = 2$ and the prepositions r_1 and r_0 not equal zero, and $(r_1 E + r_0)$ not changing sign in the integration range, we get:

$$\begin{aligned}
 \int_{E_i}^{E_{i+1}} y_i(E) dE &= \int_{E_i}^{E_{i+1}} \frac{h_3 E^3 + h_2 E^2 + h_1 E + h_0}{(r_1 E + r_0)^2} dE \\
 &= \left[\frac{h_3}{r_1^4} \left(\frac{1}{2} (r_1 E + r_0)^2 - 3 r_0 (r_1 E + r_0) \right. \right. \\
 &\quad \left. \left. + 3 r_0^2 \cdot \log(r_1 E + r_0) + \frac{r_0^3}{r_1 E + r_0} \right) \right. \\
 &\quad \left. + \frac{h_2}{r_1^3} \left((r_1 E + r_0) - 2 r_0 \log(r_1 E + r_0) - \frac{r_0^2}{r_1 E + r_0} \right) \right. \\
 &\quad \left. + \frac{h_1}{r_1^2} \left(\frac{r_1}{r_1 E + r_0} + \log(r_1 E + r_0) \right) \right. \\
 &\quad \left. - \frac{h_0}{r_1} \frac{1}{r_1 E + r_0} \right] \Bigg|_{E_i}^{E_{i+1}}
 \end{aligned}$$

Integrating the other functions we get similar expressions. But it will be shown in the following that it is in some cases numerically very difficult to evaluate these expressions.

9.6 Output of the program for non fissionable and fissionable materials

The output of the program is different whether the material is fissionable or not. A material is regarded as fissionable by the program, if the cross section type σ_f can be found in the data base KEDAK. In the other case the material is regarded as non fissionable.

For non fissionable materials the following quantities are calculated by the program:

SIGMA A, SIGMA N, SIGMA NO1, SIGMA NI, SIGMA TI,
FA, FN, FNO1, FNI, FTI

For fissionable materials the following quantities are produced:

SIGMA C, SIGMA N, SIGMA F, SIGMA NO1, SIGMA NI, SIGMA TI
FC, FN, FF, FNO1, FNI, FTI.

(The meaning of the names can be found in 9.2.)

The self shielding factors are calculated in both cases for all defined σ_0 -values.

9.7 Replacing the program built in weighting function 1/E

If the weighting function is not given pointwise, or if it is demanded in the control input, MIGROS-3 uses a built-in function, which generates 1/E. This function must be given in single precision (name PHI) and in double precision (name DPHI) (see 1.4.2). Normally the single precision function is used in MIGROS-3. But the program FSTRUK described here, demands a double precision function. Therefore if one desires to change this function, one has to add a single and double version of this function in a compile-, link- and go-step. This job must have the following job control cards:

```
// (job card)
/* (Setup-card (s) for the disk containing the KEDAK library and eventually
   other disks.)
// EXEC FHCLG,LIB=NUSYS
//C.SYSIN DD *
   (new functions PHI and DPHI)
/*
//L.SYSIN DD *
   INCLUDE LOAD(MIGROS3)
   INCLUDE OBJ(MIGROS3)
/*
   (Necessary DD-cards and control input for
   the go-step.)
//
```


9.8 Selection of different weighting functions and integration modes independent of the group boundaries

In the program FSTRUK the user can subdivide the whole energy range, given by the energy groups, into subranges, in which he can define the integration mode and the weighting function. These subranges, which are independent from the energy group boundaries, must cover the whole energy range. In the now running version of the program up to five subranges are possible. This number can be increased by changing the variables MAXEBR, MIBER and increasing the array dimensions of ENBER, NWFUN and CONWFU.

In the present version of the program the following weighting functions and integration modes can be chosen: If there is no pointwise weighting function given in the input, one can select either the program built-in function DPHI (resp. PHI) - or a linked function-, or the function CONWFU(I)/E, with CONWFU(I) given in the input. If a pointwise weighting function is existent, one can additionally choose this possibility. There are two integration modes: numerical and analytical as defined in 9.4 and 9.5. But due to numerical difficulties in the evaluation of the analytically calculated integrals in some cases (especially for great σ_0 -values and high energies), we recommend to use only the numerical (Romberg) integration.

The option described in this chapter is controlled by the variables given in BLOC 33 of the input description 2.1.1. If this BLOC is not given one energy range is used, in which numerical (Romberg) integration is made. If there exists a pointwise given weighting function, this will be used. If no pointwise function is available, the program built in or program linked function DPHI is used.

9.9 Error processing and test printoutput

The program generates and prints messages, warnings and error messages, which are self explaining. Some errors will cause a termination of the program FSTRUK, e.g. negative total cross sections.

The message

```
+++WARNING NDF. 3: THE DATA FOR ... 30190 ARE NOT INCLUDED IN THE KEDAK LIBRARY
```

has no meaning in our case and can be ignored. Due to program technical reasons it can not be suppressed. In production runs not all messages, which are generated, will be printed out. But it may be useful, to have more messages printed out in test cases in order to find errors. How to switch on this option, which is normally only used by programmers to correct errors, can be seen in the input description 2.1.1 in the BLOC 32.

9.10 Short description of the subroutines of the FSTRUK-segment

In the following all subroutines of the FSTRUK-segment will be described. All the descriptions will have the following scheme:

problem solved by the routine
definition with argument list (and entry
names if existant)
explanation of the quantities in the list
used common blocks (with an explanation of
the quantities)
called subprograms (except those, which are
FORTRAN-supplied procedures or subprograms
like IBCOM).

In the explanation lists of the arguments and of the common variables the following abbreviations will be used:

in the mode :	I	for variables which values must be defined before calling the subroutine or must be set in the common by a previous program.
column	0	for variables which are set in the subroutine (or in programs called by the subroutine) and used outside (and within) the subroutine.
	L	for arrays (or variables) which are only used for placing some storage for the disposal of the subroutine and have only the meaning of local quantities.

IO for a combination of I and O

- for quantities, which are not referenced in the subprogram, or non of the given classifications is true.

in the type :
column

R4 for REAL*4 quantities

R8 for REAL*8 quantities

I4 for INTEGER*4 quantities

L4 for LOGICAL*4 quantities

B4 for 4 Byte quantities of any type.
The actual type will be determined by additional information.

F8 for functions supplying REAL*8 values.

In the dimension column the maximal dimension of arrays will be given. For scalar quantities the word "scalar" is used.

9.10.1 Subroutine FSTRUK

Problem solved:

Calculation of energy resonance self shielding factors and of average group cross sections for infinite dilution from energy pointwise data.

Definition:

SUBROUTINE FSTRUK (MI, SIGO, NE, ENG, NFE, RFFE, EFE,
NENBER, ENBER, NWFUN, CONWFU,
EPSROM, DRINWA,
ITEST, IZPUMS, ITUMS,
ISPATE,
MIBER, GIBER, MIBERP, IIBER, CIBER,
FFAKT,
MABWF, ABWF, MABWFP,
MXINT, XINT, MXINTP,
MABQ1, ABQ1, MABQ1P,

MABQ2,ABQ2,MABQ2P,
MABQ3,ABQ3,MABQ3P,
KMROM,AUXROM,KMROMP,
RF,MRF,RFL,MRFP)

Explanation of the quantities in the list:

name	mode	type	dimension	remarks
MI	I	I4	scalar	number of σ_0 -values
SIGO	I	R4	(MI)	σ_0 -values [barn]
NE	I	I4	scalar	number of group boundaries
ENG	I	R4	(NE)	group boundaries [eV]
NFE	I	I4	scalar	number of energy points of the weighting spectrum
REFE	I	R4	(NFE)	energy points of the weighting spectrum [eV]
EFE	I	R4	(NFE)	weighting function values at the energy points of the field REFE
NENBER	I	I4	scalar	number of ranges of different weighting functions and integration modes (see BLOC 33 of the input)
ENBER	I	R4	(NENBER)	range boundaries (see BLOC 33)
NWFUN	I	I4	(NENBER)	selection of weighting functions and integration modes (see BLOC 33 of the input)
CONWFU	I	R4	(NENBER)	factor(s) in the weighting function CONWFU(I)/E (see BLOC 33 of the input)
EPSROM	I	R4	scalar	termination accuracy in Romberg integration (see BLOC 31 of the input)
DRINWA	I	R4	scalar	control of error printout in Romberg integration (see BLOC 31 of the input)
ITEST	I	I4	scalar	control of printout of messages, warnings and error messages (see BLOC 32 of the input)

name	mode	type	dimension	remarks
IZPUMS	I	I4	scalar	control of changing ITEST-conditions during the calculations (see BLOC 32 of the input)
ITUMS	I	I4	scalar	new value of "ITEST", when having changed due to IZPUMS. (see BLOC 32 of the input)
ISPATE	IO	I4	scalar	should be 0 for non fissionable and 1 for fissionable materials. But it can be redefined in the FSTRUK-segment,
MIBER	I	I4	scalar	maximum number + 1 of ranges of different weighting functions and integration modes for one group.
GIBER	L	R4	(MIBER)	range boundaries for one group. (see MIBER)
MIBERP	O	I4	scalar	necessary increase of MIBER if MIBERP is greater zero. MIBERP is always greater or equal zero.
IIBER	L	I4	(MIBER)	selection of weighting functions and integration modes within one specified group
CIBER	L	R4	(MIBER)	factor(s) in the weighting function CIBER(I)/E within one group
FFAKT	L	R4	(MI,6)	local storage for self shielding factors for one specified group
MABWF	I	I4	scalar	used for dimensioning of array ABWF
ABWF	L	R4	(MABWF,4)	representation of the pointwise given weighting function as parts of straight lines
MABWFP	O	I4	scalar	necessary increase of MABWF if MABWFP is greater than zero
MXINT	I	I4	scalar	used for dimensioning of array XINT
XINT	L	R4	(MXINT)	integration points within one group or within subintervals in this group
MXINTP	O	I4	scalar	necessary increase of MXINT if MXINTP is greater than zero
MABQ1	I	I4	scalar	used for dimensioning of array ABQ1
ABQ1	L	R4	(MABQ1,4)	representation of the cross section types σ_t , σ_a , σ_e or σ_f as parts of straight lines.

name	mode	type	dimension	remarks
MABQ1P	O	I4	scalar	necessary increase of MABQ1 if MABQ1P is greater zero
MABQ2	I	I4	scalar	used for dimensioning of array ABQ2
ABQ2	L	R4	(MABQ2,4)	representation of the cross section type μ_e as parts of straight lines.
MABQ2P	O	I4	scalar	necessary increase of MABQ2 if MABQ2P is greater zero.
MABQ3	I	I4	scalar	used for dimensioning of array ABQ3
ABQ3	L	R4	(MABQ3,4)	representation of the cross section type σ_t as parts of straight lines
MABQ3P	O	I4	scalar	necessary increase of MABQ3 if MABQ3P is greater zero
KMROM	I	I4	scalar	KMROM-1 = maximum number of bisections in Romberg integration.
AUXROM	L	R8	(KMROM)	array used in Romberg integration
KMROMP	O	I4	scalar	necessary increase of KMROM if KMROMP is greater zero
RF	L	R4	(MI,MRF)	auxiliary array for storing σ_0 -dependent-integral results.
MRF	I	I4	scalar	must have the value 7 for non fissionable and the value 8 for fissionable materials. If it has not the correct value, MRFP is set to 1, ISPATE is set to the correct value and a RETURN to the calling program is done.
RFL	L	R4	(MI,MRF)	local storing of RF-values
MRFP	O	I4	scalar	normal 0. Is set to 1, if MRF (and ISPATE) has had a wrong value (see MRF description).

Used common blocks (with an explanation of the quantities):

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
MAT	I	R8	scalar	1	name of the material
NR3	-	I4	(2)	3	dummy array. Not used in FSTRUK
NOUTP	I	I4	scalar	5	unit number for print output
JA	-	I4	scalar	6	external storage number for the output of the results. Not used in this subroutine.
NANF	I	I4	scalar	7	number of the first energy group
NEND	I	I4	scalar	8	number of the last energy group
KL	IO	I4	scalar	9	at the end of each module, KL must be enlarged by one.

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
TEST1	0	L4	scalar	1	control of test printout
TEST2	0	L4	scalar	2	control of test printout
TEST3	0	L4	scalar	3	control of test printout
LERMSG	0	L4	scalar	4	control of σ_0 -dependent test and error printout
GLSCH	0	R4	scalar	5	two numbers a and b are considered as equal, if $\frac{ a-b }{\max(a , b)} \leq \text{GLSCH}$ or if a = b = 0.
MNFTYP	0	I4	scalar	6	maximum value of NFTYP
NFTYP	0	I4	scalar	7	mode of integration and type of the weighting function

name of the common block: CFSTRU (continued)					
name	mode	type	dimension	word	remarks
ITYP	0	I4	scalar	8	type of the function to be integrated
ITYPFU	0	I4	scalar	9	subtype of the function to be integrated
UGR	0	R4	scalar	10	lower limit of the integration range
OGR	0	R4	scalar	11	upper limit of the integration range
CONST	0	R4	scalar	12	constant in the weighting function CONST/E
NR1	-	I4	(8)	13	dummy array. Not used in FSTRUK.
BSIGO	0	R4	scalar	21	actuell σ_o -value

name of the common block: CFSDUR					
name	mode	type	dimension	word	remarks
IDUR	IO	I4	scalar	1	number of groups for which calculations have been done in a previous subroutine-call.

Called subprograms:

```

FSGRAL
FSQUER
FSTRU0
FSTRU1
FSTRU2
FSTRU3
FSTRU4
FSTRU5
FSWRS9
FSWRO0
FSWRO1
FSWRO2
FSWRO3
FSWRO4
FSXIIN
FSXINT
    
```

} (entries of FSWRO0)

} (entry of FSXINT)

9.10.2 Subroutine FSTRUO

Problem solved:

Test and printout of some quantities.

Definition:

```
SUBROUTINE FSTRUO(NE,ENG,NANF,NEND,
                  NFE,REFE,EFE,
                  NENBER,ENBER,NWFUN,CONWFU,
                  EPSROM,KMROM,DRINWA,
                  ISPATE,
                  MIBER,MABWF,MXINT,
                  MABQ1,MABQ2,MABQ3,
                  MRF,MRFP,*,*)
```

Explanation of the quantities in the argument list:

name	mode	type	dimension	remarks
NE	I	I4	scalar	see 9.10.1 (argument list)
ENG	I	R4	(NE)	" "
NANF	IO	I4	scalar	" "
NEND	IO	I4	scalar	" "
NFE	I	I4	scalar	" "
REFE	I	R4	(NFE)	" "
EFE	I	R4	(NFE)	" "
NENBER	I	I4	scalar	" "
ENBER	I	R4	(NENBER)	" "
NWFUN	I	I4	(NENBER)	" "
CONWFU	I	R4	(NENBER)	" "
EPSROM	I	R4	scalar	" "
KMROM	I	I4	scalar	" "
DRINWA	I	R4	scalar	" "
ISPATE	IO	I4	scalar	" "
MIBER	I	I4	scalar	" "

name	mode	type	dimension	remarks
MABWF	I	I4	scalar	see 9.10.1 (argument list)
MXINT	I	I4	scalar	" "
MABQ1	I	I4	scalar	" "
MABQ2	I	I4	scalar	" "
MABQ3	I	I4	scalar	" "
MRF	I	I4	scalar	" "
MRFP	O	I4	scalar	" "
*	-	-	-	RETURN1 is done in the case of serious errors
*	-	-	-	RETURN2 is done, if MRFP is set to 1 in the subroutine

Used common blocks (with an explanation of the quantities):

```

BLANK COMMON MAT,NR1(2),NO
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,
              GLSCH,MNFTYP,NFTYP
COMMON/CFSDUR/IDUR
    
```

All quantities are explained in 9.10.1. (NO is NOUTP, NR1(2) is a dummy array). The mode is I for all variables, with the exception of NFTYP, which has the mode IO.

Called subprograms:

```

FSTOLE
FSWROO
FSWRO1
FSWRO2
FSWRO3
FSWRO5
FSWRO6
FSWRO7
NDFLOC
    
```

} (entries of FSWROO)

9.10.3 Subroutine FSTRU1

Problem solved:

Test of the existence of the cross section types σ_a , σ_e , σ_t and $\bar{\mu}_e$.

Definition:

```
SUBROUTINE FSTRU1(*)
```

Explanation of the arguments:

RETURN1 is done if at least one of the cross section types σ_a , σ_e , σ_t or $\bar{\mu}_e$ is not existant.

Used common blocks (with an explanation of the quantities):

```
BLANK COMMON MAT
```

```
COMMON/CFSTRU/TEST1,TEST2,TEST3,LERMSG
```

All the quantities are explained in 9.10.1 with all quantities having the mode I.

Called subprograms:

```
FSWROO
```

```
FSWRO4      (entry of FSWROO)
```

```
NDFLOC
```

9.10.4 Subroutine FSTRU2

Problem solved:

Printing some values for the actual energy group. Setting and printing of integration ranges, integration modes and weighting functions within this group.

Definition:

```
SUBROUTINE FSTRU2(IGR,NE,ENG,NIBER,MIBER,  
                  GIBER,MIBERP,IIBER,CIBER,  
                  NENBER,ENBER,NWFUN,CONWFU,  
                  *)
```

Explanation of the arguments:

name	mode	type	dimension	remarks
IGR	I	I4	scalar	actual group number
NE	I	I4	scalar	see 9.10.1 (argument list)
ENG	I	R4	(NE)	" "
NIBER	O	I4	scalar	number+1 of the integration ranges within the energy group
MIBER	I	I4	scalar	see 9.10.1 (argument list)
GIBER	O	R4	(MIBER)	" "
MIBERP	O	I4	scalar	" "
LIBER	O	I4	(MIBER)	" "
CIBER	O	R4	(MIBER)	" "
NENBER	I	I4	scalar	" "
ENBER	I	R4	(NENBER)	" "
NWFUN	I	I4	(NENBER)	" "
CONWFU	I	R4	(NENBER)	" "
*	-	-	-	RETURN1 is done for MIBERP > 0

Used common blocks (with an explanation of the quantities):

```
BLANK COMMON MAT,NR1(2),NO
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH
```

All quantities are explained in 9.10.1. NR1(2) is a dummy array. All quantities have the mode I.

Called subprograms:

```
FSTOLE
FSWROO
FSWRO3      (entry of FSWROO)
```

9.10.5 Subroutine FSTRU3

Problem solved:

Representation of the pointwise given weighting function by parts of straight lines.

Definition:

```
SUBROUTINE FSTRU3(NFE,REFE,EFE,
                  NABWF,MABWF,ABWF,MABWFP,
                  *,*)
```

Explanation of the arguments:

name	mode	type	dimension	remarks
NFE	I	I4	scalar	see 9.10.1 (argument list)
REFE	I	R4	(NFE)	" "
EFE	I	R4	(NFE)	" "
NABWF	O	I4	scalar	number + 1 of straight line parts
MABWF	I	I4	scalar	see 9.10.1 (argument list)
ABWF	O	R4	(MABWF,4)	" "
MABWFP	O	I4	scalar	" "
*	-	-	-	RETURN 1 is done if MABWF has been too small. MABWFP > 0 gives the necessary increase.
*	-	-	-	RETURN 2 is done, if the energy range of the weighting spectrum does not cover the integration range.

Used common blocks (with an explanation of the quantities):

```
BLANK COMMON NR1(4),NO
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH,
              NR2(4),UGR,OGR
```

All quantities are explained in 9.10.1. NR1 and NR2 are dummy array.
NO is NOUTP. The mode is I for all quantities.

Called subprograms:

```

FSTOLE
FSWRO2 }
FSWRO3 } (entries of FSWROO)
FSWRO7 }
    
```

9.10.6 Subroutine FSTRU4

Problem solved:

Groupwise calculation of self shielding factors and average cross sections for infinite dilution out of the integral values. Output of the calculated quantities.

Definition:

```

SUBROUTINE FSTRU4(ENG,NE,IGR,FFAKT,
                  MI,SIGO,
                  RPHI,RABS,RELA,RTOT,RFISS,RELFL,
                  RF,MRF,ISPATE)
    
```

Explanation of the arguments:

name	mode	type	dimension	remarks
ENG	I	R4	(NE)	see 9.10.1 (argument list)
NE	I	I4	scalar	" "
IGR	I	I4	scalar	actual group number
FFAKT	L	R4	(MI,6)	local storage of groupwise self shielding factors
MI	I	I4	scalar	number of σ_0 -values
SIGO	I	R4	(MI)	σ_0 -values
RPHI	I	R4	scalar	result of $\int_{UGR}^{OGR} F(E)dE$ ($F(E)$ = weighting function)

name	mode	type	dimension	remarks
RABS	I	R4	scalar	result of $\int_{UGR}^{OGR} \sigma_a(E) \cdot F(E) \cdot dE$
RELA	I	R4	scalar	result of $\int_{UGR}^{OGR} \sigma_e(E) \cdot F(E) \cdot dE$
RTOT	I	R4	scalar	result of $\int_{UGR}^{OGR} \sigma_t(E) \cdot F(E) \cdot dE$
RFISS	I	R4	scalar	result of $\int_{UGR}^{OGR} \sigma_f(E) \cdot F(E) \cdot dE$
RELFL	I	R4	scalar	result of $\int_{UGR}^{OGR} \sigma_e(E) \cdot F(E) \cdot dE$
RF	I	R4	(MI,MRF)	results of integrations necessary for the calculation of the self shielding factors
MRF	I	I4	scalar	see 9.10.1 (argument list)
ISPATE	I	I4	scalar	" "

Used common blocks (with an explanation of the quantities):

```
BLANK COMMON MAT,NR1(2),NOUTP,JA,NANF,NEND
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG
COMMON/CFSDUR/ IDUR
```

All quantities are explained in 9.10.1. NR1 is a dummy array. All quantities have the mode I.

Called subprograms:

```
FSSNGL
FSWROO
FSWRO1
FSWRO2
FSWRP3
FSWRO6
```

} (entries of FSWROO)

9.10.7 Function FSSNGL

Problem solved:

Truncation of the REAL*8 number A to the REAL*4 value FSSNGL. If necessary rounding up is done.

Definition:

```
FUNCTION FSSNGL(A)
```

Explanation of the argument:

name	mode	type	dimension	remarks
A	I	R8	scalar	value to be truncated

Used common blocks:

No common blocks are used.

Called subprograms:

No subprograms are called.

9.10.8 Subroutine FSTRU5

Problem solved:

The contents of the array A1 is stored into the array A2.

Definition:

```
SUBROUTINE FSTRU5(A1,NA1,MA1,  
                  A2,NA2,MA2,MA2P,*)
```


Explanation of the arguments:

name	mode	type	dimension	remarks
A1	I	R4	(MA1)	array of which the contents are stored in A2
NA1	I	I4	scalar	number of elements of A1 to be stored in A2
MA1	I	I4	scalar	maximum dimension of array A1
A2	O	R4	(MA2)	array which is receiving the contents of A1
NA2	O	I4	scalar	after RETURN NA2 has the same value as NA1
MA2	I	I4	scalar	maximum dimension of array A2
MA2P	O	I4	scalar	is set to NA1-MA2 if NA1 is greater than MA2
*	-	-	-	RETURN 1 is done if NA1 is greater than MA2

Used common blocks:

None

Called subprograms:

None

9.10.9 Subroutine FSQUER

Problem solved:

Retrieval of the cross sections for a specified energy group. Calculation of the straight line parameters.

Definition:

```
SUBROUTINE FSQUER(TYP,UGR,OGR
                  NAB,MAB,AB,MABP,
                  *,*)
```

Explanation of the arguments:

name	mode	type	dimension	remarks
TYP	I	R8	scalar	name of the cross section type
UGR	I	R4	scalar	lower energy limit
OGR	I	R4	scalar	upper energy limit
NAB	O	I4	scalar	number + 1 of straight line parameters
MAB	I	I4	scalar	maximal possible value for NAB
AB	O	R4	(MAB,4)	straight line parameters
MABP	O	I4	scalar	necessary increase of MAB if MABP is greater than zero
*	-	-	-	RETURN 1 is made, if the array AB has been too small
*	-	-	-	RETURN 2 is made for serious errors of the KEDAK-data

Used common blocks (with an explanation of the quantities):

```
BLANK COMMON MAT,NR1(2),NO
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH
```

All quantities are explained in 9.10.1. NR1 is a dummy array. NO is NOUTP. The mode for all quantities is I.

Called subprograms:

```
FSTOLE
FSWRO0
FSWRO2
FSWRO3
FSWRO4
FSWRO5
FSWRO6
FSWRO7
NDFLOC
```

} (entries of FSWRO0)

9.10.10 Subroutine FSWROO

Problem solved:

Control of printing messages, warnings, and error messages.

Definition:

```

SUBROUTINE  FSWROO(N)
ENTRY      FSWRO1(N,IV1)
ENTRY      FSWRO2(N,IV1,IV2)
ENTRY      FSWRO3(N,IV1,IV2,IV3)
ENTRY      FSWRO4(N,IV1,IV2,IV3,IV4)
ENTRY      FSWRO5(N,IV1,IV2,IV3,IV4,IV5)
ENTRY      FSWRO6(N,IV1,IV2,IV3,IV4,IV5,IV6)
ENTRY      FSWRO7(N,IV1,IV2,IV3,IV4,IV5,IV6,IV7)
ENTRY      FSWRO8(N,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8)
ENTRY      FSWRO9(N,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8,IV9)
    
```

Explanation of the arguments:

name	mode	type	dimension	remarks
N	I	I4	scalar	selection of the message, warning or error message.
IV1 to IV9	I	B4	scalar	additional information given to the printing routines. The type of IV1 to IV9 depends on the number N .

Used common blocks (with an explanation of the quantities):

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSWROO .
NO	I	I4	scalar	5	print output unit number .

name of the common block: CFSTRF					
name	mode	type	dimension	word	remarks
FELARR	0	I4	(NGMAX,3)	1	storage of the message, warning and error numbers that have been appeared
NGMAX	0	I4	scalar	55	maximal possible first index in FELARR (= 18)

Called subprograms:

FSWRS1

FSWRS2

FSWRS3

9.10.11 Subroutine FSWRS1

Problem solved:

Printout of messages.

Definition:

```
SUBROUTINE FSWRS1(NI,IV1,IV2,IV3,
                  IV4,IV5,IV6,
                  IV7,IV8,IV9,*)
```

Explanation of the arguments:

name	mode	type	dimension	remarks
NI	I	I4	scalar	see 9.10.10 (argument list) argument N.
IV1 to IV9	I	B4	scalar	see 9.10.10 (argument list) .
*	-	-	-	RETURN 1 is done, if NI has an invalid value.

Used common blocks (with an explanation of the quantities):

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSWRS1
NO	I	I4	scalar	5	print output unit number

Called subprograms:

None.

9.10.12 Subroutine FSWRS2

Problem solved:

Printout of warnings.

Definition:

```
SUBROUTINE FSWRS2(NI,IV1,IV2,IV3,
                  IV4,IV5,IV6,
                  IV7,IV8,IV9,*)
```

Explanation of the arguments:

name	mode	type	dimension	remarks
NI	I	I4	scalar	see 9.10.10 (argument list) argument N
IV1 to IV9	I	B4	scalar	see 9.10.10 (argument list)
*	-	-	-	RETURN 1 is done, if NI has an invalid value

Used common blocks (with an explanation of the quantities):

BLANK COMMON NR1(4),NO

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSWRS2
NO	I	I4	scalar	5	print output unit number

Called subprograms: None.

9.10.13 Subroutine FSWRS3

Problem solved:

Printout of error messages.

Definition:

```
SUBROUTINE FSWRS3(NI,IV1,IV2,IV3,  
                  IV4,IV5,IV6,  
                  IV7,IV8,IV9,*)
```

Explanation of the arguments:

name	mode	type	dimension	remarks
NI	I	I4	scalar	see 9.10.10 (argument list) argument N
IV1 to IV9	I	B4	scalar	see 9.10.10 (argument list)
*	-	-	-	RETURN 1 is done, if NI has an invalid value

Used common blocks (with an explanation of the quantities):

BLANK COMMON NR1(4), NO

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSWRS3
NO	I	I4	scalar	5	print output unit number

Called subprograms:

None.

9.10.14 Subroutine FSWRS9

Problem solved:

Printout of the array FELARR (see 9.10.10 explanation of the quantities in the common blocks).

Definition:

SUBROUTINE FSWRS9

Used common blocks (with an explanation of the quantities):

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSWRS9
NO	I	I4	scalar	5	print output unit number

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
TEST1	I	L4	scalar	1	see 9.10.1 (common blocks)
TEST2	I	L4	scalar	2	" "
TEST3	I	L4	scalar	3	" "
LERMSG	I	L4	scalar	4	" "

name of the common block: CFSTRF					
name	mode	type	dimension	word	remarks
FELARR	I	I4	(NGMAX,3)	1	see 9.10.10 (common blocks)
NGMAX	I	I4	scalar	55	" "

Called subprograms:

A8FORM	}	(entries of A8FORM)
RAMANF		
RAMEND		

9.10.15 Function FSTOLE

Problem solved:

Test of $\frac{|A-B|}{\max(|A|,|B|)} \leq \text{GLSCH}$. If true FSTOLE is set to.TRUE., else ist is set to .FALSE.

Definition:

LOGICAL FUNCTION FSTOLE(A,B,GLSCH)

Explanation of the arguments:

name	mode	type	dimension	remarks
A	I	R4	scalar	first number
B	I	R4	scalar	second number
GLSCH	I	R4	scalar	see problem solved

Used common blocks:

None

Called subprograms:

None

9.10.16 Subroutine FSXINT

Problem solved:

Construction of the energy grid used as integration basis.

Definition:

SUBROUTINE FSXINT(NXINT,MXINT,XINT,MXINTP,
 NV,V,ID1,ID2,*)
ENTRY FSXIIN(NXINT,MXINT,XINT,UGR,OGR)

(UGR and OGR are stored in XINT. The rest of the array is set equal -1.0).

Explanation of the arguments:

name	mode	type	dimension	remarks
NXINT	0	I4	scalar	number of energy points
MXINT	I	I4	scalar	dimension of XINT
XINT	0	R4	(MXINT)	energy grid
MXINTP	0	I4	scalar	see 9.10.1 (argument list)
NV	I	I4	scalar	number of points in V
V	I	R4	(ID1, ID2)	V(I,1) = points to be inserted in XINT, if the condition $UGR \leq V(I,1) \leq OGR$ is fulfilled
ID1	I	I4	scalar	used for dimensioning V
ID2	I	I4	scalar	used for dimensioning V
*	-	-	-	RETURN 1 is done, if the array XINT is too small
UGR	I	R4	scalar	lower energy group (or integration range) boundary
OGR	I	R4	scalar	upper energy group (or integration range) boundary

Used common blocks (with an explanation of the quantities:

```
BLANK COMMON NR1(4),NO
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH
```

All quantities are explained in 9.10.1. They have all the mode I.
NR1 is a dummy array, NO is NOUTP.

Called subprograms:

```
FSTOLE
FSWRO3 (entry of FSWROO)
```

9.10.17 Subroutine FSGRAL

Problem solved:

Control of the integration of the functions

$\text{PHI}(E)$, $F1(E) \cdot \text{PHI}(E)$, $F1(E) \cdot F2(E) \cdot \text{PHI}(E)$,

$$\frac{1}{F3(E)} * \text{PHI}(E), \quad \frac{1}{(F3(E))^2} * \text{PHI}(E),$$

$$\frac{F1(E)}{F3(E)} * \text{PHI}(E), \quad \frac{F1(E)}{(F3(E))^2} * \text{PHI}(E),$$

$$\frac{F1(E) * F2(E)}{F3(E)} * \text{PHI}(E), \quad \frac{F1(E) * F2(E)}{(F3(E))^2} * \text{PHI}(E)$$

Definition:

```

SUBROUTINE FSGRAL (RESULT, NXINT, XINT,
                  NABWF, ABWF, MABWF,
                  NABQ1, ABQ1, MABQ1,
                  NABQ2, ABQ2, MABQ2,
                  NABQ3, ABQ3, MABQ3,
                  KMROM, AUXROM, KMROMP, EPSROM, DRINWA,
                  IFAR, LFAR, LFARA,
                  FARIN, FARAN, IFUNAR, *, *)
    
```

Explanation of the arguments:

name	mode	type	dimension	remarks
RESULT	0	R8	scalar	result of the integration
NXINT	I	I4	scalar	see 9.10.16 (argument list)
XINT	I	R4	(NXINT)	" "

name	mode	type	dimension	remarks
NABWF	I	I4	scalar	see 9.10.5 (argument list)
ABWF	I	R4	(MABWF,4)	" "
MABWF	I	I4	scalar	" "
NABQ1	I	I4	scalar	number of data in ABQ1
ABQ1	I	R4	(MABQ1,4)	see 9.10.1 (argument list)
MABQ1	I	I4	scalar	" "
NABQ2	I	I4	scalar	number of data in ABQ2
ABQ2	I	R4	(MABQ2,4)	see 9.10.1 (argument list)
MABQ2	I	I4	scalar	" "
NABQ3	I	I4	scalar	number of data in ABQ3
ABQ3	I	R4	(MABQ3,4)	see 9.10.1 (argument list)
MABQ3	I	I4	scalar	" "
KMROM	I	I4	scalar	" "
AUXROM	L	R8	(KMROM)	" "
KMROMP	O	I4	scalar	" "
EPSROM	I	R4	scalar	" "
DRINWA	I	R4	scalar	" "
IFAR	I	I4	scalar	local index for exact attachement of error appearance in a loop
LFAR	IO	L4	(2,3)	used for collected error printout
LFARA	IO	L4	(2,3)	" " " " "
FARIN	O	R4	(2,3,2)	storage of energy range for collected error printout
FARAN	O	R4	(2,3)	storage of σ_0 for collected error printout
IFUNAR	O	I4	(2,3)	additional information for collected error printout
*	-	-	-	RETURN 1 is done, if AUXROM is too small
*	-	-	-	RETURN 2 is done, if there are σ_t cross section values less or equal zero

Used common blocks (with an explanation of the quantities):

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSGRAL
NO	I	I4	scalar	5	print output unit number

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
TEST1	I	L4	scalar	1	see 9.10.1 (common blocks)
TEST2	I	L4	scalar	2	" "
TEST3	I	L4	scalar	3	" "
LERMSG	I	L4	scalar	4	" "
GLSCH	I	R4	scalar	5	" "
MNFTYP	I	I4	scalar	6	" "
NFTYP	I	I4	scalar	7	" "
ITYP	I	I4	scalar	8	" "
ITYPFU	I	I4	scalar	9	" "
NR2	-	I4	(3)	10	dummy array. Not used in FSGRAL
AW	0	R4	scalar	13	straight line parameter for weighting function
BW	0	R4	scalar	14	straight line parameter for weighting function
A1	0	R4	scalar	15	straight line parameter for σ_t , σ_a , σ_e or σ_f
B1	0	R4	scalar	16	straight line parameter for σ_t , σ_a , σ_e or σ_f
A2	0	R4	scalar	17	straight line parameter for $\bar{\mu}_e$
B2	0	R4	scalar	18	" " " "
A3	0	R4	scalar	19	straight line parameter for σ_t
B3	0	R4	scalar	20	" " " "

name of the common block: CFSTRU					(continuation)
name	mode	type	dimension	word	remarks
BSIGO	I	R4	scalar	21	actual σ_0 -value
XIA	0	R4	scalar	22	lower limit of subinterval for the integration
XIE	0	R4	scalar	23	upper limit of subinterval for the integration
L	0	I4	scalar	24	points to the respective formulae for analytic integration
Y	L	R8	scalar	25	result for [XIA,XIE] integration of the functions
NDIMP	0	I4	scalar	27	if > 0 necessary increase for KMROM
DRUCKL	L	L4	scalar	28	control of printing in the case of errors

Called subprograms:

DPHI
 FSANO2
 FSANO3
 FSANO4
 FSANO5
 FSANO6
 FSANO7
 FSANO8
 FSANO9
 FSEXIN
 FSGRA1
 FSGRA2
 FSGRA3
 FSNUO1
 FSNUO2
 FSNUO3
 FSNUO4
 FSNUO5
 FSNUO6
 FSNUO7
 FSNUO8
 FSNUO9
 FSROMB
 FSROMI (entry of FSROMB)
 FSTOLE
 FSWROO
 FSWRO1
 FSWRO3
 FSWRO4
 FSWRO9

} (entries of FSWROO)

9.10.18 Function FSNU01

Problem solved:

Calculation of the function (with double precision)

$AW \cdot X + BW$

($AW \cdot X + BW$ is the representation of the pointwise given weighting function).

Definition:

REAL FUNCTION FSNU01 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU01
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function

Called subprograms:

None

9.10.19 Function_FSNU02

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot (AI \cdot X + BI)$$

(AW · X + BW is the representation of the pointwise given weighting function).

Definition:

REAL FUNCTION FSNU02 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU02
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function
AI	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
BI	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f

Called subprograms:

None

9.10.20 Function FSNU03

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot (A1 \cdot X + B1) \cdot (A2 \cdot X + B2)$$

(AW · X + BW is the representation of the pointwise given weighting function)

Definition:

```
REAL FUNCTION FSNU03 * 8(X)
```

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU03
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
A2	I	R4	scalar	17	straight line parameter for $\bar{\mu}_e$
B2	I	R4	scalar	18	straight line parameter for $\bar{\mu}_e$

Called subprograms:

None

9.10.21 Function FSNU04

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot \frac{1}{A3 \cdot X + B3 + BSIGO}$$

(AW · X + BW is the representation of the pointwise given weighting function).

Definition:

REAL FUNCTION FSNU04 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU04
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function
NR2	-	I4	(4)	15	dummy array. Not used in FSNU04
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.22 Function FSNU05

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot \frac{1}{(A3 \cdot X + B3 + BSIGO)^2}$$

(AW · X + BW is the representation of the pointwise given weighting function).

Definition:

REAL FUNCTION FSNU05 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU05
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function .
NR2	-	I4	(4)	15	dummy array. Not used in FSNU05 .
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_0 -value

Called subprograms:

None

9.10.23 Function FSNU06

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot \frac{(A1 \cdot X + B1)}{(A3 \cdot X + B3 + BSIGO)}$$

(AW · X + BW is the representation of the pointwise given weighting function).

Definition:

REAL FUNCTION FSNU06 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU06
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
NR2	-	I4	(2)	17	dummy array. Not used in FSNU06
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value .

Called subprograms:

None

9.10.24 Function FSNU07

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot \frac{A1 \cdot X + B1}{(A3 \cdot X + B3 + BSIGO)^2}$$

(AW · X + BW is the representation of the pointwise given weighting function).

Definition:

REAL FUNCTION FSNU07 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU07
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
NR2	-	I4	(2)	17	dummy array. Not used in FSNU06
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.25 Function FSNU08

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot \frac{(A1 \cdot X + B1) \cdot (A2 \cdot X + B2)}{(A3 \cdot X + B3 + BSIGO)}$$

(AW · X + BW is the representation of the pointwise given weighting function)

Definition:

REAL FUNCTION FSNU08 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU08
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
A2	I	R4	scalar	17	straight line parameter for $\bar{\mu}_e$
B2	I	R4	scalar	18	" " " " "
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms

None

9.10.26 Function FSNU09

Problem solved:

Calculation of the function (with double precision)

$$(AW \cdot X + BW) \cdot \frac{(A1 \cdot X + B1) \cdot (A2 \cdot X + B2)}{(A3 \cdot X + B3 + BSIGO)^2}$$

(AW · X + BW is the representation of the pointwise given weighting function)

Definition:

REAL FUNCTION FSNU09 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(12)	1	dummy array. Not used in FSNU09
AW	I	R4	scalar	13	straight line parameter for the weighting function
BW	I	R4	scalar	14	straight line parameter for the weighting function
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
A2	I	R4	scalar	17	straight line parameter for $\bar{\mu}_e$
B2	I	R4	scalar	18	" " " " "
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.27 Function DPHI

Problem solved:

Calculation of the function (with double precision)

1/E

Definition:

REAL FUNCTION DPHI * 8(E)

Explanation of the argument:

name	mode	type	dimension	remarks
E	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks:

None

Called subprograms:

None

9.10.28 Function FSANO2

Problem solved:

Calculation of the function (with double precision)

DPHI + (A1 * X + B1)

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSANO2 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(14)	1	dummy array. Not used in FSANO2
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f

Called subprograms:

None

9.10.29 Function FSAN03

Problem solved:

Calculation of the function (with double precision)

$$DPHI \cdot (A1 \cdot X + B1) \cdot (A2 \cdot X + B2)$$

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSAN03 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(14)	1	dummy array. Not used in FSAN03
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
A2	I	R4	scalar	17	straight line parameter for $\bar{\mu}_e$
B2	I	R4	scalar	18	" " " " "

Called subprograms:

None

9.10.30 Function FSANO4

Problem solved:

Calculation of the function (with double precision)

$$\text{DPHI} = \frac{1}{(A3 \cdot X + B3 + \text{BSIGO})}$$

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSANO4 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(18)	1	dummy array. Not used In FSANO4
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.31 Function FSN05

Problem solved:

Calculation of the function (with double precision)

$$\text{DPHI} \cdot \frac{1}{(A3 \cdot X + B3 + \text{BSIGO})^2}$$

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSN05 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(18)	1	dummy array. Not used in FSN05
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.32 Function FSANO6

Problem solved:

Calculation of the function (with double precision)

$$DPHI = \frac{A1 \cdot X + B1}{(A3 \cdot X + B3 + BSIGO)}$$

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSANO6 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(14)	1	dummy array. Not used in FSANO6
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
NR2	-	I4	(2)	17	dummy array. Not used in FSANO7
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.33 Function FSANO7

Problem solved:

Calculation of the function (with double precision)

$$\text{DPHI} = \frac{A1 \cdot X + B1}{(A3 \cdot X + B3 + \text{BSIGO})^2}$$

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSANO7 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(14)	1	dummy array. Not used in FSANO7
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
NR2	-	I4	(2)	17	dummy array. Not used in FSANO7
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.34 Function FSAN08

Problem solved:

Calculation of the function (with double precision)

$$\text{DPHI} = \frac{(A1 \cdot X + B1) \cdot (A2 \cdot X + B2)}{(A3 \cdot X + B3 + \text{BSIGO})}$$

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSAN08 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(14)	1	dummy array. Not used in FSAN08 .
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f -
A2	I	R4	scalar	17	straight line parameter for $\bar{\mu}_e$
B2	I	R4	scalar	18	" " " " "
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.35 Function FSAN09

Problem solved:

Calculation of the function (with double precision)

$$\text{DPHI} \cdot \frac{(A1 \cdot X + B1) \cdot (A2 \cdot X + B2)}{(A3 \cdot X + B3 + \text{BSIGO})^2}$$

(DPHI(X) is the program built in weighting function)

Definition:

REAL FUNCTION FSAN09 * 8(X)

Explanation of the argument:

name	mode	type	dimension	remarks
X	I	R8	scalar	energy value for which the function is to be calculated

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(14)	1	dummy array. Not used in FSAN09
A1	I	R4	scalar	15	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
B1	I	R4	scalar	16	straight line parameter for $\sigma_t, \sigma_a, \sigma_e$ or σ_f
A2	I	R4	scalar	17	straight line parameter for $\bar{\mu}_e$
B2	I	R4	scalar	18	" " " " "
A3	I	R4	scalar	19	straight line parameter for σ_t
B3	I	R4	scalar	20	" " " " "
BSIGO	I	R4	scalar	21	σ_o -value

Called subprograms:

None

9.10.36 Subroutine FSEXIN

Problem solved:

Analytical integration of the functions described in 9.10.18 to 9.10.26 and 9.10.27 to 9.10.34 with $DPHI(X) = \frac{1.0}{X}$.

Definition:

SUBROUTINE FSEXIN

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(11)	1	dummy array. Not used in FSEXIN
CONST	I	R4	scalar	12	see 9.10.1 (common blocks)
AW	I	R4	scalar	13	see 9.10.17 (common blocks)
BW	I	R4	scalar	14	" "
A1	I	R4	scalar	15	" "
B1	I	R4	scalar	16	" "
A2	I	R4	scalar	17	" "
B2	I	R4	scalar	18	" "
A3	I	R4	scalar	19	" ""
B3	I	R4	scalar	20	" "
BSIGO	I	R4	scalar	21	" "
XIA	I	R4	scalar	22	" "
XIE	I	R4	scalar	23	" "
L	I	I4	scalar	24	" "
Y	O	R8	scalar	25	" "

Called subprograms:

FSLOMQ

FSWRO3 (entry of FSWROO)

9.10.37 Function FSLOMQ

Problem solved:

With $Q = F \cdot (XIE - XIA) / (1 + F \cdot XIA)$ the function calculates - with double precision - $\log(1 + Q) - Q + 0.5 \cdot Q^2$ by using an expansion into series. The value is calculated with an relative error less or equal 10^{-15} .

Definition:

REAL FUNCTION FSLOMQ * 8(XIE,XIA,F)

Explanation of the arguments:

name	mode	type	dimension	remarks
XIE	I	R8	scalar	see problem solved
XIA	I	R8	scalar	" " "
F	I	R8	scalar	" " "

Used common blocks (with explanations of the quantities):

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSLOMQ
NO	I	I4	scalar	5	print output unit number

Called subprograms:

FSWRO3 (entry of FSWROO)

9.10.38 Function FSGRA1

Problem solved:

Checks if all straight line parameter ranges cover the integration sub-interval.

Definition:

LOGICAL FUNCTION FSGRA1(AB,IAB,MAB,XIA,XIE)

Explanation of the arguments:

name	mode	type	dimension	remarks
AB	I	R4	(MAB,4)	straight line parameters
IAB	I	I4	scalar	pointer to the actual straight line parameter set
MAB	I	I4	scalar	used for dimensioning AB
XIA	I	R4	scalar	lower limit of integration sub-interval
XIE	I	R4	scalar	upper limit of integration sub-interval

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSGRA1
GLSCH	I	R4	scalar	5	see 9.10.1 (common blocks)

Called subroutines:

FSTOLE

9.10.39 Subroutine FSGRA2

Problem solved:

Localisation of the actual straight line parameters. Testing if cross sections are zero or less than zero or if they are changing the sign.

Definition:

```

SUBROUTINE FSGRA2(IFUN,AB,IAB,MAB,NAB,
                  XIA,XIE,XIEE,SPRUO,SPRU3,
                  IFAR,LFAR,LFARA,
                  FARIN,FARAN,IFUNAR,
                  NUDUR)
    
```

Explanation of the arguments:

name	mode	type	dimension	remarks
IFUN	I	I4	scalar	selection of (A1,B1),(A2,B2) or (A3,B3)
AB	I	R4	(MAB,4)	straight line parameters
IAB	IO	I4	scalar	pointer to the actual straight line parameter set
MAB	I	I4	scalar	used for dimensioning AB
NAB	I	I4	scalar	maximum value of IAB
XIA	I	R4	scalar	lower subinterval limit
XIE	I	R4	scalar	upper subinterval limit
XIEE	IO	R4	scalar	XIEE \geq XIE. energy value until which - starting at XIA - the cross section is zero or has any error
SPRUO	IO	L4	scalar	test control. Switch for some tests
SPRU3	O	L4	scalar	is set .TRUE. if a cross section has been equal zero in the interval [XIA,XIE]
IFAR	I	I4	scalar	see 9.10.17 (argument list)
LFAR	IO	L4	(2,3)	" "

name	mode	type	dimension	remarks
LFARA	O	L4	(2,3)	see 9.10.17 (argument list)
FARIN	IO	R4	(2,3,2)	" "
FARAN	O	R4	(2,3)	" "
IFUNAR	IO	I4	(2,3)	" "
NUDUR	I	L4	scalar	Switch for changing sign test

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
NR1	-	I4	(3)	1	dummy array. Not used in FSGRA2
LERMSG	I	L4	scalar	4	see 9.10.1 (common blocks)
GLSCH	I	R4	scalar	5	" "
NR2	-	I4	(2)	6	dummy array. Not used in FSGRA2
ITYP	I	I4	scalar	8	see 9.10.1 (common blocks)
ITYPFU	I	I4	scalar	9	" "
NR3	-	I4	(5)	10	dummy array. Not used in FSGRA2
A1	O	R4	scalar	15	see 9.10.17 (common blocks)
B1	O	R4	scalar	16	" "
A2	O	R4	scalar	17	" "
B2	O	R4	scalar	18	" "
A3	O	R4	scalar	19	" "
B3	O	R4	scalar	20	" "
BSIGO	I	R4	scalar	21	" "

Called subprograms:

```

FSGRA1
FSTOLE
FSWRO2 }
FSWRO3 } (entries of FSWRO0)
FSWRO4 }

```

9.10.40 Subroutine FSGRA3

Problem solved:

Localisation of the desired straight line parameters for the interval [XIA,XIE]

Definition:

```
SUBROUTINE FSGRA3(AB,IAB,MAB,NAB,  
                  XIA,XIE)
```

Explanation of the arguments:

name	mode	type	dimension	remarks
AB	I	R4	(MAB,4)	see 9.10.38 (argument list)
IAB	IO	I4	scalar	" "
MAB	I	I4	scalar	" "
NAB	I	I4	scalar	maximum value of IAB
XIA	I	R4	scalar	see 9.10.38 (argument list)
XIE	I	R4	scalar	" "

Used Common blocks (with explanations of the quantities):

```
COMMON/CFSTRU/NR1(4),GLSCH
```

All quantities are explained in 9.10.38. All have the same mode.

Called subprograms:

```
FSGRA1  
FSWRO3      (entry of FSWROO)
```

9.10.41 Subroutine FSROMB

Problem solved:

Numerical integration with the Romberg method (see /4/).

Definition:

```
SUBROUTINE FSROMB(FCT,*)
      ENTRY FSROMI(EPS,NDIM,DRINWA,YF,
                  YFEPS,AUX)
```

(Passes the argument addresses to the subroutine)

Explanation of the arguments:

name	mode	type	dimension	remarks
FCT	I	F8	-	name of the function to be integrated
*	-	-	-	RETURN1 is done if the wished accuracy could not be reached within NDIM-1 bisections
EPS	I	R4	scalar	desired integration accuracy
NDIM	I	I4	scalar	NDIM-1 = possible number of bisections
DRINWA	I	R4	scalar	see 9.10.1 (argument list)
YF	IO	R4	(3)	results added for the different classes (see 9.4)
YFEPS	IO	R4	(3)	maximum relative integration error for the results of each class
AUX	L(0)	R4	(NDIM)	auxiliary array (see /4/)

Used common blocks (with explanations of the quantities):

name of the common block: BLANK COMMON					
name	mode	type	dimension	word	remarks
NR1	-	I4	(4)	1	dummy array. Not used in FSROMB
NO	I	I4	scalar	5	print output unit

Used common blocks (with explanations of the quantities):

name of the common block: CFSTRU					
name	mode	type	dimension	word	remarks
TEST1	I	L4	scalar	1	see 9.10.1 (common blocks)
TEST2	I	L4	scalar	2	" "
TEST3	I	L4	scalar	3	" "
LERMSG	I	L4	scalar	4	" "
GLSCH	I	R4	scalar	5	" "
NR2	-	I4	(2)	6	dummy array. Not used in FSROMB
ITYP	I	I4	scalar	8	see 9.10.1 (common blocks)
ITYPFU	I	I4	scalar	9	" "
NR3	-	I4	(11)	10	dummy array. Not used in FSROMB
BSIGO	I	R4	scalar	21	σ_o -value
XL	I	R4	scalar	22	lower integration limit
XH	I	R4	scalar	23	upper integration limit
NR4	-	I4	(1)	24	dummy array. Not used in FSROMB
Y	0	R8	scalar	25	result of the integration
NDIMP	0	I4	scalar	27	if > 0 necessary increase of NDIM
DRUCK	0	L4	scalar	28	is set to .TRUE., if an error printing has been done in the routine

Called subprograms:

FCT (see argument list)

FSWROO

FSWR03 (entry of FSWROO)

9.10.42 Block Data

Problem solved:

Initialisation of IDUR in COMMON/CFSDUR/.

9.10.43 Subroutine A8FORM

Problem solved:

Printing of text with "big" letters.

Definition:

The compiled program is stored in a system library as object code (see /6/).

9.10.44 Subroutine NDF

Problem solved:

Retrieval of KEDAK-data. (see /3/, /2/)

Definition:

The program is used in all parts of MIGROS-3. The definition may be found in /3/.

9.11 References

/1/ H. Huschke, B. Krieg

MIGROS-2: A Program Written in FORTRAN for the Calculation of Microscopic Group Constants from Nuclear Data.

Institut für Neutronenphysik und Reaktortechnik,
Projekt Schneller Brüter,
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KFK 1784, Juni 1973

/2/ B. Goel, B. Krieg

Status of the Nuclear Data Library KEDAK-3 October 1975.

Institut für Neutronenphysik und Reaktortechnik
Gesellschaft für Kernforschung mbH., Karlsruhe

KFK 2234, NEANDC(E) 171 "U" , Dezember 1975

/3/ B. Krieg

Handling and Service Programs for the Karlsruhe Nuclear Data File KEDAK.

Part I: Management and Retrieval Programs

Institut für Neutronenphysik und Reaktortechnik
Gesellschaft für Kernforschung mbH., Karlsruhe

KFK 1725, Juni 1973

/4/ S. Filippi

Das Verfahren von Romberg-Stiefel-Bauer als Spezialfall des allgemeinen Prinzips von Richardson.

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1964

/5/ IBM

System/360 Scientific Subroutine Package.

Version III. Programmer's Manual.

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not published, 1970

10. The calculation of group constants in the thermal group. Module 10

10.1 This module is extended against the version in MIGROS-2 by the calculation of the average total cross section, Besides this three new types are entered into the program for formal reasons, $PROBSGI_{th}$, $SGNCO_{th}$ and CHI (definition see below). These types are used to facilitate the input for a GRUBA /1/ insertion run.

10.2 It is assumed, that the thermal energy range is covered by one energy group. For the cross sections except the elastic scattering cross section a $1/v$ -law is assumed, and for the weighting function a Maxwell distribution at $T = 293.6K$ corresponding to $kT = 0.0253$ eV. The thermal group cross sections for types with a $1/v$ behaviour are then given by (/2/)

$$k_{\sigma_{x,th}} = \frac{\sqrt{\pi}}{2} \cdot k_{\sigma_x}(0.0253 \text{ eV}) \quad (10.1)$$

k = isotope
 x = neutron reaction (n,x) except (n,n) process
 th = thermal

The thermal group cross sections are calculated by formula (10.1) for all types x of neutron reactions, except those for elastic scattering. Furthermore the following group constants are calculated:

- the average elastic scattering cross section

$$k_{\sigma_{n,th}} = k_{\sigma_n}(0.0253 \text{ eV}) \quad (10.2)$$

- the average cosine of the elastic scattering

$$k_{\mu_{e,th}} = k_{\mu_e}(0.0253 \text{ eV}) \quad (10.3)$$

- the average number of secondary neutrons per fission

$$k_{\nu_{th}} = k_{\nu}(0.0253 \text{ eV}) \quad (10.4)$$

- the average α -value

$$k_{\alpha,th}^- = \frac{k_{\sigma_{\gamma,th}}^-}{k_{\sigma_{f,th}}^-} \quad \begin{array}{l} \gamma = \text{radiative capture} \\ f = \text{fission} \end{array} \quad (10.5)$$

- the average η -value

$$k_{\eta,th}^- = \frac{k_{\nu,th}^-}{1 + k_{\alpha,th}^-} \quad (10.6)$$

The assembled group constants are calculated as follows:

- the average capture cross section

$$k_{\sigma_c,th}^- = k_{\sigma_a,th}^- - k_{\sigma_f,th}^- \quad *) \quad (10.7)$$

- the average total cross section

$$k_{\sigma_t,th}^- = k_{\sigma_n,th}^- + k_{\sigma_a,th}^- + k_{\sigma_i,th}^- + k_{\sigma_{2n},th}^- \quad (10.8)$$

For obtaining consistence with the data included in the GRUBA-library, it is necessary to set the following types in this module:

- the inelastic scattering matrice in the thermal group

$$\text{PROBSGI}_{th} = 1. \quad (10.9)$$

- the elastic scattering matrice in the thermal group

$$\text{SGNCO}_{th} = 1. \quad (10.10)$$

- in the case of a fissile isotope the fission spectrum in the thermal group

$$\text{CHI} = 0. \quad (10.11)$$

10.3 The following subroutine is necessary:

THERM (NE, NTY, TYP)

*) Definition of the absorption cross-section σ_a (KEDAK-type SGA)

$$\sigma_a = \sigma_{\gamma} + \sigma_f + \sigma_p + \sigma_d + \sigma_{\alpha} \quad (\text{see } /?)$$

The following parameters are defined by the control program:

NE : number of energy group limits
NTY : number of cross section types
TYP(NTY) : one-dimensional field containing
the cross section types.

References

- /1/ D. Woll
Aufbau und Verwaltung der Gruppenkonstantenbibliothek GRUBA
KFK 1815, 1973
- /2/ K.H. Beckurts, K. Wirtz
Neutron Physics, Springer Verlag Berlin, Göttingen,
Heidelberg, New York, 1964, pages 98 - 100
- /3/ B. Goel, B. Krieg
Status of the Nuclear Data Library KEDAK-3
October 1975
KFK 2234, NEANDC(E) 171 >>U<<, 1975

11. The calculation of the weighted average $1/v$ values. Module 8

11.1 The difference between the program version in MIGROS-2 and in MIGROS-3 is a more exact method of integration. In the case of a pointwise given weighting function the MIGROS-2 version uses only the energy points of the weighting function and the energy group limits as integration points. The MIGROS-3 version starts with the same energy points and calculates the numerator and the denominator of formula 11.2. Then the distance between the integration points is bisected and the numerator and the denominator is calculated once more. This technique is continued until the relative deviation of the numerator integral calculated with n and $2*n$ energy points and of the denominator integral calculated with n and $2*n$ energy points is less than or equal to a given error limit ϵ . In the case of a weighting function given as analytic function the numerator and the denominator integral is calculated starting with 10 equidistant energy points in the respective energy group. Then the number of energy points is doubled and the calculation is done once more. This technique is stopped if the error limit is reached as explained above.

11.2 The average $1/v$ values are defined as

$$\left(\frac{1}{v}\right)_g = \frac{\int_{(g)} \frac{1}{v} \cdot F(E) dE}{\int_{(g)} F(E) dE} \quad (11.1)$$

11.3 The numerical integration is performed by the following formula:
(trapezoidal rule)

$$\left(\frac{1}{v}\right)_g = c \cdot \frac{\sum_{i=1}^n \left\{ \frac{F(E_i)}{\sqrt{E_i}} + \frac{F(E_{i+1})}{\sqrt{E_{i+1}}} \right\} \cdot \{E_{i+1} - E_i\}}{\sum_{i=1}^n \{F(E_i) + F(E_{i+1})\} \cdot \{E_{i+1} - E_i\}} \quad (11.2)$$

i : index of the integration points
E_i : integration points in energy group g
F(E_i) : weighting function
n : number of integration points in energy group g
c : constant = 7.229286 · 10⁻⁷

In the thermal group the 1/v value is set equal to $\frac{1}{2}\sqrt{\pi} \cdot \frac{c}{\sqrt{0.0253}}$.

11.4 The following subroutine is used:

EDV (NE, ENG, NSP, E, F, EPS, V, NEF, ST, FI, IW)

The following parameters must be defined:

NE : number of energy group boundaries
ENG(NE) : energy group boundaries in [eV]
NSP : number of energy points of the weighting function
E(NSP) : energy points of the weighting function in [eV]
F(NSP) : weighting function at the energy points E(NSP)
EPS : permissible integration error
NEF : dimension of the working fields ST and FI

V(NE), ST(NEF) and FI(NEF) are one-dimensional working fields, IW is a control word internally used .

12. The calculation of the fission spectrum. Module 7

12.1 The program version included in MIGROS-2 calculates the Watt-Cranberg fission spectrum using the KEDAK data type CHICR, /2/, which contains the corresponding parameters. For some isotopes the data type CHICR is not available on the KEDAK library. In such cases the module version included in MIGROS-3 calculates the Maxwellian spectrum using the KEDAK type SEDF, /2/, with the argument K=2 meaning that a Maxwell model is used and the first functional value p=1 meaning the fraction of the spectrum to the total energy distribution. Note, that if the highest energy group boundary is greater than or equal to 10.E6 eV this boundary is set equal to 20.E6 eV because otherwise

NE
 $\sum_{i=1}^{NE} \chi_i$ is not close enough to 1. (Summation is carried out over all energy groups.)

12.2 Calculation of the Watt-Cranberg spectrum

$$\chi(E) = \frac{\exp\{-\frac{E_f}{T}\}}{\sqrt{\pi \cdot E_f \cdot T}} \cdot \exp\{-\frac{E}{T}\} \cdot \sinh\{\frac{2}{T} \sqrt{E \cdot E_f}\} \quad (12.1)$$

E energy in MeV,

E_f fragment kinetic energy per nucleon in MeV,

T Watt fragment nuclear "temperature" in MeV.

The fission spectrum in energy group g is defined as

$$\chi_g = \int_{(g)} \chi(E) dE \quad (12.2)$$

E_g upper group limit in MeV,

E_{g+1} lower group limit in MeV.

Using formula (12.1) one gets

$$\begin{aligned} \chi_g = & \frac{1}{2 \cdot \sqrt{\pi}} \sqrt{\frac{T}{E_f}} \cdot \{ \exp(-x_{g+1}^2) - \exp(-x_g^2) - \exp(-y_{g+1}^2) \\ & + \exp(-y_g^2) \} - \frac{1}{2} \{ \operatorname{erf}(x_{g+1}) - \operatorname{erf}(x_g) \\ & + \operatorname{erf}(y_{g+1}) - \operatorname{erf}(y_g) \} \end{aligned} \quad (12.3)$$

with

$$x_g = \sqrt{\frac{E_g}{T}} - \sqrt{\frac{E_f}{T}} ; \quad x_{g+1} = \sqrt{\frac{E_{g+1}}{T}} - \sqrt{\frac{E_f}{T}}$$

$$y_g = \sqrt{\frac{E_g}{T}} + \sqrt{\frac{E_f}{T}} ; \quad y_{g+1} = \sqrt{\frac{E_{g+1}}{T}} + \sqrt{\frac{E_f}{T}}$$

$$\operatorname{erf}(x) = \frac{2}{\sqrt{\pi}} \int_0^x e^{-t^2} dt$$

12.3 Calculation of the Maxwellian spectrum

The assumption for the calculation of the Maxwell spectrum is the existence of the KEDAK data type SEDF, /2/, containing the nuclear temperatures Θ at the fission energies E_0 . The Maxwellian spectrum is given by formula (12.4) which was taken from /1/.

$$\chi(E) = 2/(\Theta \cdot \sqrt{\pi\Theta}) \cdot \sqrt{E} \cdot \exp\left(-\frac{E}{\Theta}\right) \quad (12.4)$$

The fission spectrum in energy group g is defined as

$$\chi_g = \int_{(g)} \chi(E) dE \quad (12.5)$$

Using formula (12.4) one gets

$$\chi_g = \operatorname{erf}\left(\sqrt{\frac{E_g}{\Theta}}\right) - \operatorname{erf}\left(\sqrt{\frac{E_{g+1}}{\Theta}}\right) - \left\{ \sqrt{\frac{E_g}{\Theta}} \cdot e^{-\frac{E_g}{\Theta}} - \sqrt{\frac{E_{g+1}}{\Theta}} \cdot e^{-\frac{E_{g+1}}{\Theta}} \right\} \cdot \frac{2}{\sqrt{\pi}} \quad (12.6)$$

For $\frac{E_g}{\Theta} < 1.E-3$ a polynomial expansion is taken.

Θ is taken or interpolated from KEDAK at the median fission energy $E_0 = 165$ keV for a typical SNR neutron energy distribution $\phi(E)$

$$\int_0^{E_0} \nu(E) \cdot \sigma_f(E) \cdot \phi(E) dE = \int_{E_0}^{\infty} \nu(E) \cdot \sigma_f(E) \cdot \phi(E) dE \quad (12.7)$$

$$= \frac{1}{2} \int_0^{\infty} \nu(E) \cdot \sigma_f(E) \cdot \phi(E) dE$$

12.4 The following subroutine is necessary

SUBROUTINE SPALT(NE,ENG,X)

The following parameters are defined by the control program :

NE number of energy group limits,
ENG(NE) one-dimensional field containing the energy group limits in [eV].

The following parameter is defined by the subroutine SPALT :

X(NE) one-dimensional field containing the fission spectrum .

The subroutine SPALT calls subroutine CHIINM which calculates the value of the Maxwellian spectrum in one energy group

SUBROUTINE CHIINM (E1,E2,TETA,X2)

The following parameters are defined by SPALT :

E1 lower energy group limit,
E2 higher energy group limit,
TETA nuclear temperature at the fission energy 165 keV.

The following parameter is defined by subroutine CHIINM :

X2 value of the Maxwellian fission spectrum in the energy region from E1 to E2 .

References

/1/ E. Kiefhaber, D. Thiem

The Influence of Fission Neutron Spectra on Integral Nuclear Quantities of Fast Reactors

KFK 1651, März 1972, page 1

/2/ B. Krieg

KEDAK Basic Management

KFK 2387 II 2.9 (1977)

Acknowledgements

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Appendix A. Sample Problem

1. Job Control Cards

```
//INR017MI JOB (0017,101,P6M1B),KRIEG,CLASS=A,TIME=11,REGION=370K
/*SETUP DEVICE=2314, ID=GFK050
/*FORMAT PR,DDNAME=SYSMMSG,FORMS=REPRO
/*FORMAT PR,DDNAME=FT06F001,FORMS=REPRO
// EXEC PGM=MIGROS3
//STEPI IB DD DSN=LOAD.NUSYS,VOL=SER=KAPROS,UNIT=3330,DISP=SHR
//FT08F001 DD UNIT=SYSDA,SPACE=(TRK,2)
//FT06F001 DD SYSOUT=A,
// DCB=(RECFM=FBA,LRECL=133,BLKSIZE=1995),SPACE=(TRK,25)
//FT01F001 DD UNIT=2314,VOL=SER=GFK050,DSN=KEDAK3,DISP=SHR
//FT03F001 DD UNIT=SYSDA,SPACE=(TRK,20)
//FT10F001 DD UNIT=SYSDA,SPACE=(TRK,200)
//FT05F001 DD *
```

2. Input

```
@U 235@ 1
@BLCC@ 3
8 1 18 18 2 14 14 4 14 14 5 5 4 5 1 1 7 25 1 8 25 1 10 26 26
@ENDE @ 111
@C 16@ 0
@BLOC@ 3
5 3 4 4 6 3 3 6 12 12 9 3 3 9 12 12
@ENDE @ 111
@ENDE @ 112
```

3. Overlay Cards

OVERLAY MIGRCS
INSERT EING,FREEDU
OVERLAY MIGRCS
INSERT FGEM,WIRQ,WIRQU,STCSS,PSIXI,EXPPX
OVERLAY MIGRCS
INSERT FSTAT,QUER,TAB,SICC,PHASE,EZZ,DMIT,DELTA,EPSI,GAMN,GAMG,GAFM
INSERT POL,SUCH
OVERLAY MIGRCS
INSERT FSTRUK,FSTOLE,CFSTRU,CFSTRF,FSWR00,FSWRS1,FSWRS2,FSWRS3,CFSMEL
OVERLAY FSTRU1
INSERT FSQUER,FSTRU2,FSTRU3,FSTRU4,FSTRU5,FSSNCL
INSERT FSXINT,FSGRAL,FSGRA1,FSGRA2,FSGRA3
OVERLAY FSTRU3
INSERT FSEXIN,FSLOMQ
OVERLAY FSTRU3
INSERT FSR08
OVERLAY FSTRU4
INSERT FSNU01,FSNU02,FSNU03,FSNLC4,FSNU05,FSNU06,FSNU07,FSNU08,FSNU09
OVERLAY FSTRU4
INSERT FSAN02,FSAN03,FSANC4,FSANC5,FSANC6,FSANC7,FSANC8,FSANC9
OVERLAY FSTRU1
INSERT FSTRU0
OVERLAY FSTRU1
INSERT FSTRU1
OVERLAY FSTRU1
INSERT FSWRS9,ABFORM
OVERLAY MIGRCS
INSERT SUND,FL,GRUP
OVERLAY MIGRCS
INSERT CRDNEB,CUTS,FIPCLA,SCAT,SINPCL,FIPCLC
OVERLAY ONE
INSERT SCATD,AKED,TRA
OVERLAY A
INSERT DACRG
OVERLAY B
INSERT NDREAD
OVERLAY B
INSERT SPECT1
OVERLAY A
INSERT SIGRG,SGINT,XINPCL
OVERLAY ONE
INSERT SCATC
OVERLAY A
INSERT ENORG,ORD1
OVERLAY A
INSERT RENUCA
OVERLAY A
INSERT REPRCE
OVERLAY A
INSERT SIMPSI,FINT,PROB,EXD,THETA,CNFAK,TEMP
OVERLAY MIGRCS

```
INSERT FLUMMI,SUM,IPCLA,PUSUM,INTEG
OVERLAY A
INSERT MIXSGT,ADD
OVERLAY A
INSERT MUKCN,PRINT
OVERLAY A
INSERT TRAFU,INFORM,PUNK
OVERLAY A
INSERT MAKKO,LUCKO,LOOK1,LOOK2,LOOK3
OVERLAY A
INSERT LEGAL,LEGPUL,LEGINT,LEGIST,LEGANS,C
OVERLAY A
INSERT GRUPIN,IPOLIN,SPRAL
OVERLAY MIGROS
INSERT SPALT,CHIINM
OVERLAY MIGROS
INSERT EDV
OVERLAY MIGROS
INSERT REMC,REMP,AMESH,IWIN,IWC,ZWIN,EGRENZ,ICSCP,ENERG,FIPCL,IPCL
OVERLAY A
INSERT KEDDAT,AUSGL,ORDNI,LININ1,SLCFM,SINT,FXINT,SEARCH,MASSIN
OVERLAY A
INSERT ISOFAL,SMORN,WAHRS,LMI,BCN,ANINT,NCRM,INTEN,FTL,WINK,FICR,AKOR
OVERLAY MIGROS
INSERT THERM
ENTRY MAIN
NAME MIGROS(R)
```

On the following pages A4 to A29 the output of the results is given. The input description, that also was printed out by the job has been omitted here. It corresponds to the input description given on pages 2.2 to 2.17.

```

STAND DER KERNDATENBIBLIOTHEK VOM 261076
AU 235a 1
@FLCC@ 2
R 1 18 18 2 14 14 4 14 14 5 5 4 5 1 1 7 25 1 8 25 1 10 26 26
@FNDE @ 111
@C 16a 0
@BLOC@ 2
5 3 4 4 6 3 3 6 12 12 9 3 3 9 12 12
@FNDE @ 111
@ENDE @ 112

```

```

*
*
*
*
*
*
*
*
*
*

```

M I G R C S - 3 TASK FOR MATERIAL U 235

FOR THE WFCIGHTING SPECTRUM THE FUNCTION PHI(E) OR DPHI(E) WILL BE USED.

DATE 22.11.76 TIME 18.01.51

IN MODULE 1 33310 WORDS ARE NOT USED IN THE REGION FIELD

PROGRAMM KENZIFFER 1
PROGRAMM ZUR BERECHNUNG VON RESONANZSELBSTARSCHIRMFAKTOREN VON AUFGELÖSTEN RESONANZPARAMETERN

	MATERIAL	TEMPERATUR	GRUPPE	GRENZEN	
	U 235	300.00	18	0.4650E+02	0.1000E+03
	SIGMA G	SIGMA N	SIGMA F	SIGMAN1	SIGMAT1
	0.23170120F+02	0.12886469E+02	0.28999680F+02	0.12886469E+02	0.65056259E+02
SIGMA 0	FG	FN	FF	FN1	FT1
C.C	0.42532988E+00	0.94356949E+00	0.44212914E+00	0.92716968E+00	0.36945707E+00
C.10000000E+02	0.49302417E+00	0.94963223E+00	0.50933707E+00	0.93204403E+00	0.42256057E+00
C.10000000E+03	0.71646893E+00	0.97010434E+00	0.72497588E+00	0.95298940E+00	0.62977850E+00
C.10000000E+04	0.93765211E+00	0.99268764E+00	0.93856294E+00	0.98639333E+00	0.90295374E+00
C.10000000E+05	0.99289553E+00	0.99910206E+00	0.99322623E+00	0.99829018E+00	0.98853195E+00
C.10000000E+06	0.99945521E+00	0.99989605E+00	0.99976951E+00	0.99979395E+00	0.99880898E+00
C.10000000E+07	0.99989414E+00	0.99999082E+00	0.99990296E+00	0.99998218E+00	0.99986422E+00

MATERIAL TEMPERATUR GRUPPE GRENZEN
 U 235 900.00 18 0.4650E+C2 0.100CF+C3

	SIGMA G	SIGMA N	SIGMA F	SIGMAN1	SIGMAT1
	0.23157272E+C2	0.12888164E+J2	0.28985733E+02	0.12888164E+02	0.65031158E+02
SIGMA C	FG	FN	FF	FN1	FT1
0.0	0.52090794E+00	0.95318604E+00	0.53101712E+00	0.93434250E+00	0.42303497E+00
0.1000000E+C2	0.58767426E+00	0.95869917E+00	0.55581017E+00	0.93998843E+00	0.48589534E+00
0.1000000E+C3	0.79037625E+00	0.97749454E+00	0.79024559E+00	0.96224260E+00	0.70428258E+00
0.1000000E+C4	0.95936489E+00	0.99570826E+00	0.95305235E+00	0.99095903E+00	0.93382698E+00
0.1000000E+C5	0.99556696E+00	0.99944174E+00	0.9552155E+00	0.99892360E+00	0.99259353E+00
0.1000000E+C6	0.99967504E+00	0.99994004E+00	0.95981242E+00	0.99987465E+00	0.95924034E+00
0.1000000E+C7	0.99994498E+00	0.9999851E+00	0.99993856E+00	0.9999207E+00	0.99990743E+00

MATERIAL TEMPERATUR GRUPPE GRENZEN
 U 235 2100.00 18 0.4650E+C2 0.1000E+03

	SIGMA G	SIGMA N	SIGMA F	SIGMAN1	SIGMAT1
	0.23122330E+02	0.12889277E+02	0.28932922E+02	0.12889277E+02	0.64944519E+02
SIGMA 0	FG	FN	FF	FN1	FT1
0.0	0.60590488E+00	0.9604739CE+00	0.607553E4E+00	0.93858165E+00	0.48321068E+00
0.1000000E+02	0.66609097E+00	0.96593255E+00	0.665525E9E+00	0.94607395E+00	0.54955190E+00
0.1000000E+03	0.84069175E+00	0.9827069CE+00	0.83474588E+00	0.96963567E+00	0.76128662E+00
0.1000000E+04	0.97142029E+00	0.99664253E+00	0.96915507E+00	0.99349582E+00	0.95181471E+00
0.1000000E+C5	0.99692833E+00	0.99961740E+00	0.99674857E+00	0.99926466E+00	0.99474430E+00
0.1000000E+C6	0.99976003E+00	0.99995834E+00	0.999842E8E+00	0.99991411E+00	0.99947912E+00
0.1000000E+C7	0.99996543E+00	0.99999750E+00	0.99997044E+00	0.99999344E+00	0.99994189E+00

IN MODULE 1 407.16 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.36.14

PROGRAMM KEANZIFFER 2
 PROGRAMM ZUR BERECHNUNG VON RESONANZSELBSTABSCHIRMFAKTOREN VON STATISTISCHEN RESONANZPARAMETERN

NUMBER OF SERIES, TAKEN INTO ACCOUNT IS IT= 6

MATERIAL		TEMPERATUR	GRUPPE	GRENZEN	
U 235		300.00	14	C.1000E+04	C.2150E+04
SIGMA G		SIGMA N	SIGMA F	SIGMAN1	SIGMAT1
0.29596672E+01		0.12280684E+02	0.66533985E+01	0.12280684E+02	0.21893692E+02
SIGMA 0	FG	FN	FF	FN1	FT1
0.0	0.80614358E+00	0.98495656E+00	0.81168741E+00	0.97353542E+00	0.81270683E+00
C.10000000E+02	0.86417347E+00	0.98894918E+00	0.86897606E+00	0.98050916E+00	0.87385619E+00
C.10000000E+03	0.96114337E+00	0.99656564E+00	0.96302807E+00	0.99361336E+00	0.96461695E+00
C.10000000E+04	0.99510652E+00	0.99955565E+00	0.99538219E+00	0.99911815E+00	0.99540108E+00
C.10000000E+05	0.99949622E+00	0.99994898E+00	0.99953932E+00	0.99990731E+00	0.99952239E+00
C.10000000E+06	0.99995041E+00	0.99999088E+00	0.99995965E+00	0.99999350E+00	0.99995458E+00
C.10000000E+07	0.10000000E+01	0.10000000E+01	0.10000000E+01	0.10000000E+01	0.10000000E+01

MATERIAL		TEMPERATUR	GRUPPE	GRENZEN	
U 235		900.00	14	C.1000E+04	C.2150E+04
SIGMA G		SIGMA N	SIGMA F	SIGMAN1	SIGMAT1
0.29596672E+01		0.12280684E+02	0.66533985E+01	0.12280684E+02	0.21893692E+02
SIGMA 0	FG	FN	FF	FN1	FT1
0.0	0.84466672E+00	0.98803872E+00	0.84577483E+00	0.97611034E+00	0.82758224E+00
C.10000000E+02	0.89723802E+00	0.99168956E+00	0.89840829E+00	0.98360044E+00	0.89160442E+00
C.10000000E+03	0.97411436E+00	0.99772322E+00	0.97460175E+00	0.99553901E+00	0.97473818E+00
C.10000000E+04	0.99691331E+00	0.99972248E+00	0.99699997E+00	0.99944031E+00	0.99701816E+00
C.10000000E+05	0.99968135E+00	0.99996656E+00	0.99970567E+00	0.99994159E+00	0.99969399E+00
C.10000000E+06	0.99996889E+00	0.99999362E+00	0.99997479E+00	0.99995452E+00	0.99997002E+00
C.10000000E+07	0.10000000E+01	0.10000000E+01	0.10000000E+01	0.10000000E+01	0.10000000E+01

MATERIAL		TEMPERATUR	GRUPPE	GRENZEN	
U 235		2100.00	14	C.1000E+04	C.2150E+04
SIGMA G		SIGMA N	SIGMA F	SIGMAN1	SIGMAT1
0.29596672E+01		0.12280684E+02	0.66533985E+01	0.12280684E+02	0.21893692E+02
SIGMA 0	FG	FN	FF	FN1	FT1
0.0	0.87722653E+00	0.99058086E+00	0.87678689E+00	0.97935218E+00	0.84990674E+00
C.10000000E+02	0.92158425E+00	0.99368620E+00	0.92151678E+00	0.98657191E+00	0.91042733E+00
C.10000000E+03	0.98162389E+00	0.99839264E+00	0.98168224E+00	0.99675894E+00	0.98138368E+00
C.10000000E+04	0.99786872E+00	0.99980968E+00	0.99788857E+00	0.99961442E+00	0.99791342E+00
C.10000000E+05	0.99978042E+00	0.99997610E+00	0.99975612E+00	0.99996030E+00	0.99978566E+00
C.10000000E+06	0.99997687E+00	0.99999410E+00	0.99998409E+00	0.99999613E+00	0.99997997E+00
C.10000000E+07	0.10000000E+01	0.10000000E+01	0.10000000E+01	0.10000000E+01	0.10000000E+01

IN MODULE 2 155.39 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.44.55

IN MODULE 4 34781 WORDS ARE NOT USED IN THE REGION FIELD

PROGRAMM KENNZIFFER 4
PROGRAMM ZUR BERECHNUNG VON GRUPPENWIRKUNGSQUERSCHNITTEN BEI UNENDLICHER VERDUENNUNG

***MESSAGE 4. 2 : STORAGE NOT SUFFICIENT TO CALCULATE MUEL

IN MODULE 4 0.31 SECONDS CPU-TIME ARE USED

IN MODULE 4 34771 WORDS ARE NOT USED IN THE REGION FIELD

PROGRAMM KENNZIFFER 4
PROGRAMM ZUR BERECHNUNG VON GRUPPENWIRKUNGSQUERSCHNITTEN BEI UNENDLICHER VERDUENNUNG

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT C.1000000CE+04 EV

L 235 MUEL GRUPPE 14 BIS 14
0.28608791E-02

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT C.1000000CE+04 EV

L 235 NVE GRUPPE 14 BIS 14
C.24232779E+01

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT C.1000000CE+04 EV

U 235 SCA GRUPPE 14 BIS 14
0.10925330E+02

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT C.1000000CE+04 EV

L 235 SCF GRUPPE 14 BIS 14
C.74818325E+01

U 235 SEC GRUPPE 14 BIS 14
0.34434577E+01

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT C.1000000CE+04 EV

L 235 SGI GRUPPE 14 BIS 14
0.0

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT 0.10000000E+04 EV

U 235 SGN GRUPPE 14 BIS 14
0.14350869E+02

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT 0.10000000E+04 EV

L 235 SG2N GRUPPE 14 BIS 14
0.0

***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT 0.10000000E+04 EV

U 235 SGT GRUPPE 14 BIS 14
0.25274826E+02

IN MODULE 4 3.14 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.45.03

PROGRAMM KENNZIFFER 5

PROGRAMM ZUR BERECHNUNG VON TRANSFORMATIZEN FUER
INELASTISCHE STREUUNG, (N,2N) - UND (N,3N) - PROZESSE

PROBSGI

PROGRAMM ZUR BERECHNUNG INELASTISCHER STREUMATRIZEN
VON DISKRETE ANREGUNGSNIVEAUS.

***WARNING NCF. 2 : THE FURTHER NAME 0.20000190E+07 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR U 235 SGIZ

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INCLUDED IN THE KEDAK LIBRARY FOR U 235 SGIZ

***WARNING NCF. 2 : THE FURTHER NAME 0.20000190E+07 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR U 235 SGIZ

PROGRAMM ZUR BERECHNUNG INELASTISCHER STREUMATRIZEN
IM ENERGIEBEREICH KONTINUIERLICHER ANREGUNGSNIVEAUS DES RESTKERNS

***WARNING NCF. 3 : THE DATA FOR 920235 30051 ARE NOT INCLUDED IN THE KEDAK LIBRARY

***WARNING NDF. 3 : THE DATA FOR 920235 30051 ARE NOT INCLUDED IN THE KEDAK LIBRARY

***WARNING 5.00 : THE CROSS-SECTION-VALUES, GIVEN FOR THE MATERIAL U 235 , TYPE SGI
***DO NOT COVER THE ENERGY-GROUP BETWEEN 0.140000E+07EV AND 0.250000E+07EV. THE LOWEST AND HIGHEST VALUES
***GIVEN ON KEDAK FOR THIS GROUP ARE 0.240000E+07EV AND 0.250000E+07EV.
***THE INTEGRATION IN THIS ENERGY-GROUP THEREFORE IS RESTRICTED.

***WARNING NDF. 3 : THE DATA FOR 920235 50053 ARE NOT INCLUDED IN THE KEDAK LIBRARY

***WARNING NCF. 3 : THE DATA FOR 920235 50053 ARE NOT INCLUDED IN THE KEDAK LIBRARY

NO INFORMATION ON THE NUCLEAR DATA LIBRARY FOR TYPE SEDIC OF MATERIAL U 235 . AN EVAPORATION MODEL WITH
 $\theta = \sqrt{E/(NUE \cdot A)}$ IS USED. FOR THE NORMALIZATION THE THRESHOLD OF SGI IS TAKEN INTO ACCOUNT.
 $U = 0.20983E+05EV, A = 0.23504E+03NUE = 0.1600E+00$

KZ=	3NAM=U 235	KD=	2	7	8	9	10	11	12	13	14	15
5	2.764E-01	5.249E-01	1.677E-01	2.321E-02	5.944E-03	1.427E-03	3.504E-04	9.537E-05	2.963E-05	1.042E-05	4.154E-06	
	16	17	18	19	20	21	22	23	24	25	26	
	1.790E-06	7.911E-07	3.611E-07	1.672E-07	7.666E-08	3.557E-08	1.660E-08	7.635E-09	3.551E-09	1.659E-09	1.420E-09	
4	2.615E-02	1.532E-01	3.559E-01	2.753E-01	1.261E-01	4.469E-02	1.137E-02	2.609E-03	5.843E-04	1.289E-04	2.765E-05	
	15	16	17	18	19	20	21	22	23	24	25	
	6.003E-06	1.304E-06	2.781E-07	6.019E-08	1.306E-08	2.783E-09	6.021E-10	1.306E-10	2.783E-11	6.021E-12	1.306E-12	
	26											
	3.551E-13											

PROGRAMM KENNZIFFER 5

PROGRAMM ZUR BERECHNUNG VON TRANSFERMATRIZEN FUER
INELASTISCHE STREUUNG, (N,2N) - UND (N,3N) - PROZESSE

PROBSG2N

KD= 0 NO TRANSFER MATRICES FOR TYPE SMTOT2N IN THE ENERGY REGION REQUIRED BY INPUT

IN MODULE 5 29730 WORDS ARE NOT USED IN THE REGION FIELD

IN MODULE 5 0.72 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.45.05

PROGRAMM KENNZIFFER 5

PROGRAMM ZUR BERECHNUNG VON TRANSFERMATRIZEN FUER
INELASTISCHE STREUUNG, (N,2N) - UND (N,3N) - PROZESSE

PROBSGI

PROGRAMM ZUR BERECHNUNG INELASTISCHER STREUMATRIZEN
VON DISKRETEN ANREGUNGSNIVEAUS.

***WARNING NDF. 2 : THE FURTHER NAME 0.20900190E+07 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR U 235 SGIZ

***WARNING NDF. 2 : THE FURTHER NAME 0.20000190E+07 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR U 235 SGIZ
***ERRCR 5.C4 : WITH INCIDENT NEUTRON ENERGIES OUT OF THE
ENERGY GROUPS REQUESTED IN THE INPUT INELASTIC SCATTERING
FROM DISCRETE LEVELS CANNOT OCCUR.

PROGRAMM ZUR BERECHNUNG INELASTISCHER STREUMATRIZEN
IM ENERGIEBEREICH KONTINUIERLICHER ANREGUNGSNIVEAUS DES RESTKERNS

***WARNING NDF. 3 : THE DATA FOR 920235 30051 ARE NOT INCLUDED IN THE KEDAK LIBRARY

***WARNING NDF. 3 : THE DATA FOR 920235 50053 ARE NOT INCLUDED IN THE KEDAK LIBRARY

***WARNING NDF. 3 : THE DATA FOR 920235 50053 ARE NOT INCLUDED IN THE KEDAK LIBRARY

NO INFORMATION ON THE NUCLEAR DATA LIBRARY FOR TYPE SEDIC OF MATERIALU 235 .AN EVAPORATION MODEL WITH
THETA=SQRT(E/(NUE*A)) IS USED.FOR THE NORMALIZATION THE THRESHOLD OF SGI IS TAKEN INTO ACCOUNT.
U= 0.20983E+05EV,A= 0.23504E+03NUE= 0.1600CE+00

KZ=	3NAM=U 235	KD= 1									
	1	2	3	4	5	6	7	8	9	10	11
1	1.273E-05	1.658E-03	2.587E-02	1.609E-01	2.859E-01	3.045E-01	1.481E-01	5.197E-02	1.616E-02	3.838E-03	8.532E-04
	12	13	14	15	16	17	18	19	20	21	22
	1.882E-04	4.120E-05	8.817E-06	1.911E-06	4.150E-07	8.846E-08	1.914E-08	4.153E-09	8.849E-10	1.915E-10	4.153E-11
	23	24	25	26							
	8.849E-12	1.915E-12	4.153E-13	1.125E-13							

- A 11 -

PROGRAMM KENNZIFFER 5

PROGRAMM ZUR BERECHNUNG VON TRANSFERMATRIZEN FUER
INELASTISCHE STREUUNG, (N,2N) - UND (N,3N) - PROZESSE

PROBSC2N

***WARNING NDF. 3 : THE DATA FOR 920235 50163 ARE NOT INCLUDED IN THE KEDAK LIBRARY

***WARNING NDF. 3 : THE DATA FOR 920235 50163 ARE NOT INCLUDED IN THE KEDAK LIBRARY

NO INFORMATION ON THE NUCLEAR DATA LIBRARY FOR TYPE SED2N OF MATERIALU 235 .AN EVAPORATION MODEL WITH
THETA=SQRT(E/(NUE*A)) IS USED.FOR THE NORMALIZATION THE THRESHOLD OF SG2N IS TAKEN INTO ACCOUNT.
U= 0.53000E+07EV,A= 0.23504E+03NUE= 0.1600CE+00

**WEIGHTED GROUP CROSS-SECTION = 0.493809E+00 FOR OUTSCATTERING - GROUP 1 U = 0.530000E+07KONT = 0

KZ=	3NAM=U 235	KD=	1	2	3	4	5	6	7	8	9	10	11
1	0.0	7.353E-04	2.331E-02	1.657E-01	2.969E-01	3.020E-01	1.424E-01	4.919E-02	1.517E-02	3.587E-03	7.958E-04		
	12	13	14	15	16	17	18	19	20	21	22		
	1.754E-04	3.838E-05	8.211E-06	1.780E-06	3.864E-07	8.237E-08	1.783E-08	3.867E-09	8.240E-10	1.783E-10	3.867E-11		
	23	24	25	26									
	8.240E-12	1.783E-12	3.867E-13	1.051E-13									

IN MODULE 5 29730 WORDS ARE NOT USED IN THE REGION FIELD

IN MODULE 5 8.18 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.45.21

IN MODULE 7 37911 WORDS ARE NOT USED IN THE REGION FIELD

PROGRAMM KENNZIFFER 7
PROGRAMM ZUR BERECHNUNG DES SPALTSPEKTRUMS

IN THIS MODULE THE HIGHEST ENERGY GROUP BOUNDARY IS SET EQUAL TO 20.E6 EV

WATT - CRANBERG SPEKTRUM

U 235	EINFALLSENERGIE = 0.0			VCN GRUPPE 25 BIS 1									
CHI 0													
	C.10703206E-09	0.32318237E-09	0.99962683E-09	0.31642278E-08	0.98986028E-08	0.31139685E-07	0.99362580E-07						
	0.31199164E-06	0.98314013E-06	0.31392719E-05	0.98584796E-05	0.31055431E-04	0.99062265E-04	0.31036930E-03						
	G.9727648CE-03	0.30689924E-02	0.93899146E-02	0.23881171E-01	0.61028179E-01	0.14057332E+00	0.20230591E+00						
	0.26991755E+00	0.18339193E+00	0.88322282E-01	C.1669265CF-01									

IN MODULE 7 0.03 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.45.21

IN MODULE 8 37511 WORDS ARE NOT USED IN THE REGION FIELD

EDV - A PROGRAM FOR THE CALCULATION OF THE 1/V AVERAGE GROUP VALUES

GRUPPE	1/V
1	0.25221425E-09
2	0.32105718E-09
3	0.40761261E-09
4	0.53069127E-09
5	0.70539374E-09
6	0.96682684E-09
7	0.13673001E-08
8	0.19336548E-08
9	0.27883800E-08
10	0.40953410E-08
11	0.60121633E-08
12	0.88176115E-08
13	0.12950604E-07
14	0.19015300E-07
15	0.27883786E-07
16	0.40953442E-07
17	0.60131640E-07
18	0.88176193E-07
19	0.12950602E-06
20	0.19015278E-06
21	0.27883755E-06
22	0.40953398E-06
23	0.60131680E-06
24	0.88176296E-06
25	0.12950604E-05
26	0.40279110E-05

IN MODULE 8 0.04 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.45.21

IN MODULE 10 37937 WORDS ARE NOT USED IN THE REGION FIELD

PROGRAMM KENNZIFFER 10
PROGRAMM ZUR BERECHNUNG DER THERMISCHEN QUERSCHNITTE

U 235 MUEL 26
C.28609300E-02

U 235	NLE	26
C.24228592E+C1		
L 235	SCA	26
C.60552198E+03		
L 235	SCF	26
C.5157E354E+03		
L 235	SGC	26
C.89748047E+02		
L 235	SGI	26
C.0		
L 235	SGN	26
C.16611298E+02		
L 235	SG2N	26
C.0		
L 235	SGT	26
C.62214307E+03		
L 235	SGNCO	26
C.1000000E+01		
L 235	PRCBSGI	26
C.1000000E+01		
L 235	CHI	26
C.0		

IN MODULE 10 0.04 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.45.22

M I G R O S - 3 TASK FOR MATERIAL 0 16

FOR THE WEIGHTING SPECTRUM THE FUNCTION PHI(E) OR DPPHI(E) WILL BE USED.

DATE 22.11.76 TIME 18.45.26

IN MODULE 3 17691 WORDS ARE NOT USED IN THE REGION FIELD

*** MESSAGE 3. 1 PROGRAMM_KENNZIFFER_2

PROGRAMM ZUR BERECHNUNG VON RESONANZSELEKTARSCHIRMFAKTOREN VON PUNKTWEISE GEGEBENEN WIRKUNGSQUERSCHNITTEN FUER DAS MATERIAL C 16 .

***WARNING NDF. 3 : THE DATA FOR 80016 30190 ARE NOT INCLUDED IN THE KEDAK LIBRARY THE CALCULATIONS WILL BE DONE FOR GROUP 4, WHICH HAS THE BOUNDARIES 1.40000E+06 EV AND 2.50000E+06 EV. THE MATERIAL IS NOT FISSIONABLE.

WARNING MESSAGES IN NUMERICAL INTEGRATION WILL BE PRINTED, IF THE ACTUAL RELATIVE ERROR IS GREATER OR EQUAL THAN 5.000E+00 TIMES THE WISHED RELATIVE ERROR = 5.000E-05.

THE FOLLOWING WEIGHTING SPECTRUM(S) IS (ARE) USED.

ENERGY RANGE	WEIGHTING SPECTRUM	TYP OF INTEGRATION
WHOLE RANGE	ORIGINAL FUNCTION DPFI=1.0D+0/E	NUMERICAL

 *D 16 GROUP= 4 LOWER BOUNDARY= 1.40000E+06 EV UPPER BOUNDARY= 2.50000E+06 EV.
 * FROM 1.40000E+06 EV TO 2.50000E+06 EV NUMERICAL INTEGRATION IS USED. DPFI IS USED AS WEIGHTING SPECTRUM.

	SIGMA A	SIGMA N	SIGMA NC1	SIGMA NI	SIGMA T1
	0.21283107E-07	0.17578802E+01	0.19009775E+00	0.19009775E+00	0.17578802E+01
SIG0	FA	FN	FN01	FN1	FT1
C.C	0.96236938E+00	0.81353301E+00	0.96001279E+00	0.93244135E+00	0.60673928E+00
C.10000000E+02	0.99562335E+00	0.97553360E+00	0.99076885E+00	0.98229152E+00	0.95218652E+00
C.10000000E+03	0.99949831E+00	0.99704301E+00	0.99886262E+00	0.99773443E+00	0.99410820E+00
0.10000000E+04	0.99994916E+00	0.99969763E+00	0.99988371E+00	0.99976742E+00	0.99939543E+00
C.10000000E+05	0.99999499E+00	0.99996978E+00	0.99998844E+00	0.99997675E+00	0.99993950E+00
0.10000000E+06	0.99999958E+00	0.99999708E+00	0.99999893E+00	0.99999779E+00	0.99999404E+00
C.10000000E+07	0.10000000E+01	0.99999992E+00	0.10000000E+01	0.99999988E+00	0.99999952E+00

*** MESSAGE 3. 2 PROGRAM 3 HAS ENDED CORRECTLY. KL HAS THE VALUE= 2.

NO WARNING- OR ERROR-MESSAGES PRODUCED IN MODULE FSTRUK.

IN MODULE 3 2.07 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.45.29

IN MODULE 6 9009 WORDS ARE NOT USED IN THE REGION FIELD

PROGRAMM KENNZIFFER 6
PROGRAMM ZUR BERECHNUNG ELASTISCHER STREUMATRIZEN

***WARNING NDF. 2 : THE FURTHER NAME 0.15830016F+08 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR 0 16 SGNC

***WARNING NDF. 2 : THE FURTHER NAME 0.15830016E+08 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR 0 16 SGNC

***MESSAGE 6.1 : WARNING NDF. 2 MAY BE IGNORED

SGNC0 ELASTISCHE STREUMATRIX 0. CRDNUNG FUER 0 16

3.GRUPPE

0.88355E+00
0.11644E+00

SGNC1 ELASTISCHE STREUMATRIX 1. CRDNUNG FUER 0 16

3.GRUPPE

0.29722E+00
-0.27920E-01

SGNC2 ELASTISCHE STREUMATRIX 2. CRDNUNG FUER 0 16

3.GRUPPE

0.19122E+00
0.96000E-03

SGNC3 ELASTISCHE STRELMATRIX 3. ORDNUNG FUER 0 16

3. GRUPPE

C.8682CE-C1
-C.52200E-C2

SGNC4 ELASTISCHE STRELMATRIX 4. ORDNUNG FUER 0 16

3. GRUPPE

0.16280E-C1
-C.3900CE-C2

SGNC5 ELASTISCHE STRELMATRIX 5. ORDNUNG FUER 0 16

3. GRUPPE

-C.15300E-C2
0.29000E-C2

ERLAUTERUNG
L-TE ORDNUNG, G-TE GRUPPE, I-TE ZEILE: MATRIXELEMENT L-TER ORDNUNG
FUER STREUUNG AUS DER G-TEN GRUPPE IN DIE (G+I-1)-TE GRUPPE, BEZOGEN
AUF DEN TOTALEN ELASTISCHEN QUERSCHNITT (TOTALES 0.MOMENT) DER
G-TEN GRUPPE

MAKROWICHTUNG F

ALLE MOMENTE WIE DAS 0. MOMENT MIT
F(E,1) (STANDARD F(E,1) = 1/E)

MIKROWICHTUNG FS (FEINSTRUKTUR)

ALLE MOMENTE MIT FS(E,1) = 1
(KEINE FEINSTRUKTURWICHTUNG)

G E S A M T W I C H T U N G F * F S

TOTALE ELASTISCHE GRUPPENSTREUQUERSCHNITTE SGN UND GRUPPENSTREUKOSINUS MUEL FUER D 16

3. GRUPPE

2.04014E+CC
2.69300E-C1

ERLAEUTERUNG

G-TE GRUPPE, 1. ZEILE: TOTALER ELASTISCHER QUERSCHNITT DER G-TEN GRUPPE

G-TE GRUPPE, 2. ZEILE: MITTLERER STREUKOSINUS DER G-TEN GRUPPE

TOTALE GRUPPENQUERSCHNITTE SGT FUER D 16

3. GRUPPE

2.04327E+CC
2.04327E+CC
2.04327E+CC
2.04327E+CC
2.04327E+CC
2.04327E+CC

ERLAEUTERUNG

G-TE GRUPPE, L-TE ZEILE: TOTALER QUERSCHNITT DER G-TEN GRUPPE, GEWICHTET WIE DAS (L-1)-TE MOMENT DER STREUMATRIX

NORMIERUNGSINTEGRALE BIS ZUM 5. MOMENT

3. GRUPPE

4.70007E-C1
4.70007E-C1
4.70007E-C1
4.70007E-C1
4.70007E-C1
4.70007E-C1

ERLAUTERUNG
G-TE GRUPPE, L-TE ZEILE: (L-1)-TES MOMENT DES WICHTUNGSSPEKTRUMS
INTEGRIERT UEBER DIE G-TE GRUPPE

IN MODULE 6 43.42 SECONDS CPU-TIME ARE USED
DATE 22.11.76 TIME 18.47.03

IN MODULE 6 9009 WORDS ARE NOT USED IN THE REGION FIELD

PROGRAMM KENNZIFFER 6
PROGRAMM ZUR BERECHNUNG ELASTISCHER STREUMATRIZEN

***WARNING NDF. 2 : THE FURTHER NAME 0.15830016E+08 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR 0 16 SGNC

***WARNING NDF. 2 : THE FURTHER NAME 0.15830016E+08 IS GREATER THAN THE GREATEST FURTHER NAME
INCLUDED IN THE KEDAK LIBRARY FOR 0 16 SGNC

***MESSAGE 6.1 : WARNING NDF. 2 MAY BE IGNORED

SGNC0 ELASTISCHE STRELMATRIX 0. ORDNUNG FUER 0 16

12.GRUPPE

0.84196E+00
0.15803E+00

SGNC1 ELASTISCHE STRELMATRIX 1. ORDNUNG FUER 0 16

12.GRUPPE

0.89880E-01
-0.48180E-01

SGNC2 FLASTISCHE STRELMATRIX 2. ORDNUNG FUER 0 16

12.GRUPPE

0.34100E-02
-0.26100E-02

SGNC3 ELASTISCHE STRELMATRIX 3. ORDNUNG FUER 0 16

12.GRUPPE

C.40000E-04
-0.40000E-04

SGNC4 ELASTISCHE STRELMATRIX 4. ORDNUNG FUER 0 16

12.GRUPPE

0.0
C.0

SGNC5 ELASTISCHE STRELMATRIX 5. ORDNUNG FUER 0 16

12.GRUPPE

-C.50000E-04
C.50000E-04

FRLAEUTERUNG
L-TE ORDNUNG, G-TE GRUPPE, I-TE ZEILE: MATRIXELEMENT L-TER ORDNUNG
FUER STREUUNG AUS DER G-TEN GRUPPE IN DIE (G+I-1)-TE GRUPPE, BEZOGEN
AUF DEN TOTALEN ELASTISCHEN QUERSCHNITT (TOTALES O.MOMENT) DER
G-TEN GRUPPE

M A K R O W I C H T U N G F

ALLE MOMENTE WIE DAS 0. MOMENT MIT
F(E,1) (STANDARD F(E,1) = 1/E)

M I K R O W I C H T U N G F S (FEINSTRUKTUR)

ALLE MOMENTE MIT FS(E,1) = 1
(KEINE FEINSTRUKTURWICHTUNG)

G E S A M T W I C H T U N G F * F S

TOTALE ELASTISCHE GRUPPENSTREUQUERSCHNITTE SGN UND GRUPPENSTREUKOSINUS MUEL FUER Q 16

12.GRUPPE

3.7000CF+00
4.17000E-02

ERLAEUTERUNG

G-TE GRUPPE, 1. ZEILE: TOTALE ELASTISCHER QUERSCHNITT DER G-TEN
GRUPPE
G-TE GRUPPE, 2. ZEILE: MITTLERER STREUKOSINUS DER G-TEN GRUPPE

TOTALF GRUPPENQUERSCHNITTE SGT FUER Q 16

12.GRUPPE

3.70003E+00
3.70003E+00
3.70003E+00
3.70003E+00
3.70003E+00
3.70003E+00

ERLAEUTERUNG

G-TE GRUPPE, L-TE ZEILE: TOTALER QUERSCHNITT DER G-TEN GRUPPE,
GEWICHTET WIE DAS (L-1)-TE MOMENT DER STREUMATRIX

NORMIERUNGSINTEGRALE BIS ZUM 5. MOMENT

12.GRUPPE

7.65807F-01
7.65807E-C1
7.65807E-C1
7.65807E-C1
7.65807F-C1
7.65807F-C1

ERLAEUTERUNG
G-TE GRUPPE, L-TE ZEILE: (L-1)-TES MOMENT DES WICHTUNGSSPEKTRUMS
INTEGRIERT UEBER DIE G-TE GRUPPE

IN MODULE 6 1.07 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.47.07

PROGRAMM KEZZIFFER 9
PROGRAMM ZUR BERECHNUNG DER ELASTISCHEN STRELMATRIZEN FUER DIE REMC-KORREKTUR

FOR MATERIAL 0 16 , TYPE SGNC THERE ARE 20 ANGULAR DISTRIBUTIONS WITH 21 ANGLE POINTS RETRIEVED FOR THIS TASK.
THE LOWEST CALCULATED ENERGY GROUP NUMBER WITH SGNC IS 2.

IN MODULE 9 128 K BYTES OF REGION.C NOT USED.

CALCULATION FOR GROUP 3

FOR THIS ENERGY GROUP CALCULATION WITH ANGULAR DISTRIBUTIONS.

NUMBER OF ENERGY POINTS RETRIEVED FOR MATERIAL 0 16 IN THE ENERGY-RANGE 2.500000E+06 , 4.000000E+06 EV.

SGT	33
SGN	31
MUEL	33

TOTAL NUMBER OF DIFFERENT POINTS 34

GROUP= 3 NUMBER OF FINE INTERVALS= 70 MATERIAL 0 16

THE INTERVAL-BOUNDARIES ARE

2.500000000D+06	2.5170707750D+06	2.5341415500D+06	2.5512123250D+06	2.5682831000D+06	2.5853538750D+06
2.6030074727D+06	2.6206610704D+06	2.6383146681D+06	2.6559682658D+06	2.6736218635D+06	2.6918781824D+06
2.7101345013D+06	2.7283908202D+06	2.7466471391D+06	2.7649034580D+06	2.7837830760D+06	2.8026626939D+06
2.8215423118D+06	2.8404219298D+06	2.8593015477D+06	2.8788257450D+06	2.8983499424D+06	2.9178741397D+06
2.9373983371D+06	2.9569225344D+06	2.9771133181D+06	2.9973041018D+06	3.0174948855D+06	3.0376856692D+06
3.0578764529D+06	3.0787565813D+06	3.0996367096D+06	3.1205168380D+06	3.1413969664D+06	3.1622770947D+06
3.1828701030D+06	3.2054631113D+06	3.2270561196D+06	3.2486491279D+06	3.2702421362D+06	3.2925723633D+06
3.3149025904D+06	3.3372328174D+06	3.3595630445D+06	3.3818932716D+06	3.4049858872D+06	3.4280785029D+06
3.4511711185D+06	3.4742637341D+06	3.4973563498D+06	3.5212373831D+06	3.5451184164D+06	3.5689994498D+06
3.5928804831D+06	3.6167615164D+06	3.6414578853D+06	3.6661542541D+06	3.6908506229D+06	3.7155465917D+06
3.7402433605D+06	3.7657829017D+06	3.7913224428D+06	3.8168619840D+06	3.8424015251D+06	3.8679410662D+06
3.8943525669D+06	3.9207640675D+06	3.9471755682D+06	3.9735870688D+06	3.9999985695D+06	

THE VALUES OF SGT

1.0834E+00	1.0891E+00	1.0970E+00	1.1005E+00	1.1038E+00	1.1085E+00	1.1121E+00	1.1146E+00	1.1177E+00	1.1215E+00
1.1259E+00	1.1301E+00	1.1328E+00	1.1357E+00	1.1393E+00	1.1433E+00	1.1483E+00	1.1511E+00	1.1524E+00	1.1542E+00
1.1563E+00	1.1588E+00	1.1616E+00	1.1651E+00	1.1694E+00	1.1731E+00	1.1773E+00	1.2102E+00	1.2683E+00	1.3391E+00
1.4284E+00	1.5361E+00	1.6403E+00	1.7403E+00	1.8771E+00	2.0272E+00	2.1975E+00	2.3608E+00	2.5067E+00	2.6964E+00
2.9286E+00	3.1488E+00	3.1416E+00	3.1065E+00	3.0625E+00	3.0117E+00	3.0163E+00	3.4876E+00	3.3902E+00	3.1098E+00
2.9511E+00	2.9673E+00	2.9900E+00	3.0184E+00	3.0377E+00	3.0171E+00	2.9866E+00	2.9630E+00	2.9482E+00	3.0611E+00
3.8995E+00	4.0912E+00	2.9131E+00	2.5995E+00	2.4398E+00	2.3468E+00	2.2748E+00	2.2145E+00	2.1558E+00	2.0816E+00

THE VALUES OF SGN

1.0834E+00	1.0891E+00	1.0970E+00	1.1005E+00	1.1038E+00	1.1085E+00	1.1121E+00	1.1146E+00	1.1177E+00	1.1215E+00
1.1259E+00	1.1301E+00	1.1328E+00	1.1357E+00	1.1393E+00	1.1433E+00	1.1483E+00	1.1511E+00	1.1524E+00	1.1542E+00
1.1563E+00	1.1588E+00	1.1616E+00	1.1651E+00	1.1694E+00	1.1731E+00	1.1773E+00	1.2102E+00	1.2683E+00	1.3391E+00
1.4284E+00	1.5361E+00	1.6403E+00	1.7403E+00	1.8771E+00	2.0272E+00	2.1975E+00	2.3608E+00	2.5067E+00	2.6964E+00
2.9286E+00	3.1488E+00	3.1416E+00	3.1065E+00	3.0625E+00	3.0117E+00	3.0163E+00	3.4876E+00	3.3902E+00	3.1098E+00
2.9511E+00	2.9673E+00	2.9900E+00	3.0184E+00	3.0377E+00	3.0162E+00	2.9844E+00	2.9599E+00	2.9441E+00	3.0562E+00
2.8939E+00	4.0849E+00	2.9059E+00	2.5910E+00	2.4288E+00	2.3323E+00	2.2560E+00	2.1942E+00	2.1161E+00	2.0104E+00

THE VALUES OF MUJEL

2.5992E-01	2.5142E-01	2.3986E-01	2.3344E-01	2.3823E-01	2.4623E-01	2.5310E-01	2.5924E-01	2.6464E-01	2.7228E-01
2.8134E-01	2.8989E-01	2.9605E-01	3.0305E-01	3.1091E-01	3.0744E-01	2.9906E-01	2.9227E-01	2.8747E-01	2.8141E-01
2.7392E-01	2.6505E-01	2.5984E-01	2.5775E-01	2.5271E-01	2.2247E-01	1.7854E-01	1.5867E-01	1.7247E-01	1.8805E-01
2.0550E-01	2.2383E-01	2.3245E-01	2.3525E-01	2.3859E-01	2.3790E-01	2.2484E-01	2.0875E-01	1.9454E-01	1.7830E-01
1.6146E-01	1.5737E-01	1.6329E-01	1.7065E-01	1.8015E-01	1.9153E-01	2.0503E-01	2.2069E-01	2.3783E-01	2.6301E-01
2.8666E-01	2.9861E-01	3.1334E-01	3.3147E-01	3.4607E-01	3.5223E-01	3.5745E-01	3.6025E-01	3.6177E-01	3.5152E-01
3.0352E-01	2.6847E-01	2.5578E-01	3.3589E-01	3.7451E-01	3.6960E-01	3.6851E-01	3.7488E-01	3.9515E-01	4.2437E-01

THE VALUES OF FLUX

2.0269E-01	2.0133E-01	1.9998E-01	1.9864E-01	1.9732E-01	2.0269E-01	2.0132E-01	1.9995E-01	1.9863E-01	1.9731E-01
2.0270E-01	2.0132E-01	1.9997E-01	1.9864E-01	1.9732E-01	2.0270E-01	2.0132E-01	1.9998E-01	1.9863E-01	1.9733E-01
2.0270E-01	2.0133E-01	1.9998E-01	1.9864E-01	1.9732E-01	2.0270E-01	2.0133E-01	1.9996E-01	1.9864E-01	1.9733E-01
2.0269E-01	2.0132E-01	1.9997E-01	1.9864E-01	1.9733E-01	2.0269E-01	2.0132E-01	1.9997E-01	1.9864E-01	1.9732E-01
2.0269E-01	2.0132E-01	1.9997E-01	1.9864E-01	1.9732E-01	2.0269E-01	2.0133E-01	1.9998E-01	1.9864E-01	1.9733E-01
2.0268E-01	2.0131E-01	1.9996E-01	1.9863E-01	1.9731E-01	2.0270E-01	2.0134E-01	1.9998E-01	1.9864E-01	1.9733E-01
2.0270E-01	2.0134E-01	1.9998E-01	1.9865E-01	1.9733E-01	2.0270E-01	2.0134E-01	1.9998E-01	1.9865E-01	1.9733E-01

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ELASTIC SCATTERING MATRIX   SGNC0 FOR C 16   GRUPE= 3
FROM GRUPE 3 TO GRUPE 3
 2.8632E-C2  7.9558E-02  1.2307E-C1  1.6376E-C1  2.1609E-01  2.7194E-01  3.2652E-01  3.7685E-01  4.2176E-01  4.6435E-01
 5.0277E-C1  5.3766E-01  5.6899E-01  5.9726E-01  6.2221E-01  6.3739E-01  6.5213E-01  6.6617E-01  6.8074E-01  6.9553E-01
 7.1061E-01  7.2600E-01  7.4295E-01  7.6184E-01  7.7901E-01  7.7885E-01  7.7749E-01  7.8457E-01  7.9851E-01  8.1060E-01
 8.2464E-C1  8.5376E-01  8.8302E-01  9.0946E-01  9.3567E-01  9.5923E-01  9.7841E-01  9.9646E-01  1.0000E+00  1.0000E+00
 1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00
 1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00
 1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00  1.0000E+00
FROM GRUPE 3 TO GRUPE 4
 9.7137E-C1  9.2044E-01  8.7693E-01  8.3624E-01  7.8391E-01  7.2806E-01  6.7348E-01  6.2315E-01  5.7824E-C1  5.3565E-01
 4.9723E-01  4.6234E-01  4.3101E-01  4.0274E-01  3.7779E-01  3.6261E-01  3.4787E-01  3.3383E-01  3.1926E-C1  3.0447E-01
 2.8939E-C1  2.7400E-01  2.5705E-01  2.3816E-01  2.2099E-01  2.2115E-01  2.2251E-01  2.1543E-01  2.0149E-C1  1.8940E-01
 1.7536E-C1  1.4624E-C1  1.1698E-01  9.0544E-02  6.4333E-02  4.0767E-02  2.1587E-02  3.5415E-02  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

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ELASTIC SCATTERING MATRIX   SGNC1 FOR C 16   GRUPE= 3
FROM GRUPE 3 TO GRUPE 3
 2.8124E-C2  7.6294E-02  1.1488E-01  1.4867E-01  1.9101E-01  2.3413E-01  2.7420E-01  3.0943E-01  3.3936E-C1  3.6692E-01
 3.9075E-C1  4.1176E-01  4.2986E-01  4.4556E-01  4.5900E-01  4.6088E-01  4.5634E-01  4.5107E-01  4.4548E-01  4.3901E-01
 4.3150E-01  4.2311E-01  4.1452E-01  4.0639E-01  3.9624E-01  3.8300E-01  3.3272E-01  3.1388E-01  3.2610E-01  3.3912E-01
 3.4956E-C1  3.4519E-01  3.3365E-01  3.1584E-01  2.9730E-01  2.7671E-01  2.4621E-01  2.1372E-01  1.9444E-01  1.7876E-01
 1.6288E-01  1.5749E-01  1.6546E-01  1.7403E-01  1.8276E-01  1.9168E-01  2.0487E-01  2.2092E-01  2.4290E-01  2.6612E-01
 2.8655E-C1  3.0207E-01  3.1737E-01  3.3280E-01  3.4607E-01  3.5239E-01  3.5744E-01  3.6040E-01  3.6177E-01  3.5346E-01
 3.0952E-01  2.6565E-01  2.5623E-01  3.3873E-C1  3.7393E-C1  3.6932E-01  3.6848E-01  3.7486E-01  3.9532E-C1  4.2424E-01
FROM GRUPE 3 TO GRUPE 4
 2.3207E-01  1.7351E-01  1.2499E-01  8.4612E-02  4.7913E-02  1.1998E-02  -2.0702E-02  -4.8798E-02  -7.2169E-02  -9.1873E-02
 -1.0833E-01  -1.2187E-01  -1.3277E-01  -1.4164E-01  -1.4958E-01  -1.5310E-01  -1.5699E-01  -1.5923E-01  -1.6035E-01  -1.6054E-01
 -1.6002E-01  -1.5827E-01  -1.5475E-01  -1.4904E-01  -1.4362E-01  -1.4882E-01  -1.5501E-01  -1.5629E-01  -1.5308E-01  -1.4981E-01
 -1.4365E-01  -1.2315E-01  -1.0122E-C1  -8.0558E-C2  -5.8867E-C2  -3.8391E-02  -2.0908E-02  -3.5040E-03  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

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ELASTIC SCATTERING MATRIX   SGNC2 FOR C 16   GRUPE= 3
FROM GRUPE 3 TO GRUPE 3
 2.7131E-02  7.0042E-02  9.9624E-02  1.2133E-01  1.4679E-01  1.6935E-01  1.8704E-01  2.0005E-01  2.0910E-01  2.1664E-01
 2.2226E-01  2.2662E-01  2.3063E-01  2.3452E-01  2.3776E-01  2.2598E-01  2.0872E-01  1.9082E-01  1.7282E-01  1.5470E-01
 1.3639E-C1  1.1801E-01  1.0039E-01  8.3672E-02  6.7266E-02  4.7688E-02  2.6604E-02  2.4064E-02  5.2627E-02  8.3693E-02
 1.1455E-01  1.2777E-01  1.3734E-01  1.4770E-01  1.6079E-01  1.7492E-01  1.8765E-01  2.0213E-01  2.0388E-01  2.0227E-01
 2.0095E-01  2.3333E-01  2.8736E-01  3.3097E-01  4.2972E-01  4.2966E-01  2.3676E-C1  2.5273E-01  2.6849E-01  2.8433E-01
 2.8402E-01  2.5871E-01  2.2710E-01  1.8440E-01  1.4484E-01  1.7285E-01  2.1613E-01  2.2445E-01  2.3206E-01  2.4794E-01
 2.4797E-C1  1.9314E-01  1.4255E-01  1.3931E-01  1.4052E-01  1.4159E-01  1.4164E-01  1.3322E-C1  1.2272E-C1  1.1216E-01
FROM GRUPE 3 TO GRUPE 4
 3.0845E-02  -2.2585E-02  -6.3029E-02  -5.2340E-C2  -1.0515E-C1  -1.1119E-01  -1.1206E-01  -1.0809E-01  -1.0089E-01  -9.1295E-02
 -7.9792E-C2  -6.6708E-02  -5.3283E-02  -3.9871E-02  -2.6700E-02  -1.8354E-02  -1.1391E-02  -4.2416E-03  3.0887E-C3  1.0504E-02
 1.8002E-02  2.5379E-02  3.2009E-02  3.7669E-02  4.3010E-C2  5.1082E-02  6.0377E-02  7.0150E-02  7.9667E-02  8.7488E-02
 9.1992E-C2  8.4364E-02  7.3982E-02  6.2793E-02  4.8863E-02  3.3915E-02  1.9594E-02  3.4296E-C3  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
 0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

```

ELASTIC SCATTERING MATRIX SGNC3 FOR 0 16 GRGUP= 2										
FROM GROUP 3 TO GROUP 3										
2.5690E-02	6.1332E-02	7.9325E-02	8.6706E-02	9.3568E-02	9.5370E-02	9.2515E-02	8.7387E-02	8.1321E-02	7.6172E-02	
7.2065E-02	6.9520E-02	6.9111E-02	7.0693E-02	7.3492E-02	6.5204E-02	5.3285E-02	4.2708E-02	3.3358E-02	2.5322E-02	
1.8492E-02	1.2826E-02	8.3665E-03	4.9604E-03	3.3713E-03	1.1791E-02	2.5271E-02	4.3613E-02	6.5881E-02	8.7423E-02	
1.0681E-01	1.1680E-01	1.2393E-01	1.2910E-01	1.2050E-01	1.2685E-01	1.1349E-01	9.5200E-02	8.7986E-02	8.4045E-02	
8.0105E-02	7.6257E-02	7.2474E-02	6.8053E-02	6.0264E-02	5.1702E-02	5.2221E-02	5.7026E-02	6.1575E-02	6.6476E-02	
7.2452E-02	7.9925E-02	8.4043E-02	8.2445E-02	8.1430E-02	9.7457E-02	1.2114E-01	1.4800E-01	1.6944E-01	1.6949E-01	
1.5988E-01	1.2594E-01	9.4662E-02	8.9508E-02	8.6907E-02	8.4169E-02	8.1324E-02	7.8267E-02	7.5335E-02	7.2314E-02	
FROM GROUP 3 TO GROUP 4										
-2.1332E-02	-5.8518E-02	-7.8137E-02	-8.5895E-02	-8.5742E-02	-7.9055E-02	-6.7663E-02	-5.3958E-02	-3.9306E-02	-2.5523E-02	
-1.2791E-02	-1.4661E-02	7.8517E-03	1.5170E-02	2.0626E-02	2.5695E-02	3.0188E-02	3.3327E-02	3.5160E-02	3.5686E-02	
3.4873E-02	3.2800E-02	2.9479E-02	2.5089E-02	1.9990E-02	1.6245E-02	1.0775E-02	5.4773E-04	-1.3815E-02	-2.7080E-02	
-2.8277E-02	-4.1731E-02	-4.2353E-02	-4.1041E-02	-3.5975E-02	-2.7858E-02	-1.7732E-02	-3.3209E-02	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
ELASTIC SCATTERING MATRIX SGNC4 FOR 0 16 GRGUP= 3										
FROM GRGUP 3 TO GROUP 3										
2.3858E-02	5.0880E-02	5.6603E-02	5.0799E-02	4.2643E-02	3.0504E-02	1.6995E-02	5.2857E-03	-3.5221E-03	-8.7091E-03	
-1.0548E-02	-9.1562E-03	-5.0435E-03	1.1569E-03	8.5279E-03	1.0982E-02	1.2291E-02	1.4348E-02	1.6877E-02	1.9585E-02	
2.2146E-02	2.4262E-02	2.5179E-02	2.4938E-02	2.3802E-02	2.7658E-02	3.1327E-02	3.0868E-02	2.6310E-02	2.0497E-02	
1.3208E-02	2.3568E-03	-9.0187E-03	-1.9135E-02	-2.6034E-02	-2.8737E-02	-2.5849E-02	-1.6022E-02	-1.5302E-02	-1.7761E-02	
-2.0138E-02	-1.1520E-02	4.1677E-03	1.7049E-02	6.3867E-03	-9.0488E-03	-5.2237E-03	7.5461E-03	2.0126E-02	3.2818E-02	
3.7446E-02	2.9567E-02	2.2637E-02	1.8102E-02	1.4312E-02	2.3076E-02	3.7011E-02	5.3558E-02	6.6910E-02	6.6900E-02	
6.1739E-02	4.4087E-02	2.7636E-02	2.4339E-02	2.2197E-02	2.0059E-02	1.8056E-02	1.7861E-02	1.8076E-02	1.8323E-02	
FROM GRGUP 3 TO GROUP 4										
-1.9492E-02	-4.7586E-02	-5.4382E-02	-4.9191E-02	-3.8882E-02	-2.4001E-02	-7.7871E-03	6.7452E-03	1.8241E-02	2.6290E-02	
3.0935E-02	3.2408E-02	3.1183E-02	2.7854E-02	2.2124E-02	1.8883E-02	1.4066E-02	8.4821E-03	2.4356E-03	-3.7926E-03	
-9.9173E-03	-1.5539E-02	-2.0186E-02	-2.3580E-02	-2.5868E-02	-2.9681E-02	-3.2378E-02	-2.9867E-02	-2.1303E-02	-1.1544E-02	
-1.0348E-03	6.8592E-03	1.3886E-02	1.9670E-02	2.2235E-02	2.0899E-02	1.5441E-02	3.1797E-03	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
ELASTIC SCATTERING MATRIX SGNC5 FOR 0 16 GRGUP= 3										
FROM GRGUP 3 TO GROUP 3										
2.1707E-02	3.9518E-02	3.4199E-02	1.9244E-02	3.3969E-03	-1.2238E-02	-2.4399E-02	-3.1099E-02	-3.2596E-02	-3.0207E-02	
-2.4718E-02	-1.7514E-02	-9.8489E-03	-2.5163E-03	3.8657E-03	9.2055E-03	1.3877E-02	1.7046E-02	1.8614E-02	1.8580E-02	
1.6927E-02	1.3771E-02	9.3943E-03	4.1947E-03	-1.5395E-03	-9.7363E-03	-1.9124E-02	-2.5922E-02	-2.7159E-02	-2.5711E-02	
-2.1778E-02	-1.8080E-02	-1.3129E-02	-7.2250E-03	-2.3140E-03	9.9944E-05	-2.1980E-04	-9.2803E-03	-1.1454E-02	-1.0651E-02	
-9.8232E-03	-7.0454E-03	-3.0412E-03	6.0373E-04	1.1132E-03	9.5204E-04	1.1082E-03	1.4350E-03	1.7714E-03	2.1302E-03	
1.8119E-03	5.1073E-04	-1.2618E-03	-3.9408E-03	-6.2896E-03	-2.0798E-03	4.2457E-03	9.3155E-03	1.3121E-02	1.2566E-02	
1.0432E-02	4.7235E-03	-6.2974E-04	-2.1325E-03	-3.2640E-03	-4.4110E-03	-5.2205E-03	-2.7156E-03	5.9883E-04	3.8816E-03	
FROM GRGUP 3 TO GROUP 4										
-1.7513E-02	-3.6185E-02	-3.1722E-02	-1.7538E-02	-1.8866E-03	1.3635E-02	2.5643E-02	3.2202E-02	3.3566E-02	3.0946E-02	
2.5365E-02	1.8047E-02	1.0210E-02	2.7337E-03	-3.7901E-03	-9.2389E-03	-1.3759E-02	-1.6875E-02	-1.8431E-02	-1.8370E-02	
-1.6678E-02	-1.3470E-02	-9.0525E-03	-3.8056E-03	1.8395E-03	8.3379E-03	1.5565E-02	2.1232E-02	2.3019E-02	2.2143E-02	
1.8538E-02	1.3058E-02	5.7690E-03	-2.4625E-03	-9.6809E-03	-1.3783E-02	-1.2866E-02	-3.0095E-03	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

IN MODULE 9 21.04 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.47.54

PROGRAMM KENNZIFFER 9
 PROGRAMM ZUR BERECHNUNG DER ELASTISCHEN STREIFUMATRIZEN FUER DIE REMO-KORREKTUR

FOR MATERIAL 0 16 , TYPE SGNC THERE ARE C ANGULAR DISTRIBUTIONS WITH 0 ANGLE POINTS RETRIEVED FOR THIS TASK.
 THE LOWEST CALCULATED ENERGY GROUP NUMBER WITH SGNC IS 11.

IN MODULE S 128 K BYTES OF REGION G NOT USED.

CALCULATION FOR GROUP 12

FOR THIS ENERGY GROUP CALCULATION WITHOUT ANGULAR DISTRIBUTIONS.

NUMBER OF ENERGY POINTS RETRIEVED FOR MATERIAL 0 16 IN THE ENERGY-RANGE 4.649996E+03 , 1.000000E+04 EV.

SGT 2
 SGN 2
 MUEL 2

TOTAL NUMBER OF DIFFERENT POINTS 2

GROUP= 12 NUMBER OF FINE INTERVALS= 70 MATERIAL 0 16

THE INTERVAL-BOUNDARIES ARE

4.6499960937D+03	4.7022783861D+03	4.7545606785D+03	4.8068429709D+03	4.8591252633D+03	4.9114075557D+03
4.9666290313D+03	5.0218505069D+03	5.0777719825D+03	5.1322934581D+03	5.1875149337D+03	5.2458408263D+03
5.3041667188D+03	5.3624926114D+03	5.4203185039D+03	5.4791443964D+03	5.5407452287D+03	5.6023540610D+03
5.6639588932D+03	5.7255637255D+03	5.7871685577D+03	5.8522366637D+03	5.9173047697D+03	5.9823728757D+03
6.0474409817D+03	6.1125090876D+03	6.1812351641D+03	6.2499612407D+03	6.3186873172D+03	6.3874133937D+03
6.4561294702D+03	6.5287291595D+03	6.6013188487D+03	6.6739085380D+03	6.7464982272D+03	6.8190879165D+03
6.8957584214D+03	6.9724289262D+03	7.0490994311D+03	7.1257699360D+03	7.2024404409D+03	7.2834211750D+03
7.3644019090D+03	7.4453826431D+03	7.5263633771D+03	7.6073441112D+03	7.6928773850D+03	7.7784106588D+03
7.8639439326D+03	7.9494772064D+03	8.0350104802D+03	8.1253522650D+03	8.2156939728D+03	8.3060357190D+03
8.3962774653D+03	8.4867192116D+03	8.5821397509D+03	8.6775602903D+03	8.7729808296D+03	8.8684013690D+03
8.9638219083D+03	9.0646067581D+03	9.1653916079D+03	9.2661764577D+03	9.3669613075D+03	9.4677461573D+03
9.5741968861D+03	9.6806476148D+03	9.7870983436D+03	9.8935490723D+03	9.9999980110D+03	

THE VALUES OF SGT

3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00

THE VALUES OF SGN

3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00
3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00	3.7000E+00

THE VALUES OF MUEL

4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02
4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02
4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02
4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02
4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02
4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02
4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02
4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02	4.1700E-02

THE VALUES OF FLUX

2.0432E-01	2.0206E-01	1.9985E-01	1.9771E-01	1.9558E-01	2.0432E-01	2.0206E-01	1.9986E-01	1.9770E-01	1.9557E-01
2.0433E-01	2.0206E-01	1.9986E-01	1.9769E-01	1.9557E-01	2.0433E-01	2.0207E-01	1.9986E-01	1.9769E-01	1.9558E-01
2.0432E-01	2.0207E-01	1.9985E-01	1.9769E-01	1.9559E-01	2.0433E-01	2.0207E-01	1.9985E-01	1.9770E-01	1.9558E-01
2.0432E-01	2.0207E-01	1.9986E-01	1.9769E-01	1.9558E-01	2.0433E-01	2.0206E-01	1.9986E-01	1.9770E-01	1.9557E-01
2.0432E-01	2.0206E-01	1.9985E-01	1.9770E-01	1.9558E-01	2.0432E-01	2.0207E-01	1.9985E-01	1.9770E-01	1.9557E-01
2.0433E-01	2.0206E-01	1.9986E-01	1.9769E-01	1.9558E-01	2.0432E-01	2.0207E-01	1.9986E-01	1.9769E-01	1.9558E-01
2.0433E-01	2.0207E-01	1.9986E-01	1.9769E-01	1.9558E-01	2.0432E-01	2.0206E-01	1.9986E-01	1.9769E-01	1.9558E-01

ELASTIC SCATTERING MATRIX SGNCO FOR D 16 GROUP= 12

FROM GROUP	12 TO GROUP	12								
2.4930E-02	7.4146E-02	1.2229E-01	1.6940E-01	2.1551E-01	2.6189E-01	3.0851E-01	3.5411E-01	3.9873E-01	4.4241E-01	
4.8633E-01	5.3749E-01	5.7369E-01	6.1596E-01	6.5732E-01	6.9893E-01	7.4076E-01	7.8168E-01	8.2171E-01	8.6089E-01	
9.0030E-01	9.3992E-01	9.7867E-01	9.9994E-01	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	
1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	
1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	
1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	
1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E+00	
FROM GROUP	12 TO GROUP	13								
9.7507E-01	9.2585E-01	8.7771E-01	8.3060E-01	7.8449E-01	7.3811E-01	6.9150E-01	6.4589E-01	6.0127E-01	5.5760E-01	
5.1367E-01	4.6951E-01	4.2631E-01	3.8404E-01	3.4268E-01	3.0107E-01	2.5924E-01	2.1832E-01	1.7829E-01	1.3911E-01	
5.9699E-02	6.0082E-02	2.1328E-02	6.4071E-05	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

```

ELASTIC SCATTERING MATRIX  SGNC1 FOR C 16      GRUP= 12
FROM GROUP 12 TO GROUP 12
  2.4195E-02  6.9073E-02  1.0876E-01  1.4351E-01  1.7356E-01  1.5979E-01  2.2210E-01  2.3993E-01  2.5352E-01  2.6308E-01
  2.6891E-01  2.7093E-01  2.6913E-01  2.6371E-01  2.5486E-01  2.4237E-01  2.2618E-01  2.0676E-01  1.8429E-01  1.5955E-01
  1.3005E-01  9.7555E-02  6.2373E-02  4.1764E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02
  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02
  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02
  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02
  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02  4.1700E-02
FROM GROUP 12 TO GROUP 13
  1.7505E-02 -2.7374E-02 -6.7056E-02 -1.0180E-01 -1.3186E-01 -1.5809E-01 -1.8040E-01 -1.9323E-01 -2.1182E-01 -2.2138E-01
  -2.2721E-01 -2.2923E-01 -2.2743E-01 -2.2201E-01 -2.1316E-01 -2.0067E-01 -1.8448E-01 -1.6506E-01 -1.4259E-01 -1.1725E-01
  -8.8349E-02 -5.5855E-02 -2.0673E-02 -6.3965E-05  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

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ELASTIC SCATTERING MATRIX  SGNC2 FOR C 16      GRUP= 12
FROM GROUP 12 TO GROUP 12
  2.2773E-02  5.9644E-02  8.4723E-02  9.9697E-02  1.0612E-01  1.0526E-01  9.8065E-02  8.5812E-02  6.9790E-02  5.1172E-02
  3.0449E-02  8.5935E-03 -1.2811E-02 -3.2821E-02 -5.0585E-02 -6.5653E-02 -7.7126E-02 -8.3682E-02 -8.4711E-02 -7.9638E-02
  -6.7489E-02 -4.7244E-02 -1.8639E-02  7.3013E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04
  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04
  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04
  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04  7.9535E-04
FROM GROUP 12 TO GROUP 13
  2.2003E-02 -5.8874E-02 -8.3954E-02 -9.8927E-02 -1.0535E-01 -1.0449E-01 -9.7295E-02 -8.5042E-02 -6.9020E-02 -5.0402E-02
  -2.9675E-02 -7.8243E-03  1.3581E-02  3.3591E-02  5.1359E-02  6.6463E-02  7.7896E-02  8.4452E-02  8.5481E-02  8.0408E-02
  6.8258E-02  4.8013E-02  1.9409E-02  6.3751E-05  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

```

```

ELASTIC SCATTERING MATRIX  SGNC3 FOR C 16      GRUP= 12
FROM GROUP 12 TO GROUP 12
  2.0758E-02  4.7165E-02  5.5412E-02  5.0870E-02  3.7988E-02  1.9964E-02 -6.1161E-04 -2.0375E-02 -3.7482E-02 -5.0550E-02
  -5.9020E-02 -6.2021E-02 -5.9341E-02 -5.1481E-02 -3.9301E-02 -2.3496E-02 -5.4317E-03  1.2577E-02  2.8380E-02  3.5653E-02
  4.3890E-02  3.7668E-02  1.7619E-02  6.3371E-05  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
FROM GROUP 12 TO GROUP 13
  -2.0759E-02 -4.7166E-02 -5.5413E-02 -5.0871E-02 -3.7989E-02 -1.9865E-02  6.1058E-04  2.0374E-02  3.7481E-02  5.0589E-02
  5.9019E-02  6.2020E-02  5.9340E-02  5.1480E-02  3.9300E-02  2.3495E-02  5.4306E-03 -1.2578E-02 -2.8381E-02 -3.5654E-02
  -4.3891E-02 -3.7669E-02 -1.7620E-02 -6.3432E-05  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

```

```

ELASTIC SCATTERING MATRIX  SGNC4  FOR C  16  GROUP= 12
FROM GROUP 12 TO GROUP 12
  1.8280E-02  3.3293E-02  2.6764E-02  9.9353E-03 -9.4075E-03 -2.6616E-02 -3.8343E-02 -4.2714E-02 -3.9891E-02 -3.1054E-02
 -1.7559E-02 -1.5954E-03  1.4121E-02  2.7240E-02  3.5906E-02  3.8857E-02  3.5161E-02  2.5138E-02  1.0466E-02 -5.5646E-03
 -2.0293E-02 -2.6227E-02 -1.5427E-02 -6.3262E-05 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07
 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07
 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07 -2.5103E-07
FROM GROUP 12 TO GROUP 13
 -1.8280E-02 -3.3294E-02 -2.6764E-02 -9.9355E-03  9.4076E-03  2.6616E-02  3.8342E-02  4.2714E-02  3.9891E-02  3.1053E-02
  1.7599E-02  1.5951E-03 -1.4122E-02 -2.7240E-02 -3.5906E-02 -3.8858E-02 -3.5161E-02 -2.5138E-02 -1.0466E-02  5.5643E-03
  2.0293E-02  2.6227E-02  1.5427E-02  6.3009E-05  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

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ELASTIC SCATTERING MATRIX  SGNC5  FOR D  16  GROUP= 12
FROM GROUP 12 TO GROUP 12
  1.5493E-02  1.9753E-02  3.8694E-03 -1.4678E-02 -2.7070E-02 -3.0199E-02 -2.4099E-02 -1.1559E-02  3.4979E-03  1.7329E-02
  2.7192E-02  3.0876E-02  2.7581E-02  1.8350E-02  5.3975E-03 -8.6760E-03 -2.0370E-02 -2.6060E-02 -2.3784E-02 -1.3665E-02
  1.7278E-03  1.5139E-02  1.2970E-02  6.2536E-05  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
FROM GROUP 12 TO GROUP 13
 -1.5493E-02 -1.9753E-02 -3.8694E-03  1.4678E-02  2.7070E-02  3.0199E-02  2.4099E-02  1.1559E-02 -3.4980E-03 -1.7329E-02
 -2.7192E-02 -3.0876E-02 -2.7581E-02 -1.8350E-02 -5.3975E-03  8.6760E-03  2.0370E-02  2.6060E-02  2.3784E-02  1.3665E-02
 -1.7278E-03 -1.5139E-02 -1.2970E-02 -6.2536E-05  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0

```

IN MODULE 9 3.40 SECONDS CPU-TIME ARE USED

DATE 22.11.76 TIME 18.48.07

Appendix B. Program Listing

On the following pages B 2 to B 144 the listing of the program MIGRØS-3 is given.

C	PROGRAMM ZUR STEUERUNG DES MIGROS-SYSTEMS	10	6 IF(MAT1.EQ.N1.AND.MAT2.NE.3) GO TO 7	560
C		20	RFAD (NF) NA	570
	REAL*8 MAT1,N1,N2,MIGROS,DD	30	READ (NF) MAT1,MAT2	580
	DIMENSION XL(5000),NXL(5000)	40	IZI=IZI+2	590
	COMMON MAT1,K(2),NOUT,LIZ	50	GC TO 9	600
	EQUVALENCE (XL(1),NXL(1))	60	7 WRITE (NOUT,8)	610
	DATA N1/'BLOC '/,N2/'ENDE '/,SGC/'SGC '/,MIGROS/'MIGR '/,	70	8 FORMAT(1H0/' ***ERROR 0. 1 : THE INPUT OF THE MCCULE NUMBERS WAS N	620
	ICC/'FT10FOO1'/'	80	10T FOUND')	630
	NINP=5	90	STCP	640
	NCUT=6	100	9 IF(MAT1.EQ.N1.AND.MAT2.EQ.4) GO TO 10	650
	KDF=1	110	NT=3	660
	LIZ=3	120	GC TO 11	670
	NF=8	130	10 READ (NF) NT	680
	N6=10	140	RFAD (NF) MAT1,MAT2	690
	CALL FSP IE	150	IZI=IZI+2	700
	READ (NINP,28) MAT1	160	11 IF(MAT1.EQ.N1.AND.MAT2.EQ.5) GO TO 12	710
28	FORMAT(A8)	170	MI=7	720
	IF(MAT1.EQ.MIGROS) GO TO 27	180	GC TO 13	730
	REWIND NINP	190	12 RFAD (NF) MI	740
	CALL EING(NOUT)	200	READ (NF) MAT1,MAT2	750
27	CALL NDFOPN (KDE,NXL,NUDAT,0)	210	IZI=IZI+2	760
	WRITE (NOUT,1) NUDAT	220	13 IF(MAT1.EQ.N1.AND.MAT2.EQ.6) GO TO 14	770
1	FORMAT(1H1/' STAND DER KERNDATENRIEHL IOTHEK VOM',IIC)	230	NTYP=8	780
	WRITE (LIZ) LIZ	240		
	BACKSPACE LIZ	250	GO TO 15	790
	WRITE (NF) NF	260	14 READ (NF) NTYP	800
	BACKSPACE NF	270	BACKSPACE NF	810
	ICON=0	280	N=M+NTYP-1	820
	N=1	290	READ (NF) NTYP,(XL(I),XL(I+200),I=M,N)	830
	CALL DDTEST (N,DD,ICON,NST)	300	24 RFAD (NF) MAT1,MAT2	840
	IF(NST.EQ.1) GO TO 29	310	IZI=IZI+2	850
	WRITE (N6) N6	320	CC 26 I=M,N	860
	BACKSPACE N6	330	IF(XL(I).EQ.SGC) NTYP=NTYP+1	870
25	CALL GARFA (XL,M,L)	340	26 CCNTINUE	880
	JADR=M+L	350	15 IF(MAT1.EQ.N1.AND.MAT2.LT.62) GC TO 22	890
	M=M+1	360	IF(MAT1.EQ.N1.AND.MAT2.GT.62) GO TO 23	900
	CALL FREE72 (NINP,NF,NOUT,XL(M),XL(M),XL(M))	370	IF(MAT1.EQ.N2) GO TO 23	910
	IZI=0	380	READ (NF) NMAT	920
2	READ (NF)	390	IZI=IZI+1	930
16	READ (NF) MAT1,MAT2	400	GO TO 25	940
	IZI=IZI+2	410	22 READ (NF)	950
	IF(MAT1.EQ.N1.AND.MAT2.EQ.1) GO TO 3	420	READ (NF) MAT1,MAT2	960
	NE=26	430	IZI=IZI+2	970
	GC TO 4	440	GC TO 15	980
3	READ (NF) NF	450	23 NMAT=1	990
	RFAD (NF) MAT1,MAT2	460	25 CC 17 I=1,IZI	1000
	IZI=IZI+2	470	17 BACKSPACE NF	1010
4	IF(MAT1.EQ.N1.AND.MAT2.EQ.2) GO TO 5	480	NM =NTYP*2+M	1020
	NFF=1	490	NZ=NM+NMAT*2	1030
	LSPEC=1	500	NENG=NZ+NMAT	1040
	GC TO 6	510	NSPEC=NENG+NE	1050
5	READ (NF) LSPEC,NFE	520	NARB=NSPEC+NFE*(LSPEC+1)	1060
	NFE=NFF+NE	530	NTEMP=NARB+NA*3	1070
	RFAD (NF) MAT1,MAT2	540	NSI=NTEMP+NT	1080
	IZI=IZI+2	550	NG=NSI+MI+1	1090
			NN1=NG+NA	1100

NN2=NN1+NA*NE	1110	NTT=4000	270
NFG=NN2+NA*NE	1120	NMAX=5	280
NFI=NFG+NA*NE	1130	ICCS=21	290
NGG=NFI+NA*NE	1140	ISM=400	300
NII=NGG+NE	1150	ISC = 1000	310
NFR=NII+NE	1160	NFCU = 2	320
I=NFR/2*2	1170	NFF=200	330
IF(I.EQ.NFR) NFR=NFR+1	1180	ISCO=ISM*ICCS	340
IF(NFR.LT.IADR) GO TO 20	1190	ISEC=ISD	350
WRITE (NOUT,21)	1200	IPEMO=0	360
21 FORMAT(1H0/' ***ERROR 0, 2 : THE REGION - FIELD IS ALREADY TOO SHO	1210	MAXERR=5	370
IRT FOR THE CONTROL MODULE')	1220	NINA=0	380
STCP	1230	READ (NF) MAT,ISTRUK	390
20 NX=NE+1	1240	WRITE(NOUT,3003)MAT	400
CALL INPUT (XL(M),XL(NM),XL(NZ),	1250	3003 FORMAT('14 T G R O S - 3 TASK FOR MATERIAL',A10,'/ ' ,45('**'))	410
1 XL(NENG),XL(NSPEC),XL(NARB),XL(NTEMP),XL(NSI),	1260	READ (NF) MAT1,MAT2	420
1 XI(NG),XL(NN1),XL(NN2),XL(NFG),XL(NFI),XL(NGG),XL(NII),	1270	ISPA=0	430
3 NMAT,MI+1,NE,LSPEC+1,NFE,NA,NT,NTYP,NFR,XL,NF,NX,IADR)	1280	C TSPA IS ONLY EXISTENT BECAUSE OF HISTORICAL REASONS	440
IZI=0	1290	IF(MAT2-11,7,8	450
READ (NF) MAT1	1300	7 READ (NF) NE,(ENG(I),I=1,NE)	460
IF(MAT1.NE.N2) GO TO 16	1310	READ (NF) MAT1,MAT2	470
I=C	1320	DO 9 I=2,NE	480
WRITE (LIZ) I,N2	1330	IF(ENG(I).LT.ENG(I-1)) GO TO 10	490
RETURN	1340	9 CONTINUE	500
END	1350	GO TO 14	510
		10 WRITE (NOUT,12) (ENG(I),I=1,NE)	520
		12 FORMAT(1H0/' ***ERROR 0, 3 : THE ENERGY GROUP BOUNDARIES'/(8E16,8)	530
		1)	540
		WRITE (NOUT,13)	550
		13 FORMAT(' ARE NOT GIVEN IN AN INCREASING ORDER')	560
		GO TO 5000	570
		8 NF=26	580
		ENG(1)=0.215	590
		ENG(2)=0.455	600
		ENG(3)=1.	610
		DC 15 K=1,5	620
		DC 15 J=1,3	630
		MC=3*(K-1)+J	640
		15 ENG(MD+3)=ENG(MD)*10,	650
		ENG(19)=0.2E6	660
		ENG(20)=0.4E6	670
		ENG(21)=0.8E6	680
		ENG(22)=1.4E6	690
		ENG(23)=2.5E6	700
		ENG(24)=4.0E6	710
		ENG(25)=6.5E6	720
		ENG(26)=1.0E7	730
		14 IF(MAT2-2)1,16,17	740
		16 READ (NF) LSP,NFE,((EF(I,J),I=1,NFE),J=1,NSPEC)	750
		READ (NF) MAT1,MAT2	760
		DC 19 I=2,NFE	770
		IF(EF(I,1).LE.EF(I-1,1)) GO TO 19	780
		18 CONTINUE	790
		GO TO 20	800
		19 WRITE (NOUT,21)	810
C	PROGRAMM ZUM LESEN UND PRUEFFEN DER EINGABE FUER DAS MICROS-SYSTEM	10	
C		20	
	SUBROUTINE INPUT (ITYP,NAME,TZ,ENG,EF,NR,TEMP,SIGC,NRE,NN1,NN2,	30	
	INFG,NFI,NG,NI,NMAT,MI,NE,NSPEC,NFE,NA,NT,NTYP,NFR,XL,NF,NX,IADR)	40	
	REAL*8 MAT1, MAT, ITYP,N2,NAME,SGC,SGA,SGF	50	
	I,DAT,TIME	60	
	DIMENSION ENG(NE),EF(NE,NSPEC),NAME(NMAT),TZ(NMAT),MAZ(2),	70	
	1 NR(3,NA),TEMP(NT),SIGC(MI),ITYP(NTYP),	80	
	1 IPM(2), NRE(NA),NN1(NA,NF),NN2(NA,NE),NFC(NA,NE),NFI(NA,NF)	90	
	2,XL(1),NG(NE),NI(NE),ENBER(5),NWFUN(5),CONWFU(5),INTYP(3)	100	
	COMMON MAT,ISTRUK,ISPA,NOUT,LIZ,NANF,NEND,KL	110	
	COMMON/CFS DUR / I DLR	120	
	EQUIVALENCE (MAT,IPM(1))	130	
	DATA N2/'ENDE ' /	140	
	1 ,SGC/'SGC ' /,SGA/'SGA ' /,SGF/'SGF ' /	150	
	CALL FSP1E	160	
	MIBER=5	170	
	MARWF=0	180	
	MAXINT=200	190	
	MABQ1=200	200	
	MABQ2=200	210	
	MABQ3=200	220	
	KPRCM=20	230	
	LDIM=1500	240	
	IRF=300	250	
	ISTE=400	260	

21	FORMAT(1H0/' ***ERROR 0. 4 : THE ENERGY POINTS OF THE MACROSCOPIC	820	115	FORMAT(1H0/' ***ERROR 0. 6 : THE MACROSCOPIC WEIGHTING FUNCTION DO	1370
	WEIGHTING FUNCTION ARE NOT GIVEN IN AN INCREASING ORDER')	830		IFS NOT INCLJDF ALL ENERGY GROUPS DESIRED')	1380
	GO TO 5000	840		GO TO 5000	1390
17	NFE=1	850	114	CONTINUE	1400
	LSP=0	860		READ (NF) MAT1,MAT2	1410
20	DC 3001 NT=2, NSPEC	870		GO TO 24	1420
	NSPEC1=NT-1	880	23	WRITE (NOUT,25)	1430
	IF(NSPEC .GT. 2)WRITE(NOUT,3002)NSPEC1	890	25	FORMAT(1H0/' ***ERROR 0. 7 : THE IDENTIFICATION NUMBERS OF MODULES	1440
3002	FORMAT(/' PRINTOUT FOR SPECTRUM NR.,I5)	900		1 TO BE CALLED CAN NOT BE FOUND')	1450
3001	CALL PRPHI(NFE,EF(1,1),EF(1,NT))	910		GO TO 5000	1460
	IF(MAT2=3)I,22,23	920	24	IF(MAT2=4)I,26,27	1470
22	READ (NF) NA,(NR(1,I),NR(2,I),NR(3,I),I=1,NA)	930	26	READ (NF) NT,(TEMP(I),I=1,NT)	1480
	DO 11 I=1,NA	940		READ (NF) MAT1,MAT2	1490
	IF(NR(2,I).GE.NR(3,I).AND.NR(2,I).LE.(NF-1)) GO TO 11	950		DO 28 I=1,NA	1500
	IF(NR(1,I).EQ.1).AND.NR(3,I).LE.NF) GO TO 11	960		IF(NR(1,I).EQ.1.OR.NR(1,I).EQ.2) GO TO 29	1510
	WRITE (NOUT,54) NR(1,I)	970	28	CONTINUE	1520
54	FORMAT(1H0/' ***ERROR 0. 5 : THE CHOICE OF ENERGY GROUP BOUNDARIES	980		WRITE (NOUT,30)	1530
	1 FOR PROGRAM',I6,' IS NOT VALID')	990	30	FORMAT(1H0/' ***WARNING 0. 2 : THE DECLARATION OF THE TEMPERATURE	1540
	GO TO 5000	1000		1 IS NOT NECESSARY AND IS IGNORED')	1550
11	CONTINUE	1010		GO TO 29	1560
	IF(NFE.EQ.1) GO TO 114	1020	27	DO 31 I=1,NA	1570
	MTN=1	1030		IF(NR(1,I).EQ.1.OR.NR(1,I).EQ.2) GO TO 32	1580
	MAX=NE-1	1040	31	CONTINUE	1590
	DO 112 I=1,NA	1050		NT=0	1600
	IF(NR(2,I).GT.MIN) MIN=NR(2,I)	1060		GO TO 29	1610
	IF(NR(3,I).LT.MAX) MAX=NR(3,I)	1070	32	IF(ISTRUK.EQ.0) GO TO 34	1620
112	CONTINUE	1080		NT=3	1630
	AN=ENG(NE-MIN)	1090		TEMP(1)=300.	1640
	END=ENG(NE-MAX+1)	1100		TEMP(2)=900.	1650
	KL=NE-MIN	1110		TEMP(3)=2100.	1660
	M=NE-MAX+1	1120		GO TO 29	1670
	J=1	1130	34	NT=1	1680
	DO 200 I=KL,M	1140		TEMP(1)=0.	1690
202	IF(ENG(I).EQ.EF(J,1)) GO TO 200	1150	29	IF(MAT2=5)I,33,35	1700
	IF(FNG(I).LT.EF(J,1)) GO TO 201	1160	33	READ (NF) MI,(SIGO(I),I=1,MI)	1710
	J=J+1	1170		MS=MI	1720
	GO TO 202	1180		IF(SIGO(MI).GE.10.**6) GO TO 2002	1730
201	DO 203 NT=1, NSPEC	1190		MS=MI+1	1740
	DO 203 N=J, NFE	1200	2002	READ (NF) MAT1,MAT2	1750
	K=NFE-N+J	1210		DO 36 I=1,NA	1760
203	EF(K+1,NT)=EF(K,NT)	1220		IF(NR(1,I).EQ.1.OR.NR(1,I).EQ.2.OR.NR(1,I).EQ.3) GO TO 37	1770
	NFE=NFE+1	1230	36	CONTINUE	1780
	IF(ENG(I).GT.(EF(J-1,1)+EF(J+1,1))*0.5) GO TO 206	1240		WRITE (NOUT,38)	1790
	DO 204 NT=2, NSPEC	1250	38	FORMAT(1H0/' ***WARNING 0. 3 : THE DECLARATION OF THE BACKGROUND C	1800
204	EF(K,NT)=EF(K+1,NT)-(EF(K+1,NT)-EF(K-1,NT))/(EF(K+1,1)-	1260		ROSS SECTIONS IS NOT NECESSARY AND IS IGNORED')	1810
	1EF(K-1,1))*(EF(K+1,1)-FNG(I))	1270		GO TO 37	1820
	GO TO 205	1280	35	DO 39 I=1,NA	1830
206	DO 207 NT=2, NSPEC	1290		IF(NR(1,I).EQ.1.OR.NR(1,I).EQ.2.OR.NR(1,I).EQ.3) GO TO 40	1840
207	EF(K,NT)=EF(K-1,NT)+(EF(K+1,NT)-EF(K-1,NT))/(EF(K+1,1)-EF(K-1,1))*	1300	39	CONTINUE	1850
	1(ENG(I)-EF(K-1,1))	1310		MI=0	1860
205	EF(K,1)=ENG(I)	1320		GO TO 37	1870
200	CONTINUE	1330	40	MI=7	1880
	IF(EF(1,1).GT.AN) GO TO 113	1340		MS=MI	1890
	IF(EF(NFE,1).GE.END) GO TO 114	1350		SIGO(1)=0.	1900
113	WRITE (NOUT,115)	1360		DO 41 I=1,6	1910

41 SIGO(I+1)=1).**I	1920	GC TO 52	2470
37 IF(MAT2-6)1,42,43	1930	50 NRES=-1	2480
42 READ (NF) NTYP,(ITYP(I),I=1,NTYP)	1940	52 IF(MAT2-12)1,56,57	2490
READ (NF)MAT1,MAT2	1950	56 READ (NF) ERROR	2500
DO 149 I=1,NTYP	1960	READ (NF) MAT1,MAT2	2510
IF(ITYP(I).EQ.SGC) GO TO 150	1970	DO 58 I=1,NA	2520
149 CONTINUE	1980	IF(NR(1,I).EQ.1) GO TO 59	2530
GC TO 151	1990	58 CONTINUE	2540
150 DO 152 J=1,NTYP	2000	WRITE (NOUT,60)	2550
IF(ITYP(J).EQ.SGA) GO TO 153	2010	60 FORMAT(1H0/' ***WARNING O. 6 : THE DECLARATION OF THE ALLOWED INT	2560
152 CONTINUE	2020	TEGRATION ERROR IS NOT NECESSARY AND IS IGNORED')	2570
ITYP(I)=SGA	2030	GO TO 59	2580
153 DO 154 J=1,NTYP	2040	57 ERROR=0.01	2590
IF(ITYP(J).EQ.SGF) GO TO 155	2050	59 DO 3004 I=1,NA	2600
154 CONTINUE	2060	IF(NR(1,I).EQ.3) GO TO 3005	2610
IF(ITYP(I).EQ.SGA) GO TO 156	2070	3004 CONTINUE	2620
ITYP(I)=SGF	2080	IP=0	2630
GO TO 151	2090	GO TO 3006	2640
156 NTYP=NTYP+1	2100	3005 IP=1	2650
ITYP(NTYP)=SGF	2110	3006 IF(MAT2-31)1,300,301	2660
GO TO 151	2120	300 IF(IP.EQ.1) GO TO 3008	2670
155 IF(ITYP(I).EQ.SGA) GO TO 151	2130	WRITE (NOUT,3007)	2680
NTYP=NTYP-1	2140	3007 FORMAT(/' ***WARNING O.16 : THE INPUT FOR MODULE 3 IS NOT NECESSAR	2690
DO 157 J=1,NTYP	2150	LY')	2700
157 ITP(J)=ITYP(J+1)	2160	3008 READ(NF) EPSROM,DRINWA	2710
151 DO 44 I=1,NA	2170	READ(NF) MAT1,MAT2	2720
IF(NR(1,I).EQ.4) GO TO 45	2180	GOTO 302	2730
44 CONTINUE	2190	301 EPSROM=5.0F-5	2740
WRITE (NOUT,46)	2200	DRINWA=5.0	2750
46 FORMAT(1H0/' ***WARNING O. 4 : THE DECLARATION OF THE CROSS SECTION	2210	302 IF(MAT2-32) 1,303,304	2760
IN TYPES IS NOT NECESSARY AND IS IGNORED')	2220	303 IF(IP.EQ.1) GO TO 3009	2770
GO TO 45	2230	WRITE (NOUT,3007)	2780
43 DO 47 I=1,NA	2240	3009 READ(NF) ITFST,IZPUMS,ITUMS	2790
IF(NR(1,I).EQ.4.OR.NR(1,I).EQ.1) GO TO 48	2250	READ(NF) MAT1,MAT2	2800
47 CONTINUE	2260	GOTO 305	2810
NTYP=0	2270	304 ITFST=0	2820
GO TO 45	2280	IZPUMS=-1	2830
48 NTYP=8	2290	ITUMS=ITEST	2840
CALL DDPW (RHMUFL ,ITYP(1))	2300	305 IF(MAT2-33) 1,306,307	2850
CALL DDPW (RHNUF ,ITYP(2))	2310	306 IF(IP.EQ.1) GO TO 3010	2860
CALL DDPW (RHSGA ,ITYP(3))	2320	WRITE (NOUT,3007)	2870
CALL DDPW (RHSGF ,ITYP(4))	2330	3010 READ(NF) NENBER,(ENBER(I),NWFUN(I),CONWFUN(I),I=1,NENBER)	2880
CALL DDPW (RHSGI ,ITYP(5))	2340	READ(NF) MAT1,MAT2	2890
CALL DDPW (RHSGN ,ITYP(6))	2350	IF(NENBER.GE.1.AND.NENBER.LE.MAXEBR) GOTO 308	2900
CALL DDPW (RHSG2N ,ITYP(7))	2360	WRITE(NOUT,3016) NENBER,MAXEBR	2910
CALL DDPW (RHSGT ,ITYP(8))	2370	3016 FORMAT(1H0/' ***ERROR O.16 : NUMBER OF INTEGRATION REGIONS NENBER	2920
45 IF(MAT2-11)1,49,50	2380	*IS EQUAL',I5,'.'/17X,'BUT IT MUST BE GREATER THAN ZERO AND LESS OR	2930
49 READ (NF) NRES	2390	* EQUAL THAN ',I2,'.')	2940
READ (NF) MAT1,MAT2	2400	GO TO 5000	2950
DO 51 I=1,NA	2410	307 NENBER=1	2960
IF(NR(1,I).EQ.1) GO TO 52	2420	ENBER(1)=-1.0	2970
51 CONTINUE	2430	IF(NFE.LF.1) NWFUN(1)=0	2980
WRITE (NOUT,53)	2440	IF(NFE.GT.1) NWFUN(1)=-1	2990
53 FORMAT(1H0/' ***WARNING O. 5 : THE DECLARATION OF THE NUMBER OF RE	2450	CONWFUN(1)=1.0	3000
SONANCES IS NOT NECESSARY AND IS IGNORED')	2460	308 DO 3011 I=1,NA	3010

IF(NR(1,I).EQ.5) GO TO 3012	302C	WRITE (NOUT,83)	3570
3011 CONTINUE	3030	135 READ (NF) NMAT,(NAME(I),TZ(I),I=1,NMAT)	3580
IP=0	3040	READ (NF) MAT1,MAT2	359C
GO TO 3013	3050	NTK=1	3600
3012 IP=1	3060	GO TO 136	361C
3013 IF(MAT2.EQ.51) GO TO 400	307C	134 NTK=0	3620
KINEM=1	3080	136 IF(MAT2-63)1,137,140	363C
GO TO 401	3090	137 IF(IP.EQ.1) GO TO 139	364C
400 IF(IP.EQ.1) GO TO 3014	3100	WRITE(NOUT,83)	3650
WRITE (NOUT,3015)	3110	139 READ (NF) MW	3660
3015 FORMAT(/' ***WARNING 0. 7 : THE INPUT FOR MODULE 5 IS NOT NECESSAR	312C	IF (MW.EQ.1) GO TO 1000	3670
IY')	3130	IF(NTK.EQ.1) GO TO 2000	3680
3014 READ(NF) KINEM	3140	WRITE (NOUT,2001)	369C
READ(NF) MAT1,MAT2	3150	2001 FORMAT(1H0/' ***ERROR 0.15 : MODULE 6 CANNOT BE STARTED, BECAUSE A	3700
401 IF(MAT2-52)1,63,64	3160	ILOC 12 MUST BE GIVEN IF MW=2 IN BLOCK 13')	3710
63 IF(IP.EQ.1) GO TO 3018	3170	GO TO 5000	3720
WRITE (NOUT,3015)	3180	MAZ(1)=0	373C
3018 READ (NF) XNUE	2190	MAZ(2)=1	374C
READ (NF) MAT1,MAT2	3200	GO TO 1001	3750
GO TO 66	321C	1000 MAZ(1)=1	376C
64 XNUE=0.16	3220	MAZ(2)=0	3770
66 IF(MAT2.EQ.53) GO TO 402	3230	1001 READ (NF) MAT1,MAT2	378C
NIN=2	324C	IF(MAZ(1).EQ.0) GO TO 138	379C
INTYP(1)=1	3250	IF(LSP.EQ.0) GO TO 138	3800
INTYP(2)=2	3260	IF(LSP-(NLE+1))142,138,138	3810
GO TO 403	3270	142 LP=NLE+1	3820
402 IF(IP.EQ.1) GO TO 3017	3280	WRITE (NOUT,143) LP	3830
WRITE (NOUT,3015)	329C	143 FORMAT(1H0/' ***ERROR 0. 8 : THE NUMBER OF WEIGHTING FUNCTIONS IS	384C
3017 READ(NF) NIN,(INTYP(IS),IS=1,NIN)	3300	'LESS THAN THE NUMBER OF LEGENDRE MOMENTS.'/15,' NUMBER OF WEIGHTING	3850
READ(NF) MAT1,MAT2	331C	2G FUNCTIONS ARE NEEDED')	3860
403 DO 77 I=1,NA	3320	GO TO 5000	3870
IF(NR(1,I).EQ.6) GO TO 78	3330	140 MAZ(1)=0	3880
77 CONTINUE	3340	MAZ(2)=0	389C
IP=0	3350	138 IF(MAT2-64)1,145,146	3900
GO TO 79	3360	145 IF(IP.EQ.1) GO TO 147	3910
78 IP=1	3370	WRITE(NOUT,83)	3920
LSPEC=NEE*LSP	3380	147 READ(NF) NK,NRR	3930
79 IF(MAT2-61)1,80,81	3390	NS=NE	394C
80 IF(IP.EQ.1) GO TO 82	340C	READ(NF) MAT1,MAT2	3950
WRITE (NOUT,83)	3410	GO TO 148	3960
83 FORMAT(1H0/' ***WARNING 0. 8 : THE INPUT FOR MODULE 6 IS NOT NECES	3420	146 NS=NE	3970
SARY')	3430	NK=70	398C
82 READ (NF) ISEL,NLE	3440	NRR=16	3990
READ (NF) MAT1,MAT2	3450	148 IF(MAT2-81)1,85,96	4000
NLA=0	3460	85 READ (NF) EPS	4010
IF(NLE.LT.1) NLE=1	3470	READ(NF) MAT1,MAT2	4020
IF(NLE.GT.5) NLE=5	3480	GO TO 87	4030
GO TO 84	349C	86 EPS=0.01	404C
81 NLA=0	3500	87 DO 68 I=1,NA	405C
NLE=5	3510	IF(NR(1,I).EQ.9) GO TO 69	4060
ISEL=2	352C	68 CONTINUE	4070
84 IF(IP.EQ.0) GO TO 141	3530	IP=0	408C
IF(NFE.GT.0.AND.EF(1,1).EQ.0) EF(1,1)=1.E-3	3540	GO TO 70	409C
141 IF(MAT2-62)1,133,134	3550	69 IP=1	4100
133 IF(IP.EQ.1) GO TO 135	3560	70 IF(MAT2-91)1,71,72	411C

71 IF(IP.EQ.1) GO TO 73	4120	NEND=NR(3,KL)	467C
WRITE (NOUT,74)	4130	CALL DATUM (DAT,TIME)	468C
74 FORMAT(1H0/' ***WARNING D. 9 : THE INPUT FOR MODULE 9 IS NOT NECES	414C	WRITE (NOUT,3000) DAT,TIME	4690
1SARY')	4150	3000 FCRMAT(/' DATE ',A8,' TIME ',A8)	47CC
73 READ (NF) ERR,NJM,NUJM	4160	IF(NR(1,KL).EQ.1) GC TO 90	4710
READ (NF) MAT1,MAT2	4170	IF(NR(1,KL).EQ.2) GC TO 91	472C
GO TO 75	4180	IF(NR(1,KL).EQ.3) GC TO 92	473C
72 IF(IP.EQ.3) GO TO 75	4190	IF(NR(1,KL).EQ.4) GC TO 93	4740
ERR=0.01	4200	IF(NR(1,KL).EQ.5) GC TO 94	475C
NJM=10	4210	IF(NR(1,KL).EQ.6) GC TO 95	4760
NUJM=10	4220	IF(NR(1,KL).EQ.7) GC TO 96	477C
75 IF(MAT2-92)1,76,103	4230	IF(NR(1,KL).EQ.8) GC TO 97	4780
76 IF(IP.EQ.1) GO TO 104	424C	IF(NR(1,KL).EQ.9) GO TO 119	4790
WRITE (NOUT,74)	425C	IF(NR(1,KL).EQ.10) GC TO 120	48CC
104 READ (NF) ISELR,NLRA,NLRE,NCALL	4260	WRITE (NOUT,98) NR(1,KL)	4810
IF(NCALL.NE.0) GO TO 158	4270	98 FCRMAT(1H0/' ***ERROR 0.12 : THE DESIRED MODULE',I6,' IS NOT CONTA	4820
READ(NF)MAT1,MAT2	428C	INFD IN MIGROS')	4830
GO TO 175	4290	GC TO 5000	4840
158 IS=0	4300	126 IRE=IRE+IREP	4850
DO 109 I=1,NA	4310	ISTE=ISTE+ISTEP	4860
IF(NR(1,I).EQ.9) IS=IS+1	4320	B=ZEIT(A)	487C
109 CONTINUE	4330	WRITE (NOUT,1004) NR(1,KL),B	4880
IF(IS.EQ.NCALL) GO TO 111	4340	90 NCR=0	4890
WRITE (NOUT,111) IS,NCALL	435C	C=0.	49CC
111 FORMAT(1H0/' ***ERROR 0. 9 : MODULE 9 IS CALLED ',I3,' TIMES, IN T	4360	A=ZEIT(C)	4910
HE INPUT BLOC 92 NCALL IS SET TO',I3)	4370	J=NF+7*M+3*NE+7*IRE+6*ISTE	492C
GO TO 5000	438C	J=IABS(IADR-IJ)	4930
110 DO 106 I=1,NCALL	4390	IF(IADR.LT.IJ) GO TO 121	494C
READ (NF)NGRF,{NN1(I,J),NN2(I,J),NFG(I,J),NFI(I,J),J=1,NGRE)	440C	WRITE (NOUT,1003) NR(1,KL),J	495C
NRE(I)=NGRE	4410	1003 FORMAT(1H0/1H0/' IN MODULE',I3,I8,' WORDS ARE NOT USED IN THE REGI	4960
DO 106 J=1,NGRE	4420	1CA FIFD')	4970
IF(NN1(I,J).GE.NN2(I,J)) GO TO 106	443C	CALL FGM(MI,SIGO,NE,ENG,NFE,FF(1,1),EF(1,2),NT,TEMP,ERRCR,NRES,	4980
WRITE (NOUT,107) I	4440	1NGR,XL(NFR),XL(NFR+7*M),IRE,IREP,XL(NFR+7*M+3*NE),XL(NFR+7*M+3	4990
107 FORMAT(1H0/' ***ERROR 0.10 : IN BLOC 92 THE INPUT OF THE ENERGY GR	4450	23*NE+IRE),XL(NFR+7*M+3*NFI+IRE*2),XL(NFR+7*M+3*NE+3*IRE),	500C
1OUPS IS NOT VALID FOR THE ',I3,'. PROGRAM CALL')	4460	3XL(NFR+7*M+3*NE+4*IRE),XL(NFR+7*M+3*NE+5*IRE),	501C
GC TO 5000	4470	4XL(NFR+7*M+3*NE+6*IRE),ISTE,ISTEP,XL(NFR+7*M+3*NE+7*IRE),	502C
106 CONTINUE	448C	5XL(NFR+7*M+3*NE+7*IRE+5*ISTE)	5030
READ(NF)MAT1,MAT2	4490	IF(IREP.GT.0.CR.ISTEP.GT.0) GO TO 126	504C
GO TO 108	4500	B=ZEIT(A)	5050
103 NLRA=0	4510	WRITE (NOUT,1004) NR(1,KL-1),B	5060
NLRE=5	4520	1004 FCRMAT(1H0/' IN MODULE',I3,F8.2,' SECCNDS CPU-TIME ARE USED')	507C
ISELR=1	453C	IF(NGR.EQ.0) GO TO 101	5080
NCALL=0	4540	KL=KL-1	5090
105 NFG(1,1)=14	4550	NR(1,KL)=2	5100
NFI(1,1)=5	4560	NANF=MIND(NE-NGR,NR(2,KL))	511C
NRE(1)=1	4570	GC TO 91	512C
108 IF(MAT1.EQ.42) GO TO 88	458C	101 IF(KL.LE.NA) GO TO 100	5130
1 WRITE (NOUT,89)	4590	GC TO 102	5140
89 FORMAT(1H0/' ***ERROR 0.11 : THE INPUT IS NOT ORDERED IN INCREASIN	460C	51 IJ=NF+35*M	5150
1G ARGUMENTS')	4610	C=0.	5160
GO TO 5000	4620	A=ZEIT(C)	517C
88 NGR=0	463C	J=IABS(IADR-IJ)	5180
KL=1	4640	IF(IADR.LT.IJ) GO TO 121	5190
ISPATF=ISPA	4650	WRITE (NOUT,1003) NR(1,KL),J	5200
100 NANF=NR(2,KL)	4660	CALL FSTAT(MI,SIGO,NE,ENG,NFE,FF(1,1),EF(1,2),NT,TEMP,XL(NFR),	5210

IXL(NFR+15*MS),XL(NFR+30*MS))	5220	IF(ISIG.EQ.1) MI=MI-1	5770
B=ZFIT(A)	5230	IF(MIBERP.GT.0.OR.MABWFP.GT.0.OR.MXINTP.GT.0.OR.MABQ1P.GT.0.OR.	5780
WRITE(NOUT,1004) NR(1,KL-1),B	5240	*MABQ2P.GT.0.OR.MABQ3P.GT.0.OR.KMR0MP.GT.0.CR.MRFP.GT.0) GOTO 125	5790
NGR=0	5250	B=ZFIT(A)	5800
IF(KL.LE.NA) GO TO 100	5260	WRITE(NOUT,1004) NR(1,KL-1),B	5810
GO TO 102	5270	IF(KL.LE.NA) GO TO 100	5820
125 MIBER=MIBER+MIBERP	5280	GC TO 102	5830
MABWF=MABWF+MABWFP	5290	124 LDIM=LDIM+LDIMP	5840
MXINT=MXINT+MXINTP	5300	B=ZFIT(A)	5850
MABQ1=MABQ1+MABQ1P	5310	WRITE(NOUT,1004) NR(1,KL),B	5860
MABQ2=MABQ2+MABQ2P	5320	93 IJ=NFR+6*NE+2*LDIM	5870
MABQ3=MABQ3+MABQ3P	5330	C=C.	5880
KMR0M=KMR0M+KMR0MP	5340	A=ZFIT(C)	5890
B=ZFIT(A)	5350	J1=IABS(IADR-IJ)	5900
WRITE(NOUT,1004) NR(1,KL),B	5360	IF(IADR.LT.IJ) GO TO 121	5910
92 ISIG=0	5370	WRITE(NOUT,1003) NR(1,KL),J1	5920
C=0.	5380	CALL SOUND(NE,ENG,NFE,EF(1,1),EF(1,2),NTYP,ITYP,XL(NFR),	5930
A=ZFIT(C)	5390	1XL(NFR+NE),XL(NFR+2*NE),XL(NFR+3*NE),XL(NFR+4*NE),XL(NFR+5*NE),	5940
IF(SIGO(MI).GE.1.E6) GO TO 144	5400	2LDIM,LDIMP,XL(NFR+6*NE),XL(NFR+6*NE+LDIM))	5950
ISIG=1	5410	IF(LDIMP.GT.0) GO TO 124	5960
MI=MI+1	5420	B=ZFIT(A)	5970
SICO(MI)=1.E6	5430	WRITE(NOUT,1004) NR(1,KL-1),B	5980
144 IF(NFE.GT.1.AND.MABWF.LT.50) MABWF=50	5440	IF(KL.LE.NA) GO TO 100	5990
MRF=1	5450	GC TO 102	6000
IF(ISPATE.EQ.0) MRF=7	5460	54 C=C.	6010
IF(ISPATE.EQ.1) MRF=8	5470	A=ZFIT(C)	6020
IJ=NFR+3*MIBER+6*MI+MXINT+4*(MABWF+MABQ1+MABQ2+MABQ3)+2*KMR0M+	5480	IF(KINEM.NE.0.AND.KINEM.NE.1.AND.KINEM.NE.2) GO TO 3	6030
*4*MRF*MI	5490	NIN=NIN-NINA	6040
IF(IADR.LT.(IJ+10000)) GOTO 244	5500	CC 208 IS=1,NIN	6050
J1=(IADR-IJ)/18	5510	INTYP(IS)=INTYP(NINA+IS)	6060
MXINT=MXINT+J1	5520	IF(INTYP(IS).NE.1.AND.INTYP(IS).NE.2.AND.INTYP(IS).NE.3) GC TO 3	6070
MABQ1=MABQ1+J1	5530	208 CONTINUE	6080
MABQ3=MABQ3+J1	5540	GO TO 6	6090
244 I1=NFR	5550	3 WRITE(NOUT,1010)	6100
L2=L1+MIBER	5560	1010 FORMAT(1H0/' PRCGRAM 5 CANNOT BE STARTED, BECAUSE KINEM WAS NOT SE	6110
L3=L2+MIBER	5570	IT EQUAL TO 0, 1 OR 2/' OR FIELD INTYP WAS NOT SET EQUAL TO 1, 2	6120
L4=L3+MIBER	5580	2CR 3 IN THE INPUT')	6130
L5=L4+6*MI	5590	KL=KL+1	6140
L6=L5+4*MABWF	5600	GC TO 5	6150
L7=L6+MXINT	5610	6 NINA=0	6160
L8=L7+4*MABQ1	5620	CALL SCAT(NE,ENG,XNUE,NFE,EF(1,1),EF(1,2),NX,KINEM,NIN,NINA,INTYP,	6170
L9=L8+4*MABQ2	5630	1XL(NFR),XL(NFR),IADR-NFR+1,IJ)	6180
L10=L9+4*MABQ3	5640	IJ=NFR+IJ	6190
L10=L10+((L10+1)-((L10+1)/2))*2)	5650	J1=IABS(IADR-IJ)	6200
L11=L10+2*KMR0M	5660	IF(IADR.LT.IJ) GC TO 121	6210
L12=L11+2*MRF*MI	5670	5 WRITE(NOUT,1003) NR(1,KL-1),J1	6220
IJ=L12+2*MRF*MI	5680	B=ZFIT(A)	6230
J1=IABS(IADR-IJ)	5690	WRITE(NOUT,1004) NR(1,KL-1),B	6240
IF(IADR.LT.IJ) GO TO 121	5700	IF(KL.LE.NA) GC TO 100	6250
WRITE(NOUT,1003) NR(1,KL),J1	5710	GO TO 102	6260
CALL FSTRUK(MI,SIGO,NE,ENG,NFE,EF(1,1),EF(1,2),	5720	123 NECU=NECU+NECUP	6270
*NFRER,FNBER,NWFUN,CONWFU,EPSRCM,DRINWA,ITEST,17PUMS,ITUMS,ISPATE,	5730	IS=ISM+ISMP	6280
*MIBER,XL(L1),MIBERP,XL(L2),XL(L3),XL(L4),MABWF,XL(L5),MABWFP,	5740	ISD=ISD+ISDP	6290
*MXINT,XL(L6),MXINTP,MABQ1,XL(L7),MABQ1P,MABQ2,XL(L8),MABQ2P,	5750	ICCS=ICCS+ICOSP	6300
*MABQ3,XL(L9),MABQ3P,KMR0M,XL(L10),KMR0MP,XL(L11),MRF,XL(L12),MRFP)	5760	ISCO=MAX0(ISM*ICCS,ISCC+ISCCP)	6310

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ISCO=MAXO(ISCC,NECU*ISD)
ISEC=MAXO(ISM*NFCU,ISEC+ISECP)
ISEC=MAXO(ISFC,ISD)
ATT=NTT+NTTP
NANF=NANF-KIM
B=ZEIT(A)
WRITE (NOUT,1004) NR(1,KL),B
95 L=NFR+5*ISM
C=C.
A=ZEIT(C)
M=L+7*ISD
N=M+2*ICOS
NN=N+4*NX
MM=NN+7*NE
IJ=MM+ISCO+ISEC+6*NFCU*NE+8*NE+2*NTT+2*ISD
JI=IABS(IADR-IJ)
IF(IADR.LT.IJ) GO TO 121
WRITE (NOUT,1003) NR(1,KL),JI
CALL FLUMMI(XL(NFR),XL(NFR+ISM),XL(NFR+2*ISM),XL(NFR+3*ISM),
1XL(NFR+4*ISM),XL(NFR+5*ISM),XL(L+ISD),XL(L+2*ISD),
2XL(L+3*ISD),XL(L+4*ISD),XL(L+5*ISD),XL(L+6*ISD),XL(L+7*ISD),
3XL(M+ICOS),XL(M+2*ICOS),XL(N+NX),XL(N+2*NX),XL(N+3*NX),ENG,
4XL(N+4*NX),XL(NN+NE), EF(1,1),EF(1,2),XL(NN+7*NE),
5XL(M+ISCO),XL(M+ISCO+ISEC),XL(MM+ISCO+ISEC+6*NECU*NE),
6XL(MM+ISCO+ISEC+6*NFCU*NE+2*NE),
8XL(MM+ISCO+ISEC+6*NFCU*NE+2*NE+NTT),NAME,TZ,
6 NIA, NLE, ISEL, NMAX, NFN, NX, NFE, LSPEC, MAZ, NTK, NMAT, ATT, NTTP,
e ICOS, ICOSP, NECU, NECUP, ISM, ISMP, ISD,
7 ISCP, ISCO, ISPOP, ISEC, ISECP, KIM, NS, NK, NRR, XL(MM+ISCO+ISEC+6*NECU*
8NF+2*NE+2*NTT),XL(MM+ISCO+ISEC+6*NECU*NE+2*NE+2*NTT+ISD),XL(MM+
9ISCO+ISEC+6*NECU*NE+2*NE+2*NTT+2*ISD))
IF(NECUP.GT.0.OR.ISMP.GT.0.OR.ISCP.GT.0.OR.ISCO.GT.0.OR.
1ICOSP.GT.0.OR.ISECP.GT.0.OR.NTT.GT.0) GC TO 123
B=ZEIT(A)
WRITE (NOUT,1004) NR(1,KL-1),B
IF(KL.LE.NA) GO TO 100
GC TO 102
96 IJ=NFR+NE
C=C.
A=ZEIT(C)
JI=IABS(IADR-IJ)
IF(IADR.LT.IJ) GO TO 121
WRITE (NOUT,1003) NR(1,KL),JI
CALL SPALT(NE,ENG,XL(NFR))
B=ZEIT(A)
WRITE (NOUT,1004) NR(1,KL-1),B
IF(KL.LE.NA) GO TO 100
GO TO 102
97 C=C.
A=ZEIT(C)
IJ=NFR+NE+2*NEF
JI=IABS(IADR-IJ)
IF(IADR.LT.IJ) GO TO 121
WRITE (NOUT,1003) NR(1,KL),JI
CALL EDV(NE,ENG,NFF,EF(1,1),EF(1,2),EPS,XL(NFR),NEF,XL(NFR+NE),

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IXL(NFR+NE+NEF),IW)
B=ZEIT(A)
WRITE (NOUT,1004) NR(1,KL-1),B
IF(IW.EQ.1) GC TO 97
IF(KL.LE.NA) GO TO 100
GC TO 102
119 IREMO=IREMO+1
C=C.
A=ZEIT(C)
IF(NCALL.EQ.C) IREMO=1
L=NANF-NEND+1
M=NRE(IREMO)
NN=NEND
IF(NCALL.EQ.0) NN1(1,1)=NANF
IF(NCALL.EQ.0) NN2(1,1)=NEND
CC 128 N=1,M
125 NG(NN)=NFG(IREMC,N)
NI(NN)=NFI(IREMO,N)
NA=NN+1
IF(NN.LE.NEND+NN1(IREMC,N)-NN2(IREMO,N)+1) GC TO 129
128 CCATINUE
IF(NN-L.EQ.NEND+L) GO TO 130
WRITE(NOUT,131)
131 FCFORMAT(140/' ***ERROR 0.13 : FOR MODULE 9 THE INPUT BLOCs 4 AND 16
1 DC NOT CORRESPOND')
KL=KL+1
GC TO 132
13C CALL REMO(NE,ENG,NFE,EF(1,2),EF(1,1),EPR,NLRA,NLRE,L,NG,NI,NJM,
1NUJM,ISEL,XL(NFR),XL(NFR),IADR-NFR+1)
B=ZEIT(A)
WRITE (NOUT,1004) NR(1,KL-1),B
132 IF(KL.LE.NA) GO TO 100
GO TO 102
120 IJ=IADR-NFR
WRITE (NOUT,1003) NR(1,KL),IJ
C=C.
A=ZEIT(C)
CALL THERM(NE,NTYP,ITYP)
B=ZEIT(A)
WRITE (NOUT,1004) NR(1,KL-1),B
IF(KL.LE.NA) GO TO 100
GO TO 102
121 WRITE (NOUT,122) NR(1,KL),JI
122 FORMAT(140/' ***ERRCR 0.14 : THE REGION PARAMETER IN THE JOB- CARD
1 IS NOT GREAT ENOUGH TO START MODULE',I3,
2' ;',I8,' WORDS ARE MISSED AT LEAST')
IDUR=0
B=ZEIT(A)
WRITE (NOUT,1004) NR(1,KL),B
IF(NR(1,KL).EQ.5.AND.NINA.GT.0.AND.NINA.LT.NIN) GO TO 94
KL=KL+1
IF(KL.LE.NA) GO TO 100
102 CALL DATUM(DAT,TIME)
WRITE (NOUT,3000) DAT,TIME
RETURN
5000 I=0
WRITE (LIZ) I,N2
STOP
END

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SLBRoutine PRPHI(NSP,E,F)
DIMENSION E(NSP),F(NSP)
COMMON A(4),NOUT
WRITE(NOUT,100)
IF(NSP.GT.1)GOTO 1
WRITE(NOUT,101)
GOTO 2
1 CALL TRAP(NSP,E,F,FINT)
WRITE(NOUT,102)NSP,FINT
2 CONTINUE
RETURN
100 FORMAT(///' FOR THE WEIGHTING SPECTRUM')
101 FORMAT(' +',27X,'THE FUNCTION PHIE) OR DPHIE) WILL BE USED.')
102 FORMAT(' +',27X,'POINTWISE INPUT-DATA WILL BE USED. NUMBER OF POINT
*S',15,'. INTEGRAL',1PE16.7,'.')
END

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SLBRoutine TRAP(N,X,Y,FINT)
C
C SIMPLE TRAPEZOIDAL INTEGRATION
C
DIMENSION X(N),Y(N)
COMMON A(4),ICUT
FINT=0.
N1=N-1
IF(N1.LE.0)GOTO 2
CC 1 I=1,N1
DX=X(I+1)-X(I)
IF(DX.LT.0.)WRITE(INOUT,100)I,X(I),X(I+1)
1 FINT=FINT+DX*(Y(I+1)+Y(I))
FINT=FINT*0.5
2 RETURN
100 FORMAT(' ***WARNING 0.15: ARGUMENTS NOT IN INCRFASING ORDER DURING
1 TRAPEZOIDAL INTEGRATION.',/
*' *** POINT I=',15,' X(I)=',1PE12.4,' X(I+1)=',E12.4)
END

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GARFA START 0
BC 15,12(0,15)
DC X(1)'07'
DC CL7'GARFA '
STM 14,12,12(13)
BALR 10,C
USING *,10
ST 13,AREA+4

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LA 4,AREA
ST 4,8(0,13)
LR 13,4
BEGIN SR 2,2
ST 2,LF+4
L 2,0(0,1)
L 3,4(0,1)
L 4,8(0,1)
L 5,16(0,0)
L 5,0(0,5)
L 5,0(0,5)
L 5,152(0,5)
L 5,8(0,5)
L 6,0(0,5)
L 7,4(0,5)
STM3 LR 8,7
CLC LF+5(3),9(6)
BH STM1
MVC LF+5(3),9(6)
STM1 SR 8,6
BE STM2
L 6,0(0,6)
B STM3
STM2 L 5,LF+4
S 5,=X'0000280C'
ST 5,LF+4
GFTMAIN VC,LA=LF,A=ADDR
LTR 15,15
BE STM4
SR 15,15
ST 15,0(0,3)
ST 15,0(0,4)
B ENDE
STM4 L 5,ADDR
SR 5,2
SRA 5,2(0)
ST 5,0(0,3)
L 5,ADDR+4
SRA 5,2(C)
ST 5,0(0,4)
ENDE L 13,AREA+4
LM 14,12,12(13)
MVI 12(13),X'FF'
BCR 15,14
DS 0F
LF DC X'00000008'
DS 1F
ADDR DS 2F
AREA DS 18F
END GARFA

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ADRESSE DES 1. ARGUMENTS
 ADRESSE DES 2. ARGUMENTS
 ADRESSE DES 3. ARGUMENTS
 CVT-ADRESSE
 TCR-ADRESSE
 D-PQE-ADRESSE
 PQE-ADRESSE
 ADRESSE DES 1. FRQE
 ADRESSE DES LETZTEN FRQE
 LAENGE DES FRQE WECSPEICHERN
 FFHLERAUSGANG
 SPEICHERN DES INKREMENTS (WCRTI)
 SPEICHERN DER LAENGE (WORTE)

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SUBROUTINE F1AG (NOUT)
WRITE (NOUT,1)
1 FORMAT(1H1/1H0/1H3/)
1* INPUT DESCRIPTION FOR THE PROGRAM SYSTEM MIGRCS-3* // 40
2* ***** // 50
2* INTRODUCTION* // 60
3* THE PROGRAM SYSTEM MIGRCS CALCULATES MICROSCOPIC GROUP* / 70
4* CONSTANTS FROM NUCLEAR CROSS SECTION DATA STORED IN THE* / 80
5* NUCLEAR DATA LIBRARY KEDAK. THE SYSTEM CONSISTS OF THE* / 90
6* FOLLOWING MODULES:* // 100
7* MODULE NO. PURPOSE* // 110
8* 1 CALCULATION OF GROUP CROSS SECTIONS FOR INFINITE* / 120
9* DILUTION AND OF RESONANCE SELF SHIELDING FACTORS* / 130
A* FROM RESOLVED RESONANCE PARAMETERS.* // 140
B* 2 CALCULATION OF GROUP CROSS SECTIONS FOR INFINITE* / 150
C* DILUTION AND OF RESONANCE SELF SHIELDING FACTORS* / 160
D* FROM STATISTICAL RESONANCE PARAMETERS.* // 170
E* 3 CALCULATION OF GROUP CROSS SECTIONS FOR INFINITE* / 180
F* DILUTION AND OF RESONANCE SELF SHIELDING FACTORS* / 190
G* FROM POINT CROSS SECTION DATA.* // 200
WRITE (NOUT,2)
2 FORMAT(
1* 4 CALCULATION OF WEIGHTED GROUP AVERAGES FOR* / 230
2* INFINITE DILUTION.* // 240
3* 5 CALCULATION OF NORMALIZED TRANSFER MATRICES FOR* / 250
4* INELASTIC SCATTERING, (N,2N) AND (N,3N) PROCESSES.* // 260
4/
5* 6 CALCULATION OF NORMALIZED ELASTIC SCATTERING* / 280
6* MATRICES UP TO 5-TH ORDER (LEGENDRE REPRESENTA- / 290
7* TION), OF ELASTIC GROUP CROSS SECTIONS, OF THE* / 300
8* AVERAGE ELASTIC SCATTERING COSINE AND OF TOTAL* / 310
9* GROUP CROSS SECTIONS WITH ORDER-DEPENDENT* / 320
A* WEIGHTING.* // 330
B* 7 CALCULATION OF FISSION SPECTRA.* // 340
C* 8 CALCULATION OF WEIGHTED 1/V GROUP AVERAGES.* // 350
D* 9 CALCULATION OF NORMALIZED ELASTIC SCATTERING* / 360
E* MATRICES UP TO 5-TH ORDER (LEGENDRE REPRESENTA- / 370
F* TION), OF WEIGHTED TOTAL AND ELASTIC SCATTERING* / 380
G* GROUP CROSS SECTIONS AND OF GROUP-AVERAGED * / 390
H* SCATTERING COSINES FOR THE REMO CORRECTION.* // 400
WRITE (NOUT,3)
3 FORMAT(
1* 10 CALCULATION OF THERMAL CROSS SECTIONS.* // 430
WRITE(NOUT,5)
5 FORMAT(1H1/1H0/1H0/
1* THE FOLLOWING INPUT MUST BE PROVIDED. IF GROUP CONSTANTS ARE* / 460
2* TO BE CALCULATED FOR SEVERAL MATERIALS THE COMPLETE INPUT MUST* / 470
3* BE REPEATED FOR EACH ONE. THE INPUT IS FORMAT-FREE FOLLOWING* / 480
4* THE FREEFD CONVENTIONS: EACH DATA RECORD STARTS IN COLUMN 1 OF* / 490
5* A DATA CARD. IF IT IS NOT POSSIBLE TO PLACE ALL THE DATA OF* / 500
6* ONE DATA RECORD ON ONE CARD, A SECOND, THIRD, ETC. CARD MAY* / 510
7* BE USED, WHICH MUST HAVE A BLANK IN COLUMN 1. OR: A NON BLANK* / 520
8* COLUMN 1 IN THE INPUT CARD IS AN INDICATION FOR A NEW INPUT* / 530
9* RECORD. ONE HAS TO DISTINGUISH BETWEEN AN ALPHAMERIC WORD OF* / 540
A* THE LENGTH REAL*4 AND OF THE LENGTH REAL*8. A REAL*4 WORD MUST* / 550

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B* BE ENCLOSED IN APOSTROPHIES AND IS STORED LEFT-ADJUSTED IN* / 560
C* THE COMPUTER AND FILLED UP WITH BLANKS IF NOT ALL 4 BYTES ARE* / 570
D* OCCUPIED. EXAMPLE: 'ARG' OR 'ABCD'. A REAL*8 WORD MAY BE' / 580
WRITE(NOUT,4)
4 FORMAT(
1* ENCLOSED IN APOSTROPHIES COMPRISING AT LEAST 5 CHARACTERS AND* / 610
2* AT MOST 8 CHARACTERS, WHICH ARE STORED LEFT-ADJUSTED IN THE * / 620
3* COMPUTER IF NOT ALL 8 BYTES ARE OCCUPIED. A SPECIAL CASE ARE* / 630
4* REAL*8 WORDS WITH A NUMBER OF OCCUPIED BYTES LESS THAN OR* / 640
5* EQUAL TO 5. THESE WORDS MAY BE ALSO ENCLOSED IN @-SIGNS. THEY* / 650
6* ARE ALSO STORED LEFT-ADJUSTED IN THE COMPUTER AND FILLED UP* / 660
7* WITH BLANKS. EXAMPLES: 'PU239'='@PU239' '@PU239@' / 670
8* 'RES'=@RES@. FIXED POINT AND FLOATING POINT NUMBERS ARE* / 680
9* WRITTEN IN THE USUAL MANNER, E. G: FIXED POINT NUMBERS: 1 10* / 690
A* 875 AND FLOATING POINT NUMBERS: 10. 5.E3 0.7E-3 0.01.* / 700
B* THE INPUT DATA ITEMS ARE SEPARATED BY ONE OR MORE BLANKS.* // 710
WRITE (NOUT,6)
6 FORMAT(1H1/1H0/1H3/)
1* CARD 1* / 740
2* MAT MATERIAL NAME IN KEDAK NOMENCLATURE* / 750
3* (8-BYTE ALPHAMERIC REPRESENTATION).* / 760
4* ISTRUK =0 : DOPPLER BROADENING IS NEGLIGIBLE AS IS TYPICAL* / 770
5* FOR S-WAVE RESONANCES OF STRUCTURAL MATERIALS.* / 780
6* =1 : DOPPLER BROADENING MUST BE ACCOUNTED FOR AS IS* / 790
7* TYPICAL FOR HEAVY NUCLEIDES.* // 800
8* MORE SPECIFICALLY: IF MODULES 1 AND 2 ARE* / 810
9* UTILIZED, INFINITE DILUTION GROUP CROSS SEC- / 820
A* TIONS AND RESONANCE SELF SHIELDING FACTORS ARE* / 830
B* CALCULATED FROM RESONANCE PARAMETERS FOR THE* / 840
C* FOLLOWING STANDARD TEMPERATURES :* / 850
D* T=0 K IF ISTRUK=0,* / 860
E* T=300, 900, 2100 K IF ISTRUK=1.* // 870
WRITE (NOUT,7)
7 FORMAT(
1* IF MODULE 3 IS UTILIZED THE SAME QUANTITIES ARE* / 900
2* CALCULATED FROM POINT DATA FOR THAT TEMPERATURE* / 910
3* FOR WHICH THE POINT DATA ARE STORED (T=0 K IN* / 920
4* THE PRESENT VERSION, KEDAK-3), REGARDLESS OF* / 930
5* THE ISTRUK VALUE.* / 940
6* IF TEMPERATURES DIFFERING FROM THE STANDARD* / 950
7* TEMPERATURES ARE TO BE USED, THIS MUST BE SPE- / 960
8* CIFIED ON CARD 9 BELOW.* // 970
9* IF GROUP BOUNDARIES DIFFERING FROM THOSE OF THE 26-GROUP ABBN* / 980
A* SET ARE TO BE USED (VIZ. 0.215eV, 0.465eV, 1eV, 2.15eV, 4.65eV* / 990
B* 10eV, 21.5eV, 46.5eV, 100eV, 215eV, 465eV, 1keV, 2.15keV,* / 1000
C* 4.65keV, 10keV, 21.5keV, 46.5keV, 100keV, 200keV, 400keV,* / 1010
D* 800keV, 1.4meV, 2.5meV, 4meV, 6.5meV, 10.5meV) TWO MORE CARDS* / 1020
E* FOLLOW: // 1030
WRITE (NOUT,8)
8 FORMAT(
1* CARD 2* / 1040
2* @BLOC@ 1 INVARIANT* / 1070
3* CARD 3* / 1080
4* NE NUMBER OF ENERGY GROUP BOUNDARIES* / 1090
5* (ARBITRARY).* / 1100

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6* (ENG(I),I=1,NE) ENERGY GROUP BOUNDARIES IN UNITS OF EV* / 1110
7* IN ASCENDING ORDER.* // 1120
9* NOTE THAT THE NUMBER OF ENERGY GROUPS THAT MIGROS CAN TREAT* / 1130
5* IS NOT RESTRICTED TO 26.* /// 1140
A* THE STANDARD WEIGHTING FUNCTION IS THE COLLISION DENSITY* / 1150
B* F(I,1)=PHI(E(I))=1./E(I). ALTERNATIVELY ONE CAN EMPLOY OTHER* / 1160
C* WEIGHTING FUNCTIONS AFTER LINKAGE OF AN APPROPRIATE FUNCTION* / 1170
D* PHI(E) WITH MIGROS. IF IN THIS CASE MODULE 3 IS USED ONE MUST* / 1180
F* LINK AN ADDITIONAL FUNCTION OPHI(E) YIELDING BASICALLY THE* / 1190
F* SAME RESULT AS PHI BUT WITH DOUBLE PRECISION. A THIRD ALTRNA-* / 1200
G* TIVE IS UTILIZATION OF A POINTWISE GIVEN COLLISION DENSITY FOR* / 1210
H* WHICH ONE NEEDS THE FOLLOWING CARDS:*) 1220
WRITE (NOUT,9) 1230
9 FORMAT(IH1/IHC/IHO/ 1240
1* CARD 4* / 1250
2* @BLOC@ 2 INVARIANT* / 1260
3* CARD 5* / 1270
4* NSPEC NUMBER OF SPECTRA,* / 1280
5* NFE NUMBER OF ENERGY GRID POINTS,* / 1290
6* (FF(I),I=1,NFE),(F(I,J),I=1,NFE),J=1,NSPEC) WITH* / 1300
7* EF: ENERGY GRID POINTS IN UNITS OF EV* / 1310
8* IN ASCENDING ORDER,* / 1320
9* F: COLLISION DENSITY VALUES.* // 1330
A* IF THE NUMBER OF SPECTRA (COLLISION DENSITY FUNCTIONS) IS* / 1340
B* GREATER THAN 1 THE SPECTRA 2, 3,... ARE INTERPRETED ONLY IN* / 1350
C* MODULE 6 WHERE THEY ARE TAKEN AS THE WEIGHTING FUNCTIONS FOR* / 1360
D* THE 1ST, 2ND,... MOMENT OF THE ELASTIC SCATTERING MATRIX* / 1370
E* (MW=1 ON CARD 35). MAKE SURE THAT THE NUMBER OF SPECTRA IS* / 1380
F* CONSISTENT WITH THE NUMBER OF MOMENTS CALCULATED. IF ONLY ONE* / 1390
G* SPECTRUM IS SPECIFIED IT WILL BE EMPLOYED FOR ALL REQUIRED*) 1400
WRITE (NOUT,10) 1410
10 FORMAT( 1420
1* MOMENTS OF THE ELASTIC SCATTERING MATRIX. A SPECIAL MODIFICA-* / 1430
1* TION, HOWEVER, ALLOWS AN IMPROVED TREATMENT OF FINE-STRUCTURE* / 1440
1* WEIGHTING (SEE CARDS 32-35). THE NUMBER OF GRID* / 1450
2* POINTS IS ARBITRARY BUT CARE SHOULD BE TAKEN THAT THE SPECTRA* / 1460
3* COVER THE WHOLE ENERGY RANGE OF INTEREST.* /// 1470
4* CARD 6* / 1480
5* @BLOC@ 3 INVARIANT* / 1490
6* CARD 7* / 1500
7* NA NUMBER OF MODULES UTILIZED,* / 1510
8* ((NR(I,J),I=1,3),J=1,NA) WITH* / 1520
9* NR(1,J) NUMBER OF MODULE,* / 1530
A* NR(2,J) NUMBER OF ENERGY GROUP WHERE CAL-* / 1540
B* CULATION WITH MODULE NR(1,J) IS* / 1550
C* TO BEGIN,* / 1560
D* NR(3,J) NUMBER OF ENERGY GROUP UP TO* / 1570
F* WHICH CALCULATION WITH MODULE* / 1580
F* NR(1,J) IS TO BE EXTENDED.*) 1590
WRITE (NOUT,11) 1600
11 FORMAT( 1610
1* THE LIMITS NR(2,J), NR(3,J) ARE* / 1620
2* TO BE GIVEN IN THE USUAL SENSE OF* / 1630
3* ASCENDING ENRGY. NOTE THAT THEM* / 1640
4* NR(3,J)<=NR(2,J), SINCE GROUPS* / 1650

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5* ARE CONVENTIONALLY LABELED IN THE* / 1660
6* REVERSE SENSE, I. E. GROUP NUMBER* / 1670
7* 1 IS ASSIGNED TO THE GROUP BE-* / 1680
8* TWEEN THE HIGHEST TWO ENERGY* / 1690
9* VALUES ON CARD 3.* // 1700
A* COMMENT:* / 1710
B* MODULES CAN BE CALLED MORE THAN ONCE. THIS IS NECESSARY IF* / 1720
C* SEVERAL UNCONNECTED RANGES OF ENERGY GROUPS MUST BE TREATED.* / 1730
D* FOR EACH RANGE ONE CALL MUST BE MADE.* / 1740
E* NR(2,J) AND NR(3,J) ARE INTERPRETED AS REFERRING TO OUT-SCAT-* / 1750
F* TERING GROUPS IN THE CASE OF ELASTIC AND INELASTIC SCATTERING*) 1760
WRITE (NOUT,12) 1770
12 FORMAT(IH1/IHC/IHC/ 1780
1* MATRICES. THE CALCULATION IS PERFORMED FOR ALL IN-SCATTERING* / 1790
2* GROUPS, I. E. ALL GROUPS LISTED IN @BLOC@ 1 INTO WHICH A* / 1800
3* NEUTRON CAN GET IN THE COURSE OF SCATTERING PROCESSES. THE* / 1810
4* THERMAL GROUP IS INCLUDED AS IN-SCATTERING GROUP.* // 1820
5* ***** // 1830
6* IF MODULE 1 AND 2 FOR CALCULATION OF SELF-SHIELDING FACTORS* / 1840
7* FROM RESOLVED AND STATISTICAL RESONANCE PARAMETERS ARE CALLED,* / 1850
8* AND TEMPERATURES OTHER THAN THE STANDARD TEMPERATURES (OKELVIN* / 1860
9* FOR STRUCTURAL MATERIALS, ISTRUK=0, 300, 900 AND 2100 KELVIN* / 1870
A* FOR HEAVY NUCLEI, ISTRUK=1) ARE NEEDED, TWO MORE CARDS MUST* / 1880
B* FOLLOW:* // 1890
C* CARD 9* / 1900
D* @BLOC@ 4 INVARIANT* / 1910
E* CARD 9* / 1920
F* NT NUMBER OF TEMPERATURES (ARBITRARY),* / 1930
G* (TEMP(I),I=1,NT) TEMPERATURES IN KELVIN.*/) 1940
WRITE(NOUT,13) 1950
13 FORMAT( 1960
1* IF SELF-SHIELDING FACTORS ARE TO BE CALCULATED (WITH MODULE 1,* / 1970
2* 2 OR 3) FOR DILUTION CROSS SECTIONS SIGMA0 (SIGO(I)) DIFFERING* / 1980
3* FROM THOSE OF THE ABBA GROUP CONSTANT SET (VIZ. 0, 10, 100,* / 1990
4* 1000, 10000, 100000 AND 1000000 BARN) THE FOLLOWING CARDS ARE* / 2000
5* NEEDED:* // 2010
6* CARD 10* / 2020
7* @BLOC@ 5 INVARIANT* / 2030
8* CARD 11* / 2040
9* MI NUMBER OF DILUTION CROSS SECTIONS* / 2050
A* (ARBITRARY),* / 2060
B* (SIGO(I),I=1,MI) DILUTION CROSS SECTION VALUES (SIGMA0-* / 2070
C* VALUES) IN BARN.* // 2080
D* ***** // 2090
E* IF WEIGHTED GROUP AVERAGES FOR INFINITE DILUTION ARE TO BE* / 2100
F* CALCULATED (WITH MODULES 4 AND 10) FOR DATA TYPES OTHER THAN* / 2110
G* THE 8 STANDARD TYPES MUEL, NUC, SGA, SGF, SGI, SGN, SG2N, AND* / 2120
WRITE (NOUT,14) 2130
14 FORMAT( 2140
1* SGT THE FOLLOWING CARDS ARE NEEDED:* // 2150
2* CARD 12* / 2160
3* @BLOC@ 6 INVARIANT* / 2170
4* CARD 13* / 2180
5* NTP NUMBER OF DATA TYPES (ARBITRARY),* / 2190
6* (ITYP(I),I=1,NTP) DATA TYPES (KFOAK NOMENCLATURE).*) 2200

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WRITE (NOUT,15)
15 FORMAT(IH1/IH0/IH0/
1* COMMENT:'
2* WEIGHTED GROUP AVERAGES CAN BE CALCULATED FOR ALL DATA TYPES' /
3* WHICH CAN BE REPRESENTED AS ONE-VALUED FUNCTIONS OF A SINGLE' /
4* ARGUMENT (INCIDENT NEUTRON ENERGY). THE POSSIBLE TYPES ARE' /
5* LISTED IN KFK 1725 OR KFK 2234. SPECIAL DEFINITIONS OF GROUP' /
6* AVERAGES ARE USED FOR COMPOSITE QUANTITIES SUCH AS ALPHA, ETA,' /
7* MUJL OR NUJL (CF. KFK 1784). IF THE CROSS SECTION TYPES SGF AND' /
8* SGA (SEE KFK 2234) ARE TREATED THE CROSS SECTION TYPE' /
9* SGC=SGA-SGF IS AUTOMATICALLY TREATED, TOO.'
A* *****
B* IF RESONANCE SELF-SHIELDING FACTORS ARE TO BE CALCULATED FROM' /
C* INDIVIDUAL RESONANCE PARAMETERS (MODULE 1), BUT ONLY WITH A' /
D* LIMITED NUMBER OF RESONANCES ON EITHER SIDE OF EACH ENERGY' /
E* GRID POINT, TWO MORE CARDS FOLLOW:*/)
WRITE (NOUT,16)
16 FORMAT(
1* CARD 14'
2* @BLOC@ 11 INVARIANT'
3* CARD 15'
4* NRES NUMBER OF RESONANCES TO BE CONSIDERED ON'
5* EITHER SIDE OF A GIVEN ENERGY.'
6* IF MODULE 1 IS TO BE EMPLOYED, BUT NOT WITH THE STANDARD VALUE' /
7* 0.01 OF THE MAXIMUM ADMISSIBLE RELATIVE ERROR FOR THE INTEGRA-' /
8* TION, ONE NEEDS THE FOLLOWING TWO CARDS:'
9* CARD 16'
A* @BLOC@ 12 INVARIANT'
B* CARD 17'
C* ERROR MAXIMUM ADMISSIBLE RELATIVE INTEGRATION'
D* ERROR.'
E* *****
F* IF GROUP CROSS SECTIONS AND SELF-SHIELDING FACTORS ARE TO BE' /
G* CALCULATED FROM POINT DATA (MODULE 3) BUT NOT WITH THE STAN-'
WRITE (NOUT,17)
17 FORMAT(
1* CARD VALUES EPSROM=5.0E-05, DRINWA=5.0, (EXPLAINED BELOW)'
2* ONE NEEDS THE FOLLOWING TWO CARDS:'
3* CARD 18'
4* @BLOC@ 31 INVARIANT'
5* CARD 19'
6* EPSROM RELATIVE ACCURACY FOR THE ROMBERG INTEGRA-'
7* TION. THE ITERATION STOPS IF THE RELATIVE'
8* DIFFERENCE BETWEEN TWO SUCCESSIVE APPROXI-'
9* MATIONS IS NOT GREATER THAN EPSROM,')
WRITE (NOUT,18)
18 FORMAT(IH1/IH0/IH0/
1* DRINWA CONTROL OF ERROR PRINTING IN THE ROMBERG'
2* ITERATION SUBROUTINE. IF THE ITERATION IS'
3* STOPPED (E. G. BY ROUND-OFF ERRORS) BEFORE' /
4* THE EPSROM CRITERION IS FULFILLED, AN ERROR' /
5* MESSAGE IS PRINTED ONLY IF THE CRITERION IS' /
6* NOT EVEN FULFILLED WITH DRINWA TIMES EPSROM.'
7//)
WRITE(NOUT,19)

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19 FORMAT(
1* IF MODULE 3 IS TO BE EMPLOYED BUT NOT WITH THE DEFAULT VALUES' /
2* ITEST=0, IZPUMS=-1 AND ITUMS=0 (CF. CARD 21), THE FOLLOWING' /
3* TWO CARDS ARE NEEDED:'
4* CARD 20'
5* @BLOC@ 32 INVARIANT'
6* CARD 21'
7* ITEST CONTROL OF ERROR MESSAGES AND WARNINGS'
8* =0: NORMAL PRINT-CUT FOR PRODUCTION RUNS,' /
9* =1: EXTENDED PRINT-OUT FOR PROGRAM' /
A* DEBUGGING,' /
B* =2: AS ITEST=1 WITH ADDITIONAL PRINT-CUT,' /
C* =3: AS ITEST=2 WITH FURTHER EXTENDED PRINT-' /
D* OUT,' /
E* =4, 5, ..9: AS ITEST=3,' /
F* =10, 11, 12, 13: AS ITEST=0, 1, 2, 3 WITH' /
G* ADDITIONAL ERROR MESSAGES FOR EACH' /
H* SIGO VALUE,')
WRITE (NOUT,20)
20 FORMAT(
1* >13: AS ITEST=13.'
2* IZPUMS CONTROL OF ITEST FOR DIFFERENT GROUPS'
3* <=-1: ITEST IS UNCHANGED,'
4* =IGR: BEGINNING WITH THE IGR-TH GROUP UP TO' /
5* THE NR(3,J)-TH GROUP (CF. CARD 7)' /
6* ITEST HAS THE NEW VALUE ITUMS (SEE' /
7* BELOW). IGR MUST BE LESS THAN OR' /
8* EQUAL TO NR(2,J) (CF. CARD 7). THIS' /
9* IS VALID FOR ALL J WITH NR(1,J)=3,' /
A* I. E. WHENEVER MODULE 3 IS CALLED.' /
B* ITUMS NEW VALUE OF ITEST.'
C* IF MODULE 3 IS TO BE UTILIZED BUT NOT WITH THE DEFAULT VALUES' /
D* NENBER=1, ENBER(I)=-1.0, CONWFU(I)=1.0, OR NOT WITH NWFUN(I)=0' /
E* IN CASE OF A CALCULATED COLLISION DENSITY, OR NOT WITH' /
F* NWFUN(I)=-1 IN CASE OF A POINTWISE GIVEN COLLISION DENSITY' /
G* (CF. CARD 23) ONE NEEDS THE NEXT TWO CARDS:*/)
WRITE (NOUT,21)
21 FORMAT(
1* CARD 22'
2* @BLOC@ 33 INVARIANT'
3* CARD 23'
4* NENBER NUMBER OF ENERGY INTERVALS WITH DIFFERENT'
5* WEIGHTING FUNCTIONS AND/OR DIFFERENT INTE-' /
6* GRATION METHODS,')
WRITE(NOUT,22)
22 FORMAT(IH1/IH0/IH0/
1* {NENBER(I),NWFUN(I),CONWFU(I),I=1,NENBER) WITH' /
2* ENBER(I): UPPER LIMIT OF I-TH ENERGY INTER-' /
3* VAL, EQUAL TO LOWER LIMIT OF (I+1)-TH' /
4* ENERGY INTERVAL, SO THAT' /
5* ENBER(I) < ENBER(I+1).' /
6* THE LOWER LIMIT FOR THE FIRST ENERGY INTER-' /
7* VAL IS TAKEN AS EQUAL TO THE BEGINNING OF' /
8* THE CURRENT ENERGY GROUP RANGE (SMALLEST' /
9* ENERGY VALUE) AS SPECIFIED ON CARD 3 (OR IN' /

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A* THE PROGRAM AND IN CARD 7 IN CASE OF SEVE- / 3310
B* RAL DISCONNECTED ENERGY GROUP RANGES). / 3320
C* FNBER(NENBER) MUST BE AT LEAST AS GREAT AS / 3330
D* THE LARGEST ENERGY OF THE CURRENT ENERGY / 3340
E* GROUP RANGE. / 3350
F* SPECIAL CASE FOR NENBER=1: / 3360
G* ENBER(1)=-1.0. THIS MEANS THE WHOLE SPECI- / 3370
  WRITE (NOUT,23)
23 FORMAT(
1* FIED ENERGY GROUP RANGE. / 3400
2* NWFUN(I): TYPE OF WEIGHTING FUNCTION AND / 3410
3* METHOD OF INTEGRATION USED IN INTERVAL I. / 3420
4* METHOD OF INTEGRATION: / 3430
5* NWFUN(I)<=0: NUMERICAL INTEGRATION WITH / 3440
6* THE ROMBERG METHOD. / 3450
7* NWFUN(I)>0: ANALYTICAL INTEGRATION. / 3460
8* TYPE OF WEIGHTING FUNCTION: / 3470
9* INWFUN(I)=C: ARBITRARY FUNCTION WITH THE / 3480
A* NAME DPHI.(CPHI=1./E BY DE- / 3490
B* FAULT IF NOT GIVEN BY THE / 3500
C* USER AS A FUNCTION SUBROUTINE / 3510
D* TO THE PROGRAM). / 3520
E* INWFUN(I)=1: POINTWISE WEIGHTING FUNCTION, / 3530
F* INWFUN(I)=2: DPHI=CONWFW(I)/E (FOR CONWFW / 3540
  WRITE (NOUT,24)
24 FORMAT(
1* SEE NEXT INPUT VARIABLE). / 3570
2* CAUTION: BECAUSE IN SOME / 3580
3* CASES ROUNDING ERRORS APPEAR / 3590
4* WHEN THE ANALYTICAL INTEGRA- / 3600
5* TION IS CHOSEN, WE RECOMMEND / 3610
6* TO USE ONLY NWFUN(I)<=0. / 3620
7* THERE IS NO DIFFERENCE IN THE / 3630
8* CPU TIMES BETWEEN ROMBERG AND / 3640
9* ANALYTICAL INTEGRATION. / 3650
A* CONWFW(I): FACTOR IN THE WEIGHTING FUNC- / 3660
B* TION DPHI=CONWFW(I)/E. ONLY / 3670
C* USED IF INWFUN(I)=2. / 3680
D* ***** / 3690
  WRITE (NOUT,25)
25 FORMAT(
1* THREE DIFFERENT OPTIONS ARE AVAILABLE FOR THE TRANSFER PROBA- / 3720
2* BILITIES NEEDED FOR THE CALCULATION (WITH MODULE 5) OF NORMA- / 3730
3* LIZED TRANSFER MATRICES FOR INELASTIC SCATTERING WITH EXCITA- / 3740
4* TION OF DISCRETE LEVELS AT EXCITATION ENERGIES EJ: / 3750
5* (1) F(EP-->E)=DELTA(E-E-EJ) IF KINEM=C, / 3760
6* WHERE DELTA DENOTES DIRAC'S DELTA FUNCTION. THIS FORM / 3770
7* WAS USED IN THE ORIGINAL VERSION OF MIGRCS-2 (KFK 1784).) / 3780
  WRITE (NOUT,26)
26 FORMAT(LH1/LH0/LH0/
1* (2) F(EP-->E)=DELTA(E-E-EJ*(A+1.)/A) IF KINEM=1 / 3810
2* THIS FORM WAS USED IN THE REVISED VERSION OF MIGRCS-2 / 3820
3* (TRANSFORMATION OF EJ FROM CMS TO LAB COORDINATES). / 3830
4* (3) F(EP-->E)=DELTA(E-E*(A**2+1.)/(A+1.))*2 / 3840
5* +EJ*A/(A+1.) IF KINEM=2 / 3850

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6* THIS APPROXIMATION WAS RECOMMENDED BY SEGEV (SEGEV, / 3860
7* NSE 45 (1971)269 AND VERTEX, NSE 52 (1973)485) AND IS / 3870
8* ALSO PROPOSED FOR THE PROCESSING OF ENDF/B DATA (DRAKE, / 3880
9* RNL 50274 (T-6C1) ENDF 102, VOL.1). / 3890
A* FORM (2), I. E. KINEM=1, IS THE DEFAULT OPTION IN MODULE 5. IF / 3900
B* EITHER FORM (1) OR (3) IS TO BE USED ONE NEEDS THE FOLLOWING / 3910
C* ADDITIONAL INPUT: / 3920
D* CARD 24 / 3930
E* @BLOC@ 51 INVARIANT / 3940
F* CARD 25 / 3950
  WRITE (NOUT,27)
27 FORMAT(
1* KINEM TAG FOR TREATMENT OF DISCRETE LEVELS / 3980
2* (SEE ABOVE). / 3990
3* IF FOR THE MATERIAL OF INTEREST THE NUCLEAR DATA LIBRARY DOES / 4000
4* NOT CONTAIN ANY INFORMATION ON THE ENERGY DISTRIBUTION OF / 4010
5* SECONDARY NEUTRONS (SEDIC, SED2N, SED3N) IN THE ENERGY REGION / 4020
6* OF CONTINUOUS LEVEL EXCITATION OF THE RESIDUAL NUCLEUS AN / 4030
7* EVAPORATION MODEL IS EMPLOYED IN MODULE 5. THE PARAMETER XNUE / 4040
8* FOR THE CALCULATION OF THE NUCLEAR TEMPERATURE, / 4050
9* THETA(EF)=SQRT(EF/(XNUE*A)), IS SET EQUAL TO XNUE=0.16/MEV BY / 4060
A* DEFAULT. (A= ATOMIC WEIGHT OF THE TARGET NUCLEUS.) IF OTHER / 4070
B* XNUE VALUES ARE TO BE USED ONE NEEDS THE FOLLOWING ADDITIONAL / 4080
C* INPUT: / 4090
D* CARD 26 / 4100
E* @BLOC@ 52 INVARIANT / 4110
F* CARD 27 / 4120
G* XNUE EVAPORATION MODEL PARAMETER / 4130
  (IN UNITS OF 1/MEV). / 4140
  WRITE (NOUT,28)
28 FORMAT(
1* IF MODULE 5 IS CALLED THE TRANSFER MATRICES FOR INELASTIC / 4170
2* SCATTERING AND FOR (N,2N) ARE CALCULATED BY DEFAULT. IF OTHER / 4180
3* REACTION TYPES ARE WANTED ONE NEEDS THE FOLLOWING ADDITIONAL / 4190
4* INPUT: / 4200
5* CARD 28 / 4210
6* @BLOC@ 53 INVARIANT / 4220
7* CARD 29 / 4230
8* NIN NUMBER OF REACTION TYPES, / 4240
9* (INTYP(I),I=1,NIN) REACTION TYPE INDICATORS: / 4250
A* INTYP=1 FOR INELASTIC SCATTERING, / 4260
B* INTYP=2 FOR (N,2N) PROCESSES, / 4270
C* INTYP=3 FOR (N,3N) PROCESSES. / 4280
D* ***** / 4290
  WRITE (NOUT,29)
29 FORMAT(LH1/LHC/LH)/
E* IF MODULE 6 IS TO BE USED BUT NOT WITH THE STANDARD VALUES / 4320
F* ISEL=2, NLE=5 ONE NEEDS THE FOLLOWING CARDS: / 4330
G* CARD 30 / 4340
H* @BLOC@ 61 INVARIANT / 4350
I* CARD 31 / 4360
1* ISEL TAG FOR POSSIBLE CROSS SECTION MODIFICATION / 4370
2* AND ADDITIONAL PRINT-OUT (DEFAULT VALUE: 2) / 4380
3* ISEL=2: NO CROSS SECTION MODIFICATION; / 4390
4* ISEL=1: BELOW LOCKE, IN THE RESOLVED / 4400

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6*          RESONANCE RANGE, THE ELASTIC* / 4410
7*          SCATTERING AND TOTAL CROSS SEC- / 4420
8*          TIONS ARE SET EQUAL TO 1 BARN* / 4430
9*          (MAINLY TO SIMPLIFY THE CALCULA- / 4440
A*          TION OF APPROXIMATE SCATTERING* / 4450
B*          PROBABILITIES AND AVERAGE ELASTIC* / 4460
C*          SCATTERING COSINES FOR HEAVY ELF- / 4470
D*          MENTS, AND TO SAVE CORE MEMORY* / 4480
E*          SPACE).*) / 4490
WRITE (NOUT,30) / 4500
30 FORMAT( / 4510
1*          ISELCO: ADDITIONAL PRINT-CUT OF INTERME- / 4520
2*          DIATE INFORMATICA.* / 4530
3*          NLE          HIGHEST ORDER IN LEGENDRE EXPANSION (MAX 5) / 4540
4*          THE ACTUAL VALUE USED IS MAX(1,NLE) BECAUSE / 4550
5*          OF THE NORMALIZATION OF THE AVERAGE SCATTE- / 4560
6*          RING COSINES TO THE KEDAK MUFL VALUES. THE* / 4570
7*          MODULE ALWAYS CALCULATES SCATTERING * / 4580
8*          MATRICES FROM MOMENT ZERO TO MOMENT NLF.* /// 4590
9*          IF MODULE 6 IS CALLED AND FINE-STRUCTURE WEIGHTING WITH* / 4600
10*         L./SGT**(L+1) IS TO BE EMPLOYED FOR THE L-TH MOMENT ADD THE * / 4610
11*         CARDS 32 UP TO 35:* / 4620
12*         ADD THE FOLLOWING CARDS:* / 4630
A*         CARD 32* / 4640
B*         @BLOC@ 62          INVARIANT* / 4650
C*         CARD 33* / 4660
D*         NMAT          NUMBER OF MATERIALS IN THE MIXTURE WHOSE* / 4670
E*         MACROSCOPIC TOTAL CROSS SECTION IS TO BE* / 4680
F*         USED FOR FINE-STRUCTURE WEIGHTING;*) / 4690
WRITE (NOUT,31) / 4700
31 FORMAT( / 4710
1*         (NAME(I),TZ(I),I=1,NMAT) WITH* / 4720
2*         NAME: MATERIAL NAME (8-BYTE ALPHAMERIC* / 4730
3*         REPRESENTATION),* / 4740
4*         TZ : NUCLEAR DENSITY (NUCLEI PER CM**3)* / 4750
5*         TIMES 1.E-24.* /// 4760
6*         IF MODULE 6 IS CALLED AND NOT ALL MOMENTS ARE TO BE WEIGHTED* / 4770
7*         BY THE COLLISION DENSITY F(I,1) (CF. CARD 5) OF THE 0-TH MO- / 4780
8*         MENT, THE FOLLOWING CARDS ARE NEEDED:* / 4790
9*         CARD 34* / 4800
A*         @BLOC@ 63          INVARIANT* / 4810
B*         CARD 35* / 4820
C*         MW          TAG FOR WEIGHTING,* / 4830
D*         MW=1: WEIGHT F(I,L+1) FOR L-TH MOMENT,* / 4840
E*         NSPEC=NLE+1 MUST OCCUR ON CARD 5 WITH* / 4850
F*         NLF GIVEN ON CARD 31 OR BY DEFAULT;*) / 4860
WRITE (NOUT,32) / 4870
32 FORMAT(IHL/IHO/IHO/ / 4880
1*         MW=2: WEIGHT F(I,1)/SGT**(L+1) FOR L-TH* / 4890
2*         MOMENT (CARD 33 MUST PRECEDE).* /// 4900
3*         IF MODULE 6 IS USED BUT NOT WITH THE STANDARD GRID POINT* / 4910
4*         NUMBERS PER GROUP (NK=70, NR=16, SEE BELOW) ONE NEEDS THE* / 4920
5*         FOLLOWING CARDS:* / 4930
6*         CARD 36* / 4940
7*         @BLOC@ 64          INVARIANT* / 4950

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8* CARD 37* / 4960
9* NK / 4970
A* NK*MIN(1,ALOG(ENG(I)/ENG(I-1)) / 4980
B* ALOG(1/ALFA)) IS THE NUMBER OF BASIC GRID* / 4990
C* POINTS IN THAT ENERGY REGION WITHIN GROUP I* / 5000
D* FROM WHICH ELASTIC SCATTERING INTO ADJACENT* / 5010
E* GROUPS IS POSSIBLE, ALFA=((A-1)/(A+1))**2,* / 5020
A= ATOMIC WEIGHT IN NEUTRON MASS UNITS;*) / 5030
WRITE (NOUT,33) / 5040
33 FORMAT( / 5050
1*          NR          NR IS THE NUMBER OF BASIC GRID POINTS IN* / 5060
2*          THAT ENERGY REGION OF EACH GROUP FROM WHICH* / 5070
3*          ELASTIC SCATTERING INTO ADJACENT GROUPS IS* / 5080
4*          IMPOSSIBLE. (THIS REGION POSSIBLY MAY NOT* / 5090
5*          EXIST, THEN NR HAS NO MEANING.)* /// 5100
6*          ***** / 5110
7*          IF 1/V AVERAGES ARE TO BE CALCULATED (WITH MODULE 8), BUT NOT* / 5120
8*          WITH THE MAXIMUM ADMISSIBLE RELATIVE INTEGRATION ERROR* / 5130
9*          EPS=0.01, ONE NEEDS THE FOLLOWING CARDS:* / 5140
A*          CARD 38* / 5150
B*          @BLOC@ 81          INVARIANT* / 5160
C*          CARD 39* / 5170
D*          EPS          MAXIMUM ADMISSIBLE RELATIVE INTEGRATION* / 5180
E*          ERROR.* /// 5190
F*          ***** / 5200
G*          IF REMO DATA ARE TO BE CALCULATED (WITH MODULE 9) BUT NOT WITH* / 5210
H*          WRITE (NOUT,34) / 5220
34 FORMAT( / 5230
1*          THE STANDARD VALUES (SEE BELOW) ERR=0.01, NJM=10, NUJM=10,* / 5240
2*          ONE NEEDS THE FOLLOWING TWO CARDS:* / 5250
3*          CARD 40* / 5260
4*          @BLOC@ 91          INVARIANT* / 5270
5*          CARD 41* / 5280
6*          ERR          MAXIMUM ADMISSIBLE RELATIVE INTEGRATION* / 5290
7*          ERROR;* / 5300
8*          NJM          2**NJM+1 IS THE MAXIMUM NUMBER OF GRID* / 5310
9*          POINTS FOR THE ANGULAR INTEGRATION;* / 5320
A*          NUJM          2**NUJM+1 IS THE MAXIMUM NUMBER OF GRID* / 5330
B*          POINTS FOR THE ENERGY INTEGRATION.* / 5340
WRITE (NOUT,35) / 5350
35 FORMAT(IHL/IHO/IHO/ / 5360
1*          IF MODULE 9 IS TO BE USED BUT NOT WITH THE DEFAULT VALUES* / 5370
2*          (EXPLAINED BELOW) ISELR=1 FOR ISTRUK=0, ISELR=0 FOR ISTRUK=1,* / 5380
3*          NLRA=0, NLRE=5, NCALL=0, NFG=14, NFI=5, ONE NEEDS THE* / 5390
4*          FOLLOWING CARDS:* / 5400
5*          CARD 42* / 5410
6*          @BLOC@ 92          INVARIANT* / 5420
7*          CARD 43* / 5430
8*          ISELR          =1: SCATTERING PROBABILITIES ARE CALCULATED* / 5440
9*          ACCORDING TO EQ. 9.3 OF KFK 1784 WITH* / 5450
A*          THE KEDAK VALUES FOR THE SCATTERING* / 5460
B*          CROSS SECTION SGN(E),* / 5470
C*          =C: IN EQ. 8.3 OF KFK 1784 THE SCATTERING* / 5480
D*          CROSS SECTION SGN(E) IS TAKEN AS 1 BARN;* / 5490
E*          NLRA          LOWEST LEGENDRE ORDER;* / 5500
F*          NLRE          HIGHEST LEGENDRE ORDER;*) / 5510
WRITE (NOUT,36) / 5520

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36 FORMAT(
1' NCALL          =C: EACH TIME MCDULF 9 IS CALLED ALL ENERGY' / 5530
2'              GROUPS ARE SUBDIVIDED INTO 14 SUBGROUPS' / 5540
3'              WITH 5 ENERGY INTERVALS EACH,' / 5550
4'              >0 NUMBER OF CALLS FOR MODULE 9 (MUST BE' / 5570
5'              CONSISTENT WITH CARD 7),' // 5580
6' IN CASE NCALL>0 THE FOLLOWING CARD IS NEEDED NCALL TIMES:' // 5590
7' CARD 44'      / 5600
8' NGRF          NUMBER OF ENERGY GROUP RANGES WITH DIFFE-' / 5610
9'              RENT ENERGY GRIDS;' / 5620
A' (N1(I),N2(I),NFG(I),NFI(I),I=1,NGRF) WITH-' / 5630
B'              N1 : NUMBER OF FIRST GROUP IN RANGE,' / 5640
C'              N2 : NUMBER OF LAST GROUP IN RANGE,' / 5650
D'              NFG: NUMBER OF SUBGROUPS PER GROUP,' / 5660
E'              NFI: NUMBER OF ENERGY INTERVALS PER ' / 5670
F'              SUBGROUP.' // 5680
G'              ***** // 5690
              WRITE (NOUT,37) / 5700
37 FORMAT(
1' THE LAST CARD FOR A GIVEN MATERIAL IS AS FOLLOWS:' // 5720
2' CARD 45'      / 5730
3' @ENDE@ 111    INVARIANT' // 5740
4'          ***** // 5750
5' CARDS 1 TO 45 HAVE TO BE REPEATED FOR EACH MATERIAL WANTED' / 5760
6' AND/OR EACH WEIGHTING SPECTRUM TO BE USED. THE LAST CARD FOR' / 5770
7' THE ENTIRE JOB IS:' // 5780
8' CARD 46'      / 5790
9' @ENDE@ 112    INVARIANT' // 5800
              ***** // 5810
              WRITE (NOUT,49) / 5820
49 FORMAT(IH1/IH0/IH0/
1' PRINTING OF THE PRESENT INPUT DESCRIPTION CAN BE SUPPRESSED BY' / 5840
2' PLACING THE FOLLOWING CARD (WITH THE M PUNCHED IN COLUMN 1) IN' / 5850
3' FRONT OF THE FIRST INPUT CARD:' // 5860
4' CARD )'      / 5870
5' MIGR          INVARIANT' // 5880
6' THIS CARD DOES NOT APPEAR IN THE FREEFD DISPLAY OF INPUT DATA.' / 5890
7' //          ***** // 5900
8' THE PROGRAM SYSTEM MIGROS REQUIRES DD-CARDS FOR THE FOLLOWING' / 5910
9' EXTERNAL STORAGE DEVICES:' // 5920
A' 8            UNIT ON WHICH THE DECODED INPUT IS WRITTEN BY FREEFD,' / 5930
B' 1            UNIT FROM WHICH THE NUCLEAR DATA LIBRARY IS AVAILABLE,' / 5940
C' 3            UNIT ON WHICH ALL MODULES WRITE RESULTS,' / 5950
D' 10           TEMPORARY INTERMEDIATE LIBRARY NEEDED ONLY BY MODULE 6.' // 5960
E' //          ***** // 5970
              WRITE (NOUT,38) / 5980
38 FORMAT(
1' THE REQUIRED ARRAY LENGTHS DEPEND ON THE INPUT AND ON THE' / 6010
2' CALLED MODULES. THE NOTATION OF THE INPUT DESCRIPTION IS USED' / 6020
3' IN WHAT FOLLOWS. ALL ARRAY LENGTHS ARE GIVEN IN TERMS OF' / 6030
4' 4-BYTE WORDS UNLESS STATED OTHERWISE.' // 6040
5' THE CONTROL PHASE NEEDS' / 6050
6' 2*NTYP+3*NMAT+NFE*(NSPEC+1)+NT*MI+1+3*NE+4*NA*(1+NE) WORDS,' / 6060
7' WHERE THE DEFAULT VALUES ARE USED FOR QUANTITIES NOT SPECIFIED' / 6070
8' IN THE INPUT, VIZ. NTYP=7, NFE=1, NSPEC=1, NT=3, MI=7, NMAT=1,' / 6080
9' AND NE=26.' // 6090

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A' TO THIS ONE MUST ADD THE MEMORY SPACE OCCUPIED BY THE UTILIZED' / 6100
B' MODULE WITH THE LARGEST STORAGE REQUIREMENT. THE STORAGE' / 6110
C' REQUIREMENTS OF THE VARIOUS MODULES ARE AS FOLLOWS:' // 6120
D' MODULE NO.    STORAGE REQUIREMENT (4-BYTE WORDS)' // 6130
E' 1            7*MI+3*NE+7*MAX(300,NUMBER OF RESONANCES ON' / 6140
F'              KEPAKI)+6*MAX(400,MAXIMUM NUMBER OF GRID ENERGIES' / 6150
G'              FOR INTEGRATION OVER ONE ENERGY GROUP) WORDS') / 6160
              WRITE (NOUT,39) / 6170
39 FORMAT(
1' COMMENT: THE USER CANNOT DETERMINE THE NUMBER OF' / 6180
2' GRID ENERGIES IN ADVANCE. IF 400 WORDS ARE NOT' / 6190
3' SUFFICIENT THE SPACE FOR DATA STORAGE IS ENLARGED' / 6210
4' PROVIDED THE AVAILABLE REGION ADMITS THIS. IF THE' / 6220
5' REGION IS NOT LARGE ENOUGH THE MODULE IS BY-' / 6230
6' PASSED. IT IS RECOMMENDED IN THIS CASE TO ENLARGE' / 6240
7' THE REGION BY AT LEAST 2K BYTES.' / 6250
8' 2            35*MI WORDS.' / 6260
9' 3            3*MIBER+6*MI+MXINT+4*(MABWF+MABQ1+MABQ2+MABQ3)' / 6270
A'              +2*KMROM+4*MRF*MI WORDS.' // 6280
              WRITE (NOUT,40) / 6290
40 FORMAT(IH1/IH0/IH0/
1' MIBER: MAXIMUM NUMBER OF RANGES WITH DIFFERENT' / 6310
2' WEIGHTING FUNCTIONS OR DIFFERENT INTEGRA-' / 6320
3' TION METHODS. MIBER IS SET EQUAL TO 5 IN' / 6330
4' THE SUBROUTINE INPUT.' / 6340
5' MABWF: MAXIMUM NUMBER OF ENERGY POINTS IN ONE' / 6350
6' GROUP OF THE POINTWISE GIVEN WEIGHTING' / 6360
7' FUNCTION. MABWF HAS THE VALUE 0 IF NO' / 6370
8' POINTWISE GIVEN WEIGHTING FUNCTION IS' / 6380
9' PROVIDED IN THE INPUT. OTHERWISE IT HAS' / 6390
A' THE MINIMUM VALUE 50.' / 6400
B' MXINT: MAXIMUM NUMBER OF ENERGY POINTS IN ONE' / 6410
C' GROUP SUMMED OVER ALL PARTICIPATING CROSS' / 6420
D' SECTIONS (AND EVENTUALLY THE POINTWISE' / 6430
E' GIVEN WEIGHTING FUNCTION), MINIMUM VALUE=' / 6440
F' 200.' // 6450
              WRITE (NOUT,41) / 6460
41 FORMAT(
1' MABQ1: MAXIMUM NUMBER OF ENERGY POINTS IN ONE' / 6480
2' GROUP FOR THE CROSS SECTION TYPES SGT,' / 6490
3' SGA, SGN AND, IF EXISTENT, SGF, MINIMUM' / 6500
4' VALUE = 200.' / 6510
5' MABQ2: MAXIMUM NUMBER OF ENERGY POINTS IN ONE' / 6520
6' GROUP FOR THE CROSS SECTION TYPE MUFL,' / 6530
7' MINIMUM VALUE = 200.' / 6540
8' MABQ3: MAXIMUM NUMBER OF ENERGY POINTS IN ONE' / 6550
9' GROUP FOR THE CROSS SECTION TYPE SGT,' / 6560
A' MINIMUM VALUE = 200.' / 6570
B' KMROM: KMROM-1 = MAXIMUM NUMBER OF BISECTIONS IN' / 6580
C' THE ROMBERG INTEGRATION ROUTINE FSROMB,' / 6590
D' MINIMUM VALUE = 20.' / 6600
E' MRF : 7 FOR NON-FISSIONABLE MATERIAL,' / 6610
F' 8 FOR FISSIONABLE MATERIAL.' // 6620
              WRITE (NOUT,42) / 6630
42 FORMAT(
1' WITH THE MINIMUM VALUES A MINIMUM MEMORY DEMAND' / 6650
2' OF 3121 4-BYTE WORDS (POINTWISE WEIGHTING SPEC-' / 6660

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3* TRUM GIVEN, FISSIONABLE MATERIAL) IS NECESSARY TO / 6670
4* RUN MODULE 3 (FSTRUK). BUT WE RECOMMEND TO USE / 6680
5* ABOUT 10000 4-BYTE WORDS, BECAUSE SCMF OR ALL OF / 6690
6* THE MINIMUM VALUES MUST BE INCREASED DURING THE / 6700
7* CALCULATIONS. / 6710
8* 4 6*NE+2*MAX(1500,NUMBER OF SGN VALUES, NUMBER OF / 6720
9* SGM VALUES ON KEDAK IN THE ENERGY INTERVAL / 6730
A* CONSIDERED) WORDS / 6740
B* 5 MAX(7*NE*NE+7*NE+2*NE27+4*NAE+3*ISG+2*NISGD, / 6750
C* 4+2*NE*NE+3*NE+NE27+2*NISGC+NISGT+NEP+4*NEP* / 6760
D* NF) WORDS / 6770
E* NE27: NUMBER OF ENERGY GROUP BOUNDARIES OF / 6780
F* IN-SCATTERING GROUPS. STANDARD ESTIMATE: 27 / 6790
WRITE (NOUT,43) 6800
43 FORMAT( 6810
1* (THE STANDARD ESTIMATES ARE USED AS STAR- / 6820
2* TING VALUES IN THE PROGRAM BUT MAY BE MODI- / 6830
3* FIED AUTOMATICALLY DEPENDING ON THE ACTUAL / 6840
4* JOB CHARACTERISTICS). / 6850
5* NAE: MAXIMUM NUMBER OF EXCITED LEVELS THAT CON- / 6860
6* TRIBUTE IN A GIVEN OUT-SCATTERING GROUP. / 6870
7* STANDARD ESTIMATE: 30. / 6880
WRITE (NOUT,44) 6890
44 FORMAT(IH1/IH0/IH0/ 6900
1* ISG : MAXIMUM NUMBER OF ENERGY GRID POINTS IN ONE / 6910
2* OF THE CONSIDERED OUT-SCATTERING GROUPS. / 6920
3* THIS NUMBER IS DETERMINED BY THE COMBINA- / 6930
4* TION OF THE ENERGY GRID POINTS OF ALL / 6940
5* EXCITED LEVELS WHICH MUST BE USED IN THE / 6950
6* OUT-SCATTERING GROUP AND OF THOSE GRID / 6960
7* POINTS OF THE SPECTRUM THAT LIE IN THE / 6970
8* OUT-SCATTERING GROUP. STANDARD ESTIMATE: 200 / 6980
9* NISGC: ISG+MAXIMUM NUMBER OF ENERGY GRID POINTS OF / 6990
A* ANY EXCITED LEVEL (SGIZ) WHICH CONTRIBUTE / 7000
B* IN THE OUT-SCATTERING GROUP. STANDARD ESTI- / 7010
C* MATE: 400. / 7020
D* NISGC: MAXIMUM NUMBER OF ENERGY GRID POINTS OF / 7030
E* SGI (SG2N, SG3N) ON KEDAK IN ONE OF THE / 7040
F* OUT-SCATTERING GROUPS. STANDARD ESTIMATE: / 7050
G* 200. / 7060
WRITE(NOUT,45) 7070
45 FORMAT( 7080
1* NISGI: MAXIMUM NUMBER OF ENERGY POINTS AS OBTAINED / 7090
2* BY COMBINING THE KEDAK POINTS OF SGI (SG2N, / 7100
3* SG3N) AND THE MESH POINTS OF THE SPECTRUM / 7110
4* IN ANY OUT-SCATTERING GROUP. STANDARD / 7120
5* ESTIMATE: 300. / 7130
6* NEP : NUMBER OF INCIDENT-NEUTRON ENERGIES, FOR / 7140
7* WHICH THE DISTRIBUTIONS SEDIC (SED2N, / 7150
8* SED3N) ARE GIVEN ON KEDAK. STANDARD ESTI- / 7160
9* MATE: 30. / 7170
A* NF : NUMBER OF DIFFERENT ANALYTICAL DISTRIBUTI- / 7180
B* TIONS GIVEN ON KEDAK FOR SEDIC (SED2N, / 7190
C* SED3N) FROM WHICH THE TOTAL DISTRIBUTION / 7200
D* MUST BE COMPOSED. STANDARD ESTIMATE: 5 / 7210
E* APPROXIMATELY 30000 (STANDARD) TO 200000 (MANY / 7220

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F* GROUPS, LARGE ENERGY DEGRADATION) WORDS. THE / 7230
G* EXACT STORAGE REQUIREMENT DEPENDS ON THE MOSTLY / 7240
WRITE (NOUT,46) 7250
46 FORMAT( 7260
1* UNKNOWN DISTRIBUTION OF THE KEDAK DATA OVER THE / 7270
2* ENERGY GROUPS. IT IS RECOMMENDED TO BEGIN WITH / 7280
3* THE STANDARD VALUE AND TO INCREASE THE STORAGE / 7290
4* SPACE ONLY IF THIS DOES NOT WORK. THE PROGRAM / 7300
5* TRIES IN ANY CASE TO ORGANIZE THE CALCULATIONS IN / 7310
6* ACCORDANCE WITH THE AVAILABLE MEMORY SPACE. / 7320
7* 7 NE WORDS. / 7330
8* 8 NE+2*NFE WORDS. / 7340
9* 9 45*NMI*IMAX*(3+NUJM)+ICOS*(4+NIV)+IMAX+2*NJM+NE / 7350
A* +15*NMAX+NZM*(2+IZV)+BUF WORDS. / 7360
B* NMI : NLR+1. / 7370
C* IMAX: MAXIMUM ENERGY DEGRADATION IN TERMS OF / 7380
D* ENERGY GROUPS (=2 FOR SIMPLE SCATTERING / 7390
E* INTO THE ADJACENT GROUP). / 7400
F* ICOS: NUMBER OF ANGULAR GRID POINTS OF THE SGNC / 7410
G* DATA ON KEDAK. / 7420
WRITE (NOUT,47) 7430
47 FORMAT( 7440
1* NIV : NUMBER OF ENERGY GRID POINTS OF THE SGNC / 7450
2* DATA ON KEDAK. / 7460
3* NMAX: MAXIMUM NUMBER OF ENERGY GRID POINTS WITHIN / 7470
4* ONE ENERGY GROUP FOR THE DATA TYPES SGT, / 7480
5* SGN OR MUEL ON KEDAK. / 7490
WRITE (NOUT,48) 7500
48 FORMAT(IH1/IH0/IH0/ 7510
1* NZM : MAXIMUM NUMBER OF ENERGY INTERVALS IN ONE / 7520
2* SUBGROUP TIMES MAXIMUM NUMBER OF SUBGROUPS / 7530
3* PER GROUP. / 7540
4* IZV : MAX(4,IMAX*NMI). / 7550
5* BUF : MAX(2+IMAX*NZM,NTOT), WHERE NTOT IS THE / 7560
6* MAXIMUM NUMBER OF DATA POINTS WITHIN ONE / 7570
7* GROUP FOR THE TYPES SGT, SGN AND MUEL (ALL / 7580
8* THREE CONSIDERED AS A JOINT POINT SET) ON / 7590
9* KEDAK. / 7600
9* 10 NO SPACE FOR DATA ARRAYS REQUIRED. // 7610
A* THE REGION PARAMETER ON THE JOB CARD IS THE SLP OF / 7620
B* -MAXIMUM LENGTH OF DATA ARRAYS. / 7630
C* -170K BYTES FOR THE MTCROS PROGRAM. / 7640
D* -BUFFER LENGTH. / 7650
RETURN 7660
END 7670

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C
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C

ROUTINE FOR PRODUCING AN UNFORMATTED INPUT-FILE

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SUBROUTINE FREEFO (INP,NFI,NFO,LF,F,NF)
DIMENSION LF(1),F(1),NF(1),JZ(2),IRFAL(2)
REAL*8 N8,NV8/5HNUFIN/,VC,REAL
LOGICAL*1 JF(8),JX(2),LVS,LVCR1,LNACHI

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1
B
17
1

10
20
30
40
50
60
70
80

INTEGER*2 NFF(80),LV(19),JY(4),LL,JKFE,STERN/2** /	90	203 RETURN	640
EQUIVALENCE (JZ(1),JF(1),JY(1),NF),(LL,JX(1))	100	3 WRITE (NFO,5)	650
EQUIVALENCE (REAL,IREAL(1),LVS)	110	5 FCRMAT(1HO/48H ERROR-CONDITION IN DATA TRANSFER CR INPLT-ERROR)	66C
EQUIVALENCE (LVOR,LVOR1),(LNACH,LNACH1)	120	STCP	670
DATA LV(1)/1H /,LV(2)/1FC/,LV(3)/1H1/,LV(4)/1H2/,LV(5)/1H3/,	130	4 IF (IY.EQ.80) GOTO 6667	680
1LV(6)/1H4/,LV(7)/1H5/,LV(8)/1H6/,LV(9)/1H7/,LV(10)/1H8/,	140	JKFE=NFE(73)	690
2LV(11)/1H9/,LV(12)/1H+/,LV(13)/1H+/,LV(14)/1H-/,LV(15)/1H./,	150	NFE(73)=STERN	70C
3LV(16)/1HE/,LV(17)/1H?/,LV(18)/1H*/,LE/4HFEXA/,LFO/4HFORM/	16C	6667 WRITE (NFO,6) (NFE(I),I=1,80)	710
4,LSPE/4HSPEC/,LNO/4HNORM/,LV(19)/1HO/	170	6 FCRMAT(1X,80A1)	72C
	18C	IF (IY.EQ.80) GOTO 6668	730
	190	NFE(73)=JKFE	74C
	200		750
	210		760
	220		77C
	23C		780
	24C	6668 IF(NF(1).EQ.LNO) GOTO 500	79C
	250	IF(NF(1).EQ.LSPE) GOTO 501	80C
	260	GOTO 502	810
	270	500 KSPNO=0	820
	280	GOTO 11	830
	29C	501 KSPNO=1	840
	300	GOTO 11	85C
	31C	502 IF(NFE(1).EQ.LV(1)) GOTO 10	860
	320	IF(N)11,11,12	87C
	330	12 IF(NF(1)13,13,144	880
	340	144 IF(KSPNO)145,145,14	890
	350	14 WRITE (NFI) N,(NF(I),I=1,N)	90C
	360	111 IF(KOUT)11,11,2	910
	370	145 WRITE (NFI) (NF(I),I=1,N)	920
	380	GOTO 111	930
	390	13 NS=NS+1	940
	400	LF(NS)=N	950
	410	N1=NS+1	960
	42C	N2=NS+N	97C
	430	N=C	980
	440	DO 15 I=N1,N2	990
	45C	N=N+1	100C
	460	15 LF(I)=NF(N)	1010
	470	NS=N2	1020
	480	GOTO 111	1030
	490	11 N=0	1040
	50C	J=0	1050
	510	GO TO 16	1060
	520	10 J=1	1070
	530	16 J=J+1	1080
	540		109C
	55C		1100
	560		1110
	57C	97 CC 20 K=1,19	112C
	580	IF(NFE(J).EQ.LV(K)) GC TC 21	1130
	590	20 CCNTINUE	1140
	60C	GC TC 3	1150
	610		1160
	62C	21 IF (LW.GT.0) GOTO 221	117C
	630	IF (K.LT.2.OR.K.GT.11) GOTO 221	1180
		JJ=J	

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8003 JJ=JJ+1
      IF (JJ.LE.IY) GOTO 8000
8002 LW=1
      GOTO 97
8000 IF (NFE(JJ).EQ.LV(1)) GOTO 8002
      IF (NFE(JJ).NE.LV(15)) GOTO 8003
      LPPP=1
      GOTO 8002
C
221 IF(K-1)30,30,22
30 IF(LS)31,31,32
31 IF(J-IY)16,33,33
C
C
C
32 IF(LPP)40,40,41
40 N=N+1
      NF(N)=LSU*MV
47 LSU=0
      LS=0
      LO=0
      LW=0
      MV=1
      V=1.
      GOTO 31
C
C
C
41 M=LP-LS
      IF(M)44,45,46
44 IF(78+M)3,3,45
46 IF(75-M)3,3,45
45 N=N+1
      VC=V
      REAL=REAL*VC*1.D+1**M
      IF (LPPP.EQ.1) GOTO 801C
      NF(N)=IREAL(1)
      N=N+1
      NF(N)=IREAL(2)
      GOTO 8011
8010 IF (IREAL(2).GE.0) GOTO 8012
      LVCR1=LVS
      IRFAL(1)=IREAL(1)+1
      LNACH1=LVS
      IF (LVOR.EQ.LNACH) GOTO 8012
      IREAL(1)=LNACH+1C48576
8012 NF(N)=IREAL(1)
8011 LP=0
      LZ=0
      LPP=0
      LPPP=0
      REAL=0.D+0
      GC TO 47
C
C

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C
22 IF(K-11)50,50,23
50 LS=LS+1
      IF (LPPP.GT.0) GOTO 8004
      IF (LS.LE.9) GOTO 8005
      IF (LSU.GT.214748364) GOTO 3
      IF ((K-2).GT.7) GOTO 3
8005 LSU=10*LSU+K-2
51 IF (J-IY) 16,32,32
8004 IF (LZ.GT.0) GOTO 8006
      IF ((K-2).EQ.0) GOTO 8006
      LZ=LZ+1
      JJ=J
      LZZ=0
9001 JJ=JJ+1
      DO 8007 KK=2,11
      IF (NFE(JJ).EC.LV(KK)) GOTO 8008
8007 CCNTINUE
      GOTO 8009
8008 LZ=LZ+1
      IF ((KK-2).NE.0) GOTO 9000
      LZZ=LZZ+1
      GOTO 9001
9000 LZZ=0
      GOTO 9001
8009 LZ=LZ-LZZ
      IF (LZ.GT.16) GOTO 3
8006 REAL=RFAL*1.D+1+K-2
      IF (LPP) 51,51,883
883 LC=-1
      J=J+1
      IF (J-IY) 884,884,32
C
C
C
23 IF(K-14)60,60,24
60 IF(LC)61,61,3
61 LO=1
      IF(K-14)62,63,63
63 V=-1.
      MV=-1
62 IF(J-IY)64,3,3
64 J=J+1
      CC 65 K=2,11
      IF(NFE(J).EQ.LV(K)) GC TO 21
65 CONTINUE
      IF(NFE(J).EQ.LV(15)) GO TO 7C
      GC TO 3
C
C
C
24 IF(K-15)70,70,25
70 IF(LP)71,71,3
71 LP=LS
      LPP=1

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LPPP=1
IF(J-IY) 72, 73, 73
73 IF(LS) 3, 3, 41
72 J=J+1
DC 74 K=2, 11
IF(NFE(J).EQ.LV(K)) GO TO 50
74 CONTINUE
IF(NFE(J).EQ.LV(1)) GO TO 73
IF(NFE(J).EQ.LV(16)) GO TO 81
IF(NFE(J).EQ.LV(19)) GOTO 9C13
LC=0
8E4 LA=C
LV1=1
LP1=0
IF(J-IY) 982, 882, 3
C
C
C
25 IF(K-16) 80, 80, 226
226 IF (K-19) 26, 8013, 8C13
8013 LPPP=2
80 IF(LPP) 3, 3, 81
81 LA=0
LC=1
LV1=1
LP1=0
IF(J-IY) 82, 3, 3
82 J=J+1
IF(NFE(J).EQ.LV(1)) GO TO 83
882 IF(NFE(J).EQ.LV(12)) GO TO 83
IF(NFE(J).EQ.LV(13)) GO TO 83
IF(NFE(J).EQ.LV(14)) GO TO 84
IF(LC) 97, 3, 85
84 LV1=-1
83 IF(J-IY) 86, 3, 3
8E J=J+1
85 CC 87 K=2, 11
IF(NFE(J).EQ.LV(K)) GO TO 88
87 CONTINUE
IF(NFE(J).EQ.LV(1)) GO TO 89
GO TO 3
89 IF(LA) 3, 3, 90
8E LA=1
LP1=10*LP1+K-2
IF(J-IY) 96, 90, 90
9C LP=LP+LP1*LV1
GO TO 41
C
C
C
26 IF(K-17) 300, 300, 301
300 M=5
K7=17
GO TO 117
301 M=4

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K7=18
117 LC=0
116 LA=C
DO 100 L=1, 4
100 JY(L)=LV(1)
110 J=J+1
IF(J-IY) 101, 102, 102
102 IF(NFE(J).EQ.LV(K7)) GCTC 120
LC=0
GCTC 121
120 J=J-1
121 IF(LC) 33, 3, 112
101 IF(NFE(J).EQ.LV(K7)) GO TO 106
GO TO 107
106 IF(LC) 105, 3, 102
107 LA=LA+1
LC=1
LL=NFE(J)
JF(LA)=JX(1)
IF(LA-M) 110, 112, 112
112 N=N+1
NF(N)=JZ(1)
IF(K-17) 433, 433, 434
433 N=N+1
NF(N)=JZ(2)
434 LC=-1
IF(NFE(J+1).EQ.LV(K7)) GOTO 110
GCTC 116
105 IF(NFE(J+1).EQ.LV(1)) GCTC 16
GO TO 3
END
C
SLRROUTINEN ZUM LESEN DER KERNDATENBIBLIOTHEK
C
C
SLRROUTINEN MDFCPN , LDFCPN ZUM ERCEFFNEN DER KERNDATENBIBLIOTHEK
C
SLRROUTINE NDF
DIMENSION IDAT(2), IAD(1003), ISATZ(880), DAT1(60), I(4), IR(3), IW(3),
INAM(4), INAM(20), KDAT1(60), MNAM(20), NUNA(2), IWINA(880), XNAM(20),
2XJDAT(880), JDAT(880), NN(4), IREST(2), DAT2(60), Z(60), XWINA(880)
EQUIVALENCE (I(1), IR(1)), (Z(1), KDAT1(1)), (IWINA(1), XWINA(1)),
1(JDAT(1), XJDAT(1))
DATA I/'KEDA', 'BIBL', 'IOTH', ' ', '/', NSZ/100, NCLTP/6/
C
ENTRY NDFOPN (LBN, ICAT, IFD, ISPR)
JJ=1
ICAT(1)=I(4)
ICAT(2)=I(4)
GCTC 50
C
ENTRY LDFOPN (LBN, IFD, *)
JJ=2

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- B 20 -

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50 NSZ=880
   DEFINE FILE 1 (6000,880,U,K8)
   MNAM(1)=0
   NUNA(1)=0
   IS=1
   READ (LBN*IS) (ISATZ(II),II=1,NSZ)
   IS=IS+1
   DO 1 J=1,3
   IF (ISATZ(J)-I(J))2,1,2
2  WRITE (NOUTP,4)
4  FORMAT(1H0/' ***ERROR NDF. 1 : THE DD-CARD FOR UNIT 1 DOES NOT CHARACTERIZE A VALID KEDAK LIBRARY')
   STOP
1  CCNTINUE
   IFD=ISATZ(4)
   IAD(1)=ISATZ(5)
   IAC(2)=ISATZ(8)
   IAD(3)=ISATZ(11)
   K=4
   IR(1)=ISATZ(6)
   IR(2)=ISATZ(9)
   IR(3)=ISATZ(12)
   IW(1)=ISATZ(7)
   IW(2)=ISATZ(10)
   IW(3)=ISATZ(13)
   DC 3 J=1,3
   N=IR(J)
   IWJ=IW(J)
   IF (IS-N-1)5,6,5
5  READ (LBN*N) (ISATZ(II),II=1,NSZ)
   IS=N+1
6  IF (J-3)10,11,11
10 L=3
   GO TO 326
11 L=4
326 IMP=IAD(J)*L+IWJ-1
8  IF (IMP-NSZ)13,14,15
14 N=1
   GO TO 16
15 N=2
16 DC 12 L=IWJ,NSZ
   IAC(K)=ISATZ(L)
12 K=K+1
   GO TO (3,17),N
17 IMP=IMP-NSZ
   IWJ=1
   READ (LBN*IS) (ISATZ(II),II=1,NSZ)
   IS=IS+1
   GC TO 8
13 CC318 L=IWJ,IMP
   IAC(K)=ISATZ(L)
318 K=K+1
3  CCNTINUE
   RETURN

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C
C   SLBROUTINEN NDFLOC , LDFLOC , IDFLCC
C
   ENTRY NDFLOC (KONTR,NNAM,DAT1,ID,KC)
   IF(NSZ.NE.880) GO TO 1004
   IC=0
   KC=0
   DC 403 LS=1,2
   IF (DAT1(LS).NE.MNAM(LS)) GC TO 104
403 CONTINUE
   MCL=2
   GC TO 107
104 MCL=1
107 J=NNAM(1)*2
   DO 51 N=1,J
51 Z(N)=DAT1(N)
   LS=1
   DO 18 N=1,J
   IF(N-4)19,218,20
19 IF(N-3)20,218,218
20 MNAM(L)=KDAT1(N)
   L=L+1
   GO TO 18
218 IPEST(LS)=KDAT1(N)
   LS=LS+1
18 CONTINUE
   KK=1
   GO TO 427
C
   ENTRY LDFLOC (KONTR,NNAM,INAM,DAT2)
   IF(NSZ.NE.880) GO TO 1004
   DO 127 LS=1,2
   IF (INAM(LS).NE.MNAM(LS)) GO TO 128
127 CONTINUE
   MCL=2
   GC TO 129
128 MCL=1
129 J=NNAM(1)*2
   DC 21 N=1,J
21 MNAM(N)=INAM(N)
   KK=2
427 K=4
   IWJ=0
   DC 22 LS=1,3,2
   IWJ=IWJ+1
   N=IAC(IWJ)*3
   DC 23 M=1,N
   IF (MNAM(LS).NE.IAD(K)) GO TO 23
   IF (MNAM(LS+1).EQ.IAC(K+1)) GC TO 26
23 K=K+3
   WRITE (NOUTP,2000) (MNAM(M),M=1,4)
2000 FORMAT(1H0/' ***WARNING NDF. 1 : THE DATA FOR **,'2A4,'**,'1X,'**,'
12A4,'** ARE NOT INCLUDED '/' IN THE CONVERSICNTABLE OF THE KEDAK LIBRARY')

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- B 21 -

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      MAAM(1)=1
      KCNTR=0
      IF(JJ-1)98,98,96
26  ALNA(IWJ)=IAC(K+2)
22  K=N+4
      GC TO (227,228),MGL

C
      ENTRY IDFLOC (KONTR,NNAM,INAM,DATE)
      IF(NSZ.NE.880) GO TO 1C04
      KK=3
      IF(INAM(1)-NUNA(1))130,131,120
131  MGL=2
      GO TO 132
130  MGL=1
122  ALNA(1)=INAM(1)
      NUNA(2)=INAM(2)
      IF(NNAM(1)-2)27,27,52
52  J=NNAM(1)
      CC 53 LS=3,J
53  MAAM(2*LS-1)=INAM(LS)
27  GO TO (227,228),MGL
227  N=IAC(3)*4
      IWJ=(IAD(1)+IAD(2))*3+4
      CC 28 LS=1,N,4
      IF(NUNA(1)-IAD(IWJ))28,29,28
28  IWJ=IWJ+4
      KCNTR=0
      GC TO 24
29  NT=IAD(IWJ+1)
      JR=IAD(IWJ+2)
      JW=IAD(IWJ+3)
228  KR=JR
      Kw=JW
      IVY=0
      IF(IS-KR-1)30,31,30
30  READ (LBN*KR) (ISATZ(II),II=1,NSZ)
      IS=KR+1
31  DC 32 LS=1,NT
      IF(NUNA(2)-ISATZ(KW))33,34,33
33  KW=KW+7
      IF(KW-NSZ)32,32,35
35  READ (LBN*IS) (ISATZ(II),II=1,NSZ)
      IS=IS+1
      KW=KW-NSZ
32  CCNTINUE
      KCNTR=0
      GC TO 24
34  Kw=KW+1
      DO 36 LS=1,6
      IF(KW-NSZ)37,37,38
38  READ (LBN*IS) (ISATZ(II),II=1,NSZ)
      IS=IS+1
      Kw=1
37  GO TO (39,40,40,41,42,43),LS
39  NNA=ISATZ(KW)

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      GOTO 36
40  NNA(LS)=ISATZ(Kw)
      GOTO 36
41  NWP=ISATZ(KW)
      GO TO 36
42  ICR=ISATZ(KW)
      GC TO 36
43  ICW=ISATZ(KW)
36  Kw=Kw+1
      IF(KK-1)46,46,47
46  NNA(4)=0
47  DC 90 LS=1,4
80  NN(LS)=NNAM(LS)
      IF(NWN)384,384,49
45  NNK=NWP
      NWR=IDR
      Nkw=IDW
      IF(IS-NWR-1)44,45,44
44  READ (LBN*NWR) (IWNA(II),II=1,NSZ)
      NWR=NWR+1
      GC TO 62
45  DC 61 LS=1,NSZ
61  IWNA(LS)=ISATZ(LS)
      NWR=NWR+1
62  DC 68 N=1,NNK
      NKC=N
      Nk=NWW
      KP=5
      JC=3
      CC 54 LS=1,NWN
      IF(IWNA(NWW)-MNA(KP))58,55,56
56  KCNTR=0
      IVY=1
      IF(KK-2)57,59,859
59  INAM(KP)=IWNA(NWW)
      GOTO 60
859  INAM(JC)=IWNA(NWW)
      GC TO 60
57  CATI(KP+2)=XWNA(NWW)
      GC TO 60
55  KONTR=1
60  KP=KP+2
      JD=JD+1
      NWW=NWW+1
      IF(NWW-NSZ)54,54,64
64  READ (LBN*NWR) (IWNA(II),II=1,NSZ)
      NWR=NWR+1
      Nkw=1
54  CCNTINUE
      GC TO 74
58  Nkw=Nw+NWN+3
      IF(NWW-NSZ)68,68,70
70  READ (LBN*NWR) (IWNA(II),II=1,NSZ)
      NWR=NWR+1
73  Nkw=NWW-NSZ

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68	CONTINUE	2410					
	KCNTR=0	242C					
	IF(KK.EQ.3) GO TO 580	243C					
	WRITE (NOUTP,2002) MNAM(5),(MNAM(II),II=1,4)	2440					
2002	FCRMT(1HO/' ***WARNING NDF. 2 : THE FURTHER NAME ',E16.8,' IS GRE	2450					
	ATER THAN THE GREATEST FURTHER NAME '/' INCLUDEC IN THE KEDAK LIBR	2460					
	ZARY FOR',1X,2A4,1X,2A4)	2470					
	GC TO 98	248C					
580	WRITE (NOUTP,581) MNAM(5),(INAM(II),II=1,2)	2490					
581	FCRMT(1HO/' ***WARNING NDF. 2 : THE FURTHER NAME',E16.8,' IS GREA	250C					
	ITER THAN THE GREATEST FURTHER NAME '/' INCLUDED IN THE KEDAK LIBRAR	2510					
	ZY FOR',2I10)	2520					
	GO TO 98	2530					
1004	WRITE (NOUTP,1005)	2540					
1005	FCRMT(1HO/' ***ERROR NDF. 2 : AT FIRST THE --CPN - ROUTINE MUST B	255C					
	IE CALLED')	2560					
	STCP	2570					
74	NWP=IWINA(NWW)	2580					
	CC 75 LS=1,2	2590					
	NWW=NWW+1	260C					
	IF(NWW-NSZ)76,76,78	2610					
78	READ (LBN'NWR) (IWINA(II),II=1,NSZ)	2620					
	NWR=NWR+1	263C					
	NWW=1	2640					
76	GC TO (81,82),LS	2650					
E1	ICR=IWINA(NWW)	2660					
	GC TO 75	2670					
E2	IDW=IWINA(NWW)	268C					
75	CONTINUE	269C					
	NWW=NWW+1	2700					
48	IF(NWN)384,384,383	2710					
384	IF(IS-IDR-1)83,385,83	272C					
383	IF(NWR-IDR-1)83,84,83	2730					
385	CC 386 L=1,NSZ	2740					
386	JDAT(L)=ISATZ(L)	2750					
	ICR=ICR+1	276C					
	GC TO 388	2770					
84	CC 85 L=1,NSZ	2780					
E5	JDAT(L)=IWINA(L)	279C					
	ICR=ICR+1	2800					
	GC TO 388	2810					
83	READ (LBN>IDR) (JDAT(II),II=1,NSZ)	2820					
	ICR=ICR+1	2830					
398	NPA=1	2840					
86	JC=NNAM(2)+NNAM(3)	2850					
	IF(KK-2)87,88,88	286C					
87	LS=NNAM(1)*2+1	2870					
	GC TO 99	2880					
88	LS=1	2890					
89	CC 90 L=1,JD	2900					
	GC TO (91,92,92),KK	291C					
91	DAT1(LS)=XJDAT(IDW)	2920					
	DAT1(LS+1)=0.	2930					
	LS=LS+2	2940					
	GO TO 93	2950					
92	DAT2(LS)=XJDAT(ICW)	2960					
	LS=LS+1	2970					
93	ICW=IDW+1	2980					
	IF(IDW-NSZ)90,90,94	2990					
94	READ (LBN>IDR) (JDAT(II),II=1,NSZ)	300C					
	ICR=ICR+1	3010					
	ICW=1	302C					
50	CONTINUE	3030					
	IF(IVY)1003,1003,98	3040					
1003	KCNTR=1	3050					
	GC TO 99	3060					
24	WRITE(NOUTP,97)NUNA(1),NUNA(2)	3070					
97	FORMAT(1HO/' ***WARNING NDF. 3 : THE DATA FOR',2I9,' ARE NCT INCLU	3080					
	ICFC IN THE KEDAK LIBRARY')	3090					
	IF(JJ-1)98,98,96	310C					
96	RETURN 1	3110					
98	RETURN	3120					
C		3130					
C		314C					
C	SLBRCUTINEN NDFNXT, LDFNXT, IDFNXT	315C					
C		316C					
	ENTRY NDFNXT (KONTR,NNAM,DAT1,IO,KC)	3170					
	IC=0	3180					
	KC=0	3190					
	LL=1	320C					
	GC TO 101	3210					
C		3220					
	ENTRY LDFNXT (KONTR,NNAM,INAM,DAT2)	3230					
	LL=2	324C					
	GC TO 101	3250					
C		326C					
	ENTRY IDFNXT (KONTR,NNAM,INAM,DAT2)	3270					
	LL=3	328C					
101	NPA=NPA+1	329C					
	IVY=0	3300					
	IF(NPA-NWP)102,102,103	3310					
103	KCNTR=C	3320					
	IF (NWN)387,387,389	3330					
389	NKC=NKO+1	3340					
	IF(NKO-NNK)391,391,387	3350					
387	RETURN	3360					
102	KCNTR=1	337C					
391	DO 304 LS=1,3	3380					
304	NNAM(LS)=NN(LS)	339C					
	IF(LL-2)105,124,106	340C					
105	NNAM(4)=0	3410					
	KCAT1(1)=MNAM(1)	342C					
	KCAT1(2)=MNAM(2)	3430					
	KCAT1(3)=IBEST(1)	3440					
	KDAT1(4)=IBEST(2)	345C					
	KCAT1(5)=MNAM(3)	3460					
	KCAT1(6)=MNAM(4)	347C					
	DO 401 II=1,6	3480					
401	DAT1(II)=Z(II)	3490					
	GC TO 125	3500					


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124 CC 126 LS=1,4
126 INAM(LS)=MNAM(LS)
GO TO 125
106 CC 327 LS=1,2
327 INAM(LS)=NUNA(LS)
125 IF(NWN)86,86,390
390 IF(KONTR)108,108,86
108 KP=NWN+3
IVY=1
L=5
CC 109 LS=1,KP
IF(NWW-NSZ)110,110,111
111 READ (LBN*NWR) (IWNA(II),II=1,NSZ)
NWR=NWR+1
NWR=1
110 IF(LS-NWN)112,112,113
112 IF(LL-2)114,115,116
114 L=L+2
KCAT1(L)=IWNA(NWW)
KCAT1(L+1)=0
DAT1(L)=Z(L)
CAT1(L+1)=Z(L+1)
GO TO 109
115 INAM(L)=IWNA(NWW)
L=L+2
GO TO 109
116 L=LS+2
INAM(L)=IWNA(NWW)
113 L=LS-NWN
GO TO (119,118,117),L
119 NWF=IWNA(NWW)
GOTO 109
118 ICR=IWNA(NWW)
GOTO 109
117 ICW=IWNA(NWW)
109 NWR=NWR+1
GO TO 398
END

FUNCTION PHI(E)
PHI=1./E
RETURN
END

SUBROUTINE DOPW(I,J)
REAL*8 I,J
J=I
RETURN
END

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REAL FUNCTION DPHI*8(E)
REAL*8 E
LOGICAL*4 DRIFUN
COMMON/CFSMEL/ DRIFUN
C THE STATEMENT "DRIFUN=.TRUE." MUST ONLY BE USED FOR THE ORIGINAL
C FUNCTION, BUT NOT FOR A FUNCTION LINKED TO THE PROGRAM BY THE
C USER.
DRIFUN=.TRUE.
DPHI=1.00+0/E
RETURN
END

SUBROUTINE FSPIE
FSPIE IS A SPECIAL ERROR-DETECTING SUBROUTINE ,WHICH IN CASE
OF AN ABNORMAL END DETERMINES THE PSW AND PRINTS THIS PSW +
A TRACE-BACK + THE REGISTER CONTENTS + THE SYSTEM COMPLETION
CODE.. FOR FSPIE IS INSTALATION DEPENDENT ITS CODE IS ACT
DISTRIBUTED HERE
RETURN
END

SUBROUTINE FGEM(NS,SIG0,NE,EAG,NEF,ES,F,NT,TFMF,PR,NMR,NFST,SUM,
ISUC,IRE,IREF,ER,L,GJ,CAT,GAN,GAG,GAF,ISTE,ISTEP,STE,STE1)
REAL*8 MATN,FEST,IFEST,AN,MM,III
DIMENSION ENGINE,ES(NEF),F(NEF),TEMP(NT),SIGC(NS),IFEST(2C),
IFEST(2C),
2 NN(4),IZAHL(4),SUMO(3),SUM(NS,7),STE(5,ISTE),SLO(NE,3),
3ER(IRE),L(IRE),GJ(IRE),CAT(IRE),GAN(IRE),GAG(IRE),GAF(IRE),
4STE1(ISTE)
COMMON MATN,ISTRUK,ISPA,NOU TP,LZWF,IR(2),KL
EQUIVALENCE (FEST(1),IFEST(1))
WRITE (NOU TP,9000)
9000 FCORMAT(IHO/IHC/' PROGRAMM KENNZIFFER 1')
WRITE (NOU TP,9001)
9001 FCORMAT(' PROGRAMM ZUR BERECHNUNG VON RESONANZSELESTARBSCHIRMFAKTORE
IN VON AUFGELOESTEN RESONANZPARAMETERN')
CALL FSPIE
CALL DOPW (8HBEST ,NN(1))
CALL DOPW (8HISOT1 ,NN(2))
CALL DOPW (8HTSCT2 ,NN(3))
CALL DOPW (8HRES ,NN(4))
CALL DOPW (8HMIGR ,MM)
IREF=0
IREF=0
ISTEP=0

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ISTEF=0
CALL EXPPX(X,X,X,X)
NEFE=NEF
IF(NEF.NE.1) GOTC 411
NEFE=0
411 PI=3.14159
NEI=NE-1
12 IZ AHL(1)=3
IFEST(1)=MATN
IFEST(2)=NN(1)
IFEST(3)=NN(2)
CALL NDFLOC(IDD, IZ AHL, FEST, IDAT, ICCD)
IF(IDD)110,111,110
110 A=FEST(4)
IFEST(3)=NN(3)
CALL NDFLOC(IDD, IZ AHL, FEST, ICAT, ICCD)
IF(ICD)115,111,115
115 RLA=FEST(4)
R=FEST(5)
SICP=4.*PI*R**2
IFEST(3)=NN(4)
NR=1
CALL NDFLOC(IDD, IZ AHL, FEST, ICAT, ICCD)
IF(IDD)112,111,112
112 ER(NR)=FEST(4)
L(NR)=IFEST(5)
GJ(NR)=FEST(7)
GAT(NR)=FEST(8)
GAN(NR)=FEST(9)
GAG(NR)=FEST(10)+FEST(12)+FEST(13)
GAF(NR)=FEST(11)
NR=NR+1
IF(NR.LE.IRE) GO TO 200
NR=1
IREF=IREF+1
200 CALL NDFNXT( IDD, IZ AHL, FEST, IDAT, ICOD)
IF(IDD)112,113,112
113 NR=NR-1
IF(IREF.EQ.0) GO TO 5
IREP=(IREF-1)*IRE+NR+1
RETURN
5 IF(NMR.EQ.-1) NMR=NR
NMIN=NMR
DC 63 IF=1,NEI
IF(ENG(IE+1)-ER(NR))63,63,64
63 CONTINUE
NLA ST=NEI
GCTO 66
64 NLA ST=IE-1
IF(NLA ST)65,65,66
65 NFST=1
GOTO 3
66 NFST =NLA ST+1
4 NANF=NE-IR(1)
IF(NANF-NLA ST)510,510,3

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510 NEND=NE-IR(2)
502 IF(NEND-NLA ST)503,503,505
503 NLA ST=NEND
NFST=0
505 DC 60 IT=1,NT
T=TEMP(IT)
NRI=1
DO 10 IE=NANF,NLA ST
DC 36 ISO=1,3
36 SLMC(ISO)=.0
DC 37 ISO=1,NS
DC 37 J1=1,7
37 SLM(ISO,J1)=.0
SUME=.0
K=1
STE(1,K)=ENG(IE)
DC 15 INR=NRI,NR
IF(ENG(IF)-ER(INR))16,15,15
16 IF(ENG(IF+1)-ER(INR))18,18,17
17 K=K+1
IF(K.LE.ISTE) GO TO 201
K=1
ISTEF=ISTEF+1
201 STE(1,K)=ER(INR)
15 CONTINUE
18 K=K+1
IF(K.LE.ISTE) GO TO 202
K=1
ISTEF=ISTEF+1
202 STE(1,K)=ENG(IE+1)
KMAX=K
IF(ISTEF.EQ.0) GO TO 250
ISTEP=(ISTEF-1)*ISTE+R+50
RETURN
250 NRI=INR
KS=KMAX
DC 2002 K=1,KS
2002 STE1(K)=STE(1,K)
DO 2011 K=1,KS
C 2011 WRITE(NDOUTP,1050) K,STE1(K)
1050 FORMAT(' K=',I10,' STE1(K)=',F14.6)
CC 19 K=1,KMAX
CALL WIRQU(NRI,STE(1,K),STE(2,K),STE(3,K),STE(5,K),NR,IRE,ER,GJ,
IGAN,GAT,GAF,L,GAG,T,A,R,RLA,NMIN)
WRITE(NDOUTP,1000) KMAX,K,STE(1,K),STF(3,K)
C 1000 FORMAT(' KMAX=',I10,' K=',I10,' STE1=',E16.8,' STE3=',E16.8)
19 STE(4,K)=STE(5,K)-STE(3,K)-STE(2,K)
22 KPX=KMAX+1
KMXI=KMAX-1
IF(KMXI)33,34,33
33 IF(KMX.LE.ISTE) GO TO 833
ISTEP=50
RETURN
833 DC 20 K=1,KMXI
KI=KMX-K

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DC 20 J1=1,5
2C STE(J1,K1+1)=STE(J1,K1)
IABF=0
DO 2000 K=1,KS
IF(STE(1,1).EQ.STE1(K)) IABF=1
IF(STE(1,3).EQ.STE1(K)) GO TO 2001
GO TO 2000
20C1 IF(IABF.EQ.1) ISI=0
2000 CONTINUE
KMAX=KMAX+1
35 STE(1,2)=(STE(1,3)+STE(1,1))/2.
CALL WIRQU(NR1,STE(1,2),STE(2,2),STE(3,2),STE(5,2),NR,IRE,ER,GJ,
IGAN,
IGAT,GAF,L,GAG,T,A,R,RLA,NMIN)
C WRITE(NOUTP,1007) STE(1,2),STE(3,2)
10C7 FORMAT (' ERGEBNIS VON WIRQU:STE(1,2)=' ,E14.6, 'STE(3,2)=' ,E14.6)
STE(4,2)=STE(5,2)-STE(3,2)-STE(2,2)
DST=STE(1,2)-STE(1,1)
C WRITE(NOUTP,1006) STE(1,1),STE(1,2),STE(1,3),ISI
10C6 FORMAT (' STE(1,1)=' ,E16.8, 'STE(1,2)=' ,E16.8, 'STE(1,3)=' ,E16.8,
1*ISI=' ,I5)
CALL STOSS(STE(1,1),STE(1,2),STE(1,3),F1,F2,F3,NEF,ES,F)
DC 21 J1=2,4
FLC1=(3.*STE(J1,1))*F1+STE(J1,3)*F3)*DST*.25
FLC2=(STE(J1,1)*F1+STE(J1,2)*F2)*DST*.5
IF(FLC1)45,21,45
45 AFL=ABS((FLC1-FLC2)/AMIN1(FLC1,FLC2))
C WRITE(NOUTP,1001) J1,FLC1,FLC2,AFL
10C1 FORMAT (' J1=' ,I10, 'FLC1=' ,E16.8, 'FLC2=' ,E16.8, 'AFL=' ,E16.8)
IF(AFL-PR ) 1021,1021,1022
1021 IF(ISI.NE.1) GO TO 1010
GC TO 21
1010 ISI=1
GC TO 22
1C22 ISI=0
GC TO 22
21 CONTINUE
DC 24 J1=1,3
24 SUMO(J1)=(STE(J1+1,1)*F1+STE(J1+1,2)*F2)*DST*.5+SUMO(J1)
SUME=SUME+(F1+F2)*DST*.5
C WRITE(NOUTP,1002) SUMO(2),SUME
DO 25 ISO=1,NS
SIG1=STE(5,1)+SIGO(ISO)
SIG2=STE(5,2)+SIGO(ISC)
SIG3=SIG1*SIG1
SIG4=SIG2*SIG2
SUM(ISO,5)=(F1/SIG3+F2/SIG4)*DST*.5+SUM(ISC,5)
SUM(ISO,1)=(F1/SIG1+F2/SIG2)*DST*.5+SUM(ISO,1)
DC 325 J1=6,7
325 SUM(ISO,J1)=(STE(J1-2,1)*F1/SIG3+STE(J1-2,2)*F2/SIG4)*DST*.5
1+SUM(ISO,J1)
DO 25 J1=2,4
25 SUM(ISO,J1)=(STE(J1,1)*F1/SIG1+STE(J1,2)*F2/SIG2)*DST*.5+SUM(ISO,J
1)
CC 27 J1=2,4

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FLC1=(STE(J1,1)*F1+3.*STE(J1,3)*F3)*DST*.25
FLC2=(STE(J1,2)*F2+STE(J1,3)*F3)*DST*.5
IF(FLC1)46,27,46
46 AFL=ABS((FLC1-FLC2)/AMIN1(FLC1,FLC2))
C WRITE(NOUTP,1001) J1,FLC1,FLC2,AFL
IF(AFL-PR )27,27,28
27 CCNT INUE
DC 29 J1=1,3
29 SUMO(J1)=(STE(J1+1,2)*F2+STE(J1+1,3)*F3)*DST*.5+SUMC(J1)
SUME=SUME+(F2+F3)*DST*.5
C WRITE(NOUTP,1002) SUMO(2),SUME
10C2 FCRMAT (' SUMO(2)=' ,E16.8, 'SUME=' ,E16.8)
DC 30 ISO=1,NS
SIG1=STE(5,2)+SIGO(ISO)
SIG2=STE(5,3)+SIGO(ISC)
SIG3=SIG1*SIG1
SIG4=SIG2*SIG2
SUM(ISO,5)=(F1/SIG3+F2/SIG4)*DST*.5
SUM(ISO,1)=(F2/SIG1+F3/SIG2)*.5*DST
DC 330 J1=6,7
330 SUM(ISO,J1)=SUM(ISO,J1)+(STE(J1-2,2)*F2/SIG3+STE(J1-2,3)*F3/
1SIG4)*DST*.5
DO 30 J1=2,4
30 SUM(ISO,J1)=SUM(ISO,J1)+(STE(J1,2)*F2/SIG1+STE(J1,3)*F3/SIG2)*DST*
1.5
DO 31 K=3,KMAX
DC 31 J1=1,5
31 STE(J1,K-2)=STE(J1,K)
KMAX=KMAX-2
GC TO 22
28 DO 32 J1=1,5
32 STE(J1,1)=STE(J1,2)
GC TO 35
34 IF(IT.EQ.1.AND.IE.EQ.NANF) GO TO 935
GO TO 934
935 INDEX=0
WRITE(LZWF) INDEX,MM
934 INDEX=6
WRITE(LZWF) INDEX,MATN ,TEMP(IT),IE,ENG(IE),ENC(IE+1)
DO 38 ISO=1,3
38 SUMC(ISO)=SUMC(ISO)/SUME
INDEX=5
SGT1=SUMO(1)+SUMO(2)+SUMO(3)
WRITE(LZWF) INDEX,SUMO(2),SUMC(3),SUMC(1),SUMO(2),SGT1
INDEX=6
WRITE(NOUTP,957)
957 FORMAT (1H0,18X,8HMATERIAL,3X,10HTEMPERATUR,2X,6HGRUPPE,7X,7HGRENZE
1A)
IV=NE-IE
WRITE(NOUTP,958)MATN ,TEMP(IT),IV,ENG(IE),ENC(IE+1)
958 FCRMAT(1H ,18X,A8,F11.2,6X,12,1X,2E12.4/1X)
WRITE(NOUTP,950)
950 FCRMAT(1H0,21X,7HSIGMA G,9X,7HSIGMA N,9X,7HSIGMA F,9X,7HSIGMAN1,
19X,7HSIGMAT1)
WRITE(NOUTP,951) SUMO(2),SUMO(3),SUMO(1),SUMO(2),SGT1

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951 FCRMAT(1H ,15X,5E16.8)
WRITE(NOUTP,952)
952 FCRMAT(1H0,6X,7HSIGMA 0,11X,2HFG,14X,2HFN,14X,2HFF,14X,3HFN1,
113X,3HFT1/1X)
DC 39 ISO=1,NS
DO 40 J1=2,4
IF(SUM0(J1-1))420,421,420
421 SLM(ISO,J1)=1.
GOTO 40
420 SLM(ISO,J1)=SUM(ISO,J1)/(SUM(ISO,1)*SUM0(J1-1))
4C CONTINUE
SUM(ISO,6)=SUM(ISO,6)/(SUM(ISO,5)*SUM0(3))
SLM(ISO,7)=SUM(ISO,7)/(SUM(ISO,5)*(SUM0(1)+SUM0(2)+SUM0(3)))
WRITE(NOUTP,953)SIGO(ISO),SUM(ISO,3),SUM(ISO,4),SUM(ISO,2)
1,SUM(ISO,6),SUM(ISO,7)
35 WRITE(LZWF) INDEX,SIGO(ISO),SUM(ISC,3),SUM(ISC,4),SUM(ISC,2)
1,SUM(ISO,6),SUM(ISO,7)
953 FCRMAT(6E16.8)
10 CCNTINUE
60 CONTINUE
3 CONTINUE
111 KL=KL+1
RETURN
END

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ST=.0
GOTO 3
1 SC=SCC*GAG(INR)*PSI/GT
SF=SOC*GAF(INR)*PSI/GT
PHI1=PHIO-ATAN(PHIO*FLOAT(L(INR)))
PHI2=.2*PHI1
ST=SOC*(PSI*COS(PHI2)+CHI*SIN(PHI2))
SIGP=4.*PI*ELA**2*FLCAT(2*L(INR)+1)*SIN(PHI1)**2
IF(ST+SIGP)10,10,3
10 WRITE(NOUTP,900)ER(INR),E,ST,SIGP
970 FCRMAT(1H0,77H***WARNING 1.01 : THE CONTRIBUTION OF THE RESONANCE
WITH THE RESONANCE ENERGY,E13.6,3H EV/1H ,18X,12HAT THE ENERGY,E14
2.6,13H IS NEGATIVE,E14.6,22H BARNS,AND ITS ABSCLUT/1H ,18X,46HVAL
3UE LARGER THAN THE POTENTIAL CROSS SECTION,F14.6,7H BARNS.)
3 RETURN
END

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SUBROUTINE WIRQ (INR,E,SF,SG,ST,IRE,
1 ER,GJ,GAN,GAT,GAF,L,GAG,T,A,R,RLA)
REAL*8 MAT
DIMENSION ER(IRE),GJ(IRE),GAN(IRE),GAT(IRE),GAF(IRE),L(IRE),GAG(IR
1E)
COMMON MAT,ISTRUK,ISPA,NOUTP
PI=3.14159
XKC=8.6165E-5
ERI=ER(INR)
ELA=R/ELA
PHIO=R/ELA
IF(ERI.LE.0.) GN=GAN(INR)*SQRT(F)*(PHIO*PHIO)**L(INR)
IF(ERI.GT.0.) GN=GAN(INR)*SQRT(E/ERI)*(E/ERI)**L(INR)
GT=GN+GAG(INR)+GAF(INR)
SOC=4.*PI*ELA**2*GJ(INR)*GN/GT
X=2.*(E-ER(INR))/GT
IT=T
IF(IT)4,5,4
5 PSI=1./(1.+X*X)
CHI=X*PSI
GOTO 6
4 DELTA=SQRT(4.*XK0*T*E/A)
TETA=(DELTA/GT)**2
CALL PSI XI(X,TETA,PSI,CHI)
6 IF(L(INR)-1)1,1,2
2 SG=.0
SF=.0

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SUBROUTINE WIRQU(NR1,E,SIFG,SIGG,SIGT,NR,IRE,
1 ER,GJ,GAN,GAT,GAF,L,GAG,
1 T,A,R,RLA,NMIN)
REAL*8 MAT
DIMENSION ER(IRE),GJ(IRE),GAN(IRE),GAT(IRE),GAF(IRE),L(IRE),GAG(IR
1E)
COMMON MAT,ISTRUK,ISPA,NOUTP
PI=3.14159
ELA=R/ELA
PHIO=R/ELA
PHI1=PHIO-ATAN(PHIO)
SIGP=4.*PI*ELA**2*(SIN(PHIO)**2+3.*SIN(PHI1)**2)
NR2=NR1+1
CC 1 I=1,NR1
NR3=NR2-1
IF(E-ER(NR3))1,2,2
1 CONTINUE
2 SIFG=0.
SIGG=.0
SIGT=SIGP
IA=NR3-NMIN
IF(IA)3,3,4
3 IA=1
4 IE=NR3+NMIN
IF(IE-NR)5,6,6
6 IE=NR
5 CC 7 INR=IA,IE
CALL WIRQ(INR,E,SF,SG,ST,IRE,
1 ER,GJ,GAN,GAT,GAF,L,GAG,T,A,R,RLA)
SIFG=SIFG+SF
SIGG=SIGG+SG
SIGT=SIGT+ST
7 CONTINUE
IF(SIGT)10,10,11
10 WRITE(NOUTP,900)SIGT,E

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GNF=GAFM(E,NS,NEY,EY,GF)
GNG=GAMG(E,NS,GG)
NY=XNYN(NS)
NFY=FXNYN(NS)
IF(NY.GT.4.OR.NFY.GT.4) GO TO 4
GO TO 8
4 WRITE(NDOUTP,100) NY,NFY,E,NS
100 FORMAT(/' ***ERROR 2.01 : THE HIGHEST NUMBER OF EXIT CHANNELS IN N
1EUTRON ELASTIC SCATTERING,NUEN,OR IN FISSION,NUFF,THAT CAN BE TREA
2TED,IS 4/' ***NUEN=',I4,'NUFF=',I4,'AT ENERGY',E12.5,'FV IN SERIE
3S',I4)
8 CC 1 I=1,2
X(I)=.0
1 Y(I)=.0
IF (ISPA.EQ.0.OR.GNF .LT.1.E-30) GO TO 6
5 NN=25
NF=25
XFN=625.
7 CC 2 I=1,NN
CC 2 J=1,NF
X1=((GNN*CHI(I,NY))**2)/(GNN*CHI(I,NY)+GNG+GNF*CHI(J,NFY))
Y1=GNN*CHI(I,NY)/(GNN*CHI(I,NY)+GNG+GNF*CHI(J,NFY))
X(1)=X(1)+X1
Y(1)=Y(1)+Y1
X(2)=X(2)+X1*GNF*CHI(J,NFY)
2 Y(2)=Y(2)+Y1*GNF*CHI(J,NFY)
EZG=X(1)/(Y(1)*GNN)
EZC=1.+2./XNYN(NS)
EZF=X(2)/(Y(2)*GNN)
DRSG=Y(1)*GNG/(GNN*XFN)
DRFS=Y(2)/(GNN*XFN)
GO TO 10
6 NN=25
XFN=25.
DC 3 I=1,NN
X1=((GNN*CHI(I,NY))**2)/(GNN*CHI(I,NY)+GNG)
Y1=GNN*CHI(I,NY)/(GNN*CHI(I,NY)+GNG)
X(1)=X(1)+X1
3 Y(1)=Y(1)+Y1
EZG=X(1)/(Y(1)*GNN)
EZC=1.+2./XNYN(NS)
EZF=.0
DRSG=Y(1)*GNG/(GNN*XFN)
DRFS=.0
10 CFAT INUE
RETURN
END

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FUNCTION DMIT(E,NS,DN,EBI)
DIMENSION DN(10)
DMIT=DN(NS)*((EBI+F)/EBI)**2*FXP(-SQRT(89.72E-6)*(SQRT(EBI+E)-
1SQRT(EBI)))
RETURN
END

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FUNCTION DELTA(E,T,NS,DEL)
DELTA=SQRT(DEL*T*E)
RETURN
END

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FUNCTION EPSI(E,T,NS,DN,EBI,DEL)
DIMENSION EP(21),EPP(21),X1(2),FX1(2),DN(10)
DATA EP/0.,1.,1.5,2.,2.5,3.,3.5,4.,5.,7.,10.,14.,20.,30.,40.,
X50.,60.,70.,80.,90.,100./,EPP/2.5066,1.7241,1.3705,1.0661,
X0.82,0.6291,0.4845,0.3758,0.23261,0.10002,0.03577,0.012276,
X0.003647,8.523E-4,2.8817E-4,1.2683E-4,5.579E-5,3.694E-5,2.5643E-5,
X1.8679E-5,8.733E-6/
X=DMIT(E,NS,DN,EBI)/DELTA(E,T,NS,DEL)
DO I I=2,21
IF(X-EP(I))4,4,1
1 CCNT INUF
4 CC 5 K=1,2
J1=I+K-2
X1(K)=EP(I1)
5 FX1(K)=EPP(I1)
EPSI=POL(X,X1,FX1)/X
RETURN
END

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FUNCTION GAMN(E,NS,GN,RQU,XL,XA)
DIMENSION GN(10),XL(10)
GAMN=GN(NS)*SQRT(E)*(E*RQU+(1.-XL(NS))*XA)/(E*RQU+XA)
RETURN
END

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FUNCTION GAMG(E,NS,GG)
DIMENSION GG(10)
GAMG=GG(NS)
RETURN
END

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FUNCTION GAFM(E,NS,NEY,EY,GF)
REAL*8 MAT
DIMENSION EY(199),GF(10,199),X1(2),FX1(2)
COMMON MAT,ISTRUK,ISPA
IF(ISPA)2,2,3
3 CALL SUCH(E,NSU,NEY,EY)
CC 1 J=1,2
NSL=NSU+J
X1(J)=FY(NSU1)
1 FX1(J)=GF(NS,NSU1)
GAFM=POL(E,X1,FX1)
GC TC 4
2 GAFM=0.
4 RETURN
END

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FUNCTION POL(X,X1,FX1)
DIMENSION X1(2),FX1(2)
IF(X1(2)-X1(1))1,2,1
2 POL=FX1(1)
GC TO 3
1 PCL=FX1(1)+(FX1(2)-FX1(1))*(X-X1(1))/(X1(2)-X1(1))
3 RETURN
END

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SUBROUTINE SUCH(E,NSU,NEY,EY)
DIMENSION EY(199)
CO 14 K=2,NEY
IF(EY(K)-E)14,13,13
14 CONTINUE
13 NSU=K-2
RETURN
END

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FUNCTION SIGC(E,NS,XA,GI,GN,EBI,GN,RQU,XL)
DIMENSION GI(10),DN(10),GN(10),XL(10)
SIGC=19.73921*XA*GI(NS)*GAMN(E,NS,GN,RQU,XL,XA)/(F*DMIT(E,NS,GN,
1 EBI))
RETURN
END

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FUNCTION PHASE(E,NS,XA,RQU,XL)
DIMENSION XL(10)
B=SQRT(RQU*E/XA)
PHASE=COS(2.*(B-XL(NS)*ATAN(B)))
RETURN
END

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SUBROUTINE FSTAT(MI,SIGO,J,ENG,AFE,REFE,EFE,MT,TFMP,SE,SM,
1XEUGZ)
REAL*8 X,IX,MAT,NN
1,MM
DIMENSION ENG(J),EFE(NFE),REFE(NFE),TEMP(MT),SIGO(MT),NADAT(2),
2EY(199),NN(5),NAME(4),X(20),IX(20),CHI(25,4),CF(10,199),
3 GN(10),XL(10),DN(10),GI(10),XNYN(10),FXNYN(10),GG(10),
4SE(3,5,MI),SM(3,5,MI), E(3),XEUGZ(5,MI),XSUGL(5),SU(5)
5,E(3))
COMMON MAT,ISTRUK,ISPA,ACOUTP,LIZ,NANF,NENC,KL
EQUIVLENCE(X(1),IX(1))
DATA CHI/8.383E-4,5.8607E-3,1.595668E-2,3.122356E-2,5.182214E-2,
X7.796678E-2,0.1110434,0.14875186,0.19382632,0.2462014,0.3066044,
X0.37595912,0.45541448,0.5464511,C.65057026,0.7714919,0.9114051,
X1.075423,1.2703559,1.5065244,1.8006327,2.1822634,2.7109872,
X3.5798648,5.9721596,2.0273F-2,6.155225E-2,0.1054415,0.15091425,
X0.198549,0.2485715,C.301227,0.35680875,0.41567075,0.47820725,
XC.544925,0.61641525,0.693415,0.77684375,0.867878,0.968046,
X1.0793867,1.2047147,1.3480617,1.5155082,1.716864,1.9695355,
X2.309333,2.832582,4.2188757,5.9001333E-2,0.1333242,0.19497146,
X0.251645,0.3074142,0.36262126,0.4181491,0.4746072,0.53251576,
XC.5965109,0.65162876,0.7165988,0.78492293,0.86624213,0.94071066,
X1.0257787,1.118885,1.2221354,1.3385186,1.4725188,1.6312598,
X1.8271452,2.0844432,2.4887964,3.497654,0.10176025,C.196785,
XC.26520225,0.32682625,C.3842565,0.43967925,0.49512475,0.545537,
X0.6059465,0.659715,0.717307,C.7769E,C.83920475,C.90493675,
X0.97467075,1.049486,1.1306795,1.2199627,1.319785,1.4337535,
X1.567579,1.7310672,1.9425085,2.205085,3.089838/
WRITE(NOUTP,9000)
9000 FORMAT(1H0/1HC/' PROGRAMM KENNZIFFER 2')
WRITE(NOUTP,9001)
9001 FORMAT(' PROGRAMM ZUR BERECHNUNG VON RESONANZSELESTABSCHIRMFAKTORE
1N VON STATISTISCHEN RESONANZPARAMETERN/')
IYDIM=199
IYDIM1=0
ISS=ISPA
NLS=0
NLS1=0
NEFE=NFE
IF(NFE.EQ.1) NEFE=C
ISIG=0
IF(SIGO(MI).GE.1.F6) GO TO 260
MI=MI+1
SICO(MI)=1.E6
ISIG=1

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260	CALL DOPW (8HFSTAT ,MM)	460	IX(3)=NN(5)	1010
	CALL DOPW (8HBEST ,NN(1))	470	IY=1	1020
	CALL DOPW (8HISOT1 ,NN(2))	480	KI=1	1030
	CALL DOPW (8HISOT2 ,NN(3))	490	CALL NDFLOC(KONTR,NAME,X,NUDAT,IS)	1040
	CALL DOPW (8HST ,NN(4))	500	IF(KONTR)128,128,74	1050
	CALL DOPW (8HSTGF ,NN(5))	510	ISPA1=0	1060
	I=0	520	IF(ISPA.NE.ISPA1) GO TO 132	1070
	WRITE (LIZ)I,MM	530	GC TO 201	1080
	NGR=J-NANF	540	ISPA=ISPA1	1090
	NEN=J+1-NEND	550	C WRITE(NOUTP,9006) MAT,ISPA	1100
	IX(1)=MAT	560	C9006 FORMAT(/' FOR MATERIAL ',A8,' THE DATA TYPE STGF IS NOT AVAILABLE	1110
	IX(2)=NN(1)	570	C 1CA THE NUCLEAR DATA LIBRARY.ISPA IS SET ',I4,' INTERNALLY')	1120
	IX(3)=NN(2)	580	GC TO 201	1130
	NAME(1)=3	590	74 ISPA1=1	1140
	CALL NDFLOC (KONTR,NAME,X,NUDAT,IS)	600	IF(ISPA.NE.ISPA1) GC TC 129	1150
	IF(KONTR)51,51,62	610	GO TO 131	1160
51	WRITE(NOUTP,153)KONTR	620	129 ISPA=ISPA1	1170
153	FORMAT(1H0,3X,7HKONTR =13)	630	C WRITE(NOUTP,9007) MAT,ISPA	1180
	GC TO 1000	640	C9007 FORMAT(/' FOR MATERIAL ',A8,'THE DATA TYPE STGF IS AVAILABLE ON TH	1190
62	DEL=344.489/X(4)	650	C IF NUCLEAR DATA LIBRARY.ISPA IS SET',I4,' INTERNALLY')	1200
	SPIN=DABS(X(6))	660	131 IF(X(4).LT.ENG(NGR+1)) GO TO 75	1210
	IX(3)=NN(3)	670	WRITE(NOUTP,9002)ENG(NGR),ENG(NGR+1)	1220
	CALL NDFLOC (KONTR,NAME,X,NUDAT,IS)	680	9002 FORMAT(1H0,37H***ERROR 2.02 : THE ENERGY GROUP FROM,E16.8,6H EV TC	1230
	IF(KONTR)51,51,63	690	1,E16.8,22H EV IS NOT POSSIBLE IN/15X,67HTHIS MCDLLE,BECAUSE NG STA	1240
63	XA=X(4)*X(4)	700	2TISTICAL INFORMATION IS AVAILABLE IN THIS/19X,21HENERGYRANGE ON KE	1250
	RQU=X(5)*X(5)	710	3CAK.)	1260
	EPI=X(6)	720	NGR=NGR+1	1270
	IX(3)=NN(4)	730	IF(NGR-NEN)131,1000,1000	1280
	IT=1	740	75 IF(X(4).LE.ENG(NGR)) GO TO 76	1290
	CALL NDFLOC (KONTR,NAME,X,NUDAT,IS)	750	IF ((IY+1).LE.IYDIM) GC TO 72	1300
	IF(KONTR)51,51,28	760	IYDIM=1	1310
28	IF(X(4) -5.E-5.LE.1.) GO TC 3000	770	GC TC 79	1320
	WRITE (NOUTP,9004)	780	72 EY(IY)=ENG(NGR)	1330
9004	FORMAT(/' ***WARNING 2.07 : CONTRIBUTIONS,THAT CORRESPOND TO L.GT	790	GF(KI,IY)=X(8)*1.E3	1340
	1.1 (L=ANGULAR MOMENTUM) ARE NEGLECTED')	800	EY(IY+1)=X(4)	1350
	NLS=NLS+1	810	CF(KI,IY+1)=X(8)*1.F3	1360
	NLS1=NLS	820	78 KI=KI+1	1370
	IT=IT-1	830	IF(KI.GT.IT.AND.NLS.EQ.0) GO TO 92	1380
	GC TC 3005	840	IF(KI.GT.IT) GC TC 81	1390
3000	XL(IT)=IX(4)	850	CALL NDFNXT(KONTR,NAME,X,NUDAT,IS)	1400
	GG(IT)=X(6)*1.E3	860	IF(KONTR)201,201,131	1410
	DN(IT)=X(7)*1.E3	870	81 CALL NDFNXT(KONTR,NAME,X,NUDAT,IS)	1420
	GN(IT)=X(8)*1.E3	880	IF(KONTR) 201,201,77	1430
	GI(IT)=(2.*X(5)+1.)/(4.*SPIN+2.)	890	77 NLS=NLS-1	1440
	FXNYN(IT)=IX(10)*1.0001	900	GC TO 78	1450
	XNYN(IT)=IX(11)*1.0001	910	92 KI=1	1460
3005	CALL NDFNXT(KONTR,NAME,X,NUDAT,IS)	920	IY=IY+1	1470
	IF(KONTR)3006,3006,66	930	IF (IY.GT.IYDIM) IYDIM=1	1480
66	IT=IT+1	940	NEY=IY-1	1490
	GC TO 28	950	NLS=NLS1	1500
3006	WRITE(NOUTP,9005) IT	960	79 CALL NDFNXT(KONTR,NAME,X,NUDAT,IS)	1510
9005	FORMAT(' NUMBER OF SERIES,TAKEN INTO ACCOUNT IS IT=*,16)	970	IF(KONTR)201,201,91	1520
404	NAME(1)=3	980	76 IF (IY.LT.IYDIM) GO TO 205	1530
	IX(1)=MAT	990	IYDIM=1	1540
	IX(2)=NN(1)	1000	GC TO 78	1550


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205 EY(IY)=X(4) 1560
GF(KI,IY)=X(8)+1.E3 1570
GC TO 78 1580
51 IF (IYDIM1.EQ.1) GO TO 71 1590
EY(IY)=X(4) 1600
GF(KI,IY)=X(8)+1.E3 1610
71 KI=KI+1 1620
IF(KI.GT.IT.AND.NLS.EQ.0) GO TO 92 1630
IF(KI.GT.IT) GO TO 81 1640
GO TO 79 1650
201 IF(IYDIM1.EQ.1) GO TO 202 1660
GO TO 204 1670
202 WRITE(NOUTP,9003) IYDIM,IY 1680
9003 FORMAT(' &&&&&IYDIM TCC SMALL,IYDIM=',I6,' ACTUAL DIMENSION OF EY 1690
IIS IY=',I6) 1700
GC TO 1000 1710
204 DO 7 I=1,MT 1720
TT=TEMP(I) 1730
IF(TT.EQ.0) GC TO 700 1740
K=NGR-1 1750
N=1 1760
IF(K+1-NEN)4,1000,1000 1770
4 K=K+1 1780
E(N)=ENG(K) 1790
16 IF(N.NE.1) GO TO 21 1800
INEXT=1 1810
NEXTGR=0 1820
ENEXT=E(N) 1830
SSSSNE=0. 1840
21 CCNTINUE 1850
CALL QUER(E(N),TT,N,SE ,SM ,XNYN,FXNYN,DEL,RQU,CHI, 1860
1DA,EBI,XA,XL,GN,GG,NEY,EY,GF,GI,IT,MI,SIGC,NEXTGR,ENEXT,INEXT, 1870
ZSSSSNE) 1880
GC TO (23,24,25),N 1890
23 IF(K+1-NEN)6,6,7 1900
6 IF(ISPA.EQ.0) GO TO 40C0 1910
IF(EY(NEY).LT.ENG(K+1)) GO TO 7 1920
40CC N=2 1930
E(N)=(ENG(K)+ENG(K+1))*C.5 1940
GC TO 16 1950
24 N=3 1960
GC TO 4 1970
25 LIJ=5 1980
IF(NEFE)300,301,300 1990
301 DC 1 IST=1,3 2000
1 EF(IST)=PHI(E(IST)) 2010
GC TO 27 2020
300 L=2 2030
DO 5 IST=1,3 2040
DC 12 KK=L,NEFE 2050
IF(REFE(KK)-E(IST))12,36,213 2060
12 CCNTINUE 2070
KK=NEFE 2080
213 EF(IST)=EFE(KK-1)+(EFE(KK)-EFE(KK-1))/(REFE(KK)-REFE(KK-1))*E(IST 2090
1)-REFE(KK-1)) 2100

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GC TO 26 2110
28 EF(IST)=EFE(KK) 2120
26 L=KK 2130
5 CCNTINUE 2140
27 F=(E(3)-E(2))*3.333333E-1 2150
DC 29 KI=1,MI 2160
DC 29 IS=1,LIJ 2170
IF(SE(1,IS,KI).NE.-99999..AND.SE(2,IS,KI).NE.-99999..AND.SE(3,IS, 2180
KI).NE.-99999.) GO TO 2000 2190
XEUGZ(IS,KI)=-99999. 2200
GO TO 29 2210
2000 XEUGZ(IS,KI)=H*(SE(1,IS,KI)*EF(1)+4.*SE(2,IS,KI)*EF(2)+SE(3,IS,KI) 2220
1*EF(3)) 2230
29 CCNTINUE 2240
DC 30 IS=1,LIJ 2250
C WRITE(NOUTP,5000) IS,SM(1,IS,1),SM(2,IS,1),SM(3,IS,1) 2260
IF(SM(1,IS,1).NE.-99999..AND.SM(2,IS,1).NE.-99999..AND.SM(3,IS,1) 2270
1.NE.-99999.) GO TO 2001 2280
SU(IS)=-99999. 2290
GO TO 2002 2300
20C1 SU(IS)=H*(SM(1,IS,1)*EF(1)+4.*SM(2,IS,1)*EF(2)+SM(3,IS,1)*EF(3)) 2310
2002 IF(SE(1,IS,MI).NE.-99999..AND.SE(2,IS,MI).NE.-99999..AND.SE(3,IS, 2320
MI).NE.-99999.) GO TO 2004 2330
XSUGI(IS)=-99999. 2340
GO TO 30 2350
2004 XSUGI(IS)=H*(SE(1,IS,MI)*EF(1)+4.*SE(2,IS,MI)*EF(2)+SE(3,IS,MI)*EF 2360
1(3)) 2370
30 CONTINUE 2380
XNE=H*(EF(1)+4.*EF(2)+EF(3)) 2390
DO 32 KI=1,MI 2400
DC 32 IS=1,LIJ 2410
IF(XEUGZ(IS,KI).NE.-99999..AND.XSUGI(IS).NE.-99999.) GO TO 2003 2420
XEUGZ(IS,KI)=-99999. 2430
GC TO 32 2440
20C3 XEUGZ(IS,KI)=XEUGZ(IS,KI)/XSUGI(IS) 2450
32 CONTINUE 2460
DC 31 IS=1,LIJ 2470
IF(SU(IS).EQ.-99999.) GO TO 31 2480
SL(IS)=SU(IS)/XNE 2490
31 CONTINUE 2500
KI=K-1 2510
IS=J-KI 2520
WRITE(NOUTP,130) MAT ,TT,IS,ENG(KI),ENG(K) 2530
130 FORMAT(1H0,16X,8HMATERIAL,2X,10HTEMPERATUR,2X,6FGRUPPE,8X,7HGRFNZE 2540
1N/1H ,16X,A9,1X,F8.2,5X,I3,2E12.4) 2550
IA=6 2560
WRITE(LI2)IN,MAT ,TT,KI,ENG(KI),ENG(K) 2570
WRITE(NOUTP,37)(SU(IS),IS=1,LIJ) 2580
37 FORMAT(1H0,20X,7HSIGMA G,9X,7HSIGMA N,9X,7HSIGMA F,9X,7HSIGMAN1, 2590
19X,7HSIGMAT1/1H ,14X,5E16.8) 2600
IA=LIJ 2610
WRITE(LI2)IN,(SU(IS),IS=1,LIJ) 2620
WRITE(NOUTP,138) 2630
138 FORMAT(1H0,5X,7HSIGMA 0,11X,2HFG,14X,2HFN,14X,2HFF,14X,3HFN1,13X, 2640
13HFT1/1X) 2650

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B 32

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DC 139 KK=1,MI 2660
WRITE(NOUTP,36)SIGO(KK),(XEUGZ(IS,KK),IS=1,LIJ) 2670
36 FCFMAT(1X,E15.8,5E16.8) 2680
IN=LIJ+1 2690
139 WRITE(LIZ)IN,SIGO(KK),(XEUGZ(IS,KK),IS=1,LIJ) 2700
40 DC 70 KK=1,MI 2710
DO 70 IN=1,LIJ 2720
SE(1,IN,KK)=SE(3,IN,KK) 2730
70 SM(1,IN,KK)=SM(3,IN,KK) 2740
E(1)=E(3) 2750
GC TO 23 2760
7CC WRITE(NOUTP,701) 2770
701 FCFMAT(1H0,93H***ERROR 2.03 : A CALCULATION OF RESONANCE SELF SHIE 278C
LDING FACTORS AT ZERO TEMPERATURE (DEGREE/17X,39KELVIN) IS NOT PO 2790
SSIBLE IN THIS MODULE,) 2800
7 CCNTINUE 2810
1000 IF(ISIG.EQ.1) MI=MI-1 2820
BACKSPACE LIZ 2830
READ(LIZ) I,NN(1) 2840
IF(I.EQ.0.AND.NN(1).EQ.MM) BACKSPACE LIZ 2850
KL=KL+1 2860
ISPA=ISS 2870
RETURN 2880
END 2890

SLBROUTINE QUER (E,TT,A,SE,SM,XNYN,FXNY,CFL,RQU,CHI, DN,ERI,XA, 10
IXL,GN,GG,NEY,EY,GFA,GI,IT,MI,SIGO,NEXTGR,FNEXT,INEXT,SSSSNE) 20
REAL*8 MAT 30
DIMENSION SIGC(MI),A(5),B(5),ACI(10), 40
IPH(10),AC(10),GFF(25),TERM(5),CHI(25,4),XNYN(10),FXNY(10),GNN(25), 50
ZSE(3,5,MI),SM(3,5,MI),DN(10),XL(10),GN(10),GG(10),EY(199), 60
ZGFA(10,199),GI(10) 70
COMMON MAT,ISTRUK,ISPA,NOUTP,LIZ,NANF,NEND,KL 80
TEST=0.0 90
C=0.5 100
DC 25 K=1,MI 110
SE(N,1,K)=0. 120
SF(N,2,K)=12.566371*RQU 130
IF(ISPA .EQ.1) GO TO 41 140
SE(N,3,K)=1. 150
GC TO 40 160
41 SE(N,3,K)=0. 170
40 SF(N,4,K)=SE(N,2,K) 180
SE(N,5,K)=SE(N,2,K) 190
SM(N,1,K)=0. 200
SM(N,2,K)=SE(N,2,K) 210
SM(N,3,K)=0. 220
SM(N,4,K)=SE(N,2,K) 230
SM(N,5,K)=SE(N,2,K) 240
ST=0. 250
DC I I=1,IT 260
AC(I)=SIGC(E,I,XA,GI,DN,ERI,GN,RQU,XL) 270

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PH(I)=PHASE(E,I,XA,RQU,XL) 280
ACI(I)=AC(I)*PH(I) 290
1 ST=ST+ACI(I) 300
ST=ST+SIGO(K)+SE(N,2,K) 310
CO 2 I=1,IT 320
ISE=0 330
IJ=1 340
KJ=3 350
CALL EZZ(E,I,FZG,EZC,EZF,DRSG,DRFS, CHI,XNYN,FXNY,GN,RQU,XL,XA, 36C
IGG,NEY,EY,GFA) 370
C=CMIT(E,I,DN,ERI) 380
DL=DELTA(E,TT,I,DEL) 390
A(1)=AC(1)*DRSG 400
G=GAMMIE,I,GN,RQU,XL,XA)+GAMG(F,I,GG)+GAFM(E,I,NEY,EY,GFA) 41C
IF(G/DL-C)22,22,922 420

522 TETA=G/DL 430
WRITE(NOUTP,923)TETA,I,TT,E 440
923 FCFMAT(1H0,31H***WARNING 2.04 : GAMMA/CFLTA =,E14.6,11F FOR SERIES 450
1,I,3,19H AT THE TEMPERATURE,E14.6/19X,31HDEGREE KELVIN,AND AT THE F 460
2ENERGY,E14.6,4F EV.) 470
22 XY=D*ACI(I)*EPSI(E,TT,I,DN,ERI,DEL)/(2.506628*E1*ST**2) 480
SPI=ST 490
SSS=ST-ACI(I) 500
SSSS=-2.*SSS+SIGO(K) 510
IF((ST-ACI(I)).GT.0) GO TO 31 520
GO TO 30 530
31 IF(N.EQ.3.AND.K.EQ.1.AND.ISE.EQ.1.AND.I.EQ.INEXT) NEXTGR=0 540
IF(NEXTGR.EQ.1) GO TO 33 550
GO TO 23 560
33 IF(N.EQ.2.AND.NEXTGR.EQ.1.AND.K.EQ.1) GO TO 32 570
GO TO 23 580
32 WRITE(NOUTP,43) ENEXT,SSSSNE 590
43 FCFMAT(/////' ***WARNING 2.05 : THE THEORY APPLIED FOR THE CALCULA 600
TION OF THE CURRENT WEIGHTED SELF-SHIELDING FACTORS IS NOT VALID'/ 610
2' ***FOR ALL VALUES OF SIGO AT ENERGY',E12.5,'EV.AT THIS ENERGY SI 620
3GC HAS TO BE GREATER THAN',E12.5,'.'/' ***FOR MORE DETAILED INFORM 630
4ATION COMPARE WARNING 2.05 FOR THE ENERGY GROUP,CALCULATED BEFORE. 640
5') 650
NEXTGR=0 660
SSSSNE=0. 670
GO TO 23 680
C DC 26 L=IJ,5 690
C SE(N,L,K)=-99999. 700
C 26 SM(N,L,K)=-99999. 710
30 WRITE(NOUTP,42)SIGO(K),I,SSS,E,SSSS 720
42 FORMAT(/' ***WARNING 2.05 : CONCERNS CALCULATION OF **FNI** AND ** 730
1FTI**,FOR SIGO=',E12.5,'SPEFF* IS NEGATIVE IN THE SRITES',I4/' *** 740
2SPFF**=',E12.5,'AT ENERGY',E12.5,'EV.'/' ***ACCORDING TO KFK 1784, 750
3APPENDIX II,FORMULA 25, THE THEORY DEVELOPED THERE IS NOT VALID IN 760
4 THIS CASE.'/' ***AT THIS ENERGY AND IN THIS SERIES THE THEORY IS 770
5VALID FOR SIGO GREATER THAN',E12.5) 780
IF(N.EQ.3.AND.K.EQ.1) GO TO 28 790
GC TO 23 800
28 NEXTGR=1 810
FNEXT=E 820

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- B 33 -

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SSSSNE=AMAX1(SSSS,SSSSNE)
INEXT=1
C GC TC 25
23 A(3)=0.
B(3)=0.
AA=0.398942*ACI(I)*C*EZC/(DL*SPI)
C WRITE (NOUTP,500) AA
500 FCRMAT (' AA=',E14.6)
IF(AA-TEST)3,3,4
3 BT=(1.-AA)*D*ACI(I)/SPI
B(1)=(1.-AA*EZG/EZC)*D*A(1)/SPI
IF(ISPA )5,5,6
6 A(3)=AC(I)*DRFS
B(3)=(1.-AA*EZF/EZC)*D*A(3)/SPI
5 A(2)=ACI(I)-A(3)-A(1)
B(2)=BT-B(1)-B(3)
C IF(ISE.EQ.0) GO TO 2000
C QF=1.+ACI(I)/(SPI+ACI(I))
C GO TO 2001
2000 QF=1.+ACI(I)/SPI
2001 BT=QF*BT
B(1)=QF*B(1)
B(2)=QF*B(2)
B(3)=QF*B(3)
IF(ISE.EQ.0) GO TO 27
A(4)=A(2)
A(5)=ACI(I)
B(4)=B(2)
B(5)=BT
27 XNEN=1./(1.-BT/D+XY*ACI(I))
IF(XNEN.GT.0) GO TO 202
WRITE (NOUTP,203)
203 FCRMAT(1H0,52H***WARNING 2.06 : INACCURATE OVERLAPPING CCRRECTION.
1)
202 CONTINUE
DC 57 L=I,J,KJ
TERM(L)=(ST-ACI(I))*XNEN*(B(L)/D-XY*A(L))
SE(N,L,K)=SE(N,L,K)+TERM(L)
7 SM(N,L,K)=SM(N,L,K)+A(L)
57 CONTINUE
GC TO 20
4 GO=GAMN(E,I,GN,RQU,XL,XA)
CI=SPI*GO*1.5707963/(ACI(I)*D)
IF(ISPA )8,8,9
8 CF=0.
NF=1
NN=25
CFF(1)=0.
NL=XNYN(I)
CN 10 M=1,NN
10 GNN(M)=GO*CHI(M,NU)
11 CAX=GAMG(E,I,GG)
BT=0.
B(1)=0.
B(2)=0.

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LC=1
CC 12 M=1,NN
GAX=GNN(M)
DO 12 NI=1,NF
GFX=GFF(NI)
GTX=GAX+GNX+GFX
XK=1.442695*ALOG(1.E5*C*I*GTX/GNX)
XT=GTX/DL
CALL FSP IE
CALL TAB (XT,XK,LG,DSJ,XABCJ,DJK)
CALL FSPI E
C WRITE(NOUTP,1000) XT,XK,XABCJ
1000 FCRMAT(' XT=',G16.8,'XK=',G16.8,'XABCJ=',G16.8)
B(3)=B(3)+GFX*XABCJ
B(1)=B(1)+XABCJ
12 BT=BT+GTX*XABCJ
AZ=NN
BZ=NF
FK=AZ*BZ
B(1)=B(1)*GAX/(PH(I)*FK)
B(3)=B(3)/(PH(I)*FK)
BT=BT/FK
GC TO 5
9 NL=XNYN(I)
A(3)=AC(I)*DRFS
NA=25
NF=25
DC 200 M=1,NN
200 GNN(M)=GO*CHI(M,NU)
GF=GAFM(F,I,NEY,EY,GFA)
NL=FXNY(I)
DC 201 M=1,NF
201 GFF(M)=GF*CHI(M,NU)
GC TO 11
20 IF(ISE.EQ.1) GO TO 21
ISE=1
FT=ST
ST=ST*0.5
IJ=4
KJ=5
GC TO 22
21 ST=FT
2 CCNT INUE
25 CCNT INUE
RETURN
ENC

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SUBROUTINE TAB(XT,XK,LG,DSJ,XABCJ,DJK)
DIMENSION XXX(20),XXT(33),XJ(660)
C DIMENSION T01(20),T02(20),T03(20),T04(20),T05(20),T06(20),T07(20),
1TC8(20),T09(20),T10(20),T11(20),T12(20),T13(20),T14(20),T15(20),
2T16(20),T17(20),T18(20),T19(20),T20(20),T21(20),T22(20),T23(20),

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2T24(20), T25(20), T26(20), T27(20), T28(20), T29(20), T30(20), T31(20), 60
 4T32(20), T33(20) 70
 EQUIVALENCE (XXX(1),R), (XXT(1),T), (XJ(1),U), 80
 1 (A,C,V), (B,D,Y), (E,H,P), (F,G,Q), (R,S,T), (U,V,W), (X,Y,Z), (AA,AB,AC,AD,AE,AF,AG,AH,AI, 90
 2(T4,Y6,XK06,J), (OK,R1), (XK1,SJ0), (XK2,SJ1), (OKA,R1,V1), (CKB,R2,V2) 100
 3, (CKC,R3,V3), (SV,N), (AB1,TD,M), (AB2,AXC), (SY1,XXT,S1), 110
 4(XK02,XJA2,S2), (XKM,XKC3,XJA3,S3), (XK04,XJB1), (RIK,XJB2), 120
 5(R2K,XJB3), (R3K,XJC1), (BETA,XJC3), (K,S,G,SJ3), (Y2,ZZK,XJ1), (Y3, 130
 EWG), (XJ3,Y4), (SY,I), (XJC2,SJ2), (XJA1,SJ4) 140
 EQUIVALENCE (XJ(1),T01(1)), (XJ(21),TC2(1)), (XJ(41),T03(1)), 150
 1(XJ(61),T04(1)), (XJ(81),T05(1)), (XJ(101),T06(1)), (XJ(121),T07(1)), 160
 2(XJ(141),T08(1)), (XJ(161),T09(1)), (XJ(181),T10(1)), (XJ(201),T11(1)) 170
 3), (XJ(221),T12(1)), (XJ(241),T13(1)), (XJ(261),T14(1)), (XJ(281),T15(180
 41)), (XJ(301),T16(1)), (XJ(321),T17(1)), (XJ(341),T18(1)), (XJ(361),T1 190
 59(1)), (XJ(381),T20(1)), (XJ(401),T21(1)), (XJ(421),T22(1)), 200
 6(XJ(441),T23(1)), (XJ(461),T24(1)), (XJ(481),T25(1)), (XJ(501),T26(1) 210
 7), (XJ(521),T27(1)), (XJ(541),T28(1)), (XJ(561),T29(1)), (XJ(581),T30(220
 E1)), (XJ(601),T31(1)), (XJ(621),T32(1)), (XJ(641),T33(1)) 230
 DATA XXX/ 5.2, 5.6, 6.0, 6.4, 6.8, 7.2, 7.6, 8.0, 8.4, 8.8, 9.2, 240
 X 5.6,10.0,10.4,11.2,11.6,12.0,12.4,12.8/ 250
 DATA XXT/0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,0.11, 260
 X0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20,0.26,0.32,0.38,0.44, 270
 X0.50,0.56,0.62,0.68,0.74,0.80,0.86,0.92,0.98/ 280
 DATA T01/348.3270,329.0620,309.3460,289.0880,266.2430,246.8240, 290
 X224.91800,202.69300,180.40300,158.38700,137.04200,116.78800, 300
 X 98.01930, 81.05280, 66.09140, 53.20820, 42.35540, 33.39130, 310
 X 26.11050, 20.28100/ 320
 DATA T02/205.0000,154.1000,183.5000,173.0000,162.5000,151.9000, 330
 X141.20000,130.20000,119.10000,107.80000, 96.43000, 85.17000, 340
 X 74.17000, 63.64000, 53.78000, 44.78000, 36.74000, 29.75000, 350
 X 23.80000, 18.85000/ 360
 DATA T03/154.4000,145.3000,136.9000,128.9000,121.2000,113.7000, 370
 X106.30000, 98.80000, 91.28000, 83.67000, 75.99000, 68.28000, 380
 X 60.61000, 53.09000, 45.83000, 38.98000, 32.65000, 26.95000, 390
 X 21.95000, 17.65000/ 400
 DATA T04/129.5430,120.8780,113.1000,105.9960, 95.3851, 93.1199, 410
 X 87.07990, 81.16910, 75.31440, 69.46550, 63.59470, 57.69990, 420
 X 51.80430, 45.95800, 40.23460, 34.72510, 29.52740, 24.73430, 430
 X 20.41850, 16.62540/ 440
 DATA T05/115.3000,106.6000, 99.0000, 92.2100, 86.0500, 80.3700, 450
 X 75.03000, 69.93000, 64.97000, 60.10000, 55.26000, 50.43000, 460
 X 45.60000, 40.81000, 36.08000, 31.47000, 27.06000, 22.93000, 470
 X 19.14000, 15.75000/ 480
 DATA T06/106.4000, 97.5700, 89.9000, 83.1800, 77.2000, 71.8000, 490
 X 66.84000, 62.19000, 57.76000, 53.47000, 49.27000, 45.13000, 500
 X 41.03000, 36.91000, 32.86000, 28.89000, 25.06000, 21.43000, 510
 X 18.05000, 14.98000/ 520
 DATA T07/100.5080, 91.4730, 83.6900, 76.9337, 71.0030, 65.7266, 530
 X 60.95750, 56.57200, 52.46730, 48.56010, 44.78500, 41.09360, 540
 X 37.45480, 33.85470, 30.29690, 26.80240, 23.40750, 20.15950, 550
 X 17.11060, 14.31330/ 560
 DATA T08/ 96.4200, 87.1900, 79.2700, 72.4300, 66.4800, 61.2400, 570
 X 56.58000, 52.35000, 48.45000, 44.79000, 41.30000, 37.93000, 580
 X 34.64000, 31.40000, 28.21000, 25.07000, 22.02000, 19.08000, 590
 X 16.29000, 13.72000/ 600

DATA T09/ 93.4500, 84.0500, 76.0200, 69.0800, 63.0800, 57.8400, 610
 X 53.22000, 49.07000, 45.30000, 41.82000, 38.53000, 35.39000, 620
 X 32.36000, 29.39000, 26.48000, 23.62000, 20.83000, 18.14000, 630
 X 15.58000, 13.19000/ 640
 DATA T10/ 91.3415, 81.7729, 73.5745, 66.5357, 60.4667, 55.1985, 650
 X 50.58150, 46.48530, 42.79780, 39.42410, 36.28530, 33.31770, 660
 X 30.47200, 27.71280, 25.01900, 22.38310, 19.81150, 17.32270, 670
 X 14.94500, 12.71180/ 680
 DATA T11/ 89.7100, 80.0100, 71.6500, 64.5600, 58.4200, 53.1100, 690
 X 48.48000, 44.40000, 40.76000, 37.47000, 34.43000, 31.59000, 700
 X 28.89000, 26.30000, 23.78000, 21.32000, 18.92000, 16.60000, 710
 X 14.30000, 12.28000/ 720
 DATA T12/ 88.4600, 78.6400, 70.2200, 62.9900, 56.7800, 51.4200, 730
 X 46.77000, 42.70000, 39.09000, 35.84000, 32.88000, 30.14000, 740
 X 27.55000, 25.09000, 22.70000, 20.39000, 18.14000, 15.97000, 750
 X 13.88000, 11.90000/ 760
 DATA T13/ 87.4785, 77.5623, 69.0480, 61.7399, 55.4611, 50.0523, 770
 X 45.37000, 41.28650, 37.68900, 34.47960, 31.57410, 28.90220, 780
 X 26.40610, 24.04060, 21.77230, 19.58010, 17.45450, 15.39730, 790
 X 13.42070, 11.54430/ 800
 DATA T14/ 86.7000, 76.7000, 68.1000, 60.7200, 54.3800, 48.9200, 810
 X 44.21000, 40.11000, 36.51000, 33.32000, 30.46000, 27.84000, 820
 X 25.41000, 23.13000, 20.96000, 18.86000, 16.84000, 14.89000, 830
 X 13.01000, 11.22000/ 840
 DATA T15/ 86.0600, 75.9500, 67.3300, 59.8900, 53.4900, 47.9800, 850
 X 43.23000, 39.11000, 35.51000, 32.34000, 29.49000, 26.92000, 860
 X 24.55000, 22.33000, 20.24000, 18.23000, 16.29000, 14.43000, 870
 X 12.64000, 10.93000/ 880
 DATA T16/ 85.5500, 75.4200, 66.6900, 59.1900, 52.7400, 47.1900, 890
 X 42.41000, 38.26000, 34.66000, 31.48000, 28.66000, 26.12000, 900
 X 23.79000, 21.63000, 19.60000, 17.66000, 15.80000, 14.01000, 910
 X 12.29000, 10.66000/ 920
 DATA T17/ 85.1184, 74.9383, 66.1636, 58.6102, 52.1123, 46.5214, 930
 X 41.70360, 37.53840, 33.91760, 30.74480, 27.93540, 25.41610, 940
 X 23.12450, 21.00880, 19.02780, 17.15060, 15.35620, 13.63380, 950
 X 11.98190, 10.40740/ 960
 DATA T18/ 84.7600, 74.5400, 65.7200, 58.1200, 51.5800, 45.9500, 970
 X 41.10000, 36.91000, 33.28000, 30.10000, 27.30000, 24.80000, 980
 X 22.53000, 20.45000, 18.52000, 16.69000, 14.95000, 13.29000, 990
 X 11.70000, 10.18000/ 1000
 DATA T19/ 84.4600, 74.2000, 65.3400, 57.7000, 51.1200, 45.4600, 1010
 X 40.58000, 36.37000, 32.72000, 29.53000, 26.73000, 24.25000, 1020
 X 22.00000, 19.96000, 18.06000, 16.28000, 14.59000, 12.97000, 1030
 X 11.43000, 9.96300/ 1040
 DATA T20/ 84.2023, 73.5074, 65.0142, 57.3417, 50.7292, 45.0336, 1050
 X 40.12650, 35.89180, 32.22580, 29.03470, 26.23560, 23.75540, 1060
 X 21.53060, 19.50740, 17.64160, 15.89810, 14.25100, 12.68360, 1070
 X 11.18790, 9.76410/ 1080
 DATA T21/ 83.2433, 72.8209, 63.7912, 55.9766, 49.2205, 43.3851, 1090
 X 38.34820, 34.00070, 30.24480, 26.99280, 24.16570, 21.69310, 1100
 X 19.51260, 17.56960, 15.81730, 14.21660, 12.73650, 11.35310, 1110
 X 10.05070, 8.82059/ 1120
 DATA T22/ 82.7808, 72.2943, 63.1548, 55.3048, 48.4693, 42.5527, 1130
 X 37.43530, 33.01150, 29.18750, 25.87920, 23.01150, 20.51690, 1140
 X 18.33520, 16.41300, 14.70340, 13.16620, 11.76780, 10.48140, 1150

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X 9.28662, 8.16990/
DATA T23/ 82.5236, 72.0012, 62.8617, 54.9281, 48.0456, 42.0794,
X 36.91170, 32.43670, 28.56450, 25.21300, 22.30550, 19.78900,
X 17.59340, 15.67080, 13.97510, 12.46640, 11.11010, 9.87782,
X 8.74691, 7.70062/
DATA T24/ 82.3662, 71.8216, 62.6574, 54.6965, 47.7842, 41.7860,
X 36.58420, 32.07560, 28.16950, 24.78600, 21.85410, 19.31000,
X 17.09880, 15.16850, 13.47470, 11.97790, 10.64360, 9.44274,
X 8.35127, 7.35063/
DATA T25/ 82.2628, 71.7037, 62.5233, 54.5442, 47.6121, 41.5923,
X 36.36750, 31.83500, 27.90470, 24.49750, 21.54360, 18.98080,
X 16.75420, 14.81430, 13.11730, 11.62440, 10.30150, 9.11911,
X 8.05277, 7.08266/
DATA T26/ 82.1914, 71.6222, 62.4304, 54.4388, 47.4928, 41.4579,
X 36.21670, 31.66690, 27.71890, 24.29400, 21.32300, 18.74490,
X 16.50530, 14.55600, 12.85400, 11.36100, 10.04260, 8.87225,
X 7.82223, 6.87307/
DATA T27/ 82.1399, 71.5634, 62.3636, 54.3629, 47.4068, 41.3608,
X 36.10770, 31.54510, 27.58380, 24.14540, 21.16120, 18.57060,
X 16.32020, 14.36230, 12.65480, 11.16000, 9.84471, 8.67993,
X 7.64071, 6.70620/
DATA T28/ 82.1016, 71.5197, 62.3138, 54.3063, 47.3427, 41.2885,
X 36.02630, 31.45410, 27.48250, 24.03370, 21.03500, 18.43850,
X 16.17910, 14.21370, 12.50080, 11.00330, 9.68843, 8.52743,
X 7.49539, 6.57129/
DATA T29/ 82.0723, 71.4863, 62.2758, 54.2621, 47.2937, 41.2331,
X 35.96400, 31.38430, 27.40480, 23.54770, 20.94470, 18.33610,
X 16.06920, 14.09740, 12.37950, 10.87900, 9.56256, 8.40460,
X 7.37737, 6.46077/
DATA T30/ 82.0494, 71.4602, 62.2461, 54.2253, 47.2554, 41.1898,
X 35.91530, 31.32960, 27.34380, 23.88010, 20.87040, 18.25520,
X 15.98200, 14.00470, 12.28240, 10.77890, 9.46232, 8.30433,
X 7.28033, 6.36520/
DATA T31/ 82.0311, 71.4394, 62.2224, 54.2024, 47.2249, 41.1553,
X 35.87640, 31.28600, 27.29510, 23.82600, 20.81000, 18.19010,
X 15.91170, 13.92570, 12.20340, 10.69720, 9.37521, 8.22151,
X 7.19965, 6.29253/
DATA T32/ 82.0164, 71.4226, 62.2032, 54.1806, 47.2002, 41.1274,
X 35.84490, 31.25060, 27.25560, 23.78210, 20.76240, 18.13710,
X 15.85430, 13.86820, 12.13850, 10.62960, 9.31019, 8.15236,
X 7.13192, 6.22775/
DATA T33/ 82.0042, 71.4088, 62.1875, 54.1628, 47.1800, 41.1045,
X 35.81900, 31.22160, 27.22310, 23.74590, 20.72250, 18.09340,
X 15.80680, 13.81720, 12.08440, 10.57320, 9.25227, 8.09408,
X 7.07449, 6.17256/
N=20
M=33
DO 1 IR=1,N
I=IB
IF(XK-XXX(I))2,3,1
1 CCNT INUE
3 IF(I-2)9,33,23
23 IF(I-N+1)33,33,9
33 XXXK=XK
GC TO 12

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2 IF(I-2)9, 5,24
24 IF(I-N+1)32,32,9
32 A=ABS(XK-XXX(I))
B=XK-XXX(I-1)
IF(B-A)4,4,5
4 XXXK=XXX(I-1)
I=I-1
GC TO 12
5 XXXK=XXX(I)
12 IF(XT-XXT(M-1))499,499,9
499 CC 6 JB=1,M
J=JB
IF(XT-XXT(JB))7,8,6
6 CCNT INUE
8 IF(J-2)9,18,28
28 IF(J-M+1)18,18,9
18 XXXT=XT
GC TO 13
7 IF(J-2)9,11,29
29 IF(J-M+1)17,17,9
17 C=ABS(XT-XXT(J))
D=XT-XXT(J-1)
IF(D-C)10,10,11
10 XXXT=XXT(J-1)
J=J-1
GC TO 13
11 XXXT=XXT(J)
13 K=(J-1)*N+I
XJB2=XJ(K)
XJA2=XJ(K-1)
XJC2=XJ(K+1)
K=K-N
XJB1=XJ(K)
XJA1=XJ(K-1)
XJC1=XJ(K+1)
K=K+2*N
XJB3=XJ(K)
XJA3=XJ(K-1)
XJC3=XJ(K+1)
DK=XXXK-XXX(I-1)
AB1=XXT(J+1)-XXXT
AB2=XXXT-XXT(J-1)
AB1=AB1/AB2
IF(LG-2)157,800,157
157 IF(XK-XXXK)159,159,70
159 XK1=(XXXK-XK)/DK
XK2=(XK-XXXK(I-1))/DK
XJ1=XK1*XJA1+XK2*XJB1
XJ2=XK1*XJA2+XK2*XJB2
XJ3=XK1*XJA3+XK2*XJB3
GC TO 71
70 XK1=(XXXK(I+1)-XK)/DK
XK2=(XK-XXXK)/DK
XJ1=XK1*XJB1+XK2*XJC1
XJ2=XK1*XJB2+XK2*XJC2

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XJ3=XK1*XJB3+XK2*XJC3 226C
71 DSJ=(AB1+1.)/(AB1*(XT-XXT(J-1))/(XJ3-XJ2)+(XT-XXT(J+1))/(XJ1-XJ2)) 2270
IF(LG)222,111,222 2280
222 XABCJ=XJ2+(XT-XXXT)*DSJ 2290
IF(LG)800,800,221 2300
221 IF(LG-1)111,111,800 2310
800 XK1=XT-XXT(J-1) 2320
XK2=XT-XXT(J+1) 2330
XJ1=AB1/(AB1+1.) 2340
CKA=XJ1*(XK1/(XJA3-XJA2)+XK2/(XJA1-XJA2)) 2350
DKB=XJ1*(XK1/(XJB3-XJB2)+XK2/(XJB1-XJB2)) 2360
DKC=XJ1*(XK1/(XJC3-XJC2)+XK2/(XJC1-XJC2)) 2370
XK1=XT-XXXT 2380
XJ1=XJA2+XK1/DKA 2390
XJ2=XJB2+XK1/DKB 2400
XJ3=XJC2+XK1/DKC 2410
DJK=(0.5*(XJ3-XJ1)+(XK-XXK)/DK*(XJ3-2.*XJ2+XJ1))/DK 2420
GC TC 111 2430
5 A)G=XT*XT 2440
IF(LG)19,1119,19 2450
19 IF(XT-6.)1119,2229,2229 2460
1119 TD=1./XG 2470
EAXG=EXP(0.25*XG) 2480
XA=XT*0.8862269*(1.-ERF(0.5*XT))*EAXG 2490
XM=1.253314*XT*(1.-ERF(7.071067E-1*XT))*EAXG*EAXG 2500
XK04=SQR(XA) 2510
WG=SQR(((1.+2.*TD)*XA-1.)/(8.*XA*TD*TD)) 252C
BETA=2.*XK*1.E-5 2530
Y=XA/BETA 254C
C WRITE(6,7000) XA, XM, XK04, BETA, Y 2550
7000 FORMAT(' XA=',G16.8,' XM=',G16.8,' XK04=',G16.8, 2560
1'BETA=',G16.8,' Y=',G16.8) 2570
IF(LG)995,995,50 2580
50 IF(LG-1)995,700,995 2590
995 SV=2.*TD 2600
T2=1./SV 2610
T4=T2*T2 2620
SXA=(-T4-T2)*XA+T4 2620
SXM=(-2.)*T4-T2)*XM+2.*T4 2640
CK=SV*X4 2650
SG=(0.5*TD*DK*(SXA+2.*XA+SV*SXA)-((1.+SV)*XA-1.)*(DK+TD*TD*SXA))/ 266C
1(SV*DK*DK*TD) 2670
XK01=SXA*0.5/XK04 2680
XK02=(XA*SXM-SXA*XM)/(XA*XA) 2690
XK03=(SXA*WG-XA*SG*0.5/WG)/(WG*WG) 2700
R1=(-17.)*XK01-16.*XK02+XK03 271C
R2=5.333333*(8.*XK01+11.*XK02-XK03) 2720
R3=5.333333*(-5.)*XK01-8.*XK02+XK03) 2730
XK05=XM/XA 2740
XK06=X4/WG 2750
R1K=32.-17.*XK04-16.*XK05+XK06 2760
R2K=5.333333*(-18.+8.*XK04+11.*XK05-XK06) 2770
R3K=5.333333*(12.-5.*XK04-8.*XK05+XK06) 2780
SY=SXA/BETA 2790
IF(Y-0.3)900,25,25 2800

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25 SV=1./(1.+Y) 2810
XJC=SQR(SV) 2820
Y1=1./Y 2830
XJ1=(1.-XJ0)*Y1 284C
XJ2=(0.5-XJ1)*Y1 2850
XJ3=(0.375-XJ2)*Y1 2860
XJ4=(0.3125-XJ3)*Y1 2870
SJO=SY*XJ0*SV*(-0.5) 2880
SY1=SY*Y1 2890
SJ1=(-SJO)*Y1-XJ1*SY1 2900
SJ2=(-SJ1)*Y1-XJ2*SY1 2910
SJ3=(-SJ2)*Y1-XJ3*SY1 2920
SJ4=(-SJ3)*Y1-XJ4*SY1 2930
GC TO 1000 294C
900 XJ5=(((1.444644*Y-0.1494459)*Y+C.154981C)*Y-C.1611802)*Y 2950
1+0.1681880)*Y-0.1761970)*Y+0.1854705)*Y-0.19638C6)*Y+0.2094726)*Y 296C
2-C.2255859)*Y+0.246C937 2970
XJ4=0.2734375-Y*XJ5 2980
XJ3=0.3125-Y*XJ4 2990
XJ2=0.375-Y*XJ3 3000
XJ1=0.5-Y*XJ2 301C
XJ0=1.-Y*XJ1 3020
SJ5=(((1.444644*Y-1.3450131)*Y+1.239848)*Y-1.1282614)*Y 3030
1+1.009128)*Y-C.880985)*Y+0.741882)*Y-0.5891418)*Y+0.4189452)*Y- 3040
20.2255859)*Y 3050
SJ4=-((SY*XJ5+Y*SJ5) 3060
SJ3=-((SY*XJ4+Y*SJ4) 3070
SJ2=-((SY*XJ3+Y*SJ3) 3080
SJ1=-((SY*XJ2+Y*SJ2) 3090
SJO=-((SY*XJ1+Y*SJ1) 3100
1000 DSJ=(-3.1415926)/(BETA*XG *XT)*(XK01*XJ0+R1*(-XJ1+2.*XJ2)+XK04 3110
1*SJO+RIK*(-SJ1+2.*SJ2)+R2*(-3.)*XJ2+4.*XJ3)+R2R*((-3.)*SJ2+4.* 3120
2SJ3)+R3*((-5.)*XJ3+6.*XJ4)+R3K*((-5.)*SJ3+6.*SJ4)) 313C
IF(LG)60,111,49 3140
49 IF(LG-1)111,111,60 3150
6C IF(XT-6.)700,220,220 3160
700 ZK=XM/XA 3170
S1=1.-XK04 3180
S2=4.-2.*XK04-2.*ZK 3190
S3=1.+0.0933333*(XA/WG-5.*XK04-8.*ZK) 3200
C WRITE(6,7001) ZK,S1,S2,S3 321C
7001 FORMAT(' ZK=',G16.8,' S1=',G16.8,' S2=',G16.8,' S3=',G16.8) 3220
6665 RI=1.+Y 323C
V0=1./SQR(RI) 3240
Y2=Y*Y 3250
Y3=Y2*Y 3260
Y4=Y2*Y2 3270
IF(Y-0.2)55,66,66 3280
55 V1=(-Y+8.)*Y/(16.*RI) 3290
IF(Y.GE.1.E-10) V1=V1+(Y3*Y3-16.*Y2*Y3+64.*Y4)/(4096.*((Y+2.)*Y+1. 3300
1)) 3310
C WRITE(6,7002) V1 3320
7002 FORMAT(' V1=',G16.8) 333C
GO TO 77 3340
66 V1=(8.-((-Y+4.)*Y+8.)*V0)/Y2 3350

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77 IF(Y-2.)88,99,99
88 SV=RI*RI
Y5=2.+Y
Y6=Y5*Y5*Y5
V2=Y/(2.*Y5*RI)-Y3*Y2/(128.*Y6*SV)
P=(3.*Y+16.)*Y+16.
V3=3.*Y2/(RI*P)
C WRITE(6,7005) V3
7005 FORMAT('VV=',G16.8)
IF(Y4.LT.1.E-30) GO TO 44
V3=V3 -3.*Y4*Y4/(16.*SV*P*P)
C WRITE(6,7003) V3
7003 FORMAT('V3=',G16.8)
GC TO 44
59 V2=(-8.-4.*Y+((Y+8.)*Y+8.)*V0)*4./Y3
V3=(((-6.)*Y-32.)*Y-32.+((Y+18.)*Y+48.)*Y+32.)*VC*12./Y4
44 XABCJ=(V0-S1*V1+S2*V2+S3*V3)*1.5707963/BETA
IF(LG)220,111,1111
1111 IF(LG-2)111,220,111
220 DJK=-0.69315*XABCJ-1.088797*Y/SX*(XKC4*SJO+R1K*(-SJ1+2.*SJ2)
+R2K*(-3.*SJ2+4.*SJ3)+R3K*(-5.*SJ3+6.*SJ4))
GC TO 111
2229 BETA=2.**XK*1.E-5
XABCJ=1.5707963/(BETA*SQRT(1.+1./BETA-6./AXG))
IF(LG)1119,111,34
34 IF(LG-1)111,111,1119
111 RETURN
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SUBROUTINE FSTRUK(MI,SIGO,NE,ENG,NFE,REFE,EFE,NENBER,ENBER,NWFUN,
*CONWU,EPSCOM,DRINWA,I TEST,I ZPUMS,ITUMS,ISPATE,MIBFR,GIBER,MIBERP,
*IIBER,CIBER,FFAKT,MABWF,ABWF,MABWFP,MXINT,XINT,MXINTP,
*MARQ1,ABQ1,MABQ1P,MABQ2,ABQ2,MABQ2F,MABQ3,ABQ3,MABQ3P,
*KMROM,AUXROM,KMROMP,RF,MRF,RFL,MRF)
LCGICAL*4 TEST1,TEST2,TEST3,LFMSG,LFAR(2,3),LFARA(2,3)
REAL*8 MAT,RESULT,RFR,RFL,RPHI,RABS,RELA,RTCT,RFISS,RELF,
*RPHIL,RABSL,RELAL,RTOTL,RFISSL,RELFLL
DIMENSION SIGC(1),ENG(1),REFE(1),EFE(1),FMAT(2),ENBER(1),NWFUN(1),
*CCNWFU(1),GIBER(1),IIBER(1),CIBER(1),FFAKT(MI,6),ABWF(MABWF,4),
*XINT(1),ABQ1(MABQ1,4),ABQ2(MABQ2,4),ABQ3(MABQ3,4),AUXROM(1),
*RFR(MI,MRF),RFL(MI,MRF),FARIN(2,3,2),FARAN(2,3),IFUNAR(2,3),
*ITTF(3),ITTFU(3)
EQUIVALENCE (MAT,EMAT(1))
COMMON MAT,NR3(2),NOUTP,JA,NANF,NEND,KL
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LFMSG,GLSCH,MFTYP,NFTYP,ITYP,
*ITYPFU,UGR,NGR,CONST,NR1(8),BSIGC
COMMON/CFSDUR/ ICUR
PROGRAM KENNZIFFER 3.
BERECHNUNG VON RESONANZSELBSTABSCHIRMFAKTOREN VON
PLAKTWEISE GEBEBENEN WIRKUNGSQUERSCHNITTEN.
B E D E U T U N G D E R F I N G A B E G R C F S S E N .
MI ZAHLE DER SIGO-WERTE.
SIGO SIGO(I),I=1,MI SIGO-WERTE.
NE ZAHLE DER GRUPPENGRENZEN.
ENG ENG(I),I=1,NE GRUPPENGRENZEN.
NFE ZAHLE DER PUNKTE DES WICHTUNGSSPEKTRUMS.
NFE<=1 SPEKTRUM N I C H T PUNKTWEISE GEBEBN.
NFE>1 SPEKTRUM PUNKTWEISE GEBEBN.
REFE REFE(I),I=1,NFE ABSZISSENWERTE DES SPEKTRUMS.
EFE EFE(I),I=1,NFE ORDINATENWERTE DES SPEKTRUMS.
NENBER ZAHLE DER ENERGIEBEREICHE FUER DIE VERSCHIEDENEN SPEKTREN
ENBER(I-1) ... ENBER(I) GUELTIGKEITSBEREICH DER ANZUWENDENDEN
WICHTUNGSFUNKTION NWFUN(I).
I LAEUFT VON 1 BIS NENBER.
DEFINITION: ENBER(0)=1.0E-5 .
SONDERFALL: ENBER(1)=-1.0 GLEICH
GESAMTEN ENERGITBEREICH.
ES MUSS GELTEN:
1.0E-5 <= ENBER(I) <= 20.0E+6 .
NWFUN(I) =NFTYP. TYP DER I-TEN WICHTUNGSFUNKTION, DIE ZUR ANWEN-
DUNG KOMMT, SOWIE ART DER AUSZUFUHRENDEN
INTEGRATION. I=1,NENBER.
(MOEGELICHE WERTE FUER NFTYP SIEHE UNTEN.)
CCNWFU(I) NORMIERUNGSKONSTANTE DER FUNKTION IM I-TEN
WICHTUNGSBEREICH. I=1,NENBER.
MOEGELICHE WERTE VON NFTYP.
NFTYP <= 0 REIN NUMERISCHE INTEGRATION.
NFTYP > 0 ANALYTISCHE INTEGRATION.
INFTYP| = 0 BELIEBIGE FUNKTION PHI.
1 PUNKTWEISE WICHTUNGSFUNKTION
2 CCNWFU(I)/X
DIE FAELE NFTYP<=-2 WERDEN WIE DER FALL NFTYP=0 BEHANDELT.
NFTYP=1 IST NUR DANN MOEGELICH, WENN NFE>1 IST.
EPSCOM GENAUIGKEITSSCHRANKE FUER ROMBERG-INTEGRATION.

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C	KPROM	2**{KMPROM-1} GLEICH MAXIMALE INTERVALLZAHL FUER	560	C	RF	HILFSFELD ZUR SPEICHERUNG DER SIGO-ABHAENGINEN	111C
C		ROMBERG-INTEGRATION.	570	C		INTEGRALRESULTATF.	1120
C	DRINWA	WARNUNGSAUSDRUCK IN NUMERISCHER INTEGRATION.	580	C	ELEMENT	INTEGRAL VON	1130
C		AUSDRUCK ERFOLG, WENN GEWUENSCHTER RELATIVER FEHLER	590	C	RF(MI,1)	F(E)/{(SGT+SIGO)}	1140
C		UM MEHR ALS DAS DRINWA-FACHE UEBERSCHRITTEN WIRD.	600	C	RF(MI,2)	F(E)/{(SGT+SIGO)**2}	1150
C	ITEST	STEUERUNG FUER AUSDRUCK DER MELDUNGEN.	610	C	RF(MI,3)	F(E)*SGN*MUEL/((SGT+STGC)}	116C
C		=0 NORMALER AUSDRUCK FUER PRODUKTIONS LAELFE.	620	C	RF(MI,4)	F(E)*SGT/((SGT+SIGO)**2)	1170
C		UNGLEICH 0 ERWEITERTER AUSDRUCK FUER TESTLAELFE.	630				
C		F I L F S F E L D F R	640				
C	CIBER(I),I=1,NIBER	INTEGRATIONSBEREICHE INNERHALB EINER GRUPPE.	650	C	RF(MI,5)	F(E)*SGN*MUEL/((SGT+SIGO)**2)	1180
C	ITBER(I),I=1,NIBER	WICHTUNGSFUNKTION(EN) UND ART(EN) DER	660	C	RF(MI,6)	F(E)*SGA/((SGT+SIGO)}	1190
C		INTEGRATION INNERHALB EINER GRUPPE (NWFUN).	670	C	RF(MI,7)	F(E)*SGN/((SGT+SIGO)}	1200
C	CIBER(I),I=1,NIBER	NORMIERUNGSKONSTANTE(N) FUER DIE FUNKTION(EN)	680	C	RF(MI,8)	F(E)*SGF/((SGT+SIGO) NUR FUER ISPATE=1 VORHANDEN	1210
C		INNERHALB EINER GRUPPE (CNWFU).	690	C	RFL	LOKALE SPEICHERUNG DER RF-WERTE.	122C
C	NIBER	MAXIMALER WERT FUER NIBER.	700	C	MRFP	NORMAL = 0 . =1 NUR DANN, WENN FESTGESTELLT WURDE,	1230
C	NIBERP	ZAHL DER ZUSAETZLICH BENDEITIGTEN WORTE IN ALLEN MIT	710	C		DASS MRF VERAENDERT WERDEN MUSS.	1240
C		NIBER DIMENSIONIERTEN FELDERN.	720	C	ITYPFU	DIENT BEI ITYP=2 ODER ITYP=6 ZUR GENAUEREN SPEZIFIZIERUNG	1250
C	((FFAKT(I,J)),I=1,MI),J=1,6)	F-FAKTOREN FUER EINE GRUPPE.	730	C		DER IM NENNER STEHENDEN ZU INTEGRIERENDEN FUNKTION ZUM ZWECKE	1260
C		DAS FELD ABWF IST NUR FUER NFE>1 VON BEDEUTUNG.	740	C		BESSERER FEHLERALS DRUCKF.	1270
C	ABWF	FELD ZUR DARSTELLUNG DER PUNKTWEISEN WICHTUNGSFUNKTION	750	C	ES	BEDEUTET:	1280
C		ALS GERADENSTUECKE.	760	C	ITYPFU	BEDEUTUNG	129C
C	ABWF(I,1)	ENERGIEWERT DES INTERVALLENDES ZU DEM DIE NACHFOLGENDEN	770	C	0	KEINE BEDEUTUNG	1300
C		A UND B WERTE GEHOREN.	780	C	1	SGT	1310
C	ABWF(I,2) UND ABWF(I,3)	A UND B WERT DES GERADENSTUECKES Y=AX+B.	790	C	2	SGA	1320
C	ABWF(I,4)	SIEHE ELEMENT (I,4) WEITER UNTEN.	800	C	3	SGN	1330
C	MABWF	MAXIMALER WERT FUER I.	810	C	4	SGF	134C
C	MABWFP	ZUSAETZLICH BENDEITIGTE WORTE IN DEN MIT MABWF	820				1350
C		DIMENSIONIERTEN FELDERN.	830	C	GOTO 3		1360
C		ACHTUNG: ABWF(I,2), ABWF(I,3) UND ABWF(I,4) SIND CHNE BEDEUTUNG.	840	C	1C0	PUNKTEGITTER VON WICHTUNGSFUNKTION IN XINT BRINGEN.	1370
C	XINT(I),I=1,NXINT	FELD ZUR ABSPEICHERUNG DER INTEGRATIONS	850	C		FUER [NFTYP] UNGLEICH 1 WIRD NICHTS WEITER GEMACHT, DA UGR UND OGR	1380
C		INTERVALLE INNERHALB EINES INTEGRATIONSBEREICHES.	860	C		SCHON IN XINT STEHEN. FUER [NFTYP]=1 WIRD ABWF(I,1) IN XINT	139C
C	NXINT	MAXIMALES NXINT.	870	C		EINGEFUEGT.	1400
C	NXINTP	ZUSAETZLICH BENDEITIGTE WORTE IN ALLEN MIT MXINT	880	C		IF(IABS(NFTYP).EQ.1) CALL FSXINT(NXINT,MXINT,XINT,MXINTP,	1410
C		DIMENSIONIERTEN FELDERN.	890	C		*NABWF,ABWF,MABWF,4,4445)	1420
C	ABQ1	FELD ZUR DARSTELLUNG DES 1. QUERSCHNITTES ALS GERADENST.	90C	C		GOTO LABXIN,(13,21,27,31,37)	1430
C	ABQ2	FELD ZUR DARSTELLUNG DES 2. QUERSCHNITTES ALS GERADENST.	910	C		INTEGRALBERECHNUNG	1440
C	ABQ3	FELD ZUR DARSTELLUNG DES 3. QUERSCHNITTES ALS GERADENST.	920	C	101	CALL FSGRAL(RESULT,NXINT,XINT,	1450
C	FUER ABQ1, ABQ2 UND ABQ3 GILT:		930	C	*	NABWF,ABWF,MABWF,	146C
C	ELEMENT (I,1)	ENERGIEWERT DES INTERVALLENDES ZU DEM DIE	940	C	*	NABQ1,ABQ1,MABQ1,NABQ2,ABQ2,MABQ2,NABQ3,ABQ3,MABQ3,	1470
C		NACHFOLGENDEN WERTE A UND B GEHOREN.	950	C	*	KMPROM,AUXROM,KMPROM,EPSPROM,DRINWA,	1480
C	ELEMENT (I,2)	A WERT DES GERADENSTUECKES Y=A*X+B.	960	C	*	IFAR,LFAR,LFARA,FARIN,FARAN,IFUNAR,8445,4446)	1490
C	ELEMENT (I,3)	B WERT DES GERADENSTUECKES Y=A*X+B.	970	C		GOTO LABGRA,(14,16,18,22,24,25,26,28,29,32,34,35,38,39)	1500
C	ELEMENT (I,4)	=0: A=B=0.	980	C	102	CC 5 K=1,3	1510
C		<0: NULLDURCHGANG IM INTERVALL.	990	C		LFAR(1,K)=.FALSE.	1520
C		>0: KEIN NULLDURCHGANG UND A ODER B UNGLEICH 0.	100C	C		LFAR(2,K)=.FALSE.	1530
C	DIE ELEMENTE (I,2), (I,3) UND (I,4)	SIND CHNE BEDEUTUNG.	1010	C		LFARA(1,K)=.FALSE.	154C
C	MABQ1	DIMENSION VON ABQ1.	102C	C	5	LFARA(2,K)=.FALSE.	155C
C	MABQ1P	ZAHL DER WORTE UM DEN MABQ1 VERGROESSERT WERDEN MUSS.	1030	C		GOTO LABFEL,(41,42,43,44,45)	1560
C	MABQ2	DIMENSION VON ABQ2.	1040	C	1C3	K=1	1570
C	MABQ2P	ZAHL DER WORTE UM DEN MABQ2 VERGROESSERT WERDEN MUSS.	105C	C	8	IF(.NOT.LFARA(K,IFAR)) GOTO 6	158C
C	MABQ3	DIMENSION VON ABQ3.	1060	C		LFAR(K,IFAR)=.FALSE.	1590
C	MABQ3P	ZAHL DER WORTE UM DIE MABQ3 VERGROESSERT WERDEN MUSS.	1070	C		LFARA(K,IFAR)=.FALSE.	1600
C	AUXROM	HILFSFELD BEI ROMBERG-INTEGRATION.	1080	C		CALL FSWR04(1008,ITTF(IFAR),ITTFU(IFAR),FARAN(K,IFAR),BSIGO)	1610
C	KMPROM	DIMENSION VON AUXROM.	1090	C		CALL FSWR02(-2005,FARIN(K,IFAR,1),FARIN(K,IFAR,2))	1620
C	KMPROMP	ZAHL DER WORTE UM DIE KMPROM VERGROESSERT WERDEN MUSS.	1100	C		IF(K.EQ.1) CALL FSWR02(-2007,IFUNAR(1,IFAR),ITTF(IFAR))	163C
				C		IF(K.EQ.2) CALL FSWR02(-2008,IFUNAR(2,IFAR),ITTF(IFAR))	1640
				C	6	IF(K.EQ.2) GOTO 7	1650


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K=2
GOTO 8
7 GOTO LABPRI, (17, 50, 51, 23, 30, 52, 33, 40, 60)
104 DC 9 L=1,3
IF(LFAR(1,L)) LFARA(1,L)=.TRUE.
IF(LFAR(2,L)) LFARA(2,L)=.TRUE.
9 CCNTINUE
ASSIGN 60 TO LABPRI
DC 60 IFAR=1,3
IF(LFARA(1,IFAR).OR.LFARA(2,IFAR)) GOTO 103
60 CCNTINUE
GOTO LABPEN, (53, 54, 55, 56, 36)
3 IF(IDUR.NE.0) GOTO 46
TEST1=.FALSE.
TEST2=.FALSE.
TEST3=.FALSE.
LERMSG=.FALSE.
IF(ITEST.LT.10) GOTO 4
LERMSG=.TRUE.
ITEST=ITEST-10
4 IF(ITEST.GE.1) TEST1=.TRUE.
IF(ITEST.GE.2) TEST2=.TRUE.
IF(ITEST.GE.3) TEST3=.TRUE.
C INITIALISIERUNG VON FEHLERARRAY.
CALL FSWROO(1)
C NULLSETZEN VON ALLEN ERWEITERUNGSGROESSEN (.....P) .
46 MIBERP=0
MABWFP=0
MXINTP=0
MABQIP=0
MABQ2P=0
MABQ3P=0
KMROMP=0
MRFP=0
C IDUR GIBT AM PROGRAMMENDE BZW. PROGRAMMANFANG DIE ZAHL DER
C GRUPPEN AN, FUER DIE BEREITS WERTE BERECNET WURDEN.
C D.H. IDUR LIEGT ZWISCHEN 0 UND NANF=NEND. (GRUPPENZAHL-1)
C BEIM ERSTEN ANLAUF FUER EINE REIHE VON GRUPPEN IST IDUR=0.
C NACH ERFOLGREICHEM PROGRAMMENDE WIRD IDUR WIEDER GLEICH NULL
C GESETZT. DIES GILT AUCH FUER EINEN ABBRUCH DES PROGRAMMS, OHNE
C DASS EIN WEITERER ANLAUF MOEGLICH IST.
C SCHREIBEN DER UEBERSCHRIFT.
IF(IDUR.EQ.0) WRITE(INCLTP,1000)
1000 FCRMAT('1')
IF(IDUR.EQ.0) CALL FSWRO2(1001,EMAT(1),EMAT(2))
C MAXIMALER BETRAG FUER NFTYP: MNFTYP
MNFTYP=2
C GLSCH SCHRANKE FUER TOLERANZ VON ZWEI GLEITK*#AZAHLEN.
C (SIEHE LOGICAL FUNCTION FSTOLE)
GLSCH=1.0E-6
C 1. GRUPPE FUER DIE BERECHNUNGEN ERFOLGEN.
ICR=NANF-IDUR
C PRUEFUNG UND AUSDRUCK EINIGER GROESSEN.
CALL FSTRUO(NE,ENG,NANF,NEND,NFE,REFE,EFE,KENBEF,ENBER,
*NWFUN,CONWFU,EPSPOM,KMRCM,DRINWA,ISPATE,MIBER,MABWF,MXINT,MABQ1,

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*MABQ2,MABQ3,MRF,MRFP,8446,8445)
SIND ALLE QUERSCHNITTSTYPEN VORHANDEN ?
IF(IDUR.EQ.0) CALL FSTRUI(8446)
C LOOP FUER ALLE GRUPPEN
1 CCNTINUE
C EVENTUELLE UMSCHALTUNG VON TEST1, TEST2, TEST3 UND LERMSG.
IF(IIZPUMS.LE.-1) GOTO 61
IF(IIZPUMS.NE.(GR.OR.ITUMS.LT.0)) GOTO 61
IITUMS=ITUMS
LERMSG=.FALSE.
IF(IITUMS.LT.10) GOTO 62
63 IITUMS=IITUMS-10
LERMSG=.TRUE.
62 TEST1=.FALSE.
TEST2=.FALSE.
TEST3=.FALSE.
IF(IITUMS.GE.1) TEST1=.TRUE.
IF(IITUMS.GE.2) TEST2=.TRUE.
IF(IITUMS.GE.3) TEST3=.TRUE.
61 CCNTINUE
C AUSDRUCK VON MATERIALNAME, GRUPPENNUMMER, GRUPPENGRENZEN,
C WICHTUNGSFUNKTIONSBEREICH(E), -TYP(EN) UND ART(EN) DER
C INTEGRATION.
C VOR DEM AUSDRUCK DER LETZTEN DREI GROESSEN: BESTIMMUNG DER
C INTEGRATIONSBEREICHE INNERHALB EINER GRUPPE. GIBER(I), I=1,NIBER
C GIBER(I)=GRUPPENANFANG. GIBER(NIBER)=GRUPPENENDE.
C ES WERDEN AUCH IIBER(I), I=1,NIBER UND CIBER(I), I=1,NIBER GESETZT.
CALL FSTRU2(IGR,NF,FNG,NIBER,MIBER,GIBER,MIBERF,IIBER,CIBER,
*MENBER,ENBER,NWFUN,CONWFU,8445)
C NULLSETZEN DER GRUPPENMITTELWERTE.
C (AN DIESE STELLE KANN GESPRUNGEN WERDEN, WENN DIE ZAHL DER
C INTEGRATIONSBEREICHE INNERHALB EINER GRUPPE ERWEITERT WURDE.)
2 CONTINUE
C LCCP UEBER ALLE INTEGRATIONSBEREICHE
RPHI=0.0
RARS=0.0
RELA=0.0
RTCT=0.0
RFISS=0.0
RELFL=0.0
RPHIL=0.0
RABSL=0.0
RFLAL=0.0
RTCTL=0.0
RFISSL=0.0
RELFL=0.0
CC 19 I=1,M1
DC 19 J=1,MRF
RFL(I,J)=0.0
15 RFL(I,J)=0.0
CC 10 IB=2,NIBER
UGR=GIBER(IB-1)
OGR=GIBER(IB)
NFTYP=IIBER(IB)
CONST=CIBER(IB)
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	IF(IABS(NFTYP).GT.MNFTYP.OR.UGR.CT.OGR) CALL FSWR03(3001,'FSTR',	2760	CALL FSXINT(NXINT,MXINT,XINT,MXINTP,NABQ1,ABQ1,MABQ1,4,3445)	3310
	*UK ',1)	2770	ITYP=2	3320
C	WENN (NFTYP)=1 MUESSEN A UND B FLER DAS PLNKTWEISE WICHTLNGS	2780	ITYPFU=1	3330
C	Spektrum berechnet werden.	2790	ASSIGN 22 TO LABGRA	3340
	IF(IABS(NFTYP).NE.1) GOTO 11	2800	GOTO 101	3350
	CALL FSTRU3(INFE,REFF,EFE,NABWF,MABWF,ABWF,MABWF,3445,3446)	2810	22 RTCTL=RESULT	3360
11	CONTINUE	2820	IF(LERMSG) GOTO 42	3370
	ASSIGN 13 TO LABXIN	2830	ASSIGN 42 TO LABFEL	3380
	GOTO 100	2840	GOTO 102	3390
C	INTEGRAL VON F(E)DE VON UGR BIS CGR.	2850	42 CC 23 I=1,MI	3400
13	ITYP=1	2860	BSIGO=SIGO(I)	3410
	ITYPFU=0	2870	ITYP=4	3420
	ASSIGN 14 TO LABGRA	2880	ITYPFU=0	3430
	GOTO 101	2890	ITTF(1)=ITYP	3440
14	RPFIL=RESULT	2900	ITTFU(1)=ITYPFU	3450
C	INTEGRAL VON SGA*PHI VON UGR BIS CGR	2910	ASSIGN 24 TO LABGRA	3460
	CALL FSQUER('SGA ',UGR,OGR,NABQ1,MABQ1,ABQ1,MABQ1P,3445,3446)	2920	IFAR=1	3470
	CALL FSXINT(NXINT,MXINT,XINT,MXINTP,NABQ1,ABQ1,MABQ1,4,3445)	2930	GOTO 101	3480
	ITYP=2	2940	24 RFL(I,1)=RESULT	3490
	ITYPFU=2	2950	IF(LERMSG) GOTO 50	3500
	ASSIGN 16 TO LABGRA	2960	ASSIGN 50 TO LABPRI	3510
	GOTO 101	2970	GOTO 103	3520
16	RABSL=RESULT	2980	50 ITP=5	3530
C	INTEGRAL VON SGA*F(E)/((SGT+SIGO) RF(MI,6) ITP=6 ITPFU=2	2990	ITYPFU=0	3540
	CALL FSQUER('SGT ',UGR,OGR,NABQ3,MABQ3,ABQ3,MABQ3P,3445,3446)	3000	ITTF(2)=ITYP	3550
	CALL FSXINT(NXINT,MXINT,XINT,MXINTP,NABQ3,ABQ3,MABQ3,4,3445)	3010	ITTFU(1)=ITYPFU	3560
	ITYP=6	3020	ASSIGN 25 TO LABGRA	3570
	ITYPFU=2	3030	IFAR=2	3580
	ITTF(1)=ITYP	3040	GOTO 101	3590
	ITTFU(1)=ITYPFU	3050	25 RFL(I,2)=RESULT	3600
	ASSIGN 18 TO LABGRA	3060	IF(LERMSG) GOTO 51	3610
	IF(LERMSG) GOTO 41	3070	ASSIGN 51 TO LABPRI	3620
	IFAR=1	3080	GOTO 103	3630
	ASSIGN 41 TO LABFEL	3090	51 ITP=7	3640
	GOTO 102	3100	ITYPFU=0	3650
41	CC 17 I=1,MI	3110	ITTF(3)=ITYP	3660
	BSIGO=SIGO(I)	3120	ITTFU(3)=ITYPFU	3670
	GOTO 101	3130	ASSIGN 26 TO LABGRA	3680
18	RFL(I,6)=RESULT	3140	IFAR=3	3690
	IF(LERMSG) GOTO 17	3150	GOTO 101	3700
	ASSIGN 17 TO LABPRI	3160	26 RFL(I,4)=RESULT	3710
	GOTO 103	3170	IF(LERMSG) GOTO 23	3720
17	CONTINUE	3180	ASSIGN 23 TO LABPRI	3730
	IF(LERMSG) GOTO 53	3190	GOTO 103	3740
	ASSIGN 53 TO LABPEN	3200	23 CCNTINUE	3750
	GOTO 104	3210	IF(LERMSG) GOTO 54	3760
C	INTEGRAL VON	3220	ASSIGN 54 TO LABPEN	3770
C	F(E)*SGT ITP=2 ITPFU=1	3230	GOTO 104	3780
C	F(E)/(SGT+SIGO) RF(MI,1) ITP=4 ITPFU=0	3240	C	INTEGRAL VON F(E)*SGN ITP=2 ITPFU=3
C	F(E)/((SGT+SIGO)**2) RF(MI,2) ITP=5 ITPFU=0	3250	54	ASSIGN 27 TO LABXIN
C	F(E)*SGT/((SGT+SIGO)**2) RF(MI,4) ITP=7 ITPFU=0	3260	GOTO 100	3810
C		3270	27	CALL FSQUER('SGN ',UGR,OGR,NABQ1,MABQ1,ABQ1,MABQ1P,3445,3446)
53	ASSIGN 21 TO LABXIN	3280	CALL FSXINT(NXINT,MXINT,XINT,MXINTP,NABQ1,ABQ1,MABQ1,4,3445)	3820
	GOTO 100	3290	ITYP=2	3830
21	CALL FSTRU5(ABQ3,NABQ3,MABQ3,ABQ1,NABQ1,MABQ1,MABQ1P,3445)	3300	ITYPFU=3	3840
				3850


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RELFL=RELFL+RELFLL          4960
CC 20 I=1,MI                4970
DO 20 J=1,MRF               4980
20 RF(I,J)=RF(I,J)+RFL(I,J) 4990
1C CCNTINUF                 5000
CALL FSTRU4(ENG,NE,IGR,FFAKT,MI,SIGO,RPHI,RABS,FELA,RTCT,RFISS, 5010
*RELFL,RF,MRF,ISPATE)      5020
C   NAECHSTE GRUPPE        5030
   ICF=IGR-1               5040
   IF(IGR.GE.NEND) GOTO 1   5050
C   PROGRAMME NACH ERFOLGREICHEM DURCHLAUF. 5060
444 KL=KL+1                 5070
   IDUR=0                   5080
   CALL FSWR01(1002,KL)     5090
C   UEBERSICHT UEBER DIE GEDRUCKTEN FEHLER- UND WARNUNGS 5100
C   MELDUNGEN.             5110
   CALL FSWRS9              5120
333 RETURN                  5130
C   PROGRAMME MIT ERNEUTEM PROGRAMMANLAUF MIT VERGROESSERTEM (N) 5140
C   DATENFELD (ERN) .      5150
445 CALL FSWR00(1003)       5160
   IF(MXINTP.EQ.0) MXINTP=MAX0(MXINT,MABQ1+MABQ1P,MABQ2+MABQ2P,MABQ3+ 5170
*   MABQ3P)-MXINT          5180
   ICUR=NANF-IGR           5190
   GOTO 333                 5200
C   ABRUCH DES PROGRAMMS KENNZIFFER 3, DA DATEN ( PROGRAMMSTEUER 5210
C   KERNDATEN ODER SPEKTRUMSDATEN ) DIF DURCHFUEHRUNG 5220
C   DER RECHNUNG NICHT ZULIESSEN. 5230
446 CALL FSWR00(3002)       5240
   IDUR=C                   5250
   KL=KL+1                  5260
   GOTO 333                 5270
   END                      5280

SUBROUTINE FSTRU4(NE,ENG,NANF,NEND,NFE,REFE,EFE,NENBER, 1C
*ENBER,NWFUN,CONWFU,EPSROM,KMROM,DRINWA,ISPATE,MIBER,MABWF,MXINT, 20
*MABQ1,MABQ2,MABQ3,MRF,MRF,*,*) 3C
C   PRUEFUNG UND AUSDRUCK EINIGER GRESSEN. 40
   DIMENSION ENG(1),ENBER(1),NWFUN(1),CONWFU(1),IH(3),RH1(3),RH2(3), 5C
*REFE(1),EFE(1),IARG2(4) 60
   LOGICAL*4 FEHLER,TEST1,TEST2,TEST3,LERMSG,FSTOLE,ORIFUN 70
   REAL*8 MAT,BEST,SGF,ARG3(5) 8C
   DATA BEST,SGF/'BEST ','SGF '/ 90
   COMMON MAT,NRI(2),NC 100
   COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH,MFTYP,NFTYP 110
   COMMON/CFSDUR/ IDUR 120
   COMMON/CFSMEL/ CRIFUN 13C
   FEHLER=.FALSE. 140
   NE >= 1 ? 150
   IF(NE.GE.1) GOTO 18 160
   FEHLER=.TRUE. 170
   CALL FSWR06(3009,'NE ',' ','NE','.GE.','THAN',1) 18C

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C   NANF >= 1 ? 190
18 IF(NANF.GE.1) GOTO 19 200
   FEHLER=.TRUE. 210
   CALL FSWR06(3009,'NANF',' ','NANF','.GE.','THAN',1) 220
C   NEND >= 1 ? 230
19 IF(NEND.GE.1) GOTO 20 240
   FEHLER=.TRUE. 250
   CALL FSWR06(3009,'NEND',' ','NEND','.GE.','THAN',1) 260
C   NENBER >= 1 ? 270
20 IF(NENBER.GE.1) GOTO 21 280
   FEHLER=.TRUE. 290
   CALL FSWR06(3009,'NENB','ER ','NENBER','.GE.','THAN',1) 300
C   MIBER >= 5 310
   IF(MIBER.GE.5) GOTO 43 320
   FEHLER=.TRUE. 330
   CALL FSWR06(3009,'MIBER','R ','MIBER','.GE.','THAN',5) 340
43 CCNTINUE 350
   IF(NFE.LE.1.OR.MABWF.GE.50) GOTO 44 360
   FEHLER=.TRUE. 370
   CALL FSWR06(3009,'MABW','F ','MABWF','.GE.','THAN',50) 380
44 CCNTINUE 400
   IF(MXINT.GE.100) GOTO 45 410
   FEHLER=.TRUE. 420
   CALL FSWR06(3009,'MXIN','T ','MXINT','.GE.','THAN',100) 430
45 CCNTINUE 440
   IF(MABQ1.GE.100) GOTO 46 450
   FEHLER=.TRUE. 460
   CALL FSWR06(3009,'MABQ','1 ','MABQ1','.GE.','THAN',100) 470
46 IF(MABQ2.GE.100) GOTO 47 480
   FEHLER=.TRUE. 490
   CALL FSWR06(3009,'MABQ','2 ','MABQ2','.GE.','THAN',100) 500
47 IF(MABQ3.GE.100) GOTO 48 510
   FEHLER=.TRUE. 520
   CALL FSWR06(3009,'MABQ','3 ','MABQ3','.GE.','THAN',100) 530
48 CCNTINUE 540
   IF(ICUR.NE.0) GOTO 3 550
C   SETZEN UND TEST VON ISPATE. IST SGF VORHANDEN, DANN MUSS ISPATE=1 560
C   SEIN. IST ES UNGLEICH 1, SO WIRD ES GLEICH 1 GESETZT. 570
C   IST SGF NICHT VORHANDEN, DANN MUSS ISPATE=0 SEIN. 580
   IARG2(1)=3 590
   ARG3(1)=MAT 600
   ARG3(2)=BEST 610
   ARG3(3)=SGF 620
   IRC=0 630
   CALL NDFLOC(IRC,IARC2,ARG3,ARG4,ARG5) 640
   IF(IRC.EQ.1) GOTO 17 650
C   KEIN SGF VORHANDEN. 660
   IF(ISPATE.EQ.0) GOTO 3 670
   ISPATE=0 680
   GOTO 3 690
C   SGF VORHANDEN. 700
17 IF(ISPATE.EQ.1) GOTO 3 710
   ISPATE=1 720
   GOTO 3 730

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- B 43 -

2	CONTINUE	740	1002	FORMAT(' ',2(' NUMBER	LOWER	UPPER	'')/	1290
C	TEST VON MRF. FUER ISPATE=0 MUSS ES 7, FUER ISPATF=1 MUSS	750	*	' ',2('	LIMIT (EV)	LIMIT (EV)	'')/	1300
C	ES 8 SEIN.	760		IF(NHELP.GT.1) WRITE(NO,1003)				1310
	IF((ISPATE.EQ.0.AND.MRF.NE.7).OR.(ISPATE.EQ.1.AND.MRF.NE.8))	770	1003	FORMAT(' ',3(' NUMBER	LOWER	UPPER	'')/	1320
	*GCTO 889	780	*	' ',3('	LIMIT (EV)	LIMIT (EV)	'')/	1330
C	TEST VON IDUR.	790		NGRANZ=NANF-NEND+1				1340
27	IF(IDUR.GE.0) GOTO 40	800		NHELP=(NGRANZ-1)/3+1				1350
	FEHLER=.TRUE.	810		DO 10 J=1,NHELP				1360
	CALL FSWR06(3009,'IDUR',	820		I=NANF-3*(J-1)				1370
40	IF(IDUR.LE.(NE-2)) GOTO 41	830		IH2=1				1380
	FEHLER=.TRUE.	840		IF((I-1).GE.NEND) IH2=2				1390
	CALL FSWR06(3009,'IDUR',	850		IF((I-2).GE.NEND) IH2=3				1400
41	CONTINUE	860		DC 11 II=1,IH2				1410
C	WENN NFE>1 TEST VON REFE.	870		IF(II)=I-II+1				1420
	IF(NFE.LE.1) GOTO 50	880		RF1(II)=ENG(NE-I+II-1)				1430
	DO 51 I=2,NFE	890	11	RF2(II)=ENG(NE-I+II)				1440
	IF(REFE(I).GT.REFE(I-1)) GOTO 51	900		WRITE(ND,1004) (IH(II),RH1(II),RF2(II),II=1,IH2)				1450
	FFHLER=.TRUE.	910	1004	FORMAT(' ',3(CPI6,2X,1PE14.6,2X,1PE14.6,2X))				1460
	CALL FSWR07(3012,'RFFE',	920	10	CONTINUE				1470
51	CONTINUE	930	5	CONTINUE				1480
50	CONTINUE	940	C	WENN ISPATE GLEICH 1 AUSDRUCK.				1490
C	NANF >= END ?	950		IF(IDUR.EQ.0.AND.ISPATE.EQ.1) WRITE(NO,1014)				1500
	IF(NANF.GE.NEND) GOTO 1	960	1014	FORMAT('OTHE MATERIAL IS F I S S I C N A B L E .')				1510
	FEHLER=.TRUE.	970	C	WENN ISPATE GLEICH NULL AUSDRUCK.				1520
	CALL FSWR02(3003,NANF,NEND)	980		IF(IDUR.EQ.0.AND.ISPATE.EQ.0) WRITE(ND,1015)				1530
1	CONTINUE	990	1015	FORMAT('OTHE MATERIAL IS N O T F I S S I O N A B L E .')				1540
C	GRUPPENNUMMERN INNERHALB VON ENERGIEGRUPPENSCHHEMA?	1000	C	ENG(I) MUESSEN >= 0 SEIN.				1550
C	GRUPPE I GEHT VON ENG(NE-I) BIS ENG(NE-(I-1)) .	1010		DO 22 I=1,NE				1560
C	D.F. I MUSS IMMER KLEINER ALS NE SEIN	1020		IF(ENG(I).GT.0.0.OR.FSTOLE(ENG(I),C.O,GLSCH)) GOTO 22				1570
	IF(NANF.LT.NE) GOTO 2	1030		FEHLER=.TRUE.				1580
	IF(NANF.EQ.NE) CALL FSWR02(2001,NANF,NE-1)	1040		CALL FSWR07(3012,'ENG ',				1590
	IF(NANF.GT.NE) CALL FSWR03(2002,NANF,NE,NE-1)	1050	22	CONTINUE				1600
	NANF=NE-1	1060	C	DRUCK VON DRINWA.				1610
	IF(NANF.GE.NEND) GOTO 2	1070		IF(IDUR.EQ.0) WRITE(NO,1016) DRINWA, EPSROM				1620
	NEND=NANF	1080	1016	FORMAT('OWARNING MESSAGES IN NUMERICAL INTEGRATION WILL BE PRINTED				1630
	CALL FSWR02(2003,NEND,NANF)	1090	*	IF THE ACTUAL RELATIVE ERROR'				1640
2	CONTINUE	1100	*	' IS GREATER OR EQUAL THAN ',1PE12.4,' TIMES THE WISHED RELATIVE E				1650
C	IDUR MUSS KLEINER GLEICH NANF-NEND SEIN.	1110		*RROR = ',1PE12.4,'.)				1660
	IF(IDUR.LE.(NANF-NEND)) GOTO 42	1120	C	UEBERPRUEFUNG DER GRUPPENGRENZEN.				1670
	FEHLER=.TRUE.	1130		NGRANZ=NANF-NEND+1				1680
	CALL FSWR06(3009,'IDUR',	1140		CC 6 J=1,NGRANZ				1690
42	CONTINUE	1150		I=NANF-(J-1)				1700
	IF(IDUR.GT.0) GOTO 5	1160		IF(ENG(NE-I).LT.ENG(NE-(I-1))) GOTO 6				1710
C	AUSDRUCK DER ENERGIEGRUPPEN FUER WELCHE DIE BERECHNUNGEN ERFOLGEN.	1170		FEHLER=.TRUE.				1720
	IF(NANF.GT.NEND) GOTO 4	1180		CALL FSWR01(3005,1)				1730
	WRITE(NO,1000) NANF,ENG(NE-NANF),ENG(NE-(NANF-1))	1190	6	CONTINUE				1740
1000	FORMAT('OTHE CALCULATIONS WILL BE DONE FOR GROUP',15,	1200	C	AUSDRUCK UND UEBERPRUEFUNG DER BEREICHE FUER DIE INTERPOLATIONS				1750
	'*, WHICH HAS THE BOUNDARIES ',1PE15.6,' EV AND ',	1210	C	FLUKTION.				1760
	*1PE15.6,' EV.')	1220		IF(IDUR.EQ.0) WRITE(NO,1005)				1770
	GCTO 5	1230	1005	FORMAT('OTHE FOLLOWING WEIGHTING SPECTRUM(S) IS (ARE) USED.')				1780
4	WRITE(NO,1001)	1240	*	' ',14X,'ENERGY RANGE',14X,7X,'WEIGHTING SPECTRUM',18X,				1790
1001	FORMAT('OTHE CALCULATIONS WILL BE DONE FOR THE FOLLOWING ENERGY GR	1250	*	' TYP OF INTEGRATION'/)				1800
	*CUPS.')	1260		DC 7 I=1,NENBER				1810
	NHELP=NANF-NEND	1270	C	ENERGIEBEREICH.				1820
	IF(NHELP.EQ.1) WRITE(NO,1002)	1280		IF(.NOT.FSTOLE(ENBER(I),-1.0,GLSCH)) GOTO 8				1830

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IF(IDUR.EQ.0) WRITE(NO,1006)
1006 FCRMAT(' ',14X,'WHOLE RANGE')
      GOTO 9
      8 IF(I.EQ.1.AND.IDUR.EQ.0) WRITE(NO,1007) ENBER(I)
1007 FCRMAT(' ',8X,'1.0E-5 EV TO ',1PE14.6,' EV')
      IF(I.GT.1.AND.IDUR.EQ.0) WRITE(NO,1008) ENBER(I-1),ENBER(I)
1008 FCRMAT(' ',1PE14.6,' EV TO ',1PE14.6,' EV')
      9 CONTINUE
C     FUNKTIONSTYP UND ART DER INTEGRATION.
      NFTYP=NWFUN(I)
      IABSNF=IABS(NFTYP)
      IF(IABSNF.LE.MNFTYP) GOTO 12
      FEHLER=.TRUE.
      CALL FSWR03(3006,I,NFTYP,MNFTYP)
      GOTO 7
      12 ISPRU=IABSNF+1
      IF(IDUR.NE.0) GOTO 13
      GOTO (14,15,16
      *),ISPRU
      CALL FSWR03(3001,'FSTR','UO ',I)
      14 ORIFUN=.FALSE.
      DPHI=DPHI(1.0D+0)
      IF(ORIFUN) WRITE(NO,1009)
      IF(.NOT.ORIFUN) WRITE(NO,1017)
1009 FCRMAT('+',40X,' ORIGINAL FUNCTION DPHI=1.0D+0/E')
1017 FCRMAT('+',40X,' FUNCTION DPHI GIVEN BY THE USER')
      GOTO 13
      15 WRITE(NO,1010)
1010 FCRMAT('+',40X,' POINTWISE GIVEN WEIGHTING SPECTRUM')
      GOTO 13
      16 WRITE(NO,1011) CONWFU(I)
1011 FCRMAT('+',40X,2X,4X,1PE13.5,'/E')
      GOTO 13
      13 CCNTINUE
C     INTEGRATIONSART.
      IF(IDUR.NE.0) GOTO 7
      IF(NFTYP.LE.0) WRITE(NC,1012)
1012 FORMAT('+',85X,' NUMERICAL')
      IF(NFTYP.GT.0) WRITE(NC,1013)
1013 FORMAT('+',85X,' ANALYTICAL')
      7 CONTINUE
C     WENN EIN PUNKTWEISES WICHTUNGSSPEKTRUM VERLANGT WIRD,
C     MUSS NFE > 1 SEIN.
      DC 23 I=1,NENBER
      IF(IABS(NWFUN(I)).NE.1.CR.NFE.GT.1) GOTO 23
      FEHLER=.TRUE.
      CALL FSWR01(3007,I)
      23 CCNTINUE
C     WEICHE FUER NENBER=1 UND NENBER > 1 .
      IF(NENBER.GT.1) GOTO 24
C     ENBER(I) MUSS ENTWEDER GLEICH -1.C ODER GROESSER GLEICH
C     ENG(NE-(NEND-1)) SEIN.
      IF(FSTOLE(ENBER(I),-1.0,GLSCH).OR.ENBER(I).GE.ENG(NE-(NEND-1))
      *.CR.FSTOLE(ENBER(I),ENG(NE-(NEND-1)),GLSCH)) GOTO 25
      FEHLER=.TRUE.

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CALL FSWR02(3004,ENBER(I),ENG(NE-(NEND-1)))
      GOTO 25
C     WENN NENBER > 1 IST MUSS ENBER(NENBER) >= ENG(NE-(NEND-1)) SEIN.
24 IF(FSTOLE(ENBER(NENBER),ENG(NE-(NEND-1)),GLSCH).CR.
      *ENBER(NENBER).GT.ENG(NE-(NEND-1))) GOTO 26
      FEHLER=.TRUE.
      CALL FSWR07(3012,'ENBE','R ',NENBER,ENBER(NENBER),'GE.',
      *'THAN',ENG(NE-(NEND-1)))
      26 CONTINUE
C     ENBER(I) MUSS GROESSER SEIN ALS ENBER(I-1)
      DO 29 I=2,NENBER
      IF(ENBER(I).GT.ENBER(I-1)) GOTO 29
      FEHLER=.TRUE.
      CALL FSWR07(3012,'ENBE','R ',I,ENBER(I),'GT.','THAN',ENBER(I-1)
      *)
      29 CONTINUE
      25 CCNTINUE
C     WENN |NWFUN(I)| >= 2 DANN MUSS CONWFU(I) UNGLEICH NULL SEIN.
      DO 30 I=1,NENBER
      IF(IABS(NWFUN(I)).LT.2.OR..NOT.FSTOLE(CONWFU(I),0.0,GLSCH))
      *GOTO 30
      FEHLER=.TRUE.
      CALL FSWR07(3012,'CCNW','FU ',I,CONWFU(I),'NE.','THAN',0.0)
      30 CONTINUE
C     TEST VON EPSROM UND KMR0M.
C     C.C <= FPSROM <= 1.C
C     LO <= KMR0M <= 40
      IF(EPSROM.GT.0.0.OR.FSTOLE(EPSROM,0.0,GLSCH)) GOTO 31
      FEHLER=.TRUE.
      CALL FSWR06(3010,'EPSR','OM ',EPSROM,'GE.','THAN',0.0)
      31 IF(EPSROM.LT.1.0.OR.FSTOLE(EPSROM,1.0,GLSCH)) GOTO 32
      FEHLER=.TRUE.
      CALL FSWR06(3010,'EPSR','OM ',EPSROM,'LE.','THAN',1.0)
      32 IF(KMR0M.GE.10) GOTO 33
      FEHLER=.TRUE.
      CALL FSWR05(3009,'KMR0','M ',KMR0M,'GE.','THAN',10)
      33 IF(KMR0M.LE.40) GOTO 34
      FEHLER=.TRUE.
      CALL FSWR06(3009,'KMR0','M ',KMR0M,'LE.','THAN',40)
      34 CCNTINUE
      IF(FEHLER) GOTO 898
      KEIN FEHLER FESTGESTELLT.
      IF(TEST1) CALL FSWR00(1004)
      333 RETURN
C     STUERDATEN LASSEN DURCHFUEHRUNG DER RECHNUNG NICHT ZU.
      888 RETURN 1
      889 MRFP=1
      RETURN 2
      ENC

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- B 45 -

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SUBROUTINE FSTRU1(*)
PRUEFT OB DIE QUERSCHNITTSTYPEN SGA, SGN, SGT UND MUEL VORHANDEN
SIND.
LOGICAL*4 FEHLER, TEST1, TEST2, TEST3, LERMSG
REAL*8 ARG3(5), NAMES(4), MAT, TEXT
DIMENSION IARG2(4), FMAT(2), TYP(2)
DATA TEXT/'BEST ', NAMES/'SGA ', 'SGN ', 'SGT ',
*'MUEL '/
EQUIVALENCE (MAT, EMAT(1)), (ARG3(3), TYP(1))
COMMON MAT
COMMON/CFSTRU/ TEST1, TEST2, TEST3, LERMSG
FEHLER=.FALSE.
IARG2(1)=3
ARG3(1)=MAT
ARG3(2)=TEXT
DO 1 I=1,4
ARG3(3)=NAMES(I)
IRC=0
CALL NDFLOC(IRC, IARG2, ARG3, ARG4, ARG5)
IF(IRC.EQ.1) GOTO 1
FEHLER=.TRUE.
CALL FSWR04(3008, EMAT(1), EMAT(2), TYP(1), TYP(2))
1 CONTINUE
IF(FEHLER) RETURN 1
IF(TEST1) CALL FSWR00(1006)
RETURN
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SUBROUTINE FSTRU2(IGR, NE, ENG, NIBER, MIBER, GIBER, MIBERP, IIBER, CIBER,
* NENBER, ENBER, NWFUN, CONWUF, *)
AUSDRUCK VON MATERIALNAME, GRUPPENNUMMER UND GRUPPENGRENZEN.
BESTIMMUNG UND AUSDRUCK VON INTEGRATIONSBEREICH(E) ART(FN)
UND TYP(FN) DER INTEGRATION INNERHALB EINER GRUPPE.
DIMENSION ENG(1), GIBER(1), IIBER(1), CIBER(1), ENBER(1), NWFUN(1),
* CONWUF(1)
LOGICAL*4 FSTOLE, TEST1, TEST2, TEST3, LERMSG
REAL*8 MAT
COMMON/CFSTRU/ TEST1, TEST2, TEST3, LERMSG, GLSCH
COMMON MAT, NRI(2), NO
WRITE(NO,1008)
1008 FORMAT('0')
WRITE(NO,1009)
1009 FORMAT(' ',126('**'))
WRITE(NO,1000) MAT, IGR, ENG(NE-IGR), ENG(NE-(IGR-1))
1000 FORMAT(' **', A8, ' GROUP=', I4, ' LCWFR BOUNDARY=', IPE14.6, ' EV
*UPPER BOUNDARY=', IPE14.6, ' FV.', I32X, '**')
SETZEN VON GIBER(I) UND CIBER(IIBER).
NIBER=2
IF(NIBER.GT.MIBER) CALL FSWR03(3001, 'FSTR', 'U2 ', 1)
GIBER(1)=ENG(NE-IGR)

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GIBER(NIBER)=ENG(NE-(IGR-1))
BESTIMMUNG DER DURCH WICHTUNGSFUNKTIONEN BEDINGTEN UNTERBEREICHE.
IIBER(1) UND CIBER(1) SIND OHNE BEDEUTUNG UND WERDEN DESHALB
GLEICH -999999 BZW. -999999.C GESETZT.
IIBER(1)=-999999
CIBER(1)=-999999.0
WEAN NENBER GLEICH 1 IST, DANN GIBT ES KEINE UNTERBEREICHE.
IF(NENBER.EQ.1) GOTO 1
SUCHE VON ENBER(I) MIT GIBER(NIBER-1)<ENBER(I)<GIBER(NIBER)
DO 2 I=1, NIBER
IF(ENBER(I).LT.GIBER(NIBER-1).OR.FSTOLE(ENBER(I), GIBER(NIBER-1), GL
* SCH)) GOTO 2
IF(ENBER(I).GT.GIBER(NIBER).OR.FSTOLE(ENBER(I), CIBER(NIBER), GLSCH)
*) GOTO 3
NIBER=NIBER+1
IF(NIBER.GT.MIBER) GOTO 2
GIBER(NIBER)=GIBER(NIBER-1)
GIBER(NIBER-1)=ENBER(I)
2 CONTINUE
3 IF(NIBER.LE.MIBER) GOTO 1
MIBERP=NIBER-MIBER
RETURN 1
1 CONTINUE
SETZEN DER WICHTUNGSFUNKTIONSTYPEN UND INTEGRATIONSARTEN.
SETZEN DER NORMIERUNGSKONSTANTEN.
IF(NENBER.GT.1) GOTO 4
IF(NIBER.GT.2) CALL FSWR03(3001, 'FSTR', 'U2 ', 2)
IIBER(2)=NWFUN(1)
CIBER(2)=CONWUF(1)
GOTO 10
4 CONTINUE
I=2
J=1
7 IF(.NOT.FSTOLF(GIBER(I), ENBER(J), GLSCH).AND.
* ENBER(J).LT.GIBER(I)) GOTO 5
IIBER(I)=NWFUN(J)
CIBER(I)=CONWUF(J)
GOTO 6
5 J=J+1
IF(J.LE.NENBER) GOTO 7
IF(I.NE.NIBER) CALL FSWR03(3001, 'FSTR', 'U2 ', 3)
IIBER(I)=NWFUN(NENBER)
CIBER(I)=CONWUF(NENBER)
GOTO 10
6 I=I+1
IF(I.LE.NIBER) GOTO 8
10 CONTINUE
AUSDRUCK DER INTEGRATIONSBEREICHE, TYPEN DER WICHTUNGSFUNKTION
UND ARTEN DER INTEGRATION.
DO 11 I=2, NIBER
WRITE(NO,1001) GIBER(I-1), GIBER(I)
1001 FORMAT(' **', I1X, 'FROM ', IPE14.6, ' EV TO ', IPE14.6, ' FV')
IF(IIBER(I).LE.0) WRITE(NO,1002)
1002 FORMAT(' **', 58X, 'NUMERICAL')
IF(IIBER(I).GT.0) WRITE(NO,1003)

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1003 FORMAT('+',58X,'ANALYTICAL')
      WRITE(NO,1004)
1004 FCFORMAT('+',68X,' INTEGRATION IS USED.')
      ISPRU=IABS(IIBER(I))+1
      GCTC (14,15,16
      *),ISPRU
      CALL FSWR03(3001,'FSTR','U2 ',4)
14 WRITE(NO,1005)
1005 FORMAT('+',89X,' DPHI IS USED AS WEIGHTING SPECTRUM.*')
      GCTC 11
15 WRITE(NO,1006)
1006 FCFORMAT('+',89X,' POINTWISE GIVEN WEIGHTING SPECTRUM.*')
      GCTC 11
16 WRITE(NO,1007) CIBER(I)
1007 FCFORMAT('+',89X,' FUNCTION ',IPE13.5,'/E USED',5X,'**/
      *',97X,'AS WEIGHTING SPECTRUM.',5X,'**')
      GCTC 11
11 CCNTINUE
      WRITE(NO,1009)
      IF(TEST1) CALL FSWR00(1007)
333 RETURN
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SUBROUTINE FSTRU3(NFE,REFE,EFE,NABWF,MABWF,ABWF,MABWF,**)
DARSTELLUNG DER PUNKTWEISEN WICHTUNGSFUNKTION DURCH GERADENSTUECKE
NABWF IST DFR INDEX BIS ZU OFM DAS FELD ABWF GEFUELLT IST.
DIMENSION REFE(1),EFE(1),ABWF(MABWF,4)
LOGICAL*4 TEST1,TEST2,TEST3,LERMSG,FSTCLE,FINBED
COMMON NR1(4),NO
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH,
*NR2(4),UGR,0GR
IF(NFE.LE.1) CALL FSWR03(3001,'FSTR','U3 ',1)
FINBED=.FALSE.
VERGLEICH VON UGR MIT REFE(1).
UGR > REFE(1) ODER FSTCLE(UGR,REFE(1),GLSCH) GLEICH .TRUE.
 ABWF(1,1)=UGR ; ABWF(1,2)=-999999.0 ;
 ABWF(1,3)=-999999.0 ;
 ABWF(1,4)=-999999.0 ;
 NABWF=1 ;
 I=2 SETZEN UND 1. REFE(I) SUCHEN, MIT UGR < REFE(I)
UGR < REFE(I) FEHLERAUSGANG.
 IF(UGR.GT.REFE(1).OR.FSTCLE(UGR,REFE(1),GLSCH)) GOTO 1
 CALL FSWR07(3015,'FIRS','T ',REFE(1),'GT.','LCWE','R ',UGR)
888 RETURN 2
1 ABWF(1,1)=UGR
 ABWF(1,2)=-999999.0
 ABWF(1,3)=-999999.0
 ABWF(1,4)=-999999.0
 NABWF=1
 NN=1
 IF(TEST2) WRITE(NO,1000) NN,(ABWF(1,J),J=1,4)
1000 FCFORMAT(' ABWF: NABWF=',I5,' E=',IPE14.6,' A=',IPE14.6,' B=',

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* IPE14.6, ' ABWF(NABWF,4)=' ,IPE12.4,'. ')
      I=2
2 IF(RFFE(I).GT.UGR) GOTO 3
      I=I+1
      IF(I.LE.NFE) GCTC 2
C KEIN ENERGIEPUNKT DES SPEKTRUMS IST GRCESSER ALS UGR.
      CALL FSWR02(3014,UGR,0GR)
      GOTO 888
3 CCNTINUE
C LCCP SOLANGE DURCHFUEHREN, BIS (EINSCHLIESSLICH) 1. REFE(I)>=0GR
C WIRD KEIN REFE(I)>=0GR, IST AUCH FSTCLE(REFE(NFE),0GR,GLSCH)
C GLEICH .TRUE. ZUGELASSEN.
      IF(FINBED) GOTO 7
4 IF(REFE(I).LT.0GR) GOTO 8
      FINBED=.TRUE.
8 NABWF=NABWF+1
C A UND B DER GERADENSTUECKE BERECHNEN.
      IF(NABWF.GT.MABWF) GOTO 5
      IF(REFE(I).LT.REFE(I-1)) CALL FSWR03(3001,'FSTR','U3 ',2)
      ABWF(NABWF,1)=REFE(I)
      Q=1.0/(REFE(I)-REFE(I-1))
      ABWF(NABWF,2)=(RFFE(I)-EFE(I-1))*Q
      ABWF(NABWF,3)=(EFE(I-1)*REFE(I)-EFE(I)*REFE(I-1))*Q
      ABWF(NABWF,4)=1.0
      IF(ABWF(NABWF,2).NE.0.0.OR.ABWF(NABWF,3).NE.0.0) GOTO 9
      ABWF(NABWF,4)=0.0
      GCTC 10
9 Y1=EFE(I-1)
      IF(NABWF.EQ.2) Y1=ABWF(2,2)*ABWF(1,1)+ABWF(2,3)
      Y2=EFE(I)
      IF(Y1*Y2.LT.0.0) ABWF(NABWF,4)=-1.0
10 IF(TEST2.AND..NOT.FINBED) WRITE(NO,1000) NABWF,(ABWF(NABWF,J),J=1,
      *4)
5 IF(FINBED) GOTO 7
      I=I+1
      IF(I.LE.NFE) GOTO 4
C KEIN REFE(I) WAR >= 0GR.
C FSTCLE(REFE(NFE),0GR,GLSCH) GLEICH .TRUE. WIRD ZUGELASSEN.
C ANDERNFALLS FEHLER.
      IF(FSTCLE(REFE(NFE),0GR,GLSCH)) GOTO 7
      CALL FSWR07(3015,'LAST',' ',REFE(NFE),'LT.','UPPE','R ',0GR)
      GCTC 888
7 IF(NABWF.LE.MABWF) GOTO 330
      *ABWF=NABWF-MABWF
      RETURN 1
330 ABWF(NABWF,1)=0GR
      ABWF(NABWF,4)=1.0
      IF(ABWF(NABWF,2).EQ.0.0.AND.ABWF(NABWF,3).EQ.0.0)CALL FSWR03(3001,
      *'FSTR','U3 ',3)
      Y1=ABWF(NABWF,2)*ABWF(NABWF-1,1)+ABWF(NABWF,3)
      Y2=ABWF(NABWF,2)*ABWF(NABWF,1) +ABWF(NABWF,3)
      IF(Y1*Y2.LT.0.0) ABWF(NABWF,4)=-1.0
      IF(TEST2) WRITE(NO,1000) NABWF,(ABWF(NABWF,J),J=1,4)
333 RETURN
      END

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		SC8N1=SG8N01	52C
		SC8T1=RTCT/RPHI	53C
		IF(ISPATE.EQ.1) SG8F=RFISS/RPHI	540
		SIGA=FSSNGL(SC8A)	550
		SIGN=FSSNGL(SG8N)	56C
		SIGN01=FSSNGL(SG8N01)	570
		SIGN1=FSSNGL(SG8N1)	580
		SIGT1=FSSNGL(SG8T1)	590
		SIGF=FSSNGL(SG8F)	60C
	10	CCONTINUE	610
	2C	F-FAKTOREN BILDEN.	620
	3C	BFI VORKOMMENDEN DIVISIONEN DURCH NULL WIRD DER F-FAKTOR	63C
	40	GLEICH 1.0 GESETZT.	640
	5C		650
	60	IF(LERMSG) GOTC 34	660
	7C	DC 33 J=1,6	670
	80	LFAR1(J)=.FALSE.	680
	90	LFAR2(J)=.FALSE.	690
	100	LFARIA(J)=.FALSE.	700
	110	LFAR2A(J)=.FALSE.	710
	120	33 CONTINUE	720
	13C	34 CC 12 I=1,MI	730
	140	J=C	740
	150	13 J=J+1	750
	160	IF(J.EQ.1.OR.LERMSG) GOTC 41	760
	17C	IF(.NOT.LFAR1A(J-1)) GOTC 42	770
	180	CALL FSWR03(2017,HELP4,FARIAN(J-1),SIGO(I-1))	78C
	190	LFAR1(J-1)=.FALSE.	790
	200	LFARIA(J-1)=.FALSE.	800
	210	42 IF(.NOT.LFAR2A(J-1)) GOTC 41	81C
	220	CALL FSWR03(2018,HELP4,FAR2AN(J-1),SIGO(I-1))	820
	230	LFAR2(J-1)=.FALSE.	830
	24C	LFAR2A(J-1)=.FALSE.	840
	250	41 IF(J.GT.6) GOTC 12	850
	26C	IF(J.EQ.3.AND.ISPATE.EQ.1) J=J+1	86C
	27C	HFLP1=SG8A-SG8F	870
	280	IF(J.NE.1.OR.ISPATE.EQ.C) GOTC 14	880
	290	HFLP4=TF(7)	890
	300	IF(HELP1.NE.0.0.AND.RF(I,1).NE.0.0) GOTC 15	900
	310	IF(LERMSG) GOTC 37	91C
	320	IF(LFAR1(J)) GOTC 13	920
	330	LFAR1(J)=.TRUE.	93C
	340	FARIAN(J)=SIGC(I)	940
	350	GOTC 13	950
	36C	37 CALL FSWR02(2014,HFLP4,SIGO(I))	96C
	370	18 CALL FSWR06(-1014,RF(I,6),RF(I,1),RF(I,8),RF(I,1),SIGA,SIGF)	970
	380	GOTC 13	98C
	390	15 HELP2=RF(I,6)-RF(I,8)	990
	400	IF(.NOT.LERMSG.AND.LFAR1(J)) LFAR1A(J)=.TRUE.	1000
	410	FFAKT(I,1)=FSSNGL((HELP2/RF(I,1))/HELP1)	101C
	420	IF(HELP2.EQ.0.0) GOTC 45	1020
	43C	IF(.NOT.LERMSG.AND.LFAR2(J)) LFAR2A(J)=.TRUE.	103C
	44C	GOTC 13	1040
	45C	45 IF(LERMSG) GOTC 38	1050
	460	IF(LFAR2(J)) GOTC 13	106C
	47C		
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	50C		
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LFAR2(J)=.TRUE.
FAR2AN(J)=SIGO(I)
GCTC 13
38 CALL FSWRO2(2016,HELP4,SIGO(I))
GOTO 18
14 HELP4=TF(J)
GOTO (21,22,23,24,25,26),J
CALL FSWRO3(3001,'FSTR','U4 ',2)
21 HELP1=RF(I,6)
HELP3=SG8A
GCTC 16
22 HELP1=RF(I,7)
HELP3=SG8N
GOTO 16
23 HELP1=RF(I,8)
HELP3=SG8F
GCTC 16
24 HELP1=RF(I,3)
HELP3=SG8N01
16 HELP2=RF(I,1)
GCTC 30
25 HELP1=RF(I,5)
HELP3=SG8N1
GCTC 17
26 HELP1=RF(I,4)
HELP3=SG8T1
17 HELP2=RF(I,2)
30 HELP23=HELP2*HELP3
IF(HELP23.NE.0.0) GOTO 31
IF(LERMSG) GOTO 39
IF(LFAR1(J)) GOTO 13
LFAR1(J)=.TRUE.
FAR1AN(J)=SIGO(I)
GCTC 13
39 CALL FSWRO2(2014,HELP4,SIGO(I))
32 CALL FSWRO3(-1013,HELP1,HELP2,HELP3)
GOTO 13
31 FFAKT(I,J)=FSSNGL(HELP1/HELP23)
IF(.NOT. LERMSG.AND. LFAR1(J)) LFAR1A(J)=.TRUE.
IF(HELP1.EQ.0.0) GOTO 44
IF(.NOT. LERMSG.AND. LFAR2(J)) LFAR2A(J)=.TRUE.
GOTO 13
44 IF(LERMSG) GOTO 40
IF(LFAR2(J)) GOTO 13
LFAR2(J)=.TRUE.
FAR2AN(J)=SIGC(I)
GCTC 13
40 CALL FSWRO2(2016,HELP4,SIGO(I))
GOTO 32
12 CCNTINUE
IF(LERMSG) GOTO 35
CG 36 J=1,6
HELP4=TF(J)
IF(J.EQ.1.AND.ISPATE.NE.0) HELP4=TF(7)
IF(LFAR1(J)) CALL FSWRO3(2017,HELP4,FAR1AN(J),SIGO(MI))

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IF(LFAR2(J)) CALL FSWRO3(2018,HELP4,FAR2AN(J),SIGC(MI))
36 CCNTINUE
C AUSTRUCK UND AUSSCHREIBEN DER GRUPPENQUERSCHNITTE UND F-FAKTOREN.
C FUER IDUR=0 UND IGR=NANF 1. RECORD SCHREIBEN.
35 IF(IDUR.LT.0) CALL FSWRO3(3001,'FSTR','U4 ',3)
IF(IDUR.GT.0.OR.IGR.NE.NANF) GOTO 3
NN=0
WRITE(JA) NN,STRK
IF(TFST2) CALL FSWRC1(1005,JA)
3 CCNTINUE
NN=5
C AUSGABE DER MITTLEREN QUERSCHNITTE.
IGRINT=NE-IGR
TF(IGRINT.LT.1) CALL FSWRO3(3001,'FSTR','U4 ',4)
WRITE(JA) NN,MAT,IGRINT,UGR,0GR
IF(ISPATE.EQ.1) GOTO 4
IF(ISPATE.NE.0) CALL FSWRO3(3001,'FSTR','U5 ',4)
NN=5
WRITE(JA) NN,SIGA,SIGN,SIGN01,SIGN1,SIGT1
WRITE(NOUTP,1000) SIGA,SIGN,SIGN01,SIGN1,SIGT1
1000 FCRMAT('0',22X,'SIGMA A',11X,'SIGMA N',10X,'SIGMA NC1',9X,
*'SIGMA N1',10X,'SIGMA T1'//16X,5E18.8)
GCTC 5
4 SG8C=SG8A-SG8F
SIGC=SG8C
NN=6
WRITE(JA) NN,SIGC,SIGA,SIGF,SIGN01,SIGN1,SIGT1
WRITE(NOUTP,1001) SIGC,SIGN,SIGF,SIGN01,SIGN1,SIGT1
1001 FCRMAT('0',22X,'SIGMA C',11X,'SIGMA N',11X,'SIGMA F',10X,
*'SIGMA N01',9X,'SIGMA N1',10X,'SIGMA T1'//16X,6E18.8)
5 CCNTINUE
C F-FAKTOREN AUSGEBEN.
IF(ISPATE.EQ.1) GOTO 6
IF(ISPATE.NE.0) CALL FSWRO3(3001,'FSTR','U4 ',6)
WRITE(NOUTP,1002)
1002 FCRMAT('0',5X,'SIGO',15X,'FA',16X,'FN',16X,'FAC1',14X,'FN1',15X,
*'FT1'/)
LRJ=2
GCTC 7
6 WRITE(NOUTP,1003)
1003 FORMAT('0',5X,'SIGO',15X,'FC',16X,'FN',16X,'FF',14X,'FAC1',14X,
*'FN1',15X,'FT1'/)
LRJ=3
7 CCNTINUE
NN=LRJ+4
CC 8 I=1,MI
WRITE(JA) NN,SIGO(I),(FFAKT(I,J),J=1,LRJ),(FFAKT(I,J),J=4,6)
WRITE(NOUTP,1004) SIGO(I),(FFAKT(I,J),J=1,LRJ),(FFAKT(I,J),J=4,6)
1004 FCRMAT(F16.8,6E18.8)
8 CONTINUE
333 RETURN
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FUNCTION FSSNGL(A)
C TRUNCATION OF THE REAL*8 NUMBER A TO THE REAL*4 VALUE FSSNGL.
C IF NECESSARY ROUNDING UP IS DONE.
REAL*8 A,AL
LOGICAL*1 L(8),LE(4)
DIMENSION FL(2)
EQUIVALENCE (AL,FL(1),L(1)),(LE(1),E),(FL(2),I)
DATA 01/Z00000001/
AL=A
FSSNGL=FL(1)
IF(1.GE.0) GOTO 333
E=D1
LE(1)=L(1)
FSSNGL=FSSNGL+E
333 RETURN
END

SUBROUTINE FSTRU5(A1,NA1,MA1,A2,NA2,MA2,MA2P,*)
C DER INHALT DES FELDDES A1 WIRD IN DAS FELD A2 UMGESPEICHERT.
C WENN DIE DIMENSION NICHT AUSREICHT, WIRD MA2P > C GESETZT
C UND RETURN 1 GEMACHT.
C
DIMENSION A1(MA1,4),A2(MA2,4)
IF(NA1.GT.MA2) GOTO 773
NA2=NA1
DO 1 I=1,NA2
DO 1 J=1,4
1 A2(I,J)=A1(I,J)
322 RETURN
773 MA2P=NA1-MA2
RETURN 1
END

SUBROUTINE FSQUER(TYP,UGR,OGR,NAB,MAB,AB,MABP,*,*)
C VON DEM QUERSCHNITTSTYP TYP DES MATERIALS MAT WERDEN VON UGR BIS
C OGR IN DEM FELD AB DIE ENTSPRECHENDEN GERADENSPEZIFIKATIONEN
C ABGESPEICHERT.
C REICHT DIE FELDLAENGE NICHT AUS, SO WIRD MABP>C GESETZT
C UND RETURN 1 GEMACHT.
C BEI FEHLERN IN DEN DATEN AUF KEINER WIRD RETURN 2 GEMACHT.
C
REAL*8 TYP,MAT,ARG3,BEST,TYPL,TYPSGT,TYPSGN,TYPSGA,TYPSGF
LOGICAL*4 TEST1,TEST2,TEST3,LERMSG,FSTOLE,INSERT,FIRST,PRINT,
*FELCCN
DIMENSION AB(MAB,4),IARG2(4),ARG3(5),ETYPL(2),EMAT(2)
EQUIVALENCE (ETYPL(1),TYPL),(EMAT(1),MAT)
DATA BEST/'BEST',TYPSGT,TYPSGN,TYPSGA,TYPSGF/'SGT',
*'SGN','SGA','SGF'/'
COMMON MAT,NRI(2),NU

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COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH
TYPL=TYP
INSERT=.FALSE.
IF(UGR.GE.OGR.OR.MAB.LT.2) CALL FSWRO3(3001,'FSQU','ER',1)
IGEL=ZAHL DER VON DER LIBRARY GELESFENEN PUNKTE.
ICFL=0
C IAKZ=ZAHL DER AKZEPTIERTEN PUNKTE. IAKZ<=IGEL.
IAKZ=0
C 1. PUNKT DES QUERSCHNITTS HCLFA.
IARG2(1)=3
ARG3(1)=MAT
ARG3(2)=BEST
ARG3(3)=TYP
IRC=0
CALL NDFLOC(IRC,IARG2,ARG3,ARG4,ARG5)
IF(IRC.NE.1) CALL FSWRO3(3001,'FSQU','ER',2)
IF(IARG2(2).NE.1.OR.IARG2(3).NE.1.OR.IARG2(4).NE.C) CALL FSWROO(30
*C1)
ENERGA=ARG3(4)
QUERA=ARG3(5)
IGEL=IGEL+1
IF(TEST2) CALL FSWRC7(1011,'FIRS',EMAT(1),EMAT(2),ETYPL(1),ETYPL(2
*),ENERGA,QUERA)
(1,) MIT DUMMY WERTEN FUELEN.
AB(1,1)=UGR
AB(1,2)=-999999.0
AB(1,3)=-999999.0
AB(1,4)=-999999.0
NAB=1
C LAGE VON UGR UND OGR BEZUEGLICH DER VON DER LIBRARY GELESFENEN
C PUNKTE. (= BEDEUTET IMMER GLEICHHEIT IM SINNE VON TOLERANT.)
C IFALL BEDEUTUNG AKTION
C 10 1.G.D.P.(1.GELESENER DATENPUNKT) WEITERE DATENPUNKTE
<=UGR. NOCH KEINE INFORMATION EINLESEN.
UEBER OGR.
C 11 WIE 10. ZUSAETZLICH 1.G.D.P. WARNUNG DRUCKEN. Q.S. VOM
(LFTZTER GELESENER DATENPUNKT) 1.G.D.P. VON UGR BIS UGR
<=UGR. VERWENDEN. RETURN.
C 12 WIE 10. ZUSAETZLICH 1.G.D.P. NORMALFALL. SUBROUTINE
>=OGR. ABSCHLIESSEN. RETURN.
C 13 WIE 10. ZUSAETZLICH 1.G.D.P. WARNUNG DRUCKEN. Q.S. VOM
ZWISCHEN UGR UND OGR LIEGEND. 1.G.D.P. BIS OGR VERWENDEN
RETURN.
C 20 1.G.D.P. >= OGR. NOCH KEINE WARNUNG DRUCKEN. Q.S. VOM
INFORMATION UEBER OGR. 1.G.D.P. VON UGR BIS OGR
VERWENDEN. RETURN.
C 30 1.G.D.P. ZWISCHEN UGR UND OGR. WEITERE DATENPUNKTE
SONST NOCH KEINE INFORMATION. EINLESEN.
C 31 WIE 30. ZUSAETZLICH 1.G.D.P. FEHLER AUF LIBRARY.
<=UGR. FEHLERDRUCK. RETURN 2.
C 32 WIE 30. ZUSAETZLICH 1.G.D.P. Q.S. VOM 1.G.D.P. VON UGR
>=OGR. BIS ZUR ENERGIIE DES
1.G.D.P. VERWENDEN. DANN
NORMAL WEITER. RETURN.
C 33 WIE 30. ZUSAETZLICH 1.G.D.P. Q.S. VOM 1.G.D.P. UND

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C	ZWISCHEN UGR UND OGR LIEGEND.	L.G.D.F. IN DEM BEREICH	720	106	NAB=NAB+1	1270
C		VERWENCEN, WO KEINF	730		IF(NAB.GT.MAB) GCTO 330	1280
C		DATEN VERHANDEN SIND.	740		AB(NAB,1)=OGR	1290
C		SONST NORMAL. RETURN.	750		AB(NAB,2)=0.0	1300
C	IFALL SETZEN.		760		AB(NAB,3)=QUERN	1310
	IFALL=0		770		AB(NAB,4)=0.0	1320
	IF(ENERGA.LT.UGR.OR.FSTCLE(ENERGA,UGR,GLSCH)) GOTO 10		780		IF(AB(NAB,3).NE.0.0) AB(NAB,4)=1.0	1330
	IF(ENERGA.GT.OGR.OR.FSTOLE(ENERGA,CGR,GLSCH)) GCTO 20		790		GCTO 330	1340
C	IFALL=30		800	105	CCNTINUE	1350
20	IFALL=30		810	C	IFALL=11	1360
	GOTO 100		820		IFALL=11	1370
10	IFALL=10		830		CALL FSWR07(1011,' LAS',EMAT(1),EMAT(2),ETYPL(1),ETYPL(2),	1380
	GCTO 100		840		*ENERGN,QUERN)	1390
20	IFALL=20		850		CALL FSWR04(-2013,QUERN,' UGR',UGR,OGR)	1400
	IAKZ=IAKZ+1		860		GCTO 106	1410
	IF(.NOT.TEST2) CALL FSWR07(1011,' FIRS',EMAT(1),EMAT(2),		870	104	CCNTINUE	1420
	*ETYPL(1),ETYPL(2),ENERGA,QUERA)		880	C	(IFALL=30). VERGLEICHE L.G.D.P. MIT UGR UND CGR.	1430
	CALL FSWR04(2013,QUERA,' UGR',UGR,CGR)		890		IF(ENERGA.LT.UGR.OR.FSTOLE(ENERGA,UGR,GLSCH)) GOTO 107	1440
	NAB=NAB+1		900		IF(ENERGA.GT.CGR.OR.FSTCLE(ENERGA,CGR,GLSCH)) CALL FSWR03(3001,	1450
	IF(NAB.GT.MAB) CALL FSWR03(3001,'FSQU','ER ',3)		910		*'FSQU','ER ',6)	1460
	AB(NAB,1)=OGR		920	C	IFALL=33	1470
	AB(NAB,2)=0.0		930		IFALL=33	1480
	AB(NAB,3)=QUERA		940		GOTO 116	1490
	AB(NAB,4)=0.0		950	C	IFALL=31	1500
	IF(AB(NAB,3).NE.0.0) AB(NAB,4)=1.0		960		IFALL=31	1510
	GCTO 330		970	107	IFALL=31	1520
C	WEITERE DATENPUNKTE EINLESEN.		980		CALL FSWR04(3017,EMAT(1),EMAT(2),ETYPL(1),ETYPL(2))	1530
100	QUERN=QUFRA		990	102	CCNTINUE	1540
	ENFRGN=ENERGA		1000		ENERGN=ARG3(4)	1550
	IF(IFALL.EQ.30) INSERT=.TRUE.		1010		QLFRN=ARG3(5)	1560
101	ENERGA=ENERGN		1020		ICEL=IGEL+1	1570
	CLERA=QUERN		1030		IF(TEST3) CALL FSWR02(1012,ENERGA,QUERN)	1580
	IRC=0		1040	C	PRUEFUNG OB ENERGIEN ANSTEIGEN.	1590
	CALL NDFNXT(IRC,IARG2,ARG3,ARG4,ARG5)		1050		IF(ENERGN.GT.ENERGA) GCTO 108	1600
C	ENDE DER DATEN DES BETREFFENDEN TYPS ERREICHT?		1060		CALL FSWR04(3017,EMAT(1),EMAT(2),ETYPL(1),ETYPL(2))	1610
	IF(IRC.EQ.1) GOTO 102		1070		GCTO 773	1620
	IF(FSTCLE(ENERGA,OGR,GLSCH)) GOTO 113		1080	108	CCNTINUE	1630
C	KEIN PUNKT DES BETREFFENDEN QUERSCHNITTS MEHR VERHANDEN.		1090	C	PUNKT EINFUEGEN?	1640
C	IGEL MUSS >= 2 SEIN.		1100		IF(INSERT) GOTO 109	1650
	IF(IGEL.LT.2) CALL FSWR05(3016,EMAT(1),EMAT(2),ETYPL(1),		1110	C	ENERGN > UGR ?	1660
	*ETYPL(2),IGEL)		1120		IF(ENERGN.LT.UGR.OR.FSTOLE(ENERGN,UGR,GLSCH)) GCTO 101	1670
	IF(IGEL.LT.2) GOTO 773		1130		IF(ENERGA.LT.UGR.OR.FSTCLE(ENERGA,UGR,GLSCH)) GCTO 110	1680
	IF(IFALL.EQ.10) GOTO 103		1140		CALL FSWR04(3017,EMAT(1),EMAT(2),ETYPL(1),ETYPL(2))	1690
	IF(IFALL.EQ.30) GOTO 104		1150		GCTO 773	1700
	CALL FSWR03(3001,'FSQU','ER ',4)		1160	110	INSERT=.TRUE.	1710
103	CCNTINUE		1170	109	IAKZ=IAKZ+1	1720
	(IFALL=13). VERGLEICHE L.G.D.P. MIT UGR UND CGR.		1180	C	GERADE BERECHNEN.	1730
	IF(ENERGA.LT.UGR.OR.FSTOLE(ENERGA,UGR,GLSCH)) GOTO 105		1190		NAB=NAB+1	1740
	IF(ENERGA.GT.OGR.OR.FSTCLE(ENERGA,CGR,GLSCH)) CALL FSWR03(3001,		1200		IF(NAB.GT.MAB) GCTO 111	1750
	*'FSQU','ER ',5)		1210		AB(NAB,1)=ENERGN	1760
C	IFALL=13		1220		C=1.0/(ENERGN-ENERGA)	1770
	IFALL=13		1230		AB(NAB,2)=(QUERN-QUERA)*C	1780
116	CALL FSWR07(1011,' LAS',EMAT(1),EMAT(2),ETYPL(1),ETYPL(2),		1240		AB(NAB,3)=(QUERA*ENFRGN-QUERN*ENERGA)*C	1790
	*ENERGA,QUERA)		1250		AB(NAB,4)=1.0	1800
	CALL FSWR04(-2013,QUERN,' ER',ENERGA,CGR)		1260		IEND=1	1810

114	IF(AB(NAB,2).NE.0.0.OR.AB(NAB,3).NE.0.0) GOTO 112	1820	773	RETURN 2	237C
	AB(NAB,4)=0.0	1830		END	2380
	CCTO 111	1840			
112	Y1=QUFRA	1850			
	IF(NAB.EQ.2) Y1=AB(2,2)*AB(1,1)+AB(2,3)	1860			
	Y2=QUERN	1870			
	IF(IEND.EQ.2) Y2=AB(NAB,2)*AB(NAB,1)+AB(NAB,3)	1880			
	IF(Y1*Y2.LT.0.0) AB(NAB,4)=-1.0	1890			
111	IF(IEND.EQ.2) GOTO 115	1900		SLBRoutine FSWR00(N)	10
C	ENFRGN >= OGR ?	1910	C	DRUCKT MELDUNGEN, WARNUNGEN UND FEHLERMELDUNGEN.	20
	IF(ENERGN.LT.OGR) GOTO 101	1920	C	N=1 NULLSETZEN VON FELARR.	30
113	IF(NAB.GT.MAB) GOTO 115	1930	C	1000+1 <= N <= 1000+NMMAX MELDUNGEN.	40
	AP(NAB,1)=OGR	1940	C	2000+1 <= N <= 2000+NMMAX WARNUNGEN.	50
	IFAD=2	1950	C	3000+1 <= N <= 3000+NEMAX FEHLER.	60
	CCTO 114	1960	C		70
115	IF(TEST3) WRITE(ND,1001) IGEL,IAKZ	1970		INTEGER FELARR	80
1001	FORMAT(' SUBROUTINE FSQUER. IGEL=',I6,' IAKZ=',I6,'.')	1980		DIMENSION FELARR(18,3)	90
330	IF(.NOT.TEST3) GOTO 332	1990		COMMON NRI(4),NC	100
	DO 331 I=1,NAB	2000		COMMON/CFSTRF/ FELARR,NGMAX	110
	WRITE(NO,1000) I,(AB(I,J),J=1,4)	2010	999	CONTINUE	120
1000	FCRMA(' AB: I=',I5,' E=',IPE13.6,' EV A=',IPE13.6,' B=',	2020		NIN=N	130
	*IPE13.6,' AB(I,4)=',IPE12.4,'.')	2030		NMMAX=15	140
331	CONTINUE	2040		NWMAX=18	150
332	CONTINUE	2050		NEMAX=17	160
C	BEI NAB .GT. MAB KEINE PRUEFUNG DER QUERSCHNITTE AUF C ODER < 0.	2060	C	NGMAX=MAXO(NMMAX,NWMAX,NEMAX)	170
	IF(NAB.GT.MAB) GOTO 77C	2070		VRSCHUB NUR, WENN N>0.	180
C	FUER TYP=SGT,SGN,SGA,SGF TEST OB NEGATIV ODER =C.	2080		IF(ININ.GT.0) WRITE(ND,1000)	190
C	BEI SGT NEGATIV ODER GLEICH 0 WARNUNGS AUSDRUCK UND FEHLERSTOP.	2090	1000	FCRMA(' '	200
C	SONST NUR WARNUNGS AUSDRUCK.	2100		NIN=IABS(NIN)	210
	IF(TYP.NE.TYPSGT.AND.TYP.NE.TYPSGN.AND.TYP.NE.TYPSGA.AND.	2110	C	TYP DER MELDUNG.	220
	*TYP.NE.TYPSGF) GOTO 329	2120		ITYP=0	230
	FIRST=.TRUE.	2130		IF(ININ.EQ.1) ITYP=4	240
	PRINT=.FALSE.	2140		IF(ININ.GE.1001.AND.NIN.LE.(1000+NMMAX)) ITYP=1	250
	FELCON=.FALSE.	2150		IF(ININ.GE.2001.AND.NIN.LE.(2000+NMMAX)) ITYP=2	260
	CO 120 I=2,NAB	2160		IF(ININ.GE.3001.AND.NIN.LE.(3000+NEMAX)) ITYP=3	270
	IF(AB(I,4).GT.0.0) GOTO 121	2170		IF(ITYP.EQ.0) GOTO 770	280
	PRINT=.TRUE.	2180	C	TYPVERTFILER.	290
	FELCON=.TRUE.	2190		GC TO(1,2,3,4),ITYP	300
	IF(FIRST) GOTO 122	2200			
123	BE=AB(I,1)	2210		GOTO 770	310
	GC TO 120	2220	1	NI=NIN-1000	320
122	BA=AB(I-1,1)	2230	C	M E L D U N G E N . LABELS 1001, 1002, ...	330
	FIRST=.FALSE.	2240	C	FORMATSTATEMENTS 11001, 11002, ...	340
	GC TO 123	2250		FELARR(NI,1)=FELARR(NI,1)+1	350
121	IF(.NOT.PRINT) GOTO 120	2260		CALL FSWRS1(NI,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8,IV9,8770)	360
	PRINT=.FALSE.	2270			
	CALL FSWR06(2015,EMAT(1),EMAT(2),ETYPL(1),ETYPL(2),PA,BE)	2280		GOTO 333	370
120	CONTINUE	2290	2	NI=NIN-2000	380
	IF(PRINT) CALL FSWR06(2015,EMAT(1),EMAT(2),ETYPL(1),ETYPL(2),BA,BE	2300	C	W A R N U N G E N . LABELS 2001, 2002, ...	390
	*)	2310	C	FORMATSTATEMENTS 12001, 12002, ...	400
	IF(FELCON.AND.TYP.EQ.TYPSGT) GOTO 773	2320		FELARR(NI,2)=FELARR(NI,2)+1	410
329	IF(NAB.GT.MAB) GOTO 770	2330		CALL FSWRS2(NI,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8,IV9,8770)	420
333	RETURN	2340		GOTO 333	430
77C	MAB=NAB-MAB	2350	3	NI=NIN-3000	440
777	RETURN 1	2360	C	F E H L E R . LABELS 3001, 3002, ...	450
			C	FORMATSTATEMENTS 13001, 13002, ...	460
				FELARR(NI,3)=FELARR(NI,3)+1	470
				CALL FSWRS3(NI,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8,IV9,8770,8773)	480
				GOTO 333	490

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C      NULLSETZEN VON FELARR.
4      CC 6 I=1,NGMAX
      DC 6 J=1,3
      6 FELARR(I,J)=0
      GCTC 333
333    RETURN
C      NICHT DEFINIERTE NACHRICHTENNUMMER.
770    NULL=0
      WRITE(NO,3000) NULL
3000   FCRMAT('O***  ERROR 3.',I2)
      WRITE(NO,771) N,NMMAX,NkMAX,NEMAX
771    FCRMAT('+',16X,' PROGRAM OR MACHINE ERROR IN FSWRCC. N HAS THE VA
*LLI',I12,'.'/'
*' ',16X,' BUT IT MUST BE IN ONE OF THE FOLLOWING INTERVALS:/'
*' ',16X,' 1001 TO 1000+',I4/
*' ',16X,' 2001 TO 2000+',I4/
*' ',16X,' 3001 TO 3000+',I4)
773    WRITE(NO,772)
772    FCRMAT('O',120('**')/' ',45('**'),' PROGRAM STOP ',
*45('**')/' ',120('**'))
777    STCP
      ENTRY FSWR01(N,IV1)
      GCTC 999
      ENTRY FSWR02(N,IV1,IV2)
      GCTC 999
      ENTRY FSWR03(N,IV1,IV2,IV3)
      GCTC 999
      ENTRY FSWR04(N,IV1,IV2,IV3,IV4)
      GCTC 999
      ENTRY FSWR05(N,IV1,IV2,IV3,IV4,IV5)
      GCTC 999
      ENTRY FSWR06(N,IV1,IV2,IV3,IV4,IV5,IV6)
      GCTC 999
      ENTRY FSWR07(N,IV1,IV2,IV3,IV4,IV5,IV6,IV7)
      GCTC 999
      ENTRY FSWR08(N,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8)
      GCTC 999
      ENTRY FSWR09(N,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8,IV9)
      GCTC 999
      END

      SUBROUTINE FSWRS1(NI,IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8,IV9,*)
      COMMON NRI(4),NO
C      * E L D U N G E N . LABELS 1001, 1002, ...
C      FCRMATSTATEMENTS 11001, 11002, ...
      WRITE(NO,1000) NI
1000   FCRMAT(' *** MESSAGE 3.',I2)
      GOTO (1001,1002,1003,1004,1005,1006,1007,1008,1009,1010,1011,1012,
*1013,1014,1015
*) ,NI
      GCTC 770
1001   WRITE(NO,11001) IV1,IV2

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11001 FCRMAT('+',16X,' PROGRAMM KENNZIFFER 3' /
* ' ',16X,' _____' /
*'0',16X,' PROGRAMM ZUR BERECHNUNG VON RESONANZSELBSTABSCHIRMFAKTO
*REN VON PUNKTWEISF GEGEBENEN' /
*' ',16X,' WIRKUNGSQUERSCHNITTEN FLUR CAS MATERIAL ',2A4,'.'/' )
      GCTC 333
1002   WRITE(NO,11002) IV1
11002   FORMAT('+',16X,' PROGRAM 3 HAS ENDED CORRECTLY. KL HAS THE VALUE=
*' ,I4,'.'')
      GOTO 333
1003   WRITE(NO,11003)
11003   FORMAT('+',16X,' AFTER CHANGING ARRAY DIMENSICNS PROGRAM WILL BE
*CALLED ONCE MCRE.'')
      GCTC 333
1004   WRITE(NO,11004)
11004   FCRMAT('+',16X,' PROGRAM-CONTROL-DATA HAVE BEEN CHECKED. NO ERROR
* S FOUND.'')
      GCTC 333
1005   IF(IV1.LT.10) WRITE(NO,11005) IV1
11005   FORMAT('+',16X,' FIRST RECORD WRITTEN ON FT',I1,'FOO1.'')
      IF(IV1.GT.10) WRITE(NO,21005) IV1
21005   FORMAT('+',16X,' FIRST RECORD WRITTEN ON FT',I2,'FOO1.'')
      GCTC 333
1006   WRITE(NO,11006)
11006   FCRMAT('+',16X,' ALL CROSS SECTION TYPES NEEDED FOR THE FOLLOWING
* CALCULATIONS FOUND ON KEDAK.'')
      GCTC 333
1007   WRITE(NO,11007)
11007   FORMAT('+',16X,' INTEGRATION BOUNDARIES AND ASSOCIATED VALUES FOR
* ONE GROUP HAVE BEEN DEFINED.'')
      GCTC 333
1008   WRITE(NO,11008)
11008   FCRMAT('+',16X,' INTEGRATION OF THE FUNCTION(S)')
      IF(IV1.LT.1.OR.IV1.GT.9) IV1=1
      GCTC (1,2,3,4,5,6,7,8,9),IV1
1      WRITE(NO,12008)
      GCTC 10
2      WRITE(NO,13008)
      GCTC 10
3      WRITE(NO,14008)
      GCTC 10
4      WRITE(NO,15008)
      GCTC 10
5      WRITE(NO,16008)
      GCTC 10
6      WRITE(NO,17008)
      GCTC 10
7      WRITE(NO,18008)
      GCTC 10
8      WRITE(NO,19008)
      GCTC 10
9      WRITE(NO,20008)
      GCTC 10
12008 FCRMAT('+',51X,'F(E)')
13008 FCRMAT('+',51X,' * F(E)')

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14008 FCRMAT('+',51X,'SGN * MUEL * F(E)')
15008 FCRMAT('+',51X,'1.0 / (SGT + SIGO) * F(E)')
16008 FCRMAT('+',51X,'1.0 / ((SGT + SIGO)**2) * F(E)')
17008 FCRMAT('+',51X,' / (SGT + SIGO) * F(E)')
18008 FCRMAT('+',51X,'SGT / ((SGT + SIGO)**2) * F(E)')
19008 FCRMAT('+',51X,'SGN * MUEL / (SGT + SIGO) * F(E)')
20008 FCRMAT('+',51X,'SGN * MUEL / ((SGT + SIGO)**2) * F(E)')
10 IF(IV1.NE.2.AND.IV1.NE.6) GOTO 11
IF(IV2.EQ.1) WRITE(ND,21008)
IF(IV2.EQ.2) WRITE(ND,22008)
IF(IV2.EQ.3) WRITE(ND,23008)
IF(IV2.EQ.4) WRITE(ND,24008)
21008 FCRMAT('+',51X,'SGT')
22008 FCRMAT('+',51X,'SGA')
23008 FCRMAT('+',51X,'SGN')
24008 FCRMAT('+',51X,'SGF')
11 IF(IV1.GE.4) WRITE(ND,26008) IV3,IV4
26008 FCRMAT(31X,'( FIRST SIGO=',1PE12.6,' LAST SIGO=',1PE12.6,' )')
GOTO 333
1009 WRITE(ND,11009) IV1,IV2,IV3,IV4,IV5,IV6,IV7,IV8,IV9
11009 FCRMAT('+',56X,'EXACT PCRTICN',13X,' INACCURATE PCRTICNS'/
*' ',60X,' YF(2)',16X,' YF(1)',12X,' YF(3)'/
*' ',16X,' VALUE ',32X,1PE13.6,8X,1PE13.6,4X,1PE13.6/
*' ',16X,' VALUE IN % OF YF(1)+YF(2)+YF(3) ',10X,0PF6.2,15X,
*0PF6.2,7X,0PF6.2/
*' ',16X,' RELATIVE ERROR BETTER OR EQUAL THAN ',2X,1PE13.6,
*8X,1PE13.6,4X,1PE13.6)
GOTO 333
1010 WRITE(ND,11010) IV1,IV2,IV3,IV4,IV5,IV6
11010 FCRMAT('+',16X,' ',A3,A4,' WEIGHTED INTEGRAL FRCM=',1PE13.6,
*' EV TO=',1PE13.6,' EV OF REACTION TYPE ',A3,'=',1PE12.6,'.')
GOTO 333
1011 WRITE(ND,11011) IV1,IV2,IV3,IV4,IV5,IV6,IV7
11011 FCRMAT('+',16X,' ',A4,' T PCINT FOR MATERIAL ',2A4,' CROSS SECTION
* TYPE ',2A4,' HAS BEEN READ.'/' ',16X,' E(1)=',1PE13.6,' EV Q(1)
*=',1PE13.6,' BARN.')
GOTO 333
1012 WRITE(ND,11012) IV1,IV2
11012 FCRMAT('+',16X,' E=',1PE13.6,' EV C=',1PE13.6,' BARN.')
GOTO 333
1013 WRITE(ND,11013) IV1,IV2,IV3
11013 FCRMAT('+',16X,' TERM TO CALCULATE WAS: ',
*1PE13.6,' / (',1PE13.6,'**',1PE13.6,').')
GOTO 333
1014 WRITE(ND,11014) IV1,IV2,IV3,IV4,IV5,IV6
11014 FCRMAT('+',16X,' TERM TO CALCULATE WAS: '/
*' ',16X,' (',1PE13.6,' /',1PE13.6,' -',1PE13.6,' /',1PE13.6,
*' ) / (',1PE13.6,' -',1PE13.6,')')
GOTO 333
1015 WRITE(ND,11015) IV1,IV2,IV3
11015 FCRMAT('+',16X,' RESULT FRCM=',1PE13.6,' EV TC=',1PE13.6,
*' EV IS=',1PE13.6,'.')
GOTO 333
333 RETURN
77C RETURN 1
END

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1170
1180
1190
1200
1210
1220

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```

SLBRCUTINE FSWRS2(NI, IV1, IV2, IV3, IV4, IV5, IV6, IV7, IV8, IV9, *)
COMMON NR1(4),NO
C W A R N U N G E N . LABELS 2001, 2002, ...
C FCRMATSTATEMENTS 12001, 12002, ...
WRITE(ND,2000) NI
2000 FCRMAT(' *** WARNING 3.',I2)
GOTO ( 2001,2002,2003,2004,2005,2006,2007,2008,2009,2010,2011,2012,
*2C13,2014,2015,2C16,2017,2018
*),NI
GOTO 770
2001 WRITE(ND,12001) IV1,IV2
12001 FCRMAT('+',16X,' FOR GROUP NUMBER',I4,' NO CALCULATIONS CAN BE DO
*NE. IT IS THE GROUP WITH THE LOWER BOUNDARY IN THE'/
*' ',16X,' THERMAL REGION. THE GROU NUMBER FOR WHICH THE CALCULAT
*ICNS WILL START IS SET TO',I4,'.')
GOTO 333
2002 WRITE(ND,12002) IV1,IV2,IV3
12002 FCRMAT('+',16X,' THE GROUP NUMBER',I4,' IS OUTSIDE THE GROUP STRU
*CTURE DEFINED BY THE',I4,' GROUP BOUNCARIES.'/
*' ',16X,' THE GROUP NUMBER FOR WHICH THE CALCULATIONS WILL START
*IS SET TO',I4,'.')
GOTO 333
2003 WRITE(ND,12003) IV1,IV2
12003 FCRMAT('+',16X,' ADDITIONALLY THE GROUP NUMBER FOR WHICH THE CALC
*ULATIONS SHOULD END IS SET TO',I4,'.'/
*' ',16X,' BECAUSE IT HAS BEEN GREATER THAN',I4,'.')
GOTO 333
2004 WRITE(ND,12004)
12004 FCRMAT('+',16X,' IN ROMBERG INTEGRATION DESIRED ACCURACY COULD NO
*T BE REACHED BECAUSE OF ROUNDING ERRORS.'/
*' ',16X,' APPROXIMATION TAKEN AND OTHER INFORMATION IS PRINTED IN
* THE FOLLOWING.')
GOTO 333
2005 WRITE(ND,12005) IV1,IV2
12005 FCRMAT('+',16X,' FROM=',1PE13.6,
*' EV TO=',1PE13.6,' EV HAS BEEN GIVEN THE RESULT ZERO BECAUSE')
GOTO 333
2006 WRITE(ND,12006)
12006 FCRMAT('+',16X,' THE POINTWISE GIVEN WEIGHTING SPECTRUM IS ZERO I
*N THE GIVEN INTEGRATION RANGE.')
GOTO 333
2007 WRITE(ND,12007)
12007 FCRMAT('+',16X,38X,' IS COMPLETELY ZERO IN THE GIVEN INTEGRATION R
*ANGE.')
10 IF(IV1.EQ.3) WRITE(ND,13007)
IF(IV1.EQ.1.AND.IV2.GT.3) WRITE(ND,14007)
IF(IV1.EQ.2.AND.IV2.GT.3) WRITE(ND,15007)
IF(IV1.EQ.1.AND.IV2.LE.3) WRITE(ND,16007)
IF(IV1.EQ.2.AND.IV2.LE.3) WRITE(ND,17007)
13007 FCRMAT('+',23X,'THE FUNCTION IN THE DENOMINATOR')
14007 FCRMAT('+',19X,'THE FIRST FUNCTION IN THE NUMEFATOR')

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15007 FCRMAT('+',18X,'THE SECCND FUNCTION IN THE NUMERATOR')	520	GOTO 333	1070
16007 FORMAT('+',36X,'THE FIRST FUNCTION')	530	333 RETURN	1080
17007 FORMAT('+',35X,'THE SECCND FUNCTION')	540	770 RETURN 1	1090
GCTO 333	550	END	1100
2008 WRITE(NO,12008)	560		
12008 FCRMAT('+',54X,' CHANGES THE SIGN IN THE GIVEN INTEGRATION RANGE.')	570		
GCTO 10	580		
2009 WRITE(NO,12009)	590		
12009 FCRMAT('+',16X,' ADDITIONALLY/' ',54X,' IS COMPLETELY ZERO IN TH	600		
* THE GIVEN INTEGRATION RANGE.')	610		
GCTO 10	620	SUBROUTINE FSWRS3(NI, IV1, IV2, IV3, IV4, IV5, IV6, IV7, IV8, IV9, *, *)	10
2010 WRITE(NO,12010)	630	COMMON NR1(4),NO	20
12010 FORMAT('+',16X,' ADDITIONALLY/' ',54X,' CHANGES THE SIGN IN THE G	640	C F E L L E R . LABELS 3001, 3002, ...	30
* IVEN INTEGRATION RANGE.')	650	C FORMAT STATEMENTS 13001, 13002, ...	40
GCTO 10	660	WRITE(NO,3000) NI	50
2011 WRITE(NO,12011) IV1	670	3000 FCRMAT(' *** ERROR 3.',12)	60
12011 FCRMAT('+',16X,' THE RESULT MAY BE INACCURATE. WISHED RELATIVE ER	680	GOTO (3001,3002,3003,3004,3005,3006,3007,3008,3009,3010,3011,3012,	70
*RCR=' ',1PE13.6,'.')	690	*3013,3014,3015,3016,3017	80
GCTO 333	700	*) ,NI	90
2012 WRITE(NO,12012)	710	GCTO 770	100
12012 FCRMAT('+',16X,' THE AVERAGE GROUP CROSS SECTIONS FOR INFINITE DI	720	3001 WRITE(NO,13001) IV1, IV2, IV3	110
*LUTION ARE SET TO ZERO BECAUSE/' ',16X,' THE INTEGRAL OF THE WEI	730	13001 FORMAT('+',16X,' PROGRAM- OR MACHINE-ERROR IN SUBROUTINE ',	120
*GHTING FUNCTION IS ZERO IN THE GIVEN INTEGRATION RANGE.')	740	*A4,A2,' TESTPCINT',I4,'.')	130
GCTO 333	750	GCTO 773	140
2013 WRITE(NO,12013) IV1, IV2, IV3, IV4	760	3002 WRITE(NO,13002)	150
12013 FCRMAT('+',16X,' THIS CROSS-SECTION VALUE (',1PE13.6,	770	13002 FORMAT('+',16X,' THE PROGRAM CONTROL DATA CR THE DATA GIVEN IN KE	160
*' BARN) WILL BE TAKEN FROM',A4,'=',1PE13.6,' EV TC DGR=',	780	*DAK CR IN THE WEIGHTING SPECTRUM'/	170
*1PE13.6,' EV.')	790	*' ',16X,' WILL NOT ALLOW CALCULATION OF AVERAGE GROUP CROSS SECTI	180
GCTO 333	800	*CNS FOR INFINITE DILUTION AND OF'/	190
2014 WRITE(NO,12014) IV1, IV2	810	*' ',16X,' ENERGY RESONANCE SELF SHIELDING FACTORS FROM ENERGY POI	200
12014 FCRMAT('+',16X,' THE SELF SHIELDING FACTOR ',A4,' (SIGO=',	820	*NT WISE DATA IN THE RESONANCE REGION.')	210
*1PE13.6,') HAS BEEN SET TO 1.0,/'	830	GCTO 333	220
*' ',16X,' BECAUSE IN CALCULATING THIS FACTOR A DIVISION BY ZERO H	840	3003 WRITE(NO,13003) IV1, IV2	230
*AD TO BE DONE.')	850	13003 FCRMAT('+',16X,' THE NUMBER OF THE FIRST GROUP=',I4,	240
GCTO 333	860	*' FOR WHICH CALCULATIONS SHOULD BE DONE IS LESS'/	250
2015 WRITE(NO,12015) IV1, IV2, IV3, IV4, IV5, IV6	870	*' ',16X,' THAN THE NUMBER OF THE LAST GROUP=',I4,'.')	260
12015 FORMAT('+',16X,' FOR MATERIAL ',2A4,' THE CROSS SECTION TYPE ',	880	GCTO 333	270
*2A4,' IS LESS OR EQUAL ZERO AT LEAST'/	890	3004 WRITE(NO,13004) IV1, IV2	280
*' ',16X,' IN SOME PARTS OF THE ENERGY RANGE ',1PF13.6,	900	13004 FCRMAT('+',16X,' IN THE CASE OF ONE AND ONLY ONE ENERGY SPECTRUM	290
*' EV UNTIL ',1PE13.6,' EV.')	910	*ENBER(1) HAS THE VALUE ',1PE14.6,'.)/	300
GCTO 333	920	*' ',16X,' BUT IT MUST BE EQUAL -1.0 OR GREATER OR EQUAL ',1PF14.6	310
2016 WRITE(NO,12016) IV1, IV2	930	*,.')	320
12016 FCRMAT('+',16X,' THE SELF SHIELDING FACTOR ',A4,' (SIGO=',	940	GCTO 333	330
*1PE12.6,') HAS BEEN CALCULATED AS ZERO, BECAUSE')	950	3005 WRITE(NO,13005) IV1	340
GCTO 333	960	13005 FORMAT('+',16X,' ERRANDUES ENERGY GROUP BOUNDARIES IN GRUP',	350
2017 WRITE(NO,12017) IV1, IV2, IV3	970	*I5,'.')	360
12017 FORMAT('+',16X,' THE SELF SHIELDING FACTOR(S) ',A4,	980	GOTO 333	370
*' FROM SIGO=',1PE12.6,' TO SIGO=',1PE12.6)	990	3006 WRITE(NO,13006) IV1, IV2, IV3	380
WRITE(NO,13017)	1000	13006 FCRMAT('+',16X,' IN THE',I3,'. WEIGHTING SPECTRUM RANGE ABSOLUTE	390
13017 FCRMAT(' ',16X,' HAVE BEEN SET TO 1.0, BECAUSE IN CALCULATING TH	1010	*VALUE OF ACTUELL NFTYP=',I3/' ',16X,' IS GREATER THAN THE MAXIMUM	400
*S FACTORS, DIVISION(S) BY ZERO HAD TO BE DONE.')	1020	* POSSIBLE VALUE MNFTYP=',I3,'.')	410
GCTO 333	1030	GOTO 333	420
2018 WRITE(NO,12018) IV1, IV2, IV3	1040	3007 WRITE(NO,13007) IV1	430
WRITE(NO,12018)	1050	13007 FCRMAT('+',16X,' IN THE',I3,'. WEIGHTING SPECTRUM RANGE A POINTWIS	440
12018 FCRMAT(' ',16X,' HAVE BEEN CALCULATED AS ZERO.')	1060	*E SPECTRUM WAS WISHED.)/' ',16X,	450
		*' NO SUCH SPECTRUM HAS BEEN MADE AVAILABLE TO THE PROGRAM.')	460
		GOTO 333	470


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3008 WRITE(NO,13008) IV1,IV2,IV3,IV4 480
13008 FORMAT('+',16X,' NO DATA FOUND FOR MATERIAL ',2A4,' TYP ',2A4,'.' 490
*) 500
GOTO 333 510
3009 WRITE(NO,13009) IV1,IV2, IV3, IV4, IV5,IV6 520
13009 FORMAT('+',16X,' THE VARIABLE ',A4,A2,' HAS THE VALUE ',I12,'./' 530
*' ',16X,' BUT IT MUST BE ',A4,' ',A4,' ',I12,'.'') 540
GOTO 333 550
3010 WRITE(NO,13010) IV1,IV2, IV3, IV4, IV5,IV6 560
13010 FORMAT('+',16X,' THE VARIABLE ',A4,A2,' HAS THE VALUE ',IPE14.6,' 570
*' ',16X,' BUT IT MUST BE ',OPA4,' ',A4,' ',IPE14.6,'.'') 580
GOTO 333 590
3011 WRITE(NO,13011) IV1,IV2,IV3, IV4, IV5, IV6,IV7 600
13011 FORMAT('+',16X,' THE ARRAY ELEMENT ',A4,A2,'( ',I5,' ) HAS THE VALU 610
*' ',I12,'.'/' ',16X,' BUT IT MUST BE ',A4,' ',A4,' ',I12,'.'') 620
GOTO 333 630
3012 WRITE(NO,13012) IV1,IV2,IV3, IV4, IV5, IV6,IV7 640
13012 FORMAT('+',16X,' THE ARRAY ELEMENT ',A4,A2,'( ',I5,' ) HAS THE VALU 650
*' ',IPE14.6,'.'/' ',16X,' BUT IT MUST BE ',CPA4,' ',A4,' ', 660
*'IPE14.6,'.'') 670
GOTO 333 680
3013 WRITE(NO,13013) IV1,IV2,IV3,IV4, IV5 690
13013 FORMAT('+',16X,' THE VARIABLE ',A4,A2,' HAS THE VALUE ',I12,'./' 700
*' ',16X,' BUT IT MUST BE EQUAL ',I2,' OR EQUAL ',I2,'.'') 710
GOTO 333 720
3014 WRITE(NO,13014) IV1,IV2 730
13014 FORMAT('+',16X,' THE PCINTWISE WEIGHTING SPECTRUM IS NOT DEFINED 740
*'IN THE ENERGY RANGE ',IPE14.6,' EV TO ',IPE14.6,' EV.'') 750
GOTO 333 760
3015 WRITE(NO,13015) IV1,IV2,IV3,IV4,IV5,IV6,IV7 770
13015 FORMAT('+',16X,' THE ',A4,A1,' ENERGY POINT OF THE PCINTWISE WEIG 780
*TING SPECTRUM ='',IPE14.6,' EV IS ',A4,' THAN THE ',A4,A1/ 790
*' ',16X,' BOUNDARY OF THE INTEGRATION RANGE ='',IPE14.6,' EV.'') 800
GOTO 333 810
3016 WRITE(NO,13016) IV1,IV2,IV3,IV4,IV5 820
13016 FORMAT('+',16X,' FOR MATERIAL ',2A4,' CROSS SECTION TYPE ', 830
*2A4,' ONLY ',I1,' PCINT(S) HAVE BEEN FOUND ON THE LIBRARY.'/ 840
*' ',16X,' ERRANDEUS LIBRARY ') 850
GOTO 333 860
3017 WRITE(NO,13017) 870
13017 FORMAT('+',16X,' LIBRARY HAS BEEN FOUND ERRANCFUS. CHECK LIBRARY. 880
*) 890
GOTO 333 900
333 RETURN 910
770 RETURN 1 920
773 RETURN 2 930
END 940

SUBROUTINE FSWRS9 10
C AUSDRUCK VON FELARR. 20
LOGICAL*4 TEST1,TEST2,TEST3,LERMSG,PRINT 30
INTEGER FELARR 40
DIMENSION FELARR(18,3) 50

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COMMON NRI(4),NO 60
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG 70
COMMON/CFSTRF/ FELARR,NGMAX 80
DC 1 I=1,NGMAX 90
DO 1 J=2,3 100
IF(FELARR(I,J).EQ.0) GOTO 1 110
GOTO 3 120
1 CONTINUE 130
WRITE(NO,1000) 140
1000 FORMAT('0ND WARNING- OR ERROR-MESSAGES PRODUCED IN MODULE FSTRUK.' 150
*) 160
330 IF(.NOT.TEST1.AND..NOT.TEST2.AND..NOT.TEST3) GOTO 333 170
WRITE(NO,1001) 180
1001 FORMAT('0TABLE OF MESSAGES PRODUCED OR PRINTED IN MODULE FSTRUK.'/ 190
*'0MESSAGE NUMBER CCOUNT'/) 200
DC 2 I=1,NGMAX 210
IF(FELARR(I,1).EQ.0) GOTO 2 220
IP=I+1000 230
WRITE(NO,1002) IP,FELARR(I,1) 240
1002 FORMAT(' ',5X,I4,7X,I4) 250
2 CONTINUE 260
333 RETURN 270
3 PRINT=.TRUE. 280
DC 4 I=1,NGMAX 290
IF(FELARR(I,2).EQ.0) GOTO 4 300
IF(.NOT.PRINT) GOTO 6 310
WRITE(NO,1006) 320
1006 FORMAT(IHI) 330
CALL RAMANF(NC) 340
CALL ABFORM(NO,'WARNINGS') 350
CALL ABFORM(NC,'PRODUCEC') 360
CALL RAMEND(NO) 370
WRITE(NO,1003) 380
1003 FORMAT('0TABLE OF WARNINGS PRINTED IN MODULE FSTRUK.'/ 390
*'0WARNING NUMBER COUNT'/) 400
PRINT=.FALSE. 410
6 IP=I+2000 420
WRITE(NO,1002) IP,FELARR(I,2) 430
4 CONTINUE 440
PRINT=.TRUE. 450
DC 5 I=1,NGMAX 460
IF(FELARR(I,3).EQ.0) GOTO 5 470
IF(.NOT.PRINT) GOTO 7 480
WRITE(NO,1006) 490
CALL RAMANF(NO) 500
CALL ABFORM(NO,' ERRORS ') 510
CALL ABFORM(NC,'PRODUCED') 520
CALL RAMEND(NO) 530
WRITE(NO,1004) 540
1004 FORMAT('0',I20('**')/' ',46('**'),' ERRORS IN MODULE FSTRUK. ', 550
*46('**')/' ',I20('**')/ 560
*'0TABLE OF ERRORS PRINTED IN MODULE FSTRUK.'/ 570
*'0ERROR NUMBER COUNT.'/ 580
PRINT=.FALSE. 590
7 IP=I+3000 600

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```

WRITE(NO,1005) IP,FELARR(I,3)
1005 FORMAT(' ',4X,I4,6X,I4)
5 CONTINUE
GOTO 330
END

```

```

LOGICAL FUNCTION FSTOLE(A,B,GLSCH)
C A TOLERANT ( AUSDRUCK NACH VORSCHLAG VON G. WILLERDING ) B
C GENAU DANN WENN
C 1) A=B
C ODER
C 2) ABS((A-B)/AMAX1(ABS(A),ABS(B))) <= GLSCH
C WENN A TOLERANT B IST, HAT FSTOLE DEN WERT .TRUE. ANDERNFALLS
C DEN WERT .FALSE.
C DIE RELATION IST SYMMETRISCH, D.H. A TOLERANT B GENAU DANN WENN
C B TOLERANT A IST.
C
IF(A.EQ.B) GOTO 2
IF(ABS((A-B)/AMAX1(ABS(A),ABS(B)))<=GLSCH) GOTO 2
1 FSTOLE=.FALSE.
GOTO 333
2 FSTOLE=.TRUE.
333 RETURN
END

```

```

SUBROUTINE FSXINT(NXINT,MXINT,XINT,MXINTP,NV,V,ID1,ID2,*)
C DIE WERTE V(J,1),J=1,NV, WELCHE DER BEDINGUNG
C XINT(I) <= V(J,1) <= XINT(MXINT)
C GEFUEGEN, WERDEN IN XINT EINGEFUEGT.
C (DIE WERTE IN V MUESSEN GROESSER GLEICH 0.0 SEIN, SOWIE
C UND EINE AUFSTIEGENDE REIHENFOLGE HABEN.)
C WERTE IN V, DIE NICHT BEI WERTEN IN XINT LIEGEN, WERDEN
C NICHT UEBERNOMMEN.
C WIRD NXINT > MXINT SO WIRD MXINTP GESETZT UND RETURN 1 GEMACHT.
C NXINT MUSS BEI FINE# FSXINT AUFRUF IMMER >= 2 SEIN. D.H. ES MUSS
C VORHER EIN FSXIN AUFRUF GEMACHT WORDEN SEIN.
LOGICAL*4 FSTOLE,TEST1,TEST2,TEST3,LFRMSG
DIMENSION XINT(1),V(ID1,ID2)
COMMON NR1(4),NO
CC#MGN/CFSTRU/ TEST1,TEST2,TEST3,LFRMSG,GLSCH
C
IF(NXINT.GT.MXINT.OR.MXINT.LT.1.OR.NV.LT.1.OR.NXINT.LT.2.OR.
*XINT(1).GE.XINT(NXINT)) CALL FSWR03(3001,'FSXI','NT ',1)
I = LOOPINDEX IN XINT.

```

610
620
630
640
65C

1C
20
30
4C
50
60
7C
80
9C
100
110
120
130
14C
150
160
17C
180

10
20
30
40
5C
60
7C
80
90
10C
110
12C
130
140
150
160
170
180
190

```

C J = LOOPINDEX IN V.
I=1
J=1
C TEST VON V(J,1).
10 IF(V(J,1).LT.0.0) CALL FSWR03(3001,'FSXI','NT ',2)
IF(J.LE.1) GOTO 2
IF(V(J,1).LT.V(J-1,1)) CALL FSWR03(3001,'FSXI','NT ',3)
2 CONTINUE
C VERGLEICHE V(J,1) MIT XINT(I)
IF(FSTOLE(V(J,1),XINT(I),GLSCH)) GOTO 11
IF(V(J,1).GT.XINT(I)) GOTO 12
C V(J,1) IST KLEINER ALS XINT(I). WENN I GROESSER ALS 1, WERT
C EINFUEGEN UND J HOCHZAEHLEN.
C FUER I=1 NUR J HOCHZAEHLEN.
13 IF(I.LE.1) GOTO 23
NXINT=NXINT+1
IF(NXINT.GT.MXINT) GOTO 88
I=I+1
DO 3 II=I,NXINT
3 XINT(NXINT+I-II)=XINT(NXINT+I-II-1)
XINT(I-1)=V(J,1)
23 J=J+1
IF(J.LE.NV) GOTO 10
C ALLE WERTE EINGEFUEGT. RETURN.
330 IF(TEST2) WRITE(NO,1000) NXINT,(XINT(II),I=1,NXINT)
1000 FORMAT('INTEGRATIONSINTERVALS: NXINT=',I6,'.*/
*(' ',IP5E14.6,6X))
333 RETURN
C FELD XINT ZU KLEIN.
88 MXINTP=NV-J+1
888 RETURN 1
11 CONTINUE
V(J,1) GLEICH XINT(I). J HOCHZAEHLEN.
GOTO 23
12 CONTINUE
V(J,1) GROESSER ALS XINT(I). I HOCHZAEHLEN.
I=I+1
C WENN I > NXINT WIRD, SIND ALLE WERTE <= XINT(NXINT) EINGEFUEGT.
C RETURN.
IF(I.LE.NXINT) GOTO 10
GOTO 330
ENTRY FSXIN(NXINT,MXINT,XINT,UGR,OGR)
INITIALISIERUNGSENTRY. DAS FELD XINT WIRD GLEICH -1.0 GESETZT.
XINT(1) WIRD GLEICH UGR UND XINT(2) WIRD GLEICH OGR GESETZT.
UGR MUSS KLEINER ALS OGR SEIN.
NXINT GIBT AN, WIE WEIT DAS FELD GEFUELLT IST. ES WIRD GLEICH 2
GESETZT.
IF(UGR.GE.OGR.OR.FSTOLE(UGR,OGR,GLSCH).OR.MXINT.LT.3)
*CALL FSWR03(3001,'FSXI','NT ',4)
XINT(1)=UGR
XINT(2)=OGR
NXINT=2
DO 1 II=3,MXINT
1 XINT(II)=-1.0
GOTO 330
END

```

200
210
220
23C
240
25C
260
270
28C
290
30C
310
32C
33C
340
35C
360
370
380
390
40C
410
420
430
440
45C
460
470
480
49C
50C
510
52C
530
540
55C
560
57C
580
59C
600
610
62C
630
64C
650
660
67C
680
69C
700
71C
720
73C
740
750

```

SLBRoutine FSGRAL(RFSULT,NXINT,XINT,NABWF,ABWF,MARWF, 1C
* NABQ1,ABQ1,MARQ1,NABQ2,ABQ2,MABQ2,NABQ3,ABQ3,MABQ3, 20
* KMROM,AUXRCM,KMROMP,EPSROM,CRINWA, 30
* IFAR,LFAR,LFARA,FARIN,FARAN,IFUNAR,*,*) 40
C INTEGRATION EINER FUNKTION ENTSPRECHEND ITYP. 50
ITYP INTEGRAL VCN 60
C 1 PHI 70
C 2 F1 * PHI 80
C 3 F1*F2 * PHI 90
C 4 1/F3 * PHI 100
C 5 1/F3**2 * PHI 110
C 6 F1/F3 * PHI 120
C 7 F1/F3**2 * PHI 130
C 8 F1*F2/F3 * PHI 140
C 9 F1*F2/F3**2 * PHI 150
C PHI IST DURCH ABWF BZW. FORMELMAESSIG ODER ALS FUNKTION - JE NACH 160
WFRT VCN NFTYP - GEGEBEN. 170
C F1, F2 UND F3 SIND DURCH ABQ1, ABQ2 BZW. ABQ3 GEGEBEN. 180
C DURCHFUEHRUNG DER INTEGRATION IN DEN INTERVALLEN 190
C XINT(I-1) ... XINT(I) MIT I=2,NXINT. 200
C RETURN 1 WIRD GEMACHT, WENN KMROM VERGROESSERT WERDEN MUSS. 210
C DANN IST KMROMP GROSSER ALS 0. 220
C RETURN 2 WIRD GEMACHT, WENN SGT <= 0 FESTGESTELLT WIRD. 230
C 240
EXTERNAL DPHI,FSNU01,FSNU02,FSNU03,FSNU04,FSNU05,FSNU06,FSNU07, 250
*FSNU08,FSNU09,FSANO2,FSANO3,FSANC4,FSANO5,FSANC6,FSANO7, 260
*FSANO8,FSANO9 270
LOGICAL*4 TEST1,TEST2,TEST3,SPRUC,FSGRA1,FSTOLE,CRUCK,CRUCKL, 280
* SPRU3,LERMSG,LFAR(2,3),LFARA(2,3) 290
REAL*8 RFSULT,Y,FSNU01,FSNU02,FSNU03,FSNU04,FSNU05,FSNU06,FSNU07, 300
*FSNU08,FSNU09,FSANO2,FSANO3,FSANC4,FSANO5,FSANC6,FSANO7,FSANO8, 310
*FSANO9 320
DIMENSION XINT(1),ABWF(MABWF,4),ABQ1(MABQ1,4),AEC2(MABQ2,4), 330
* ABQ3(MABQ3,4),AUXRCM(1),YF(3),YFP(3),FARIN(2,3,2), 340
* FARAN(2,3),IFUNAR(2,3),YFEPS(3) 350
COMMON NR1(4),AC 360
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH,MNFTYP,NFTYP,ITYP, 370
* ITYPFU,NR2(3), AW,BW,A1,B1,A2,B2,A3,B3,BSIGO, 380
* XIA,XIE,L,Y,ACIMP,CRUCKL 390
C FEHLFRABFRAGEN. 400
IF(ITYP.LT.1.OR.ITYP.GT.9.OR.NXINT.LT.2) CALL FSWR03(3001, 410
*'FSGR','AL ',1) 420
C STEUERGRÖSSEN FUER INTEGRALBERECHNUNG IM TESTFALL DRUCKEN. 430
IF(TEST3) WRITE(NO,100) NFTYP,XINT(1),NXINT,XINT(NXINT) 440
100 FORMAT('0SUBROUTINE FSGRAL. NFTYP=',I3, 450
*' XINT(1)=' ,1PE13.6,' NXINT=',OPI6,' XINT(NXINT)=' , 460
*'1PE13.6,'. ') 470
IF(TEST3) CALL FSWR04(1008,ITYP,ITYPFU,BSIGO,BSIGO) 480
C RESULT GLEICH NULL SETZEN. 490
RESULT=0.0 500
C PCINTER FUER PUNKTWEISE FUNKTIONEN SETZEN. 510

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IABWF=2 520
IABQ1=2 530
IABQ2=2 540
IABQ3=2 550
C SETZEN VON ANFANGSWERTEN FUER A UND B. 560
AW=ABWF(IABWF,2) 570
BW=ABWF(IABWF,3) 580
A1=ABQ1(IABQ1,2) 590
B1=ABQ1(IABQ1,3) 600
A2=ABQ2(IABQ2,2) 610
B2=ABQ2(IABQ2,3) 620
A3=ABQ3(IABQ3,2) 630
B3=ABQ3(IABQ3,3) 640
C ANFANGSWERTE FUER FEHLERDRUCKSTEUERUNG BEI FSROMB FEHLERN. 650
DRUCKL=.FALSE. 660
DRUCK=.FALSE. 670
C ANFANGSWERTE FUER MIKROINTEGRALWERT UND YF UND YFEPS. 680
Y=0.0 690
DO 53 I=1,3 700
YF(I)=0.0 710
53 YFEPS(I)=0.0 720
C FEHLERTEST 730
IF(ABS(NFTYP).GT.MNFTYP) CALL FSWR03(3001,'FSGR','AL ',2) 740
BEI NUMERISCHER INTEGRATION FSROMB INITIALISIEREN. 750
IF(NFTYP.LE.0) CALL FSR0MI(EPSROM,KMROM,DRINWA,YF,YFEPS,AUXROM) 760
C SETZEN VON IGRIAR. 770
GOTO (1000,2000,3000,4000,5000,6000,7000,8000,9000),ITYP 780
CALL FSWR03(3001,'FSGR','AL ',3) 790
1000 CONTINUE 800
IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 1901 810
IF(NFTYP.EQ.1) GOTO 1910 820
IF(NFTYP.EQ.2) GOTO 1920 830
IF(NFTYP.EQ.-1) GOTO 1902 840
CALL FSWR03(3001,'FSGR','AL ',4) 850
1901 ASSIGN 1001 TO IGRIAR 860
GOTO 9 870
1902 ASSIGN 1002 TO IGRIAR 880
GOTO 9 890
1910 ASSIGN 1010 TO IGRIAR 900
GOTO 9 910
1920 ASSIGN 1020 TO IGRIAR 920
GOTO 9 930
2000 CONTINUE 940
IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 2901 950
IF(NFTYP.EQ.1) GOTO 2910 960
IF(NFTYP.EQ.2) GOTO 2920 970
IF(NFTYP.EQ.-1) GOTO 2902 980
CALL FSWR03(3001,'FSGR','AL ',5) 990
2901 ASSIGN 2001 TO IGRIAR 1000
GOTO 9 1010
2902 ASSIGN 2002 TO IGRIAR 1020
GOTO 9 1030
2910 ASSIGN 2010 TO IGRIAR 1040
GOTO 9 1050
2920 ASSIGN 2020 TO IGRIAR 1060

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GOTO 9
3000 CCNTINUE
      IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 3901
      IF(NFTYP.EQ.1) GOTO 3910
      IF(NFTYP.EQ.2) GOTO 3920
      IF(NFTYP.EQ.-1) GOTO 3902
      CALL FSWR03(3001,'FSGR','AL ',6)
3901 ASSIGN 3001 TO IGRIAR
      GOTO 9
3902 ASSIGN 3002 TO IGRIAR
      GOTO 9
3910 ASSIGN 3010 TO IGRIAR
      GOTO 9
3920 ASSIGN 3020 TO IGRIAR
      GOTO 9
4000 CCNTINUE
      IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 4901
      IF(NFTYP.EQ.1) GOTO 4910
      IF(NFTYP.EQ.2) GOTO 4920
      IF(NFTYP.EQ.-1) GOTO 4902
      CALL FSWR03(3001,'FSGR','AL ',7)
4901 ASSIGN 4001 TO IGRIAR
      GOTO 9
4902 ASSIGN 4002 TO IGRIAR
      GOTO 9
4910 ASSIGN 4010 TO IGRIAR
      GOTO 9
4920 ASSIGN 4020 TO IGRIAR
      GOTO 9
5000 CONTINUE
      IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 5901
      IF(NFTYP.EQ.1) GOTO 5910
      IF(NFTYP.EQ.2) GOTO 5920
      IF(NFTYP.EQ.-1) GOTO 5902
      CALL FSWR03(3001,'FSGR','AL ',8)
5901 ASSIGN 5001 TO IGRIAR
      GOTO 9
5902 ASSIGN 5002 TO IGRIAR
      GOTO 9
5910 ASSIGN 5010 TO IGRIAR
      GOTO 9
5920 ASSIGN 5020 TO IGRIAR
      GOTO 9
6000 CCNTINUE
      IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 6901
      IF(NFTYP.EQ.1) GOTO 6910
      IF(NFTYP.EQ.2) GOTO 6920
      IF(NFTYP.EQ.-1) GOTO 6902
      CALL FSWR03(3001,'FSGR','AL ',9)
6901 ASSIGN 6001 TO IGRIAR
      GOTO 9
6902 ASSIGN 6002 TO IGRIAR
      GOTO 9
6910 ASSIGN 6010 TO IGRIAR
      GOTO 9

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6520 ASSIGN 6020 TO IGRIAR
      GOTO 9
7000 CCNTINUE
      IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 7901
      IF(NFTYP.EQ.1) GOTO 7910
      IF(NFTYP.EQ.2) GOTO 7920
      IF(NFTYP.EQ.-1) GOTO 7902
      CALL FSWR03(3001,'FSGR','AL ',10)
7901 ASSIGN 7001 TO IGRIAR
      GOTO 9
7902 ASSIGN 7002 TO IGRIAR
      GOTO 9
7910 ASSIGN 7010 TO IGRIAR
      GOTO 9
7920 ASSIGN 7020 TO IGRIAR
      GOTO 9
8000 CCNTINUE
      IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 8901
      IF(NFTYP.EQ.1) GOTO 8910
      IF(NFTYP.EQ.2) GOTO 8920
      IF(NFTYP.EQ.-1) GOTO 8902
      CALL FSWR03(3001,'FSGR','AL ',11)
8901 ASSIGN 8001 TO IGRIAR
      GOTO 9
8902 ASSIGN 8002 TO IGRIAR
      GOTO 9
8910 ASSIGN 8010 TO IGRIAR
      GOTO 9
8920 ASSIGN 8020 TO IGRIAR
      GOTO 9
9000 CONTINUE
      IF(NFTYP.EQ.0.OR.NFTYP.LE.-2) GOTO 9901
      IF(NFTYP.EQ.1) GOTO 9910
      IF(NFTYP.EQ.2) GOTO 9920
      IF(NFTYP.EQ.-1) GOTO 9902
      CALL FSWR03(3001,'FSGR','AL ',12)
9901 ASSIGN 9001 TO IGRIAR
      GOTO 9
9902 ASSIGN 9002 TO IGRIAR
      GOTO 9
9910 ASSIGN 9010 TO IGRIAR
      GOTO 9
9920 ASSIGN 9020 TO IGRIAR
      GOTO 9
C      LCCP UEBER ALLE INTERVALLF.
      9 XIE=XINT(1)
        I=1
        I=I+1
        IF(I.GT.NXINT) GOTO 3
        XIA=XIE
        XIE=XINT(I)
      8 SFRUO=.FALSF.
        XIEF=-1.0E+10
        IF(XIA.GE.XIE) CALL FSWR03(3001,'FSGR','AL ',13)
C      PUNKTWEISE WICHTUNGSFUUNKTION ?

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IF(IABS(NFTYP).NE.1) GOTO 4
C EVENTUELL POINTER FUER ABWF HOCHZAEHLEN.
IF(XIE.LE.ABWF(IABWF,1)) GOTO 52
IABWF=IABWF+1
IF(IABWF.GT.NABWF) CALL FSWR03(3001,'FSGR','AL ',14)
AW=ABWF(IABWF,2)
BW=ABWF(IABWF,3)
52 IF(FSGRA1(ABWF,IABWF,MABWF,XIA,XIE)) CALL FSWR03(3001,
*'FSGR','AL ',15)
C WICHTUNGSFUNKTION = 0 ?
IF(ABWF(IABWF,4).NE.0.0) GOTO 4
C SPRUNGEEDINGUNG SETZEN. XIEE AUF ABWF(IABWF,1) SETZEN. WARNUNG
C DRUCKEN. I HOCHZAEHLEN.
IF(.NOT.FSTOLE(ABWF(IABWF-1,1),XIA,GLSCH)) CALL FSWR03(3001,
*'FSGR','AL ',16)
SPRUO=.TRUE.
XIEE=ABWF(IABWF,1)
CALL FSWR03(2005,ITYP,XIA,XIEE)
CALL FSWR03(-2006)
4 CCNTINUE
C PRUEFUNG DER "QUERSCHNITTSGERADEN" ENTSPRECHEND IITYP.
IF(IITYP.EQ.1) GOTO 5
IF(IITYP.EQ.2) GOTO 10
IF(IITYP.EQ.3) GOTO 20
IF(IITYP.GE.4.AND.IITYP.LE.9) GOTO 30
CALL FSWR03(3001,'FSGR','AL ',17)
30 CCNTINUE
C FUNKTION F3.
CALL FSGRA2(3,ABQ3,IABQ3,MABQ3,NABQ3,XIA,XIE,XIEE,SPRUO,SPRU3,
*IFAR,LFAR,LFARA,FARIN,FARAN,IFUNAR,.TRUE.)
IF(SPRU3) GOTO 777
IF(IITYP.EQ.6.OR.IITYP.EQ.7) GOTO 10
IF(IITYP.EQ.4.OR.IITYP.EQ.5) GOTO 5
20 CCNTINUE
C FUNKTION F2.
CALL FSGRA2(2,ABQ2,IABQ2,MABQ2,NABQ2,XIA,XIE,XIEE,SPRUO,SPRU3,
*IFAR,LFAR,LFARA,FARIN,FARAN,IFUNAR,.FALSE.)
10 CCNTINUE
C FUNKTION F1.
CALL FSGRA2(1,ABQ1,IABQ1,MABQ1,NABQ1,XIA,XIE,XIEE,SPRUO,SPRU3,
*IFAR,LFAR,LFARA,FARIN,FARAN,IFUNAR,.TRUE.)
5 CCNTINUE
C WENN KEIN FEHLER, MIT INTEGRALBERECHNUNG BEGINNEN.
C ANDERNFALLS I UND ENTSPRECHENDE IAB.. HOCHZAEHLEN UND ZUM
C SCHLEIFENENDE SPRINGEN.
IF(.NOT.SPRUO) GOTO 6
C I HOCHZAEHLEN.
7 I=I+1
IF(I.GT.XINT) GOTO 3
IF(XINT(I).LT.XIEE.OR.FSTOLE(XINT(I),XIEE,GLSCH)) GOTO 7
XIA=XINT(I-1)
XIE=XINT(I)
C IAB HOCHZAEHLEN
IF(IITYP.EQ.1) GOTO 41
IF(IITYP.EQ.2) GOTO 11

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IF(IITYP.EQ.3) GOTO 21
IF(IITYP.GE.4.AND.IITYP.LE.9) GOTO 31
CALL FSWR03(3001,'FSGR','AL ',18)
31 CCNTINUE
IABQ3 HOCHZAEHLEN.
CALL FSGRA3(ABQ3,IABQ3,MABQ3,NABQ3,XIA,XIE)
A3=ABQ3(IABQ3,2)
R3=ABQ3(IABQ3,3)
IF(IITYP.EQ.6.OR.IITYP.EQ.7) GOTO 11
IF(IITYP.EQ.4.OR.IITYP.EQ.5) GOTO 41
21 CCNTINUE
IABQ2 HOCHZAEHLEN
CALL FSGRA3(ABQ2,IABQ2,MABQ2,NABQ2,XIA,XIE)
A2=ABQ2(IABQ2,2)
B2=ABQ2(IABQ2,3)
11 CCNTINUE
IABQ1 HOCHZAEHLEN
CALL FSGRA3(ABQ1,IABQ1,MABQ1,NABQ1,XIA,XIE)
A1=ABQ1(IABQ1,2)
B1=ABQ1(IABQ1,3)
41 CCNTINUE
IF(IABS(NFTYP).NE.1) GOTO 8
IABWF HOCHZAEHLEN.
CALL FSGRA3(ABWF,IABWF,MABWF,NABWF,XIA,XIE)
AW=ABWF(IABWF,2)
BW=ABWF(IABWF,3)
GOTO 8
6 CCNTINUE
C I N T E G R A T I O N .
C VERTIFILIER FUER DIE VERSCHIEDENEN INTEGRALE UND INTEGRATIONSARTEN.
GOTO IGRIAR,(1001,1002,1010,1020,2001,2002,2010,2020,
*3001,3002,3010,3020,4001,4002,4010,4020,5001,5002,5010,5020,
*6001,6002,6010,6020,7001,7002,7010,7020,8001,8002,8010,8020,
*9001,9002,9010,9020)
C IITYP=1. INTEGRAL VON PHI.
1001 CALL FSROMB(DPHI,4445)
GOTO 1
1002 CALL FSROMB(FSNU01,4445)
GOTO 1
1010 L=11
GOTO 60
1020 L=12
GOTO 60
C IITYP=2. INTEGRAL VON F1 * PHI.
2001 CALL FSROMB(FSANO2,4445)
GOTO 1
2002 CALL FSROMB(FSNU02,4445)
GOTO 1
2010 L=21
GOTO 60
2020 L=22
GOTO 60
C IITYP=3. INTEGRAL VON F1*F2 * PHI.
3001 CALL FSROMB(FSANC3,4445)
GOTO 1

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- B 60 -

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3002 CALL FSROMB(FSNU03,8445)
  GCTO 1
3010 L=31
  GOTO 60
3020 L=32
  GOTO 60
C   ITYP=4. INTEGRAL VON 1/F3 * PHI.
4001 CALL FSROMB(FSANO4,8445)
  GCTO 1
4002 CALL FSROMB(FSNU04,8445)
  GOTO 1
4010 L=41
  GOTO 60
4020 L=42
  GCTO 60
C   ITYP=5. INTEGRAL VON 1/F3**2 * PHI.
5001 CALL FSROMB(FSANO5,8445)
  GOTO 1
5002 CALL FSROMB(FSNU05,8445)
  GCTO 1
5010 L=51
  GCTO 60
5020 L=52
  GOTO 60
C   ITYP=6. INTEGRAL VON F1/F3 * PHI.
6001 CALL FSROMB(FSANO6,8445)
  GCTO 1
6002 CALL FSROMB(FSNU06,8445)
  GCTO 1
6010 L=61
  GOTO 60
6020 L=62
  GCTO 60
C   ITYP=7. INTEGRAL VON F1/F3**2 * PHI.
7001 CALL FSROMB(FSANO7,8445)
  GCTO 1
7002 CALL FSROMB(FSNU07,8445)
  GCTO 1
7010 L=71
  GCTO 60
7020 L=72
  GCTO 60
C   ITYP=8. INTEGRAL VON F1*F2/F3 * PHI.
8001 CALL FSROMB(FSANO8,8445)
  GCTO 1
8002 CALL FSROMB(FSNU08,8445)
  GCTO 1
8010 L=81
  GOTO 60
8020 L=82
  GCTO 60
C   ITYP=9. INTEGRAL VON F1*F2/F3**2 * PHI.
9001 CALL FSROMB(FSANO9,8445)
  GCTO 1
9002 CALL FSROMB(FSNU09,8445)

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3800
3810

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```

  GCTO 1
9010 L=91
  GCTO 60
9020 L=92
  GCTO 60
C   LCCP ENDF FUER LCOP UEBER ALLE INTERVALLE
  1 IF(DRUCKL) DRUCK=.TRUE.
  RESULT=RESULT+Y
  GCTO 2
  2 RESULT=RESULT
C   FEHLERTEST.
  IF(NFTYP.GT.0) GOTO 50
C   FALLS DRUCK=.TRUE. COEF NFTYP<=0 UND ANTEIL VON YF(1) BZW. YF(3)
C   AM ERGEBNIS RESULT MEHR ALS 1% AUSMACHEN: WARNUNGSAUSDRUCK.
  IF(RESULT.EQ.0.0) GOTO 50
  IF(ABS(YF(1)/RESULT).GE.1.0E-1.NR. ABS(YF(3)/RESULT).GE.1.0E-2)
  *DRUCK=.TRUE.
  50 IF(.NOT.TEST3.AND..NOT.DRUCK) GOTO 333
  CALL FSWR04(1008,ITYP,ITYPFU,BSIGO,BSIGO)
  CALL FSWR03(-1015,XINT(1),XINT(NXINT),RESULT)
  IF(DRUCK) CALL FSWR01(-2011,EPSROM)
  IF((NFTYP.GT.0).OR.(.NOT.TEST3.AND..NOT.DRUCK)) GOTO 333
  YFP(1)=0.0
  YFP(2)=0.0
  YFP(3)=0.0
  IF(RESULT.EQ.0) GOTO 51
  YFP(1)=ABS(YF(1)/RESULT)*100.0
  YFP(2)=ABS(YF(2)/RESULT)*100.0
  YFP(3)=ABS(YF(3)/RESULT)*100.0
  51 CALL FSWR09(-1009,YF(2),YF(1),YF(3),YFP(2),YFP(1),YFP(3),
  *YFEP(2),YFEP(1),YFEP(3))
333 RETURN
445 KMRDMP=NDIMP
  RETURN 1
777 RETURN 2
  60 CALL FSEXIN
  IF(TEST2) WRITE(NO,101) ITYP,ITYPFU,BSIGO,XIA,XIE,Y
101 FORMAT(' ANALYT ITYP=',I2,' ITYPFU=',I2,' SIGO=',IPE13.6,
  * ' XL=',IPE13.6,' XH=',IPE13.6,' Y=',IPE13.6)
  GCTO 1
  END

```

```

REAL FUNCTION FSNU01*(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW
FSNU01=DBLE(AW)*X+DBLE(BW)
RETURN
END

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4210
4220

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```

REAL FUNCTION FSNU02*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,A1,B1
FSNU02=(DBLE(AW)*X+DBLE(BW))*(DBLE(A1)*X+DBLE(B1))
RETURN
END

```

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4C
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```

REAL FUNCTION FSNU07*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,A1,B1,NR2(2),A3,B3,BSIGO
FSNU07=(DBLE(AW)*X+DBLE(BW))*(DBLE(A1)*X+DBLE(B1))/
*((DBLE(A3)*X+DBLE(B3)+DBLE(BSIGO))**2)
RETURN
END

```

10
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50
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70

```

REAL FUNCTION FSNU03*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,A1,B1,A2,B2
FSNU03=(DBLE(AW)*X+DBLE(BW))*(DBLE(A1)*X+DBLE(B1))*(DBLE(A2)*X+DBL
*(B2))
RETURN
END

```

10
20
30
4C
50
60
7C

```

REAL FUNCTION FSNU08*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,A1,B1,A2,B2,A3,B3,BSIGO
FSNU08=(DBLE(AW)*X+DBLE(BW))*(DBLE(A1)*X+DBLE(B1))*(DBLE(A2)*X+
*(DBLE(B2)))/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIGO))
RETURN
END

```

10
20
3C
40
5C
60
70

```

REAL FUNCTION FSNU04*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,NR2(4),A3,B3,BSIGO
FSNU04=(DBLE(AW)*X+DBLE(BW))/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIGO))
RETURN
END

```

10
2C
30
40
5C
60

```

REAL FUNCTION FSNU09*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,A1,B1,A2,B2,A3,B3,BSIGO
FSNU09=(DBLE(AW)*X+DBLE(BW))*(DBLE(A1)*X+DBLE(B1))*(DBLE(A2)*X+
*(DBLE(B2)))/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIGO))**2)
RETURN
END

```

1C
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3C
40
5C
6C
70

```

REAL FUNCTION FSNU05*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,NR2(4),A3,B3,BSIGO
FSNU05=(DBLE(AW)*X+DBLE(BW))/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIGO))**2
*)
RETURN
END

```

10
20
3C
4C
50
6C
7C

```

REAL FUNCTION FSAN02*8(X)
REAL*8 X,DPHI
COMMON/CFSTRU/ NR1(14),A1,B1
FSAN02=DPHI(X)*(DBLE(A1)*X+DBLE(B1))
RETURN
END

```

10
20
3C
40
50
60

```

REAL FUNCTION FSNU06*8(X)
REAL*8 X
COMMON/CFSTRU/ NR1(12),AW,BW,A1,B1,NR2(2),A3,B3,BSIGO
FSNU06=(DBLE(AW)*X+DBLE(BW))*(DBLE(A1)*X+DBLE(B1))/
*(DBLE(A3)*X+DBLE(B3)+DBLE(BSIGO))
RETURN
END

```

10
20
30
4C
50
60
70

```

REAL FUNCTION FSAN03*8(X)
REAL*8 X,DPHI
COMMON/CFSTRU/ NR1(14),A1,B1,A2,B2
FSAN03=DPHI(X)*(DBLE(A1)*X+DBLE(B1))*(DBLE(A2)*X+DBLE(B2))
RETURN
END

```

1C
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50
6C

REAL FUNCTION FSAN04*8(X)	10	REAL FUNCTION FSAN09*8(X)	10
REAL*8 X,DPHI	20	REAL*8 X,DPHI	20
COMMON/CFSTRU/ NR1(18),A3,B3,BSIG0	30	COMMON/CFSTRU/ NR1(14),A1,B1,A2,B2,A3,B3,BSIG0	30
FSAN04=DPHI(X)/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIG0))	40	FSAN09=DPHI(X)*(DBLE(A1)*X+DBLE(B1))*(DBLE(A2)*X+DBLE(B2))/	40
RETURN	50	*(DBLE(A3)*X+DBLE(B3)+DBLE(BSIG0))**2)	50
END	60	RETURN	60
		END	70
REAL FUNCTION FSAN05*8(X)	10	SUBROUTINE FSEXIN	10
REAL*8 X,DPHI	20	EXPLICIT ANALYTISCHE INTEGRATION.	20
COMMON/CFSTRU/ NR1(18),A3,B3,BSIG0	30	REAL*8 YR9,H0,H1,H2,H3,RO,R1,Z1,Z2,Z3,Z4,Z5,Z6,Z7,FSLOMQ,CQ,FF,	30
FSAN05=DPHI(X)/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIG0))**2)	40	* DA1,DA2,DB1,DB2,DAW,DBW,DXIA,DXIE,DD,Y,ZL,Q	40
RETURN	50	COMMON/CFSTRU/ NR1(11),CONST,AW,BW,A1,B1,A2,B2,A3,B3,BSIG0,	50
END	60	*XIA,XIE,L,Y	60
		CA1=DBLE(A1)	70
		DB1=DBLE(B1)	80
		CA2=DBLE(A2)	90
		DB2=DBLE(B2)	100
		CAW=DBLE(AW)	110
		DBW=DBLE(BW)	120
		DXIA=DBLE(XIA)	130
		DXIE=DBLE(XIE)	140
		CD=DXIE-DXIA	150
		LSPR=L/10	160
		LSPR=2*LSPR+(L-LSPR*10-2)	170
		GOTO (11,12,21,22,31,32,41,42,51,52,61,62,71,72,81,82,91,92),LSPR	180
		ITP=1	190
		GOTO 770	200
		C INTEGRAL VON F=(AW*X+BW)	210
		11 N=0	220
		ILNNUL=1	230
		H1=DAW	240
		H2=DAW	250
		GOTO 1	260
		C INTEGRAL VON F=CONST/X	270
		12 N=0	280
		ILNNUL=0	290
		F=C=1.00+0	300
		GOTO 2	310
		C INTEGRAL VON F=(AW*X+BW)*(A1*X+B1)	320
		21 N=0	330
		ILNNUL=2	340
		F2=DAW*DA1	350
		H1=DAW*DB1+DBW*CA1	360
		F2=DBW*DB1	370
		GOTO 1	380
		C INTEGRAL VON F=CONST/X * (A1*X+B1)	390
		22 N=0	400
		ILNNUL=1	410
		H1=DA1	420
		F=C=1	430
		GOTO 2	440
REAL FUNCTION FSAN06*8(X)	10		
REAL*8 X,DPHI	20		
COMMON/CFSTRU/ NR1(14),A1,B1,NR2(2),A3,B3,BSIG0	30		
FSAN06=DPHI(X)*(DBLE(A1)*X+DBLE(B1))/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIG0))**2)	40		
RETURN	50		
END	60		
REAL FUNCTION FSAN07*8(X)	10		
REAL*8 X,DPHI	20		
COMMON/CFSTRU/ NR1(14),A1,B1,NR2(2),A3,B3,BSIG0	30		
FSAN07=DPHI(X)*(DBLE(A1)*X+DBLE(B1))/(DBLE(A3)*X+DBLE(B3)+DBLE(BSIG0))**2)	40		
RETURN	50		
END	60		
REAL FUNCTION FSAN08*8(X)	10		
REAL*8 X,DPHI	20		
COMMON/CFSTRU/ NR1(14),A1,B1,A2,B2,A3,B3,BSIG0	30		
FSAN08=DPHI(X)*(DBLE(A1)*X+DBLE(B1))*(DBLE(A2)*X+DBLE(B2))/	40		
*(DBLE(A3)*X+DBLE(B3)+DBLE(BSIG0))	50		
RETURN	60		
END	70		

C	INTEGRAL VON F=(AW*X+BW)*(A1*X+B1)*(A2*X+B2)	450	ILNNUL=2	1000
31	N=0	460	F2=DAW*DA1	1010
	ILNNUL=3	470	H1=DAW*DB1+DBW*DA1	1020
	Z1=DA1*DA2	480	H0=DBW*DB1	1030
	Z2=DA1*DB2+DB1*DA2	490	GCTO 1	1040
	Z3=DA1*DB2	500	C	INTEGRAL VON F=CONST/X * (A1*X+B1)/((A3*X+B3+BSIGO)**2)
	H3=DAW*Z1	510	72	N=2
	H2=DAW*Z2+DBW*Z1	520	ILNNUL=1	1070
	H1=DAW*Z3+DBW*Z2	530	H1=DA1	1080
	HC=DBW*Z3	540	H0=DB1	1090
	GCTO 1	550	GCTO 2	1100
C	INTEGRAL VON F=CONST/X * (A1*X+B1)*(A2*X+B2)	560	C	INTEGRAL VON F=(AW*X+BW)*(A1*X+B1)*(A2*X+B2)/(A3*X+B3+BSIGO)
32	N=C	570	E1	N=1
	ILNNUL=2	580	ILNNUL=3	1130
	H2=DA1*DA2	590	Z1=DA1*DA2	1140
	H1=DA1*DB2+DB1*DA2	600	Z2=DA1*DB2+DB1*DA2	1150
	HC=DA1*DB2	610	Z3=DA1*DB2	1160
	GOTO 2	620	H3=DAW*Z1	1170
C	INTEGRAL VON F=(AW*X+BW)/(A3*X+B3+BSIGO)	630	H2=DAW*Z2+DBW*Z1	1180
41	N=1	640	H1=DAW*Z3+DBW*Z2	1190
	ILNNUL=1	650	HC=DBW*Z3	1200
	H1=DAW	660	GCTO 1	1210
	HC=DBW	670	C	INTEGRAL VON F=CONST/X * (A1*X+B1)*(A2*X+B2)/(A3*X+B3+BSIGO)
	GCTO 1	680	82	N=1
C	INTEGRAL VON F=CONST/X * 1.0/(A3*X+B3+BSIGO)	690	ILNNUL=2	1230
42	N=1	700	H2=DA1*DA2	1240
	ILNNUL=0	710	H1=DA1*DB2+DB1*DA2	1250
	HC=1.00+0	720	HC=DB1*DB2	1260
	GCTO 2	730	GOTO 2	1270
C	INTEGRAL VON F=(AW*X+BW)/((A3*X+B3+BSIGO)**2)	740	C	INTEGRAL VON F=(AW*X+BW)*(A1*X+B1)*(A2*X+B2)/((A3*X+B3+BSIGO)**2)
51	N=2	750	51	N=2
	ILNNUL=1	760	ILNNUL=3	1300
	H1=DAW	770	Z1=DA1*DA2	1310
	H0=DBW	780	Z2=DA1*DB2+DB1*DA2	1320
	GCTO 1	790	Z3=DA1*DB2	1330
C	INTEGRAL VON F=CONST/X * 1.0/((A3*X+B3+BSIGO)**2)	800	H3=DAW*Z1	1340
52	N=2	810	H2=DAW*Z2+DBW*Z1	1350
	ILNNUL=0	820	H1=DAW*Z3+DBW*Z2	1360
	H0=1.00+0	830	HC=DBW*Z3	1370
	GCTO 2	840	GCTO 1	1380
C	INTEGRAL VON F=(AW*X+BW)*(A1*X+B1)/(A3*X+B3+BSIGO)	850	C	INTEGRAL VON F=CONST/X * (A1*X+B1)*(A2*X+B2)/((A3*X+B3+BSIGO)**2)
61	N=1	860	92	N=2
	ILNNUL=2	870	ILNNUL=2	1410
	F2=DAW*DA1	880	H2=DA1*DA2	1420
	H1=DAW*DB1+DBW*DA1	890	H1=DA1*DB2+DB1*DA2	1430
	H0=DBW*DB1	900	HC=DB1*DB2	1440
	GCTO 1	910	GCTO 2	1450
C	INTEGRAL VON F=CONST/X * (A1*X+B1)/(A3*X+B3+BSIGO)	920		1460
62	N=1	930	C*****	1470
	ILNNUL=1	940	C*****	1480
	F1=DA1	950	C INTEGRATION VON F1=(H3*X**3+H2*X**2+H1*X+HC)/(R1*X+RC)**N	N=C,1,2 1490
	HC=DB1	960	C*****	1500
	GOTO 2	970	C*****	1510
C	INTEGRAL VON F=(AW*X+BW)*(A1*X+B1)/(A3*X+B3+BSIGO)**2)	980	1 YRE=0.00+0	1520
71	N=2	990	IF(N.EQ.0) GOTO 1055	1530
			R1=DBLE(A3)	1540

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RO=DBLE(B3)+DBLE(B5IG0)
IF(N.EQ.1) GOTC 1155
IF(N.EQ.2) GOTO 1255
ITF=2
770 CALL FSWR03(3C01,'FSEX','IN ',ITP)
333 Y=YR8
RETURN
1055 CONTINUE
C N=0 R1 UND R0 OHNE BEDEUTUNG.
C F1=H3*X**3+H2*X**2+H1*X+H0
C INTEGRAL VON F1 = 0.25*H3*X**4+0.33333333*H2*X**3+
C 0.5*H1*X**2+H0*X
ITP=3
GCTO (10551,10552,10553),IUNNUL
GOTO 770
10553 YR8=YR8+0.250*0*H3*(DXIF**2+DXIA**2)*(DXIF+DXIA)*DD
10552 YR8=YR8+0.3333333333333333333333*H2*CD*(3.0D+0*DXIA**2+DD*(3.0D+0*DXIA
**CD))
10551 YR8=YR8+(0.5C+0*H1*(CXIF+DXIA)+H0)*DD
IF(N.EQ.1) YR8=YR8/R0
IF(N.EQ.2) YR8=YR8/(R0**2)
GCTO 333
1155 CONTINUE
C N=1
C TEST VON R1 UND R0.
IF(R1.EQ.0.0) GOTO 1151
IF(R0.EQ.0.0) GOTC 1190
1199 CONTINUE
C N=1 R1 UND R0 UNGLEICH NULL.
C F1=(H3*X**3+H2*X**2+H1*X+H0)/(R1*X+R0)
C INTEGRAL VON F1 = H3/(R1**4)*(0.33333333*(R1*X+R0)**3
C -1.5*R0*(R1*X+R0)**2+3.0*R0**2*(R1*X+R0)-R0**3*ALOG(R1*X+R0))
C +2/(R1**3)*(0.5*(R1*X+R0)**2-2.*(R0*(R1*X+R0)
C +R0**2*ALCG(R1*X+R0))
C +H1/(R1**2)*(R1*X-R0*ALCG(R1*X+R0))
C +H0/R1*ALOG(R1*X+R0)
ITP=4
FF=R1/R0
Q=FF*DD/(1.0D+0+FF*DXIA)
Z1=FSLOMQ(DXIE,DXIA,FF)
Z5=Z1-0.5*Q*Q
Z1=Z5+Q
GCTO (11991,11992,11993),IUNNUL
GOTO 770
11993 YR8=YR8+H3/(R1**4)*(R1**3*DD*(DXIA+DXIA+DXIA)*DD+
*C.333333333333333333333333D+0*DD*DD-DXIA/(1.0D+0+FF*DXIA)*(DXIA+0.5D+0*
*CD*(2.0D+0+FF*DXIA)/(1.0D+0+FF*DXIA))-R0**3*Z1)
11992 YR8=YR8+H2/R1**3*(R1*R1*DD*(0.5D+0*DC+FF*DXIA*DXIA/(
*1.0D+0+FF*DXIA))+R0*R0*Z5)
11991 YR8=YR8+H1/(R1**2)*(R1*CD*FF*DXIA/(1.0D+0+FF*DXIA)-R0*Z5)
* +H0/R1*Z1
GCTO 333
1151 CONTINUE
C N=1 R1=0.0
ITF=5

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1550
156C
1570
1580
1590
1600
161C
1620
1630
1640
1650
166C
1670
1680
1690
1700
171C
1720
173C
1740
1750
176C
1770
1780
1790
180C
181C
1820
183C
1840
185C
186C
1870
188C
1890
1900
1910
1920
1930
1940
1950
1960
1970
1980
199C
2000
2010
202C
2030
204C
2050
2060
207C
2080
209C

```

IF(R0.EQ.0.0) GCTO 770
C N=1 R1=0.0 RO UNGLEICH NULL.
C FUNKTION UND INTEGRAL WIE 1055 VERSEHEN MIT FAKTOR 1/R0.
GCTO 1055
1190 CONTINUE
C N=1 R1 UNGLEICH NULL R0=0.0
C F1=1/R1*(H3*X**2+H2*X+H1+H0/X)
C INTEGRAL VON F1 = 1/R1*(0.33333333*H3*X**3+C.5*H2*X**2
C +H1*X+H0*ALOG(X))
ITP=6
GCTO (11901,11902,11903),IUNNUL
GOTO 770
11903 YR8=YR8+0.3333333333333333333333*H3*DD*(3.0D+0*DXIA**2+DD*(3.0D+0*DXIA
**DD))
11902 YR8=YR8+0.5D+0*H2*DD*(DXIE+DXIA)
11901 YR8=YR8+H1*DD + H0*ALCG(DXIE/DXIA)
YR8=YR8/R1
GCTO 333
1255 CONTINUE
C N=2
C TEST VON R1 UND R0.
IF(R1.EQ.0.0) GOTO 1251
IF(R0.EQ.0.0) GOTO 1290
1295 CONTINUE
C N=2 R1 UND R0 UNGLEICH NULL.
C F1=(H3*X**3+H2*X**2+H1*X+H0)/((R1*X+R0)**2)
C INTEGRAL VON F1 = H3/(R1**4)*(0.5*(R1*X+R0)**2-2.*R0*(R1*X+R0)
C +3.0*R0**2*ALOG(R1*X+R0)+(R0**3)/(R1*X+R0))
C +2/(R1**3)*(R1*X+R0)-2.0*R0*ALCG(R1*X+R0)-(R0**2)/(R1*X+R0))
C +1/(R1**2)*(R0/(R1*X+R0)+ALOG(R1*X+R0))
C -H0/R1*1.0/(R1*X+R0)
ITP=7
FF=R1/R0
Q=FF*DD/(1.0D+0+FF*DXIA)
CC=1.0D+0/((1.0D+0+FF*DXIE)*(1.0D+0+FF*DXIA))
Z4=-FF*DD*DD
Z1=FSLOMQ(DXIE,DXIA,FF)
Z5=Z1-0.5*Q*Q
Z1=Z5+Q
Z7=Z5*FF*FF*DD*DXIE*CC
GCTO (12991,12992,12993),IUNNUL
GCTO 770
12993 YR8=YR8+H3/(R1**4)*(R1*R1*DD*(0.5D+0*CC+(DC+FF*DXIA*(FF*DXIE*DXIA
* -DD))*DD)+3.0D+0*R0*R0*Z5)
12992 YR8=YR8+H2/(R1**3)*R0*(FF*FF*DD*DXIA/(1.0D+0+FF*DXIA)-Z5-Z7)
12991 YR8=YR8+(1.0D+0/R1)*(H1/R1*Z7 - H0*Z4/R0)
GCTO 333
1251 CONTINUE
C N=2 R1=0.0
ITP=8
IF(R0.EQ.0.0) GOTO 770
C N=2 R1=0.0 RO UNGLEICH NULL.
C FUNKTION UND INTEGRAL WIE 1055 MIT FAKTOR 1.0/(R0**2).
GCTO 1055
1290 CONTINUE

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2100
2110
212C
213C
2140
215C
2160
217C
2180
2190
220C
2210
2220
2230
224C
225C
2260
227C
2280
2290
230C
2310
2320
2330
2340
235C
2360
2370
2380
2390
240C
2410
2420
2430
244C
2450
2460
2470
248C
249C
2500
2510
2520
253C
254C
2550
256C
2570
258C
259C
260C
2610
2620
263C
2640

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C N=2 R1 UNGLEICH NULL RO=0.0 2650
C F1=1.0/R1**2*(H3*X+H2+H1/X+HC/X**2) 266C
C INTEGRAL VON F1 = 1.0/R1**2*(0.5*H3*X**2+H2*X+f1*ALOG(X)-HO/X) 2670
ITP=9 2680
GCTO (12901,12902,12903),IUNMJL 2690
GOTO 770 2700
12903 YR8=YR8+0.5*H3*(DXIE+DXIA)*DC 2710
12902 YR8=YR8+H2*DD 2720
12901 YR8=YR8+H1*DLOG(DXIE/DXIA)-HC*(1.0/DXIE-1.0/DXIA) 2730
YR8=YR8/R1**2 274C
GOTO 333 2750
C***** 2760
C***** 2770
C INTEGRATION VON F2=CONST*(H2*X**2+H1*X)+HC)/(X*(R1*X+RC)**N) N=0,1,2 2780
C***** 279C
C***** 2800
2 YR8=0.0D+0 2810
IUNSP=IUNNUL+1 2820
IF(N.EQ.0) GOTO 2055 283C
R1=DBLE(A3) 284C
RO=DBLE(B3)+DBLE(BSIGO) 2850
IF(N.EQ.1) GOTO 2155 2860
IF(N.EQ.2) GOTO 2255 2870
ITP=10 2880
GCTO 770 289C
2055 CCNT INUE 2900
C N=0 R1 UND RO OHNE BEDEUTUNG. 291C
C F2=CONST*(H2*X+H1+HO/X) 2920
C INTEGRAL VON F2 = CONST*(0.5*H2*X**2+H1*X+HC*ALOG(X)) 293C
ITP=11 2940
GOTO (20550,20551,20552),IUNSP 2950
GCTO 770 296C
20552 YR8=YR8+0.5*H2*(DXIE**2-DXIA**2) 2970
20551 YR8=YR8+H1*DC 2980
20550 YR8=YR8+HO*DLOG(DXIE/DXIA) 2990
IF(N.EQ.1) YR8=YR8/RO 3000
IF(N.EQ.2) YR8=YR8/(RO**2) 3010
2000 YR8=CONST*YR8 3020
GCTO 333 3030
2155 CONTINUE 3040
C N=1 3050
C TEST VON R1 UND RO. 306C
IF(R1.EQ.0.0) GOTO 2151 3070
IF(RO.EQ.0.0) GOTO 2190 308C
2155 CONTINUE 3090
C N=1 R1 UND RO UNGLEICH 0.0 3100
C F2={H2*X**2+H1*X+HO}/(X*(R1*X+RO)) 3110
C INTEGRAL VON F2 = H2/R1**2*(R1*X-RO*ALOG(R1*X+RC)) 3120
+H1/R1*ALOG(R1*X+RO) 313C
-HO/R0*(ALOG(R1*X+RC)-ALOG(X)) 3140
ITP=12 3150
FF=R1/RO 316C
C=FF*DD/(1.0D+0+FF*DXIA) 3170
Z1=FSLQM(DXIE,DXIA,FF)-0.5*C*Q+C 3180
GOTO (21990,21991,21992),IUNSP 3190

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GCTO 770 3200
21592 YR8=YR8+H2/(R1**2)*(R1*DD-RO*Z1) 3210
21991 YR8=YR8+H1/R1*Z1 3220
21590 YR8=YR8-HO/RO*(Z1-DLOG(DXIE/DXIA)) 3230
GCTO 2000 3240
2151 CCNT INUE 3250
C N=1 R1=C.0 3260
ITP=13 3270
IF(RO.EQ.0.0) GCTO 770 328C
C N=1 R1=0.0 RO UNGLEICH 0.0 3290
C FLAKTION UND INTEGRAL WIE 2055 MIT FAKTOR 1/RO 330C
GOTO 2055 3310
2190 CCNT INUE 3320
C N=1 R1 UNGLEICH 0.0 RO=0.0 3330
C F2=1/R1*(H2+H1/X+HO/X**2) 3340
C INTEGRAL VON F2 = 1/R1*(H2*X+H1*ALOG(X)-HO/X) 3350
ITP=14 3360
GCTO (21900,21901,21902),IUNSP 3370
GOTO 770 3380
21902 YR8=YR8+H2*DD 3390
21901 YR8=YR8+H1*DLOG(DXIE/DXIA) 340C
21900 YR8=YR8-HO*(1.0/DXIE-1.0/DXIA) 3410
YR8=YR8/R1 3420
GOTO 2000 3430
2255 CONTINUE 3440
C N=2 345C
C TEST VON R1 UND RO. 3460
IF(R1.EQ.0.0) GOTO 2251 3470
IF(RO.EQ.0.0) GOTO 2290 3480
2290 CCNT INUE 3490
C N=2 R1 UND RO UNGLEICH 0.0 3500
C F2={H1*X**2+H1*X+HO}/(X*(R1*X+RO)**2) 3510
C INTEGRAL VON F2 = H2/(R1**2)*(RO/(R1*X+RO)+ALOG(R1*X+RO)) 3520
-H1/R1*1.0/(R1*X+RO) 3530
-HO/(RO**2)*(ALOG(R1*X+RC)-ALOG(X)+R1*X/(R1*X+RO)) 3540
ITP=15 3550
FF=R1/RO 3560
Q=FF*DD/(1.0D+0+FF*DXIA) 357C
DQ=1.0D+0/((1.0D+0+FF*DXIE)*(1.0D+0+FF*DXIA)) 3580
Z1=FSLQM(DXIE,DXIA,FF) 3590
Z5=Z1-0.5*Q*Q 360C
Z1=Z5+Q 3610
Z4=-FF*DD*DQ 362C
Z7=Z5+FF*FF*DD*DXIE*DQ 3630
GCTO (22990,22991,22992),IUNSP 3640
GOTO 770 3650
22992 YR8=YR8+H2/(R1**2)*Z7 3660
22551 YR8=YR8-H1/R1*Z4/RO 367C
22990 YR8=YR8-HO/(RO**2)*(Z1-DLOG(DXIE/DXIA)+R1*(DXIE/(
R1*DXIE+RO)-DXIA/(R1*DXIA+RO))) 3680
GOTO 2000 3700
2251 CCNT INUE 3710
C N=2 R1=0.0 3720
ITP=16 3730
IF(RO.EQ.0.0) GOTO 770 3740

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C      N=2 R1=0.0 RO UNGLEICH 0.0          3750
C      FUNKTION UND INTEGRAL WIE 2055 MIT FAKTOR 1.0/(RC**2) 3760
C      GOTO 2055                            3770
2290  CONTINUE                             3780
C      N=2 R1 UNGLEICH 0.0 RO=0.0         3790
C      F2=1.0/(R1**2)*(H2/X+H1/X**2+H0/X**3) 3800
C      INTEGRAL VON F2 = 1.0/(R1**2)*(H2*ALOG(X)-H1/X-C.5*H0/X**2) 3810
C      ITP=17                               3820
C      GOTO (22900,22901,22902),IUNSP     3830
C      GCTO 770                             3840
22902 YR8=YR8+H2*DLOG(DXIE/DXIA)          3950
22901 YR8=YR8-H1*(1.0/DXIE-1.0/DXIA)      3860
22900 YR8=YR8-C.5*H0*(1.0/(DXIE**2)-1.0/(DXIA**2)) 3870
C      YR8=YR8/(R1**2)                    3880
C      GCTO 2000                           3890
C      END                                  3900

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```

323 CONTINUE                               360
      RETURN                                370
      END                                   380

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REAL FUNCTION FSLOMQ*8(XIE,XIA,F)          10
C      ES IST Q = F*(XIE-XIA)/(1+F*XIA)    20
C      DAMN GILT                           30
C      LOG((1+F*XIE)/(1+F*XIA)) = LOG(1+Q) 40
C      FSLOMQ BERECHNET LOG(1+Q)-Q+0.5*Q**2 50
C      ES MUSS GELTEN: XIE,XIA > 0 ; XIE>XIA ; 60
C      REAL*8 XIE,XIA,F,DLOGM,FEL1,FEHLER,FELREL,FDLOGM,FELEND,C 70
C      COMMON NR1(4),ND                    80
C      IF(XIE.LE.0.OD+0.0R.XIA.LE.0.OD+C.0R.XIE.LE.XIA) 90
C      *CALL FSWRO3(3001,'FSLC','MQ ',1)    100
C      NMAX=20                             110
C      C=1.0D+0/(1.0D+0+F*XIA)            120
C      DLOGM=DLOG((1.0D+0+F*XIE)*Q)       130
C      Q=F*(XIE-XIA)*Q                    140
C      DLGCM=DLOGM-Q*(1.0D+0-0.5D+0*Q)    150
C      IF(DABS(DLOGM).GT.1.0E-4.0R.DABS(Q).GE.1.0D+0) GCTO 33C 160
C      FELEND=DFLOAT(NMAX+1)*DLOG10(DABS(C))-DLOG10(DFLOAT(NMAX+1))- 170
C      *DLOG10(DABS(DLOGM))                180
C      IF(Q.LT.0.0) FELEND=FELEND-DFLOAT(NMAX+1)*DLOG10(1.0D+C*Q) 190
C      IF(FELEND.GT.-15.0D+0) GOTO 330     200
C      FSLOMQ=0.0D+0                      210
3      A=3                                  220
C      FEL1=0.3333333333333333333333333333*Q**3 230

1      FSLOMQ=FSLOMQ+FEL1                  240
C      FEL1=(-1)**N*Q**(N+1)/(N+1)        250
C      IF(Q.GE.0.0) FEHLER=FEHL1          260
C      IF(Q.LT.0.0) FEHLER=FEL1/((1.0D+C*Q)**(N+1)) 270
C      FELREL=DABS(FEHLER/FSLOMQ)         280
C      IF(FELREL.LE.1.0E-15) GCTO 333     290
C      N=N+1                               300
C      IF(N.LE.NMAX) GOTO 1               310
C      WRITE(ND,1000) XIE,XIA,F,DLOGM,FELEND,FSLOMQ,FEHLER,FELREL,N,NMAX 320
1000  FORMAT(' ',1P6E15.7/' ',1P2E15.7,0P2I12) 330
C      CALL FSWRO3(3001,'FSLQ','MQ ',2)   340
330  FSLOMQ=DLOGM                          350

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      LOGICAL FUNCTION FSGRA1(AB,IAB,MAB,XIA,XIE) 10
      LOGICAL*4 FSTOLE                       20
      DIMENSION AB(MAB,4)                   30
      COMMON/CFSTRU/ NR1(4),GLSCH          40
      FSGRA1=.FALSE.                        50
      IF((AB(IAB-1,1).GT.XIA.AND..NOT.FSTOLE(AB(IAB-1,1),XIA,GLSCH)).OR. 60
      * (AB(IAB,1).LT.XIE.AND..NOT.FSTOLE(AB(IAB,1),XIE,GLSCH))) 70
      *FSGRA1=.TRUE.                        80
      RETURN                                 90
      END                                    100

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      SUBROUTINE FSGRA2(IFUN,AB,IAB,MAB,NAB,XIA,XIE,XIEE,SPRUO,SPRU3, 10
      *IFAR,LFAR,LFARA,FARIN,FARAN,IFUNAR,NUDUR) 20
      LOGICAL*4 SPRUC,FSGRA1,FSTOLE,NUDUR,SPRU3,LERMSG,LFAR(2,3), 30
      *LFARA(2,3)
      DIMENSION AB(MAB,4),FARIN(2,3,2),FARAN(2,3),IFUNAR(2,3) 40
      COMMON/CFSTRU/ NR1(3),LERMSG,GLSCH,NR2(2),ITYP,ITYPFU,NR3(5), 50
      *A1,R1,A2,B2,A3,B3,BSIGO
      SPRU3=.FALSE.                          60
      IF(XIE.LT.AB(IAB,1).OR.FSTOLE(XIE,AB(IAB,1),GLSCH)) GOTO 5 90
      IAB=IAB+1                               100
      IF(IAB.GT.NAB) CALL FSWRO3(3001,'FSGR','A2 ',1) 110
      IF(IFUN.LE.0.0R.IFUN.GT.3) CALL FSWRO3(3001,'FSCR','A2 ',2) 120
      GCTO (11,12,13),IFUN                  130
11  A1=AB(IAB,2)                             140
      B1=AB(IAB,3)                             150
      GCTO 5                                   160
12  A2=AB(IAB,2)                             170
      P2=AB(IAB,3)                             180
      GCTO 5                                   190
13  A3=AB(IAB,2)                             200
      B3=AB(IAB,3)                             210
      GOTO 5                                   220
5  IF(FSGRA1(AB,IAB,MAB,XIA,XIE)) CALL FSWRO3(3001,'FSGR','A2 ',3) 230
      IF(SPRUC) GOTO 1                         240
      F=0?                                     250
      IF(AB(IAB,4).NE.0.0) GCTC 2            260
      IPRINT=1                                 270
3  IF(.NOT.FSTOLE(AB(IAB-1,1),XIA,GLSCH)) CALL FSWRO3(3001, 280
      *'FSGR','A2 ',4)
      SPRUC=.TRUE.                            290
      SPRU3=.TRUE.                            300
      XIEE=AMAX1(XIEE,AB(IAB,1))             310
      IF(LERMSG.OR.ITYP.LE.3) GOTO 14        320
      IF(LFAR(IPRINT,IFAR)) GCTO 15         330
      GCTO 15                                 340

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- B 67 -

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LFAR(IPRINT,IFAR)=.TRUE.
FARIN(IPRINT,IFAR,1)=XIA
FARIN(IPRINT,IFAR,2)=XIEE
FARAN(IPRINT,IFAR)=BSIGC
IFUNAR(IPRINT,IFAR)=IFUN
GOTO 333
15 IF(FARIN(IPRINT,IFAR,1).NE.XIA.AND.FARIN(IPRINT,IFAR,2).NE.XIEE
*.AND.IFUNAR(IPRINT,IFAR).NE.IFUN) CALL FSWR03(3001,'FSGR','A2 ',
*5)
GOTO 333
14 CALL FSWR04(1008,ITYP,ITYPFU,BSIGC,BSIGC)
CALL FSWR02(-2005,XIA,XIEE)
IF(IPRINT.EQ.1) CALL FSWR02(-2007,IFUN,ITYP)
IF(IPRINT.EQ.2) CALL FSWR02(-2008,IFUN,ITYP)
GOTO 333
C F NULL DURCHGANG?
2 IF(.NOT.NUDUR) GOTO 331
IF(ABS(IAB,4).GE.0.0) GOTO 332
IFFINT=2
GOTO 3
1 CCNTINUE
IF(.NOT.LERMSG) GOTO 333
C ZUSAETZLICHE TEST BEI SCHON VORHANDENEM FEHLER IM INTERVALL XIA
C RIS XIEE.
J=IAB
4 IF(J.GT.NAB.OR.AB(J-1,1).GE.XIEE.OR.FSTOLF(AB(J-1,1),XIEE,GLSCH))
* GOTO 333
IF(NUDUR.AND.AB(J,4).LT.0.0) CALL FSWR02(-2010,IFUN,ITYP)
IF(ABS(J,4).EQ.0.0) CALL FSWR02(-2009,IFUN,ITYP)
J=J+1
GOTO 4
321 IF(LFRMSG.OR.ITYP.LE.3) GOTO 333
IF(LFAR(1,IFAR)) LFARA(1,IFAR)=.TRUE.
322 IF(LERMSG.OR.ITYP.LE.3) GOTO 333
IF(LFAR(2,IFAR)) LFARA(2,IFAR)=.TRUE.
GOTO 333
323 RETURN
END

SUBROUTINE FSGRA3(AB,IAB,MAB,NAB,XIA,XIE)
DIMENSION AB(MAB,4)
LOGICAL*4 FSTOLF,FSGRA1
COMMON/CFSTRU/ NR1(4),GLSCH
2 IF(XIE.LF.AB(IAB,1)) GOTO 1
IAB=IAB+1
IF(IAB.GT.NAB) CALL FSWR03(3001,'FSGR','A3 ',1)
GOTO 2
1 IF(IAB.GT.NAB.OR.FSGRA1(AB,IAB,MAB,XIA,XIE)) CALL FSWR03(3001,
*'FSGR','A3 ',2)
323 RETURN
END

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SUBROUTINE FSROMB(FCT,*)
BERECHNET MIT HILFE DER ROMBERG METHODE DAS INTEGRAL VON FCT(X)
VON XL BIS XH.
BESCHREIBUNG DER PARAMETER.
XL UNTERE INTEGRATIONSGRENZE.
XH OBERE INTEGRATIONSGRENZE.
EPS OBERE GRENZE FUER BETRAG DES RELATIVEN FEHLERS.
NCIM DIMENSION DES HILFELDES AUX.
NDIM-1=MAXIMAL MOEGLICHE ZAHL DER HALBIERUNGEN
DERS INTERVALLS XL...XH.
NDIMP ZUSAETZLICH BENUTZTE WORTER IN AUX.
CRINWA SCHRANKE FUER FEHLERAUSDRUCK. BESCHREIBUNG SIEHE FSTRUK.
DRUCK LOGISCHE VARIABLE. .FALSE. : KEIN TEST- ODER FEHLER-
AUSDRUCK IST ERFOELCT.
.TRUE. : TEST- ODER FEHLER-AUSDRUCK
IST ERFOELCT.
FCT NAME DER ZU INTEGRIERENDEN FUNKTION.
Y ERGEBNIS DER BERECHNUNG. ( APPROXIMATION FUER DAS
INTEGRAL. )
YF FELD, ZU DEM Y ADDIERT WIRD. AUSWAHL DES ELEMENTES
ERFOLGT NACH FOLGENDEM SCHEMA:
YF(1) ZAHL DER HALBIERUNGEN WAR KLEINER ALS 3.
(NCIMAK<=4). RELATIVER FEHLER WURDE ERREICHT
ODER UNTERSCHRITTEN.
YF(2) ZAHL DER HALBIERUNGEN WAR >= 3 (NCIMAK>=4).
RELATIVER FEHLER WURDE ERREICHT ODER UNTER=
SCHRITTEN.
ODER:
BEI NDIMAK=4 TRATEN RUNDUNGSFEHLER AUF. ES WIRD DER
WERT VON NDIMAK=3 GENOMMEN, FALLS DAS ZUGEHORIGE
DELREL SCHON KLEINER ODER GLEICH DEM GEWUNSCHTEN
RELATIVEN FEHLER WAR.
YF(3) ZAHL DER HALBIERUNGEN WAR >= 3 (NDIMAK>=4).
RELATIVER FEHLER WURDE WEGEN RUNDUNGSFEHLER
NICHT ERREICHT. (U.U. FEHLERAUSDRUCK.
STEFFE DRINWA.)
AUX HILFSFELD DER DIMENSION NDIM.
RETURN I WIRD EPS NICHT INNERHALB VON NDIM-1 HALBIERUNGEN
ERREICHT, SO WIRD NCIMP=1 GEFSETZT UND RETURN I GEMACHT.
LOGICAL*4 TEST1,TEST2,TEST3,LERMSG,DRUCK,INTKLE
REAL*8 SM,AUX,H,Q,HH,X,P,HD,FCT,Y
DIMENSION AUX(1),YF(3),YFEPS(3)
COMMON NR1(4),NC
COMMON/CFSTRU/ TEST1,TEST2,TEST3,LERMSG,GLSCH,NR2(2),ITYP,ITYPFU,
*NR3(11),BSIGC,XL,XH,NR4(1),Y,NDIMP,DRUCK
FEHLFRABFRAGE.
IF(XL.GT.XH.OR.NDIM.LT.4) CALL FSWR03(3001,'FSRC','MB ',1)
VORBEREITUNGEN FUER DEN ROMBERG-LOOP.
ALX(1)=0.5*(FCT(DBLE(XL))+FCT(DBLE(XH)))
H=XH-XL
NCIMAK=1
IADD=0
IF(H.EQ.0.0) GOTO 12
INTKLE=.FALSE.

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IF(ABS((XH-XL)/XH).LE.10.0*GLSCH) INTKLF=.TRUE.
2 FF=H
DELT2=0.0
P=1.0
JJ=1
IF(TEST3) WRITE(NO,1001)
1001 FCRMAT(' ROMBERG. PRINTOUT OF ARRAY ALX. ')
IF(TEST3) WRITE(NO,1002) AUX(1)
I7=0
CC 7 I=2,NDIM
NDIMAK=1
Y=AUX(1)
DFLT1=DELT2
FD=HH
FF=0.5*HH
P=C.5*P
X=XL+HH
SM=0.0D+0
DO 3 J=1,JJ
SM=SM+FCT(X)
3 X=X+HD
ALX(I)=0.5*AUX(I-1)+P*SM
C R C M B E R G EXTRAPOLATION.
C=1.0
JI=I-1
DO 4 J=1,JI
II=I-J
C=C+Q
Q=Q+Q
4 AUX(II)=AUX(II+1)+(AUX(II+1)-AUX(II))/(Q-1.0)
C TESTAUSDRUCK.
IF(TEST3) WRITE(NO,1002) (AUX(J),J=1,NDIMAK)
1002 FCRMAT(' ',1P6D21.12)
C ENDE DER ROMBERG EXTRAPOLATION.
DFLT2=DABS(Y-AUX(1))
IF(TEST3) WRITE(NO,1003) DELT2
1003 FCRMAT(' DELT2=',1PE13.6)
C BEI GROSSEN INTERVALLEN NOCH KEINE FEHLERABFRAGE IN DEN ERSTEN
C ZWEI HALBIERUNGEN.
IF(I.LT.4.AND..NOT.INTKLF) GOTO 7
C RELATIVER FEHLER KLEINER GLEICH EPS?
IF(DELT2.EQ.0.0) GOTO 13
DELREL=DELT2/DMAX1(DABS(Y),DABS(ALX(1)))
IF(TEST3) WRITE(NO,1004) DELREL
1004 FCRMAT(' DELREL=',1PE13.6)
IF(DELREL.LE.EPS) GOTO 12
IF(I.LT.4) GOTO 7
IF(DELT2.GE.DFLT1) GOTO 11
7 JJ=JJ+JJ
NDIMP=1
RETURN 1
11 I7=I7+1
IF(I7.LE.1) GOTO 7
IADD=3
DELREL=-1.0

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IF(Y.NE.0.0) DELREL=DELT1/DABS(Y)
Y=H*Y
IF(DELREL.GT.EPS) GOTO 200
IADD=2
GOTO 201
13 DELREL=0.0
12 Y=H*AUX(1)
200 IF(IADD.NE.0) GOTO 201
IF(NDIMAK.LT.4) IADD=1
IF(NDIMAK.GE.4) IADD=2
201 YF(IADD)=YF(IADD)+Y
YFEPS(IADD)=AMAX1(YFEPS(IADD),DELREL)
C
CRUCK=.FALSE.
IF(DELREL.GT.CRINWA*EPS.OR.DELREL.EQ.-1.0) DRUCK=.TRUE.
IF(DRUCK) CALL FSWRCC(2004)
IF(TEST2.OR.DRUCK) WRITE(NO,1000) ITYP,ITYPFU,BSIGC,XL,XH,Y,EPS,
*DELREL,DELT1,DELT2,IADD,NDIMAK,(AUX(J),J=1,NDIMAK)
1000 FCRMAT(' ROMBERG ITYP=',I2,' IYTPFU=',I2,' SIGC=',1PE13.6,
*' XL=',1PE13.6,' XH=',1PE13.6,' Y=',1PE13.6/
*' ',8X,' EPS=',1PE13.6,' DELREL=',1PE13.6,' DFLT1=',1PE13.6,
*' DELT2=',1PE13.6,' IADD=',0P11,4X,'AUX(I),I=1,',I3,': '/
*(' ',8X,1P5E18.6))
333 RETURN
ENTRY FSR0MI(FPS,NDIM,CRINWA,YF,YFEPS,AUX)
GOTO 333
END
BLOCK DATA
COMMON/CFSOUR/ ICUR
DATA IDUR/0/
END
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NEFE=NFE
IF(NFF.EQ.1) NFFE=0
NCR=MM-NANF
NFA=MM+1-NENC
CALL DDPW (8HBEST ,NFEST(2))
CALL DDPW (8HSGA ,NN(1))
CALL DDPW (8HSGF ,NN(2))
CALL DDPW (8HSGN ,NN(3))
CALL DDPW (8HMUFL ,NN(4))
CALL DDPW (8HMUE ,NN(5))
CALL DDPW (8HSGC ,NN(6))
CALL DDPW (8HSTR ,NN(7))
CALL DDPW (8HALPHA ,NN(8))
CALL DDPW (8HETA ,NN(9))
CALL DDPW (8HSGG ,NN(10))
CALL DDPW (8HH 01 ,NN(11))
CALL DDPW (8HSGKE ,MMM)
INR=0
NFEST(1)=MAT
NFEST(3)=NN(2)
NSATZ(1)=3
CALL NDFLOC (NSUCH1,NSATZ,FFST,NUDAT,NC)
IF(NSUCH1) 1000,1000,1001
1000 ISPA=0
GO TO 1002
1001 ISPA=1
1002 IF(ISPA.EQ.IIS) GO TO 1003
1003 IF(ISPA.EQ.0) GO TO 2
LL=0
DO 3 I=1,ITYP
IF(ITNAM(I).EQ.NN(1)) GO TO 4
IF(ITNAM(I).NE.NN(2)) GO TO 3
4 LL=LL+1
IF(LL.EQ.2) GO TO 5
2 CONTINUE
8 WRITE (NOUTP,6) MAT
6 FORMAT(1H0/' ***WARNING 4. 1 : THE GROUP CROSS SECTION SGC CANNOT
BE CALCULATED FOR ',A9/19X,'BECAUSE THE REACTION TYPES SGA AND SGF
2 ARE NOT SPECIFIED IN THE INPUT')
GO TO 5
C
2 DO 7 I=1,ITYP
IF(ITNAM(I).EQ.NN(1)) GO TO 5
7 CONTINUE
GO TO 8
C
5 IGRUP=NEN-1
DO 9 I=NGR,IGRUP
9 SGC(I)=0.
JJJ=1
C
DO 10 JJ=1,ITYP
LETA=0
LALF=0

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IF(ITNAM(JJ).EQ.NN(5)) GO TO 124
IF(ITNAM(JJ).EQ.NN(9)) GO TO 124
IF(ITNAM(JJ).NE.NN(9)) GO TO 11
C
124 IF(ISPA.NE.0) GO TO 12
WRITE (NOUTP,13) MAT,ITNAM(JJ)
13 FORMAT(1H0/' ***WARNING 4. 2 : THE GROUP CROSS SECTION FOR ',2A9,
1' CANNOT BE CALCULATED, '/ 19X,'BECAUSE THE VALUES OF SCF ARE ZERO'
1)
DO 170 M=NGR,IGRUP
170 XINTF(M)=0.
K=NGR
GO TO 200
12 IF(ITNAM(JJ).NE.NN(5)) GO TO 14
81 NFEST(3)=NN(2)
GO TO 15
14 NFEST(3)=NN(10)
GO TO 15
C
11 IF(ITNAM(JJ).NE.NN(4)) GO TO 32
NFEST(3)=NN(3)
C
15 CALL NDFLOC (NSUCH1,NSATZ,FEST,NUDAT,NC)
MOD=0
JE=1
IF(NSUCH1)16,16,17
16 WRITE (NOUTP,18) (NFEST(I),I=1,3),ITNAM(JJ)
18 FORMAT(1H0/' ***WARNING 4. 3 : DATA FOR ',3A9,' COULD NOT BE FOUND
1 IN THE KEDAK LIBRARY '/19X,'THIS TYPE IS USED TO CALCULATE THE GR
2 GROUP CROSS SECTION ',A9)
SE(1)=ENG(NGR)
FSE(1)=0.
SE(2)=ENG(NEN)
FSE(2)=0.
GO TO 31
17 SE(1)=FEST(4)
FSE(1)=FEST(5)
IF(SE(1)-ENG(NGR))47,47,20
20 WRITE (NOUTP,21) ENG(NGR),(NFEST(I),I=1,3),SE(1)
21 FORMAT(1H0/' ***WARNING 4. 4 : THE LOWER ENERGY GROUP BOUNDARY ',
1E16.8,'EV IS NOT IN THE AVAILABLE ENERGY RANGE (N KEDAK FOR '/19X,
23A9,' THE LOWER ENERGY GROUP BOUNDARY HAS BEEN MODIFIED TO ',
3E16.8,'EV')
47 M=2
26 CALL NDFNXT (NSUCH1,NSATZ,FEST,NUDAT,NC)
IF(NSUCH1)22,22,23
23 IF(FFEST(4)-FNG(NGR))24,24,25
24 SF(1)=FEST(4)
FSE(1)=FEST(5)
GO TO 26
25 IF(JB.EQ.2) GO TO 902
IF(FEST(5).EQ.0.AND.FSE(1).EQ.0.AND.ITNAM(JJ).EQ.NN(5)) GO TO 900
IF(FEST(5).EQ.0.AND.FSE(1).EQ.0.AND.ITNAM(JJ).EQ.NN(4)) GO TO 24
IF(FEST(5).EQ.0.AND.FSE(1).EQ.0.AND.LETA.EQ.1) GO TO 24
GO TO 175
900 FEST(5)=1.E20
MOD=1

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WRITE (NOUTP,901) SE(1),FEST(4)
901 FORMAT(1H0/' ***MESSAGE 4. 8 : FOR THE CALCULATION OF NUE SGF IS
IMODIFIED FROM 0. TO 1.E20'/19X,'AT THE ENERGYPOINTS',E16.8,' AND',
2E16.8)
GO TO 902
175 JB=2
902 IF(FEST(4)-ENG(NEN))27,28,28
27 SE(M)=FEST(4)
FSE(M)=FEST(5)
M=M+1
IF(M-LDIM)26,26,29
29 M=1
LDIF=LDIF+1
GO TO 26
22 M=M-1
GO TO 30
28 SE(M)=FEST(4)
FSE(M)=FEST(5)
IF(MOD.EQ.1.AND.ITNAM(JJ).EQ.NN(5)) FSE(1)=1.E20
30 DO 180 I=1,M
IF(FSE(I).GE.0) GO TO 180
172 WRITE (NOUTP,171) FEST(1),FEST(3),SE(I),FSE(I)
171 FORMAT(/2A1),' ENERGY',E16.8,' CROSS SECTION ON KEDAK NEGATIVE',
1E16.8)
180 CONTINUE
IF(LDIF.EQ.0) GO TO 31
LDIMP=(LDIF-1)*LDIM+M+1
WRITE (NOUTP,400) ITNAM(JJ)
400 FORMAT(1H0/' ***MESSAGE 4. 2 : STORAGE NOT SUFFICIENT TO CALCULATE
1 ',A9)
RETURN
C
31 IS=1
GO TO 34
32 IS=0
34 DO 33 I=NGR,IGRUP
ZINT(I)=0.
XNEN(I)=0.
33 DUE(I)=0.
I=NGR
K=NGR
C
IF(ITNAM(JJ).EQ.NN(4)) GO TO 125
IF(ITNAM(JJ).NE.NN(5)) GO TO 35
125 NFEST(3)=ITNAM(JJ)
476 E(3)=AMAX1(ENG(I),SF(1))
42 IF(E(3).LT.ENG(I+1)) GO TO 76
I=I+1
IF(I.GT.IGRUP) GO TO 10
GO TO 42
76 CALL NDFLOC (NSUCH1,NSATZ,FEST,NUDAT,NC)
IF(NSUCH1) 36,36,37
36 WRITE (NOUTP,38) (NFEST(J),J=1,3)
38 FORMAT(1H0/' ***WARNING 4. 5 : DATA FOR ',A9,' COULD NOT BE FOUND
1 IN THE KEDAK LIBRARY')
GO TO 300

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37 IF(FEST(4)-E(3) ) 39,39,40
40 WRITE (NOUTP,21) ENG(I),(NFEST(J),J=1,3),FEST(4)
IF(FEST(4)-ENG(I+1))39,304,304
39 E(1)=FEST(4)
F(1)=FEST(5)
IF(FEST(3).EQ.NN(4)) GO TO 173
IF(F(1).GE.0) GO TO 173
WRITE (NOUTP,171) FEST(1),FEST(3),E(1),F(1)
173 CALL NDFNXT (NSUCH1,NSATZ,FEST,NUDAT,NC)
IF(NSUCH1)43,43,44
43 WRITE (NOUTP,45) (FEST(J),J=1,3)
45 FORMAT (1H0/' ***WARNING 4. 6 : DATA FOR ',A9,' ARE NOT AVAILABLE
1 ON KEDAK IN THE DESIRED ENERGY GROUPS')
GO TO 10
44 IF(FEST(4)-E(3) )39,39,46
46 IF (F(1).EQ.0.AND.FEST(5).EQ.0) GO TO 39
E(2)=FEST(4)
F(2)=FEST(5)
IF(FEST(3).EQ.NN(4)) GO TO 174
IF(F(2).GE.0) GO TO 174
WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)
C
174 E(3)=AMAX1(ENG(I),E(1),SE(1))
921 IF(E(3).LT.ENG(I+1)) GO TO 925
I=I+1
IF(I.LE.IGRUP) GO TO 921
WRITE (NOUTP,477) MAT,ITNAM(JJ),NFEST(3)
477 FORMAT(' ***WARNING 4. 8 : ',A9,' TYPE ',A9,' CANNOT BE CALCULATED,
1 BECAUSE ',A9,' IS NOT'/19X,'AVAILABLE ON KEDAK IN THE DESIRED ENE
2RGY RANGE')
GO TO 10
925 MARK=0
WRITE(NOUTP,48)E(3)
48 FORMAT(1H0/' ***MESSAGE 4. 1 : BEGIN OF THE INTEGRATION AT',E16.8,
1' EV')
K=I
II=1
SF(1)=FSE(1)
F(3)=F(1)
IF(E(3).EQ.SE(1)) GO TO 49
L=0
IF(E(3).EQ.E(1)) GO TO 50
L=1
50 DO 60 II=1,M
IF(SE(II)-E(3))60,260,61
260 IF(ITNAM(JJ).NE.NN(5)) GO TO 903
IF(MOD.EQ.0) GO TO 903
CALL GRUP (I,II,M,ENG,SE,FSE,SF(1),MOD)
903 SF(1)=FSE(II)
GO TO 261
60 CONTINUE
61 II=II-1
IF(ITNAM(JJ).NE.NN(5)) GO TO 907
IF(MOD.EQ.0) GO TO 907
CALL GRUP (I,II,M,ENG,SE,FSE,SF(1),MOD)
907 SF(1)=FSE(II)+(FSE(II+1)-FSE(II))/(SE(II+1)-SE(II))*(E(3)-SE(II))

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261 IF(L.EQ.0) GO TO 51	2410		
49 F(3)=F(1)+(F(2)-F(1))/(E(2)-E(1))*(E(3)-E(1))	2420		
C	2430		
51 IF(NFE.EQ.1) GO TO 56	2440		
DO 53 NI=1,NFE	2450		
IF(REFE(NI)-E(3))53,54,55	2460		
53 CONTINUE	2470		
54 FLUSS(1)=EFE(NI)	2480		
NI=NI+1	2490		
GO TO 56	2500		
55 FLUSS(1)=EFE(NI-1)+(EFE(NI)-EFE(NI-1))/(REFE(NI)-REFE(NI-1))*(E(3)-REFE(NI-1))	2510		
C	2520		
56 II=II+1	2530		
67 KW=0	2540		
C	2550		
IF(NFE.EQ.1) GO TO 57	2560		
E(4)=AMINI(ENG(I+1),E(2),SE(II),REFE(NI))	2570		
IF(ITNAM(JJ).NE.NM(5)) GO TO 911	2580		
IF(MOD(EQ.0) GO TO 911	2590		
IF(MARK.EQ.0) GO TO 911	2600		
MARK=0	2610		
CALL GRUP (I,II,M,ENG,SE,FSE,SF(1),MOD)	2620		
911 IF(E(4).EQ.ENG(I+1)) GO TO 58	2630		
IF(E(4).EQ.E(2)) GO TO 59	2640		
IF(E(4).EQ.SE(II)) GO TO 62	2650		
FLUSS(2)=EFE(NI)	2660		
NI=NI+1	2670		
63 CALL FL (FSE(II-1),FSE(II),SE(II-1),SE(II),E(4),SF(2))	2680		
164 CALL FL(F(1),F(2),E(1),E(2),E(4),F(4))	2690		
GO TO 66	2700		
58 IF(E(4).NE.E(2).AND.E(4).NE.SE(II).AND.E(4).NE.REFE(NI)) GO TO 1157	2710		
1157	2720		
IW=0	2730		
IK=0	2740		
IF=0	2750		
IF(E(4).EQ.E(2)) GO TO 158	2760		
162 IF(E(4).EQ.SE(II)) GO TO 159	2770		
163 IF(E(4).EQ.REFE(NI)) GO TO 160	2780		
GO TO 165	2790		
158 F(4)=F(2)	2800		
E(1)=E(2)	2810		
F(1)=F(2)	2820		
CALL NDFNXT(INSUCH1,NSATZ,FEST,NUDAT,NC)	2830		
IF(INSUCH1.LE.0) GO TO 161	2840		
E(2)=FEST(4)	2850		
F(2)=FEST(5)	2860		
IW=1	2870		
IF(FEST(3).EQ.MN(4)) GO TO 162	2880		
IF(F(2).GE.0) GO TO 162	2890		
WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)	2900		
GO TO 162	2910		
159 SF(2)=FSE(II)	2920		
II=II+1	2930		
IK=1	2940		
	2950		
		GO TO 163	2960
		160 FLUSS(2)=EFE(NI)	2970
		NI=NI+1	2980
		IF=1	2990
		165 IF(IF.EQ.0) GO TO 166	3000
		167 IF(IK.EQ.1.AND.IW.EQ.0) GO TO 164	3010
		IF(IK.EQ.1.AND.IW.EQ.1) GO TO 66	3020
		IF(IK.EQ.0.AND.IW.EQ.0) GO TO 63	3030
		CALL FL (FSE(II-1),FSE(II),SE(II-1),SE(II),E(4),SF(2))	3040
		GO TO 66	3050
		166 CALL FL (EFE(NI-1),EFE(NI),REFE(NI-1),REFE(NI),E(4),FLUSS(2))	3060
		GO TO 167	3070
		157 CALL FL(EFE(NI-1),EFE(NI),REFE(NI-1),REFE(NI),E(4),FLUSS(2))	3080
		GO TO 63	3090
		59 F(4)=F(2)	3100
		E(1)=E(2)	3110
		F(1)=F(2)	3120
		CALL NDFNXT(INSUCH1,NSATZ,FEST,NUDAT,NC)	3130
		IF(INSUCH1.GT.0) GO TO 65	3140
		161 WRITE(NOUTP,68) (FEST(J),J=1,3),E(2)	3150
		68 FORMAT(1H0/' ***WARNING 4. 7 : FOR',3A9,' NO DATA ARE AVAILABLE AF	3160
		ITER',E16.8,' EV')	3170
		KW=1	3180
		GO TO 73	3190
		65 E(2)=FEST(4)	3200
		F(2)=FEST(5)	3210
		IF(FEST(3).EQ.MN(4)) GO TO 176	3220
		IF(F(2).GE.0) GO TO 176	3230
		WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)	3240
		176 IF(E(4).NE.SE(II).AND.E(4).NE.REFE(NI)) GO TO 152	3250
		IW=0	3260
		IF(E(4).EQ.SE(II)) GO TO 153	3270
		155 IF(E(4).EQ.REFE(NI)) GO TO 154	3280
		153 SF(2)=FSE(II)	3290
		II=II+1	3300
		LW=1	3310
		IF(E(4).NE.REFE(NI)) GO TO 156	3320
		154 FLUSS(2)=EFE(NI)	3330
		NI=NI+1	3340
		IF(LW.EQ.1) GO TO 66	3350
		CALL FL (FSE(II-1),FSE(II),SE(II-1),SE(II),E(4),SF(2))	3360
		GO TO 66	3370
		152 CALL FL (FSE(II-1),FSE(II),SE(II-1),SE(II),E(4),SF(2))	3380
		156 CALL FL(EFE(NI-1),EFE(NI),REFE(NI-1),REFE(NI),E(4),FLUSS(2))	3390
		GO TO 66	3400
		62 SF(2)=FSE(II)	3410
		II=II+1	3420
		IF(E(4).NE.REFE(NI)) GO TO 150	3430
		FLUSS(2)=EFE(NI)	3440
		NI=NI+1	3450
		GO TO 151	3460
		150 CALL FL(EFE(NI-1),EFE(NI),REFE(NI-1),REFE(NI),E(4),FLUSS(2))	3470
		151 CALL FL(F(1),F(2),E(1),E(2),E(4),F(4))	3480
		66 IF(LALF.EQ.1) GO TO 77	3490
		_ZINT(1)=ZINT(1)+(F(3)*SF(1)*FLUSS(1)+F(4)*SF(2)*FLUSS(2))*0.5*(3500

1E(4)-E(3))	3510		
XNEN(I)=XNEN(I)+(SF(1)*FLUSS(1)+SF(2)*FLUSS(2))*0.5*(E(4)-E(3))	3520	70 Z2=0.	4060
79 E(3)=E(4)	3530	X2=0.	4070
FLUSS(1)=FLUSS(2)	3540	EE33=E(3)	4080
F(3)=F(4)	3550	FLUSS(1)=PHI(EE33)	4090
SF(1)=SF(2)	3560	SF(1)=S	4100
IF(E(4).NE.ENG(I+1)) GO TO 67	3570	F(3)=FF	4110
73 XINTE(I)=ZINT(I)/XNEN(I)	3580	LL=1	4120
I=I+1	3590	69 EE44=E(3)+(E(4)-E(3))/FLOAT(MN)*FLOAT(LL)	4130
MARK=1	3600	121 CALL FL(FSE(II-1),FSE(II),SE(II-1),SE(II),EE44,SF(2))	4140
E(3)=E(4)	3610	CALL FL(F(1),F(2),E(1),E(2),EE44,F(4))	4150
F(3)=F(4)	3620	FLUSS(2)=PHI(EE44)	4160
IF(E(4).EQ.SE(II)) II=II+1	3630	IF(LALF.EQ.1) GO TO 77	4170
IF(E(4).NE.E(2)) GO TO 115	3640	Z2=Z2+(F(3)*SF(1)*FLUSS(1)+F(4)*SF(2)*FLUSS(2))*0.5*(EE44-EE33)	4180
E(1)=E(2)	3650	X2=X2+(SF(1)*FLUSS(1)+SF(2)*FLUSS(2))*0.5*(EE44-EE33)	4190
F(1)=F(2)	3660	80 LL=LL+1	4200
CALL NDFNXT(NSUCH1,NSATZ,FEST,NUDAT,NC)	3670	EE33=EE44	4210
IF(NSUCH1.GT.0) GO TO 64	3680	F(3)=F(4)	4220
264 WRITE (NOUTP,68) (FEST(J),J=1,3),E(2)	3690	SF(1)=SF(2)	4230
GO TO 200	3700	FLUSS(1)=FLUSS(2)	4240
64 E(2)=FEST(4)	3710	IF(LL.LT.MN) GO TO 69	4250
F(2)=FEST(5)	3720	IF(LL.GT.MN) GO TO (71,72),L	4260
IF(FEST(3).EQ.NN(4)) GO TO 115	3730	EE44=E(4)	4270
IF(F(2).GE.0) GO TO 115	3740	GO TO 121	4280
WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)	3750	71 Z1=Z2	4290
115 IF(KW.EQ.1) GO TO 200	3760	X1=X2	4300
IF(I.GT.IGRUP) GO TO 200	3770	MN=MN*2	4310
GO TO 67	3780	L=2	4320
	3790	GO TO 70	4330
C	3800	72 IF(Z1.EQ.0..OR.X1.EQ.0.) GO TO 111	4340
57 E(4)=AMINI(ENG(I+1),E(2),SF(II))	3810	IF((Z1-Z2)/Z1.GT.RFEHL. OR.(X1-X2)/X1.GT.RFEHL) GO TO 71	4350
IF(ITNAM(JJ).NE.NN(5)) GO TO 912	3820	GO TO 112	4360
IF(MOD.EQ.0) GO TO 912	3830	111 IF(Z1.EQ.0..AND.X1.EQ.0.) GO TO 114	4370
IF(MARK.EQ.0) GO TO 912	3840	IF(Z1.EQ.0.) GO TO 113	4380
MARK=0	3850	IF((Z1-Z2)/Z1.GT.RFEHL) GO TO 71	4390
CALL GRUP (I,I),M,ENG,SE,FSE,SF(1),MOD)	3860	GO TO 112	4400
912 IF((E(4)-E(3))/E(3).GE.1.E-3) GO TO 143	3870	113 IF((X1-X2)/X1.GT.RFEHL) GO TO 71	4410
IF(E(4).EQ.E(3)) GO TO 114	3880	112 ZINT(I)=ZINT(I)+Z2	4420
FLUSS(1)=PHI(E(3))	3890	XNEN(I)=XNEN(I)+X2	4430
FLUSS(2)=PHI(E(4))	3900	114 IF(E(4).EQ.ENG(I+1)) GO TO 73	4440
CALL FL (FSE(II-1),FSE(II),SE(II-1),SE(II),E(4),SF(2))	3910	E(3)=E(4)	4450
CALL FL (F(1),F(2),E(1),E(2),E(4),F(4))	3920	F(3)=F(4)	4460
IF(LALF.EQ.1) GO TO 144	3930	IF(E(4).EQ.E(2)) GO TO 74	4470
Z2=(F(3)*SF(1)*FLUSS(1)+F(4)*SF(2)*FLUSS(2))*0.5*(E(4)-E(3))	3940	II=II+1	4480
X2=(SF(1)*FLUSS(1)+SF(2)*FLUSS(2))*0.5*(E(4)-E(3))	3950	GO TO 57	4490
GO TO 145	3960	74 E(1)=E(2)	4500
144 Z2=(SF(1)*FLUSS(1)+SF(2)*FLUSS(2))*0.5*(E(4)-E(3))	3970	F(1)=F(2)	4510
X2=(F(3)*FLUSS(1)+F(4)*FLUSS(2))*0.5*(E(4)-E(3))	3980	CALL NDFNXT(NSUCH1,NSATZ,FEST,NUDAT,NC)	4520
145 F(3)=F(4)	3990	IF(NSUCH1.LE.0) GO TO 73	4530
SF(1)=SF(2)	4000	E(2)=FEST(4)	4540
FLUSS(1)=FLUSS(2)	4010	F(2)=FEST(5)	4550
GO TO 112	4020	IF(FEST(3).EQ.NN(4)) GO TO 177	4560
143 L=1	4030	IF(F(2).GE.0) GO TO 177	4570
MN=3	4040	WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)	4580
S=SF(1)	4050	177 IF(E(1).EQ.SE(II)) II=II+1	4590
FF=F(3)		GO TO 57	4600

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C
35 IF(ITNAM(JJ).EQ.NN(8)) GO TO 123
   IF(ITNAM(JJ).NE.NN(9)) GO TO 75
123 IF(LETA.EQ.0) GO TO 82
   NFEST(3)=NN(5)
   GO TO 476
82 NFEST(3)=NN(2)
   LALF=1
   GO TO 476
77 IF(NFE.EQ.1) GO TO 78
   ZINT(I)=ZINT(I)+(SF(1)*FLUSS(1)+SF(2)*FLUSS(2))*0.5*(E(4)-E(3))
   XNEN(I)=XNEN(I)+(F(3)*FLUSS(1)+F(4)*FLUSS(2))*0.5*(E(4)-E(3))
   GO TO 79
78 Z2=Z2+(SF(1)*FLUSS(1)+SF(2)*FLUSS(2))*0.5*(EE44-EE33)
   X2=X2+(F(3)*FLUSS(1)+F(4)*FLUSS(2))*0.5*(EE44-EE33)
   GO TO 80

C
75 NFEST(3)=ITNAM(JJ)
   CALL NDFLOC (NSUCH1,NSATZ,FEST,NUDAT,NC)
   IF(NSUCH1)36,36,83
83 IF(FEST(4)-ENG(I))84,84,85
85 WRITE (NOUTP,21) ENG(I),(NFEST(J),J=1,3),FEST(4)
87 IF(FEST(4)-ENG(I+1))84,86,86
86 XINTE(I)=0.
   I=I+1
   IF(I-IGRUP)87,87,303
84 E(1)=FEST(4)
   F(1)=FEST(5)
   IF(FEST(3).EQ.NN(4)) GO TO 181
   IF(F(1).GE.0) GO TO 181
   WRITE (NOUTP,171) FEST(1),FEST(3),E(1),F(1)
181 CALL NDFNXT(NSUCH1,NSATZ,FEST,NUDAT,NC)
   IF(NSUCH1)43,43,88
88 IF(FEST(4)-ENG(I))84,84,89
89 E(2)=FEST(4)
   F(2)=FEST(5)
   IF(FEST(3).EQ.NN(4)) GO TO 178
   IF(F(2).GE.0) GO TO 178
   WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)
178 E(3)=AMAX1(ENG(I),E(1))
   WRITE (NOUTP,48)E(3)
91 IF(E(3).LT.ENG(I+1)) GO TO 90
   I=I+1
   IF(I.GT.IGRUP) GO TO 10
   GO TO 91
90 K=I
   F(3)=F(1)+(F(2)-F(1))/(E(2)-E(1))*(E(3)-E(1))

C
   IF(NFE.EQ.1) GO TO 96
   DO 93 NI=1,NFE
   IF(REFE(NI)-E(3))93,94,95
93 CONTINUE
94 FLUSS(1)=EFE(NI)
   NI=NI+1
   GO TO 96
95 FLUSS(1)=EFE(NI-1)+(EFE(NI)-EFE(NI-1))/(REFE(NI)-REFE(NI-1))*(E(3)

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1-REFE(NI-1))
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96 KW=0
   IF(NFE.EQ.1) GO TO 105
   E(4)=AMIN1(ENG(I+1),E(2),REFE(NI))
   IF(E(4).EQ.ENG(I+1)) GO TO 97
   IF(E(4).EQ.E(2)) GO TO 98
   FLUSS(2)=EFE(NI)
   NI=NI+1
100 CALL FL (F(1),F(2),E(1),E(2),E(4),F(4))
   GO TO 99
97 IF(E(4).NE.E(2).AND.E(4).NE.REFE(NI)) GO TO 131
   IW=0
   IK=0
   IF(E(4).EQ.E(2)) GO TO 132
136 IF(E(4).EQ.REFE(NI)) GO TO 133
   GO TO 140
132 F(4)=F(2)
   E(1)=E(2)
   F(1)=F(2)
   IW=1
   CALL NDFNXT(NSUCH1,NSATZ,FEST,NUDAT,NC)
   IF(NSUCH1.LE.0) GO TO 135
   E(2)=FEST(4)
   F(2)=FEST(5)
   IF(FEST(3).EQ.NN(4)) GO TO 136
   IF(F(2).GE.0) GO TO 136
   WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)
   GO TO 136
133 FLUSS(2)=EFE(NI)
   NI=NI+1
   IK=1
140 IF(IW.EQ.1.AND.IK.EQ.1) GO TO 99
   IF(IW.EQ.1.AND.IK.EQ.0) GO TO 137
   GO TO 100
137 CALL FL (EFE(NI-1),EFE(NI),REFE(NI-1),REFE(NI),E(4),FLUSS(2))
   GO TO 99
131 CALL FL (EFE(NI-1),EFE(NI),REFE(NI-1),REFE(NI),E(4),FLUSS(2))
   GO TO 100
98 F(4)=F(2)
   E(1)=E(2)
   F(1)=F(2)
   CALL NDFNXT(NSUCH1,NSATZ,FEST,NUDAT,NC)
   IF(NSUCH1.GT.0) GO TO 102
135 WRITE (NOUTP,68) (FEST(J),J=1,3),E(2)
   KW=1
   GO TO 103
102 E(2)=FEST(4)
   F(2)=FEST(5)
   IF(FEST(3).EQ.NN(4)) GO TO 179
   IF(F(2).GE.0) GO TO 179
   WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)
179 IF(E(4).EQ.REFE(NI)) GO TO 130
   CALL FL(EFE(NI-1),EFE(NI),REFE(NI-1),REFE(NI),E(4),FLUSS(2))
   GO TO 99

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130 FLUSS(2)=EFE(NI)
    NI=NI+1
99 ZINT(I)=ZINT(I)+(F(3)*FLUSS(1)+F(4)*FLUSS(2))*0.5*(E(4)-E(3))
    XNEN(I)=XNEN(I)+(FLUSS(1)+FLUSS(2))*0.5*(E(4)-E(3))
    IF(MAT.NE.NN(11)) GO TO 104
    IF(ITNAM(JJ).NE.NN(3)) GO TO 104
    EN=ALOG(E(4)/E(3))
    SF1=F(3)*FLUSS(1)
    SF3=F(4)*FLUSS(2)
    DUE(I)=DUE(I)+SF1*EN+SF3-SF1-(SF3-SF1)/(E(4)-E(3))*E(3)*EN
104 E(3)=E(4)
    FLUSS(1)=FLUSS(2)
    F(3)=F(4)
    IF(E(4).NE.ENG(I+1)) GO TO 96
103 XINTE(I)=ZINT(I)/XNEN(I)
    IF(MAT.EQ.NN(11).AND.ITNAM(JJ).EQ.NN(3)) STREU(I)=DUE(I)/XNEN(I)
    I=I+1
    E(3)=E(4)
    F(3)=F(4)
    IF(E(4).NE.E(2)) GO TO 120
    E(1)=E(2)
    F(1)=F(2)
    CALL NDFNXT(NSUCH1,NSATZ,FEST,NUDAT,NC)
    IF(NSUCH1.GT.0) GO TO 101
265 WRITE (NOUTP,68) (FEST(J),J=1,3),E(2)
    GO TO 200
101 E(2)=FEST(4)
    F(2)=FEST(5)
    IF(FEST(3).EQ.NN(4)) GO TO 120
    IF(F(2).GE.0) GO TO 120
    WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)
120 IF(KW.EQ.1) GO TO 200
    IF(I.GT.IGRUP) GO TO 200
    GO TO 96
C
105 E(4)=AMINI(ENG(I+1),E(2))
    IF((E(4)-E(3))/E(3).GE.1.E-3) GO TO 141
    FLUSS(1)=PHI(E(3))
    FLUSS(2)=PHI(E(4))
    CALL FL (F(1),F(2),E(1),E(2),E(4),F(4))
    Z2=(F(3)*FLUSS(1)+F(4)*FLUSS(2))*0.5*(E(4)-E(3))
    X2=(FLUSS(1)+FLUSS(2))*0.5*(E(4)-E(3))
    IF(MAT.NE.NN(11)) GO TO 142
    IF(ITNAM(JJ).NE.NN(3)) GO TO 142
    EN=ALOG(E(4)/E(3))
    SF1=F(3)*FLUSS(1)
    SF3=F(4)*FLUSS(2)
    Z3=SF1*EN+SF3-SF1-(SF3-SF1)/(E(4)-E(3))*E(3)*EN
142 FLUSS(1)=FLUSS(2)
    F(3)=F(4)
    GO TO 117
141 L=1
    MN=3
    FF=F(3)
110 Z2=0.

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Z3=0.
X2=0.
EE33=E(3)
FLUSS(1)=PHI(EE33)
F(3)=FF
LL=1
107 EE44=E(3)+(E(4)-E(3))/FLOAT(MN)*FLOAT(LL)
122 CALL FL (F(1),F(2),E(1),E(2),EE44,F(4))
    FLUSS(2)=PHI(EE44)
    Z2=Z2+(F(3)*FLUSS(1)+F(4)*FLUSS(2))*0.5*(EE44-EE33)
    X2=X2+(FLUSS(1)+FLUSS(2))*0.5*(EE44-EE33)
C
    IF(MAT.NE.NN(11)) GO TO 106
    IF(ITNAM(JJ).NE.NN(3)) GO TO 106
    EN=ALOG(EE44/EE33)
    SF1=F(3)*FLUSS(1)
    SF3=F(4)*FLUSS(2)
    Z3=Z3+SF1*EN+SF3-SF1-(SF3-SF1)/(EE44-EE33)*EE33*EN
C
106 LL=LL+1
    EE33=EE44
    F(3)=F(4)
    FLUSS(1)=FLUSS(2)
    IF(LL.LT.MN) GO TO 107
    IF(LL.GT.MN) GO TO (108,109),L
    EE44=E(4)
    GO TO 122
108 Z1=Z2
    X1=X2
    MN=MN*2
    L=2
    GO TO 110
109 IF(Z1.EQ.0..OR.X1.EQ.0.) GO TO 116
    IF((Z1-Z2)/Z1.GT.RFEHL..OR.(X1-X2)/X1.GT.RFEHL) GO TO 108
    GO TO 117
116 IF(Z1.EQ.0..AND.X1.EQ.0.) GO TO 118
    IF(Z1.EQ.0.) GO TO 119
    IF((Z1-Z2)/Z1.GT.RFEHL) GO TO 108
    GO TO 117
119 IF((X1-X2)/X1.GT.RFEHL) GO TO 108
117 ZINT(I)=ZINT(I)+Z2
    XNEN(I)=XNEN(I)+X2
118 IF(MAT.EQ.NN(11).AND.ITNAM(JJ).EQ.NN(3)) DUE(I)=DUE(I)+Z3
    IF(E(4).EQ.ENG(I+1)) GO TO 103
    E(3)=E(4)
    F(3)=F(4)
    E(1)=E(2)
    F(1)=F(2)
    CALL NDFNXT(NSUCH1,NSATZ,FEST,NUDAT,NC)
    IF(NSUCH1.LE.0) GOTO 103
    E(2)=FEST(4)
    F(2)=FEST(5)
    IF(FEST(3).EQ.NN(4)) GO TO 105
    IF(F(2).GE.0) GO TO 105
    WRITE (NOUTP,171) FEST(1),FEST(3),E(2),F(2)

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C      GC TO 105
C      AUSDRUCKEN DER ERGEBNISSE
C
200 IF(ITNAM(JJ).NE.NN(9)) GO TO 211
    IF(LETA.EQ.1) GO TO 213
    DO 212 N=K,IGRUP
212 STREU(N)=XINTE(N)
    LETA=1
    LALF=0
    GO TO 81
213 DO 214 N=K,IGRUP
214 XINTE(N)=XINTE(N)/(1.+STREU(N))
211 IF(JJJ.EQ.2) GO TO 201
    N=0
    WRITE (JA) N,MMM
    JJJ=2
201 NNN=NEN-1
    N=2
    WRITE (JA) N,K,NNN
    IST=MM-K
    NI=MM-NNN
    WRITE (NOUTP,202) MAT,ITNAM(JJ),IST,NI
202 FORMAT(IH0,2A9,3X,'GRUPPE',I3,' BIS',I3)
    N=4
    WRITE (JA) N,MAT,ITNAM(JJ)
    N=NEN-K
    WRITE (JA) N,(XINTE(LL),LL=K,IGRUP)
    WRITE (NOUTP,203) (XINTE(LL),LL=K,IGRUP)
203 FORMAT(IH ,7E16.8/(1X,7E16.8))
    IF(ITNAM(JJ).EQ.NN(1)) GO TO 204
    IF(ITNAM(JJ).EQ.NN(2)) GO TO 205
    GO TO 206
204 DO 207 N=K,IGRUP
207 SGC(N)=SGC(N)+XINTE(N)
    IF(INR.EQ.1) GO TO 210
    INR=1
    GO TO 10
205 DO 209 N=K,IGRUP
209 SGC(N)=SGC(N)-XINTE(N)
    IF(INR.EQ.1) GO TO 210
    INR=1
    GO TO 10
210 N=2
    WRITE (JA) N,K,NNN
    N=4
    WRITE (JA) N,MAT,NN(6)
    N=NEN-K
    WRITE (JA) N,(SGC(LL),LL=K,IGRUP)
    WRITE (NOUTP,202) MAT,NN(6),IST,NI
    WRITE (NOUTP,203) (SGC(LL),LL=K,IGRUP)
    GO TO 10
206 IF(MAT.NE.NN(11)) GO TO 10
    IF(ITNAM(JJ).NE.NN(3)) GO TO 10
    N=2

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    WRITE (JA) N,K,NNN
    N=4
    WRITE (JA) N,MAT,NN(7)
    N=NEN-K
    WRITE (JA) N,(STREU(LL),LL=K,IGRUP)
    WRITE (NOUTP,202) MAT,NN(7),IST,NI
    WRITE (NOUTP,203) (STREU(LL),LL=K,IGRUP)
    GO TO 10
C
300 IF(I-IGRUP)301,301,303
301 DO 302 N=I,IGRUP
302 XINTE(N)=0.
    GO TO 303
304 XINTE(I)=0.
    I=I+1
    IF(I-IGRUP)37,37,303
303 NNN=NEN-1
    IF(MM-K.LT.MM-NNN) GO TO 10
    GO TO 200
10 CONTINUE
C
    ISPA=IIS
    KL=KL+1
    RETURN
    END
    SLBRCUTINE FL(EFE1,EFE2,REFE1,REFE2,E,ERG)
    FRG=EFE1+(EFE2-EFE1)/(REFE2-REFE1)*(E-REFE1)
    RETURN
    END
    SLBROUTINE GRUP (I,II,M,ENG,SE,FSE,SF,MDC)
    DIMENSION ENG(I),SE(M),FSE(M)
    DC 1 NI=II,M
    IF( SE(NI).GE.ENG(I+1)) GO TO 2
1 CONTINUE
2 IF(FSE(NI).EQ.1.E20) GO TO 4
    CC 3 MI=1,NI
3 IF(FSE(MI).EQ.1.E20) FSE(MI)=0.
    IF(SF.EQ.1.F2C) SF=0.
    MDC=0
4 RETURN
    END

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C*****SUBROUTINE SCAT.DATE OF LAST CHANGE 21.12. 1976.(LINES 10 TO
C*****3650)
C CALCULATION OF THE INELASTIC SCATTERING PROBABILITIES
C
SUBROUTINE SCAT(INX,EG,XNUE,NFE,EF,FI,NE27,KINEI,NIN,NINA,INTYP,X,
IIX,MMAXX,MFELD)
REAL*8 NAM,NAM4,NP
DIMENSION EG(NX),EF(NFE),FI(NFE),X(MMAXX),IX(MMAXX),NP(3),NAM4(3),
IINTYP(3),MFELDC(3)
COMMON NAM,ISTRUK,ISPA,NA,LIZ,NAF,NEND,KL
AUSDRUCK DER DIMENSIONEN FUER HILFSFELDER
C WRITE(NA,2000) (EG(I GEN),IGEN=1,AX)
C2000 FCRMAT(6E15.9)
IA=0
NAB=0
IAC=0
NABD=0
IAC=0
NABC=0
IFELD=0
IT=1
KI=2
MFELD=0
MFELDD=0
MFELDC(1)=0
MFELDC(2)=0
MFELDC(3)=0
46 DO 44 I=1,MMAXX
X(I)=0.
44 IX(I)=0
CALL DOPW(8HSMTOT ,NAM4(1))
CALL DOPW(8HSMTOT2N ,NAM4(2))
CALL DOPW(8HSMTOT3N ,NAM4(3))
CALL DOPW(8HPROBSGI ,NP(1))
CALL DOPW(8HPROBSG2N,NP(2))
CALL DOPW(8HPROBSG3N,NP(3))
IF(INTYP(IT).EQ.2.OR.INTYP(IT).EQ.3) GO TO 45
C*****ESTIMATED VALUES OF THE DIMENSIONS OF THE WORKING FIELDS
C*****USED IN SCATD.
NAEP=0
ISGP=0
NISGP=0
NAE=30
ISG=200
NISG=400
C*****ORGANIZATION OF THE WORKING FIELDS FOR SUBROUTINE SCATD.
7 NAE=NAE+NAEP
ISG=ISG+ISGP
NISG=NISG+NISGP
NAEP=0
ISGP=0
NISGP=0
IF(INTYP(IT).EQ.2) CALL DOPW(8HSG2N ,TYP)
IF(INTYP(IT).EQ.3) CALL DOPW(8HSG3N ,TYP)
C WRITE(NA,1013) NAE,ISG,NISG,NAEP,ISGP,NISGP
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C1013 FCRMAT('NAE=',I10,' ISG=',I10,' NISG=',I10,
C */' NAEP=',I10,' ISGP=',I10,' NISGP=',I10)
C WIRD MAXIMALE DIMENSION UEBERSCHRITTEN?
L1=1
L2=L1+NX*NX
L3=(L2+NX)/2*2+3
L4=L3+2*NX
L5=L4+2*NX
L6=L5+2*NE27
L7=L6+2*NAE
L8=L7+NX
L9=L8+NX
L10=L9+ISG
L11=L10+NAE
L12=L11+ISG*NAE
L13=(L12+ISG)/2*2+3
L14=L13+2*NISG
MFELDD=L14
C WRITE(NA,1006) L14,MMAXX
C1006 FORMAT('/' BENOETIGTE FELDLAENGE',I10,
C */ ' VERFUEGBARE FELDLAENGE',I10)
IF(L14.LE.MMAXX) GO TO 4
C WRITE(NA,1014) L14,MMAXX
C1014 FORMAT('OSUMME DER LAENGEN ALLER EINZELNEN HILFSFELDER GLEICH ',
C *I12,' WORTE'/' DIESE ZAHL UEBERSTEIGT DIE MAXIMALE DIMENSION VON
C *I12,' WORTEN.'/' VERGROESSERN SIE DIF REGION UM DIE MAXIMALE DI
C *MENSION MMAXX UND STARTEN SIE DAS PROGRAMM ERNEUT. ')
MFELDD=L14
IFELD=1
NINA=IT
GC TC 100
4 CONTINUE
45 WRITE(NA,9000)
9000 FORMAT('///// PROGRAMM KENNZIFFER 5')
WRITE(NA,9001)
9001 FCRMAT('OPROGRAMM ZUR BERECHNUNG VON TRANSFERMATRIZEN FUER '/
* ' INELASTISCHE STREUUNG, (N,2N) - UND (N,3N) - PROZESSE')
WRITE(NA,9018) NP(INTYP(IT))
9018 FORMAT('HO/' ',A8/Ix)
IF(INTYP(IT).EQ.2.OR.INTYP(IT).EQ.3) GO TO 40
L3=L3-1
DO 1 L=L1,L31
1 X(L)=0.
CALL SCATD(INX,EG,NFE,EF,FI,NE27,X(L1),X(L2),X(L3),
*X(L4),X(L5),X(L6),X(L7),X(L8),X(L9),X(L10),X(L11),X(L12),
*X(L13),NISG,NISGP,NAE,NAEP,ISG,ISGF,KINEM,IAD,NABD)
C*****X(L1).....X(L2-1) : NORMALIZED TRANSFER PROBABILITIES
C*****PICGH,X(L2).....X(L3-1) : ENERGY INTEGRAL OF DISCRETE
C*****LEVEL INELASTIC SCATTERING CROSS SECTION MULTIPLIED BY
C*****WEIGHTING FUNCTION SIGD. (G MEANS GROUP NUMBER OF CUT
C*****SCATTERING GROUP,H GROUP NUMBER OF INSCATTERING GROUP)
IF(NAEP.EQ.0.AND.ISGP.EQ.0.AND.NISGP.EQ.C) GO TC 2
WRITE(NA,9007) NAE,ISG,NISG,NAEP,ISGP,NISGP
9007 FORMAT(' NAE=',I6,' ISG=',I6,' NISG=',I6,
* 'NAEP=',I6,' ISGP=',I6,' NISGP=',I6)
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GO TO 7
2 IF (IAD.EQ.0.AND.NABD.EQ.0) GO TO 43
N)2=NX*NX
C****IG : EXTERNAL ENERGY GROUP COUNT (1 CORRESPONDS TO ENERGY GROUP
C****WITH HIGHEST ENERGY
DO 8 IG=1,NX
C****MC : INTERNAL ENERGY GROUP COUNT (1 CORRESPONDS TO ENERGY GROUP
C****WITH LOWEST ENERGY.
MC=NE27-IG
C****NXMH : NUMBER OF DOWNSCATTERING GROUPS INCLUDING OUTSCATTERING
C****GROUP.
8 NXMH=NX-IG+1
C****MH : COUNT OF INSCATTERING (DOWNSCATTERING) GROUPS.MH=1 MEANS
C****SCATTERING INTO OUTSCATTERING GROUP.MH=2 MEANS SCATTERING INTO
C****THAT ENERGY GROUP,THAT ENERGETICALLY LIES ONE GROUP BELOW THE
C****OUTSCATTERING GROUP.MH=3 MEANS SCATTERING INTO THAT ENERGY GROUP.
C****THAT ENERGETICALLY LIES TWO GROUPS BELOW THE OUTSCATTERING GROUP.
C 8 WRITE(NA,9002) (X(L1+(MH-1)*NX+MG-1),MH=1,NXMH)
C9002 FORMAT(10E12.5)
DO 5 IG=1,NX
5 MC=NE27-IG
C 5 WRITE(NA,9006) MG,IG,X(L2-1+MG)
C9006 FORMAT(' MG=',I6,' IG=',I6,' QDOT(IG)=' ,E12.5)
C****CALCULATION OF SIDG*PIDGH.
DO 9 IG=1,NX
MG=NE27-IG
NXMH=NX-IG+1
DO 10 MH=1,NXMH
10 X(L1+(MH-1)*NX+MG-1)=X(L1+(MH-1)*NX+MG-1)*X(L2-1+MG)
9 CCNTINUE
DO 11 IG=1,NX
MG=NE27-IG
NXMH=NX-IG+1
C 11 WRITE(NA,9002) (X(L1+(MH-1)*NX+MG-1),MH=1,NXMH)
11 CCNTINUE
GO TO 43
40 L1=1
L2=L1+NX*NX
L3=(L2+NX)/2*2+3
C****ESTIMATION OF DIMENSIONS OF WORKING FIELDS USED IN SCATC
43 NISG=200
NISGI=300
NEP=30
NF=5
NISGP=0
NISGIP=0
NEPP=0
NFP=0
C****ORGANIZATION OF THE WORKING FIELDS FOR SUBROUTINE SCATC.
15 NISG=NISG+NISGP
NISGI=NISGI+NISGIP
NEP=NEP+NEPP
NF=NF+NFP
NISGP=0
NISGIP=0

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NEPP=0
NFP=0
L4=L3+NX*NX
L5=L4+NX
L6=L5+NE27
L7=L6+NISG
L8=L7+NISGI
L9=L8+NISGI
L10=L9+NEP
L11=L10+NEP*NF
L12=L11+NEP*NF
L13=L12+NEP*NF
L14=L13+NEP*NF
L15=L14+NX
MFELDC(INTYP(IT))=L15
C WRITE(NA,1006) L15,MMAXX
IF(L15.LE.MMAXX) GO TO12
C WRITE(NA,1014) L15,MMAXX
IFELD=1
NINA=IT
GO TO 100
12 L51=L15-1
DO 13 L=L3,L51
13 X(L)=0.
IR=0
CALL SCATC(NX,EG,XNUE,NFE,EF,FI,NE27,INTYP(IT),X(L3),X(L4),X(L5),
*X(L6),X(L7),X(L8),X(L9),X(L10),X(L11),X(L12),X(L13),
*NISG,NISGP,NISGI,NISGIP,NEP,NEPP,NF,NFP,IAC,NABC,IR)
C****X(L3).....X(L4-1) : NORMALIZED TRANSFER PROBABILITIES FOR INELAST
C****IC SCATTERING IN CONNECTION WITH THE EXCITATION OF CONTINUOUS LEVEL
C****LS OF THE RESIDUAL NUCLEUS (OR FOR (N,2N)- OR (N,3N)-REACTIONS
C****PICGH.X(L4).....X(L5-1) : ENERGY GROUP INTEGRAL OVER THE PRODUCT
C****OF CONTINUOUS LEVEL INELASTIC SCATTERING CROSS SECTION (OR (N,2N)
C****OR (N,3N)-CROSS-SECTION) AND THE WEIGHTING FUNCTION SIGG
IF (IR.EQ.1) GO TO 50
GO TO 51
50 KL=KL+1
GO TO 52
51 IF(NISGP.EQ.0.AND.NISGIP.EQ.0.AND.NEPP.EQ.0.AND.NFP.EQ.0) GO TO 14
WRITE(NA,9008) NISG,NISGP,NISGI,NISGIP,NEP,NEPP,NF,NFP
9008 FORMAT(' NISG=',I6,' NISGP=',I6,' NISGI=',I6,' NISGIP=',I6,
*'NEP=',I6,'NEPP=',I6,'NF=',I6,'NFP=',I6)
GO TO 15
14 IF(INTYP(IT).EQ.2.OR.INTYP(IT).EQ.3) GO TO 41
IF(IAD.EQ.0.AND.NABD.EQ.0) GO TO 41
IF(IAC.NE.0) IA=MINO(IAD,IAC)
IF(IAC.EQ.0) IA=IAD
IF(NABC.NE.0) NAB=MAXO(NABD,NABC)
IF(NABC.EQ.0) NAB=NABD
GO TO 42
41 IA=IAC
NAB=NABC
42 KD=NAB-IA+1
IF(NAB.EQ.0.AND.IA.EQ.0) KD=0
C WRITE(NA,9004) IA,NAB,KD,IAD,NABD,IAC,NABC

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C9004 FORMAT(' IN SCAT IA=',I6,'NAB=',I6,'KD=',I6,'IAD=',I6,'NABD=',I6 2210
C 1,'IAC=',I6,'NABC=',I6) 2220
IF (KD.NE.0) GO TO 48 2230
WRITE(NA,9022) KD,NAM4(INTYP(IT)) 2240
9022 FORMAT(/' KD=',I6,' NO TRANSFER MATRICES FOR TYPE ',A8,'IN THE 2250
1 ENERGY REGION REQUIRED BY INPUT'/)
GO TO 240 226C
48 IA7=NE27-IA 2270
NAB7=NE27-NAB 2280
WRITE(NA,9012) IA7,NAB7 2290
C9012 FCRMAT(' IN SCAT IA7=',I6,'NAB7=',I6) 2300
NX2=NX*NX 231C
C*****IG : EXTERNAL ENERGY GROUP COUNT ( 1 CORRESPONDS TO ENERGY GROUP 2320
C*****WITH HIGHEST ENERGY). 2330
DC 16 IG=NAB7,IA7 2340
C*****MG : EXTERNAL ENERGY GROUP COUNT ( 1 CORRESPONDS TO ENERGY GROUP 2350
C*****WITH LOWEST ENERGY). 236C
MG=NE27-IG 2370
C*****NXMH : NUMBER OF DOWNSCATTERING GROUPS INCLUDING OUTSCATTERING 2380
C*****GRUP. 2390
16 NXMH=NX-IG+1 240C
C*****MH : GROUP COUNT FOR DOWNSCATTERING GROUPS,MH=1 MEANING 2410
C*****INSCATTERING GROUP CORRESPONDS TO OUTSCATTERING GROUP,MH=2 2420
C*****MEANS INSCATTERING GROUP IS THAT ENERGY GROUP,THAT ENERGETICALLY 2430
C*****IS NEXT LOWER TO OUTSCATTERING,MH=3 REFERS TO INSCATTERING 2440
C*****GROUP ENERGETICALLY TWO GROUPS LOWER THAN OUTSCATTERING GROUP. 2450
C 16 WRITE(NA,9002) (X(L3+(MH-1)*NX+MG-1),MH=1,NXMH) 2460
DO 17 IG=NAB7,IA7 247C
17 MG=NE27-IG 2480
C 17 WRITE(NA,9009) MG,X(L4-1+MG) 2490
C9009 FORMAT(' MG=',I6,'QUOTC(MG)=' ,E12.5) 2500
C*****CALCULATION OF SICG*PICGH 2510
DO 18 IG=NAB7,IA7 252C
MG=NE27-IG 2530
NXMH=NX-IG+1 2540
DO 19 MH=1,NXMH 2550
19 X(L3+(MH-1)*NX+MG-1)=X(L3+(MH-1)*NX+MG-1)*X(L4-1+MG) 2560
18 CONTINUE 2570
DC 20 IG=NAB7,IA7 2580
MG=NE27-IG 2590
20 NXMH=NX-IG+1 2600
C 20 WRITE(NA,9002) (X(L3+(MH-1)*NX+MG-1),MH=1,NXMH) 2610
C*****CALCULATION OF THE COMBINATION OF DISCRETE LEVEL AND CONTINUOUS 262C
C*****LEVEL INELASTIC TRANSFER PROBABILITY : 2630
C*****P IGH=(PIDGH*SIDG+PICGH*SICG)/(SIDG+SICG). 264C
DC 21 IG=NAB7,IA7 2650
MG=NE27-IG 2660
NXMH=NX-IG+1 2670
DC 22 MH=1,NXMH 2680
X(L1+(MH-1)*NX+MG-1)=X(L1+(MH-1)*NX+MG-1)+X(L3+(MH-1)*NX+MG-1) 2690
XC=(X(L2-1+MG)+X(L4-1+MG)) 270C
IF (XD.NE.0.) 2710
IX(L1+(MH-1)*NX+MG-1)=X(L1+(MH-1)*NX+MG-1)/XD 2720
22 CONTINUE 2730
21 CONTINUE 274C
2750
DC 23 IG=NAB7,IA7 276C
MG=NE27-IG 2770
23 NXMH=NX-IG+1 2780
C 23 WRITE(NA,9002) (X(L1+(MH-1)*NX+MG-1),MH=1,NXMH) 279C
IF(KD.NE.0) GO TO 47 2800
GC TO 240 2810
47 MZ=0 2820
WRITE(LIZ) MZ,NAM4(INTYP(IT)) 2830
C WRITE(NA,9014) MZ,NAM4(INTYP(IT)) 2840
C9014 FORMAT(' MZ=',I6,'NAM4=',A8) 2850
KZ=KI+1 286C
WRITE(LIZ) KZ,NAM,KD 2870
WRITE(NA,9013) KZ,NAM,KD 2880
9013 FORMAT(' OKZ=',I6,'NAM=',A8,'KD=',I6) 2890
C*****IG1 : EXTERNAL ENERGY GROUP COUNT ( 1 CORRESPONDS TO ENERGY GROUP 2900
C*****WITH HIGHEST ENERGY).IG : EXTERNAL ENERGY GROUP COUNT.IG IS 291C
C*****INTRODUCED TO OBTAIN AN OUTPUT ,THAT STARTS WITH THE OUTSCATTERING 2920
C*****GROUP OF LOWEST ENERGY. 2930
DC 24 IG1=NAB7,IA7 2940
IG=IA7+NAB7-IG1 2950
NULL=0 2960
C*****THE MEANING OF MG,NXMH AND MH CORRESPONDS TO THE MEANING 297C
C*****THEY HAVE IN THE WRITE COMMANDS AFTER RETURNING FROM SCATD 2980
C*****ANC SCATC RESPECTIVELY. 2990
MG=NE27-IG 3000
NXMH=NX-IG+1 3010
NXMH1=NXMH 3020
DO 25 MH=1,NXMH 3030
MH1=NXMH-MH+1 304C
IF(X(L1+(MH1-1)*NX+MG-1).LE.0..AND. NULL.EQ.0) GO TO 26 3050
NULL=1 3060
GO TO 25 3070
26 NXMH1=NXMH1-1 3080
25 CCNTINUE 309C
IF(NXMH1.NE.0) GO TO 27 3100
WRITE(NA,9020) 3110
9020 FORMAT(' ***WARNING 5.10 :THE INELASTIC SCATTERING MATRIX IS FOUND 3120
ITC BE EQUAL TO ZERO IN AN ENERGY GROUP'/' ,WHERE THE INELASTIC SCAT 3130
2TERING CROSS SECTION IS GREATER THAN ZERO.CHECK NUCLEAR DATA 3140
3KD GETS A WRONG VALUE.' ) 3150
GC TO 24 3160
27 NXMH1=NXMH1+1 3170
WRITE(NA,9010) IG,NXMH1 3180
C9010 FCRMAT(' @@@@@@IG=',I6,'NXMH1=',I6,' @@@@@@') 3190
C WRITE(NA,9011) (X(L1+(MH-1)*NX+MG-1),MH=1,NXMH1) 3200
C9011 FCRMAT(10E12.5) 3210
WRITE (LIZ) NXMH1,IG,(X(L1+(MH-1)*NX+MG-1),MH=1,NXMH1) 3220
C ORGANIZATION OF THE OUTPUT ON LISTING IN THE FCMP OF MAXIMUM 11 3230
C SCATTERING PROBABILITIES PER LINE STARTING WITH THE OUTSCATTERING 3240
C GROUP OF LOWEST ENERGY(LARGEST GROUP NUMBER ACCORDING TO ABN-SET) 3250
NZ=NXMH1 326C
DO 30 LN=1,NZ 3270
IX(L14+LN-1)=IG+LN-1 3280
30 CONTINUE 3290
KJ=NZ/11 3300
KJJ=KJ*11 3310
IF(NZ.NE.KJJ) GOTO 31 3320

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KJ1=KJ 3320
GOTO 32 3340
31 KJ1=KJ+1 3350
32 DC 37 LI=1,KJ1 3360
IF(LI.NE.1) GOTO 33 3370
LIM=1 3380
GO TO 34 3390
33 LIM=(LI-1)*11+1 3400
IF(LI.EQ.KJ1) GOTO 35 3410
34 IF(KJ1.LE.1) GOTO 35 3420
L11=L1*11 3430
GO TO 36 3440
35 L11=NZ 3450
36 IF(LIM.GT.L11) GOTO 37 3460
WRITE(NA,9015) (IX(L14+LM-1),LM=LIM,L11) 3470
9015 FCRMAT(10X,11(3X,13,5X)) 3480
IF(LI.NE.1) GOTO 38 3490
C IG-OUTSCATTERING GROUP ACCORDING TO THE COUNTING IN THE ABN-SET 3500
C I.E. LOWEST GROUP NUMBER CORRESPONDS TO HIGHEST ENERGY BOUNDARIES 3510
C X(L1+(MH-1)*NX+MG-1)-PROBABILITY FOR INELASTIC SCATTERING CUT OF 3520
C GROUP IG INTO GROUP (MH+IG-1). 3530
WRITE(NA,9016) IG,(X(L1+(MH-1)*NX+MG-1),MH=1,L11) 3540
9016 FCRMAT(3X,I2,5X,11(1PE10.3,1X)) 3550
GO TO 37 3560
38 WRITE(NA,9017)(X(L1+(MH-1)*NX+MG-1),MH=LIM,L11) 3570
9017 FCRMAT(10X,11(1PE10.3,1X)) 3580
37 CONTINUE 3590
24 CCNTINUE 3600
C WRITE(NA,9021) KD,IT,NIN 3610
C9021 FCRMAT(' AFTER STATEMENT 24 KD=',I6,'IT=',I6,'NIN=',I6) 3620
240 IT=IT+1 3630
IF(IT.LE.NIN) GO TO 46 3640
3 KL=KL+1 3650
100 MFELD=MAXO(MFELDD,MFELDC(1),MFELDC(2),MFELDC(3)) 3660
IF(IFELD.EQ.1) WRITE(NA,9019) NP(INTYP(NINA)) 3670
9019 FCRMAT(/' *****CALCULATION OF ',A8/) 3680
52 RETURN 3690
END 3700

SUBROUTINE RENUA(TYP,KONT,SGIZC,EZ,EU,FC,NACT,NISG, 10
INISGP) 20
C*****SUBROUTINE READS TYPE SGIZC FROM THE NUCLEAR LIBRARY WITHIN THE EN 30
C*****ENERGY LIMITS EU AND EQ. 40
C DIMENSION EZ(NISG),SGIZC(NISG),NAME(3),NNAM(3),QUER(2),NN(5) 50
C DIMENSION FZ(NISG),SGIZC(NISG),NAME(6),NNAM(4),QLER(2),NN(5) 60
C REAL*8 NAM,TYP,NAME,NN,NIVEAU 70
C REAL*8 NAM,TYP,NAME,NN,NIVEAU,BEST 80
C CMCMCN NAM,ISTRUK,ISPA,NA,LIZ 90
KONTG=1 100
NISGF=0 110
NCPY=0 120
NACT=0 130
IEW=0 140
EW=0. 150
SW=0. 160

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C WRITE(NA,I03) EU,EC 170
C 103 FCRMAT(' EU=',F12.6,'EC=',E12.6) 180
CALL DOPW(8HSGIZC ,NN(1)) 190
CALL DOPW(8HSGIZ ,NN(2)) 200
CALL DOPW(8HSGT ,NN(3)) 210
CALL DCPW(8HSG2N ,NN(4)) 220
CALL DCPW(8HSG3N ,NN(5)) 230
CALL DOPW(8HBEST ,BEST) 240
IF(TYP.EQ.NN(1).OR.TYP.EQ.NN(4).OR.TYP.EQ.NN(5)) GO TO 1 250
IF(TYP.EQ.NN(2)) GO TO 4 260
1 I=1 270
C NAAM(1)=2 280
NAAM(1)=3 290
NAME(1)=NAM 300
NAME(2)=BEST 310
NAME(2)=TYP 320
NAME(3)=TYP 330
C 19 CALL LDFLOC(KENNZ,NNAM,NAME,QUER) 340
19 CALL NDFLOC(KENNZ,NNAM,NAME,ADAT,NCO) 350
IF (KENNZ.EQ.0) GO TO 2 360
21 QUER(1)=NAME(4) 370
QLER(2)=NAME(5) 380
C 21 IF(QUER(1).LT.EU) GO TO 20 390
IF(QUER(1).LT.EU) GO TO 20 400
IF(QUER(1).EQ.EU) GO TO 12 410
IF(QUER(1).GT.EU.AND.QUER(1).LE.EQ.AND.EW.GT.C.E.AND.I.EQ.1.AND. 420
INISGF.EQ.0) GO TO 10 430
IF(QUER(1).GE.EQ) GO TO 22 440
IF(QUER(1).GT.EU.AND.QUER(1).LT.EC) GO TO 12 450
22 NOPT=1 460
IF(IEW.EQ.1.AND.I.EC.1) GO TO 10 470
GO TO 12 480
10 EZ(I)=EW 490
SGIZC(I)=SW 500
I=I+1 510
12 FZ(I)=QUER(1) 520
SGIZC(I)=QUER(2) 530
IF(NOPT.EQ.1) GO TO 6 540
I=I+1 550
IF (I.LE.NISG) GO TO 3 560
GO TO 5 570
C 2 WRITE(NA,I00) NAM,TYP 580
C 100 FORMAT(' *** FOR THE ISOTOPE ',A8,'THE DATA TYPE ',A8,'IS NOT AV 590
C IAILABLE ON THE NUCLEAR LIBRARY') 600
2 KONT=0 610
GO TO 9 620
20 CONTINUE 630
EW=QUER(1) 640
SW=QUER(2) 650
IEW=1 660
C 3 CALL LDFNXT(KENNZ,NNAM,NAME,QUER) 670
3 CALL NDFNXT(KENNZ,NNAM,NAME,ADAT,ACC) 680
QUER(1)=NAME(4) 690
QLER(2)=NAME(5) 700
IF (KENNZ.EQ.0) GO TO 23 710

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GC TC 21
23 I=I-1
GC TC 6
5 I=1
NISGF=NISGF+1
GC TC 3
6 IF(I.GT.1) GO TO 7
C WRITE(NA,101) TYP,NAM,EU,EO
C 101 FORMAT(' ***NO DATA FOR',A8,' OF MATERIAL',A8,' AVAILABLE IN THE ENR
C IRCY REGION',G14.6,G14.6)
KCATG=0
GO TO 9
7 NACT=I
IF(NISGF.NE.0) GO TO 8
IF(KENNZ.EQ.0) NACT=I-1
IF (SGIZC(1).EQ.0..AND.SGIZC(2).EQ.0.) GC TC 24
GC TC 9
24 IF(NACT.GT.2) GC TC 31
NACT=0
GC TC 29
31 NACTI=NACT-1
CC 25 NTH=1,NACTI
EZ(NTH)=EZ(NTH+1)
25 SCIZC(NTH)=SGIZC(NTH+1)
NACT=NACTI
IF (EZ(1).GE.EO) NACT=0
GC TC 9
E NISGP=I+NISG*(NISGF-1)
GC TC 9
4 F=C.
C NNAAM(1)=3
NNAAM(1)=4
NAME(1)=NAM
NAME(2)=BEST
NAME(2)=TYP
NAME(3)=TYP
C NAME(3)=0
NAME(4)=0
C CALL LDFLOC(KENNZ,NNAAM,NAME,QUER)
CALL NDFLOC(KENNZ,NNAAM,NAME,ADAT,NCO)
IF(KENNZ.EQ.1) GO TO 13
16 CALL LDFLOC(KENNZ,NNAAM,NAME,ADAT,NCC)
16 CALL LDFLOC(KENNZ,NNAAM,NAME,QUER)
IF(KENNZ.EQ.0) GO TO 17
C 12 NIVEAU=NAME(3)
13 NIVEAU=NAME(4)
15 QUER(1)=NAME(5)
QUER(2)=NAME(6)
C 15 F=AMAX1(F,QUER(1))
F=AMAX1(F,QUER(1))
C CALL LDFNXT(KENNZ,NNAAM,NAME,QUER)
CALL NDFNXT(KENNZ,NNAAM,NAME,ADAT,NCO)
IF(KENNZ.EQ.1) GC TC 15
IF(NAME(3).GT.NIVEAU) GO TO 16
IF(NAME(4).GT.NIVEAU) GO TO 16

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C GC TC 17
C 14 WRITE(NA,100) NAM,TYP
17 IF(F.GE.EU.AND.E.LE.EO) GO TO 19
KCATG=0
TYP=NN(3)
C WRITE(NA,101) TYP,NAM,EU,EO
C 18 WRITE(NA,102) E
C 102 FORMAT(' UPPER ENERGY OF TYPE SGIZ IS',G14.6,' E')
C NNAAM(1)=2
18 NNAAM(1)=3
NAME(2)=NN(3)
NAME(3)=NN(3)
TYP=NN(3)
EU=AMAX1(EU,E)
I=1
GC TC 19
9 IF(EZ(1).GE.EC) NACT=0
IF(SGIZC(1).EQ.0..AND.NACT.GE.2) GC TC 30
GC TC 29
30 IF((FZ(2)-EZ(1))/FZ(2).GT.1.F-2) GC TC 27
GC TC 29
27 IF(NISG.GE.(NACT+2)) GC TC 28
NISGF=NISGF+1
NISGP=NISGP+2
GC TC 29
2P FZ1=(EZ(2)-FZ(1))*0.1+EZ(1)
FZ2=(EZ(2)-EZ(1))*0.1+EZ1
SGIZC1=FPOLA(EZ(1),EZ(2),SGIZC(1),SGIZC(2))
SGIZC2=FPOLA(EZ(1),EZ2,EZ(2),SGIZC(1),SGIZC(2))
DC 26 I=2,NACT
FZ(NACT-I+4)=EZ(NACT-I+2)
2E SGIZC(NACT-I+4)=SGIZC(NACT-I+2)
FZ(2)=EZ1
EZ(3)=EZ2
SGIZC(2)=SGIZC1
SGIZC(3)=SGIZC2
NACT=NACT+2
C WRITE(NA,104) (I,EZ(I),SGIZC(I),I=1,NACT)
C 104 FORMAT(2(' I=',I6,' FZ=',E12.5,' SGIZC=',E12.5))
29 RETURN
ENC

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C*****SUBROUTINE SCATC.DATE OF LAST CHANGE 21.12.1976.(LINES 3660 TO 10
C*****6460)
SUBROUTINE SCATC(NX,EG,XNUE,NFE,EF,FI,NE27,INTYP,WEINC,QUCTC,ENG, 20
*EZ,SGIZC,EI,EP,F1,F2,F3,F4,NISG,NISGP,NISGI,NISGIP,NEP,NEPP,NF,NFP 30
*,IA,NAB,IR)
DIMENSION EG(NX),EF(NFE),FI(NFE),WEINC(NX,NX),QCTC(NX),ENG(NE27), 40
*EZ(NISG),SGIZC(NISG),EI(NISGI),EP(NEP),F1(NF,NEP),F2(NF,NEP), 50
*F3(NF,NEP),F4(NF,NEP),NN(8)
COMMON NAM,ISTRUK,ISPA,NA,LIZ,NANF,NEND,KL 60
REAL *8 NAM,TYP,NN 80
IF (INTYP.EQ.1) WRITE(NA,9000) 90

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- B 81 -

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9000 FORMAT(///' PROGRAMM ZUR BERECHNUNG INELASTISCHER STREUMATRIZEN ' / 120
1' IM ENERGIEBEREICH KONTINUIERLICHER ANREGUNGSNIVEAUS DES RESTKERN 130
2S' /) 140
IA=0 150
NAB=0 16C
EPS=0.01 170
EPSSP=0.0001 180
A=C. 190
NMAX=100000 200
KEN=NFE 210
IF (NFE.EQ.1) KEN=0 220
CALL DOPW(8HSGIZC ,NN(1)) 230
CALL DOPW(8HSGIZ ,NN(2)) 240
CALL DOPW(8HSGI ,NN(3)) 250
CALL DOPW(8HSEDIC ,NN(4)) 26C
CALL DOPW(8HSG2N ,NN(5)) 270
CALL DOPW(8HSED2N ,NN(6)) 280
CALL DOPW(8HSG3N ,NN(7)) 290
CALL DOPW(8HSED3N ,NN(8)) 300
NUGRE=0 31C
IF (EG(1)-1.E-3) 40,40,25 320
40 NE=NX 330
DC 26 I=1,NX 34C
26 ENG(NX)=EG(NX) 350
GO TO 41 36C
C***** : ADDING THERMAL GROUP TO INSCATTERING GROUPS 370
25 DC 28 I=1,NX 380
28 ENG(NE27-I+1)=EG(NX-I+1) 390
NE=NE27 400
ENG(1)=1.E-3 41C
41 DO 29 IG=1,NX 420
DO 29 IH=1,NX 430
29 WEINC(IG,IH)=0. 440
IG1=NE27-NANF 450
IG2=NE27-NEND 46C
DO 42 IGE=IG1,IG2 470
IF(INTYP.EQ.1) GO TO 5 480
ITYP=2*INTYP+1 490
GO TO 8 500
5 ITYP=1 51C
GO TO 8 520
7 ITYP=ITYP+1 53C
8 KONT=1 540
TYP=NN(ITYP) 550
3 REU =ENG(IGE) 56C
REO=ENG(IGE+1) 570
CALL RENUA (TYP,KONT,SGIZC,EZ,REU,REG, 580
*NACT,NISG,NISGP) 590
C WRITE(NA,119) NISG,NISGP,KONT 600
C 119 FORMAT(' NISG=',I6,'NISGP=',I6,'KONT=',I6) 61C
9002 FORMAT(/' ***WARNING 5.00 : THE CROSS-SECTION-VALUES,GIVEN FOR THE 620
1 MATERIAL ',A8,',TYPE ',A8/' ***DO NOT COVER THE ENERGY-GROUP BETW 630
2EEN ',E14.6,'EV AND ',E14.6,'EV.THE LOWEST AND HIGHEST VALUES '/' 640
3***GIVEN ON KEDAK FOR THIS GROUP ARE ',E14.6,'EV AND ',E14.6, 650
4'EV.'/' ***THE INTEGRATION IN THIS ENERGY-GROUP THEREFORE IS RESTR 660
5ICTED.' )
IF(KONT.EQ.0) GO TO 6 670
IF(NISGP.NE.0) GO TO 49 680
IF (NACT.EQ.0) GO TO 52 700
GO TO 51 710
C 52 WRITE(NA,9003) NAM,TYP,ENG(IGE),ENG(IGE+1) 720
C9003 FORMAT(' NO ENERGY-POINTS ON KEDAK FOR MATERIAL ',A8,'TYPE ',A8/ 730
C 2' IN THE ENERGY-REGION BETWEEN ',E12.5,'EV AND ',E12.5,'EV') 740
52 CCATINUE 75C
GO TO 42 760
51 IF(NISGI.GE.NACT) GO TO 33 770
NISGIP=NACT-NISGI 780
C IF(NISGIM.GE.NACT) GO TO 35 790
C WRITE(NA,117) NACT,NISGIM 800
C 117 FORMAT(' NISGIM TOO SMALL,NACT=',I6,'NISGIM=',I6) 810
GO TO 49 820
C 25 NISGI=NISGI+NISGIP 830
NISGIP=0 840
C 33 IF(EZ(1).GT.ENG(IGE).OR.EZ(NACT).LT.ENG(IGE+1)) 850
1WRITE(NA,9002) NAM,TYP,ENG(IGE),ENG(IGE+1),EZ(1),EZ(NACT) 860
DC 17 I=1,NACT 870
17 EI(I)=EZ(I) 880
C*****EZ(1)...EZ(NACT) : ENERGY POINTS OF SGIZC 890
C*****EF(1)...EF(NFE) : ENERGY POINTS OF THE SPECTRUM 900
C*****EI(1)...EI(KMAX) : SUM OF EZ AND EF AND ENERGY GRUPLIMITS 910
GO TO 9 920
C 1 IF((NISG+NISGP).LE.NISGM ) GO TO 2 930
C WRITE(NA,100) NISGM 940
C 100 FORMAT(' &&DIMENSION NISGMAX TOO SMALL') 95C
GO TO 49 960
C 2 NISG=NISG+NISGP 97C
NISGP=0 980
C KONT=1 99C
C GO TO 3 100C
6 IF(ITYP.EQ.1) GO TO 7 1010
WRITE(NA,9001) NN(ITYP) 1020
9001 FORMAT(' NO INFORMATION FOR TYPE',A8,'ON THE NUCLEAR LIBRARY') 1030
GO TO 49 1040
9 IF(KEN.NE.0) GO TO 14 105C
KMAX=NACT 1060
EI(1)=AMAX1(ENG(IGE),EI(1)) 1070
EI(NACT)=AMIN1(ENG(IGE+1),EI(NACT)) 1080
GO TO 12 1090
14 CALL ENORG(ENG(IGE),ENG(IGE+1),EI,EF,NACT,KMAX,NFE,NISGI, 110C
*NISGIP) 1110
C WRITE(NA,107) NISGI,NISGIP 1120
C 107 FORMAT(' NISGI=',I6,'NISGIP=',I6) 1130
IF(NISGIP.NE.0) GO TO 49 1140
GO TO 36 1150
C 34 IF((NISGI+NISGIP).LE.NISGIM) GO TO 37 1160
C WRITE(NA,118) NISGI,NISGIP,NISGIM 1170
C 118 FORMAT('***NISGIM TOO SMALL NISGI=',I6,'NISGIP=',I6,'NISGIM=',I6) 118C
C GO TO 49 1190
C 37 NISGI=NISGI+NISGIP 120C
NISGIP=0 1210

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C	GO TO 14	1220	C*****SCATTERING GROUP IGE. (SUMW) (NM=2)	1770
C	36 WRITE(NA,108) (EI(KS),KS=1,KMAX)	1230	SUMW=0.	1780
C	108 FORMAT(' ',E12.5)	1240	IF(KEN.EQ.0) GO TO 60	1790
	36 CONTINUE	1250	DO 46 IE=1,KMAX1	1800
	12 KONT=1	1260	IF(EI(IE+1).LE.EMINW) GO TO 47	1810
	CALL REPROB(INTYP,KONT,EP,F1,F2,F3,F4,NEP,NEPP,NF,NFP)	1270	IF(EI(IE).GE.EMAXW) GO TO 47	1820
	IF (KONT.EQ.0) GO TO 15	1280	C WRITE(NA,126) EI(IE),EI(IE+1),NM	1830
	U=F4(1,1)	1290	C 126 FORMAT(' ENTER SIMPSI E(IE)=' ,E12.5,'E(IE+1)=' ,E12.5,'NM=' ,I6)	1840
	GO TO 11	1300	CALL SIMPSI(NUGRE,U,A,XNUE,EI(IE),EI(IE+1),EPS,NMAX,WINT,N,EZ,	1850
15	IF (INTYP.EQ.1) TYP=NN(4)	1310	1SGIZC,EF,FI,ENG,NACT,NFE,NE,NM,EP,F1,F2,F3,F4,NEP,NF,KONT,ERR,	1860
	IF (INTYP.EQ.2) TYP=NN(6)	1320	2INTG)	1870
	IF (INTYP.EQ.3) TYP=NN(8)	1330	C WRITE(NA,127) EI(IE),EI(IE+1),NM,WINT	1880
	U=F4(1,2)	1340	C 127 FORMAT(' AFTER SIMPSI EI(IE)=' ,E12.5,'EI(IE+1)=' ,E12.5,'NM=' ,I6,	1890
	IF(A.EQ.F4(1,1)) GO TO 11	1350	C 1' WINT=' ,E12.5)	1900
	A=F4(1,1)	1360	GC TO 48	1910
	WRITE(NA,109) TYP,NAM,NN(2*INTYP+1),U,A,XNUE	1370	C 47 WRITE(NA,128)	1920
109	FORMAT(/' NO INFORMATION ON THE NUCLEAR DATA LIBRARY FOR TYPE ',A8	1380	C 128 FORMAT(' 47 47 47 47 47 47 47 47 47')	1930
	1,'OF MATERIAL',A8,'AN EVAPORATION MODEL WITH/' THETA=SQRT(E/(NUE	1390	47 WINT=0.	1940
	2*A)) IS USED.FOR THE NORMALIZATION THE THRESHOLD OF ',A8,' IS	1400	48 SUMW=SUMW+WINT	1950
	3TAKEN INTO ACCOUNT.'/' U=' ,E12.5,'EV,A=' ,E12.5,'NUE=' ,E12.5/)	1410	C WRITE(NA,124) SUMW	1960
	11 IF (EZ(1).LT.U) GO TO 65	1420	C 124 FORMAT(' &&&&&SUMW=' ,E12.5,'&&&&&')	1970
	IF(NEPP.EQ.0.AND.NFP.EQ.0) GO TO 50	1430	C WRITE(NA,9020) IE,EI(IE),EI(IE+1),WINT,SUMW	1980
	GC TO 49	1440	C 9020 FORMAT(' IE=' ,I6,'EI(IE)=' ,E12.5,'EI(IE+1)=' ,E12.5/	1990
C*****	CALCULATION OF SIGMA*WEIGHTING FUNCTION.(SUM) (NM=0)	1450	C 1' WINT=' ,E12.5,'SUMW=' ,E12.5)	2000
50	SUM=0.	1460	46 CONTINUE	2010
	KMAX1=KMAX-1	1470	GO TO 61	2020
	NM=0	1480	60 CALL SIMPSI(NUGRE,U,A,XNUE,EMINW,EMAXW,EPSSP,NMAX,WINT,N,EZ,	2030
	IF(KEN.GT.0)GOTO 30	1490	1SGIZC,EF,FI,ENG,NACT,NFE,NE,NM,EP,F1,F2,F3,F4,NEP,NF,KONT,ERR,	2040
	EF1=0.	1500	2INTG)	2050
	EFKEN=1.E+20	1510	C WRITE (NA,9004) EMINW,EMAXW,WINT	2060
	GCTO 31	1520	C 9004 FORMAT(' EMINW=' ,E12.5,'EMAXW=' ,E12.5,'WINT=' ,E12.5)	2070
30	EF1=EF(1)	1530	SUMW=SUMW+WINT	2080
	EFKEN=EF(KEN)	1540	61 SUMQQ=SUM/SUMW	2090
31	CONTINUE	1550	NIGE=NE-IGE	2100
	EMIN=AMAX1(EZ(1),ENG(IGE),EF1)	1560	C*****SUMQQ = WEIGHTED GROUP CROSS-SECTION.	2110
	EMAX=AMIN1(EZ(NACT),ENG(IGE+1),EFKEN)	1570	SUMQ=SUM	2120
	EMINW=AMAX1(ENG(IGE),EF1)	1580	C WRITE(NA,125) SUMQ	2130
	EMAXW=AMIN1(ENG(IGE+1),EFKEN)	1590	C 125 FORMAT(' &&&&&SUMQ=' ,E12.5,'&&&&&')	2140
	DO 16 IE=1,KMAX1	1600	IF(INTYP.EQ.2.OR.INTYP.EQ.3) WRITE(NA,115) SUMQQ,NIGE,U,KONT	2150
	IF (EI(IE+1).LE.EMIN) GO TO 18	1610	115 FORMAT(/' **WEIGHTED GROUP CROSS-SECTION = ' ,E12.6,' FOR OUTSCATT	2160
	IF(EI(IE).GE.EMAX) GO TO 18	1620	IERING - GROUP ',I6,' U = ' ,E12.6,'KONT = ' ,I6)	2170
	CALL SIMPSI(NUGRE,U,A,XNUE,EI(IE),EI(IE+1),EPS,NMAX,RESINT,N,EZ,	1630	QUOTC(IGE)=SUMQ	2180
	1SGIZC,EF,FI,ENG,NACT,NFE,NE,NM,EP,F1,F2,F3,F4,NEP,NF,KONT,ERR,INTG	1640	NM=1	2190
	2)	1650	C*****CALCULATION OF THE INTEGRAL OF SIGMA*SPECTRUM*TRANSFER-PROBABILITY	2200
	GC TO 19	1660	C*****OVER THE OUTSCATTERING GROUP IGE. (PROSUM) (NM=1)	2210
18	RESINT=0.	1670	PRSUM=0.	2220
19	CONTINUE	1680	NIE=NE-IGE	2230
C	WRITE(NA,9010) IE,EI(IE),EI(IE+1),RESINT,SUM	1690	DO 22 NUGR1=NIE,NX	2240
C 9010	FORMAT(' IE=' ,I6,'EI(IE)=' ,E12.5,'EI(IE+1)=' ,E12.5/	1700	INTG=0	2250
C	1' RESINT=' ,E12.5,'SUM=' ,E12.5)	1710	INTG1=0	2260
	16 SUM=SUM+RESINT	1720	PROSUM=0.	2270
C	WRITE(NA,111) SUM	1730	NUGRE=NE-NUGR1	2280
C 111	FORMAT(' SUM=' ,E12.5)	1740	DO 20 IE=1,KMAX1	2290
	NM=2	1750	IF (EI(IE+1).LE.EMIN) GO TO 21	2300
C*****	CALCULATION OF THE INTEGRAL OF THE WEIGHTING SPECTRUM OVER THE OUT	1760	IF (EI(IE).GE.EMAX) GO TO 21	2310

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CALL SIMPSI(NUGRE,U,A,XNUE,EI(IE),EI(IE+1),EPS,NMAX,PRINT,N,EZ,
1SGIZC,EF,F1,ENG,NACT,NFE,NE,NM,EP,F1,F2,F3,F4,NEP,NF,KONT,ERR,
2INTG1)
C WRITE(NA,116) INTG
C 116 FORMAT(' *****INTG=',I6,' *****')
IF (INTG1.EQ.1) INTG=1
IF(N.GE.NMAX.AND.ERR.GT.EPS) INTG=1
C WRITE(NA,112) IE,EI(IE),EI(IE+1),NUGRE,PRINT
112 FORMAT(' IE=',I6,'EI(IE)=' ,E12.5,'EI(IE+1)=' ,E12.5,'NUGRE=' ,I6,
1'PRINT=' ,E12.5)
C WRITE(NA,112) IE,EI(IE),EI(IE+1),NUGRE,PRINT
C 112 FORMAT(' IE=',I6,'EI(IE)=' ,E12.5,'EI(IE+1)=' ,E12.5,'NUGRE=' ,I6,
C 1'PRINT=' ,E12.5)
GC TO 23
21 PRINT=0.
C WRITE(NA,115) EI(IE),EI(IE+1)
C 115 FORMAT(' NO CONTRIBUTION TO THE INTEGRAL IN INTERVAL EI(IE)=' ,
C 1E12.5,'EI(IE+1)=' ,E12.5)
23 PRCSUM=PROSUM+PRINT
C WRITE(NA,113) PROSUM
113 FORMAT(' PROSUM=' ,E12.5)
20 CONTINUE
IF(INTG.EQ.1) WRITE(NA,114) NIE,NUGR1,PROSUM
114 FORMAT(' *OUTSCATTERING GROUP = ' ,I6,' INSCATTERING GROUP = ' ,I
16/' TOTAL CONTRIBUTION OF SIGMA*SPECTRUM*TRANSFER-PROBABILITY = ' ,
2IPE14.6/)
NUGRI=NUGRI-NIE+1
IF (SUM.EQ.0.) GO TO 55
WEINC(IGE,NUGRI)=PRCSUM/SUM
22 PRSUM=PRSUM+WEINC(IGE,NUGRI)
C WRITE(NA,116) PRSUM
C 116 FORMAT(' *****PRSUM=' ,E12.5,' *****')
NE1=NE-1
IF(PRSUM*0.9995.LE.1..AND.PRSUM*1.0005.GE.1.) GO TO 53
CO 54 INU=1,NE1
54 WEINC(IGE,INU)=WEINC(IGE,INU)/PRSUM
C WRITE(NA,114) (IGR,WEINC(IGE,IGR),IGR=1,NE1)
C 114 FORMAT(2(' IGR=' ,I6,'WEINC(IGE,IGR)=' ,E12.5))
GO TO 53
55 NE1=NE-1
DC 56 INU=1,NE1
56 WEINC(IGE,INU)=0.
GO TO 42
53 IF(IA.EQ.0) IA=IGE
NAB=IGE
42 CONTINUE
C WRITE(NA,130) IA,NAB
C 130 FORMAT(' IA=' ,I6,'NAB=' ,I6)
GO TO 49
49 RETURN
65 WRITE(NA,131) EZ(1),U
131 FORMAT('/' THE LOWEST ENERGY OF SGIZC (SG2N,SG3N) ON KEDAK , E=' ,E
112.5,' EV LIES BELOW THE THRESHOLD/' OF THE CORRESPONDING REACTIO
2N (GIVEN IN SEDIC (SED2N,SED3N) OR SGI RESPECTIVELY) U=' ,E12.5,' E
3V.'/'
*****CHECK NUCLEAR DATA*****'
IR=1
RETURN
END

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SUBROUTINE REPROB(INTYP,KONT,EP,F1,F2,F3,F4,NEP,NEPP,NF,NFF)
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C   6  FORMAT(' FOR THE ISOTOPE',A9,' THE DATA TYPE',A7,' IS NOT
C   7  AVAILABLE ON THE KEDAK-LIBRARY',///)
C   8  KCAT=0
C   9  GO TO 11
C  10  II=II+1
C  11  IF((I.LF.NEP) GO TO 23
C  12  NEPF=NEPF+1
C  13  II=1
C  14  EP(II)=SNGL(NAME(3))
C  15  EP(II)=SNGL(NAME(4))
C  16  WRITE(NA ,7) EP(II),II
C  17  7  FORMAT(/,' EP=',E16.8,' II=',I6)
C  18  WRITE(NA ,13)
C  19  13  FORMAT(/,'          K           F           THETA/A/EC/
C  20  1U/B/           ')
C  21  4  ANSW(1)=NAME(5)
C  22  ANSW(2)=NAME(6)
C  23  ANSW(3)=NAME(7)
C  24  ANSW(4)=NAME(8)
C  25  4  F1(I,II)=ANSW(1)
C  26  F1(I,II)=ANSW(1)
C  27  F2(I,II)=ANSW(2)
C  28  F3(I,II)=ANSW(3)
C  29  F4(I,II)=ANSW(4)
C  30  IF(F1(I,II).NE.1.0) WRITE(NA,101) EP(II),F1(I,II)
C  31  101  FORMAT(' ***WARNING 5.01 : FOR PRIMARY NEUTRON ENERGY EP=',E14.8,'
C  32  1EV , K IS EQUAL TO ',E10.4)
C  33  SUM=SUM+ANSW(2)
C  34  CALL LDFNXT(KENNZ,NNAM,NAME,ANSW)
C  35  CALL NDFNXT(KENNZ,NNAM,NAME,NDAT,NC0)
C  36  IF (KENNZ.EQ.0) GO TO 24
C  37  GC TC 28
C  38  I=I+1
C  39  IF((I.LE.NF) GO TO 4
C  40  NFF=NFF+1
C  41  I=1
C  42  GC TO 4
C  43  28  IF((ABS(SUM)-1.).GT.1.E-4) WRITE(NA ,12) SUM
C  44  12  FORMAT(' WARNUNG: SUMME ALLER P=',G16.8)
C  45  WRITE(NA ,8) (F1(J,II),F2(J,II),F3(J,II),F4(J,II),J=1,I)
C  46  8  FORMAT(4E16.8)
C  47  I=1
C  48  IF(SNGL(NAME(3)).GT.EP(II)) GO TO 5
C  49  IF(SNGL(NAME(4)).GT.EP(II)) GO TO 5
C  50  KCAT=1
C  51  IF (NEPF.NE.0) GO TO 25
C  52  INEP=II
C  53  GC TO 26
C  54  25  NEPP=((NEPF-1)*NEP)+II
C  55  26  IF(NFF.NE.0) GO TO 27
C  56  INF=I
C  57  GO TO 11
C  58  27  NFF=((NFF-1)*NF)+I
C  59  11  CONTINUE
C  60  IF (KONT.EQ.0) GO TO 14

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GC TO 15
14  IF(INTYP.EQ.1) CALL DOPW(8HSGI ,TYP)
   IF(INTYP.EQ.2) CALL DOPW(8HSG2N ,TYP)
   IF(INTYP.EQ.3) CALL DOPW(8HSG3N ,TYP)
C   NNAM(1)=2
C   NNAM(1)=3
C   NAME(1)=NAM
C   NAME(2)=TYP
C   NAME(3)=TYP
C   U=0.
C   CALL LDFLOC(KENNZ,NNAM,NAME,ANSW)
C   CALL NDFLOC(KENNZ,NNAM,NAME,NDAT,NC0)
C   IF (KENNZ.EQ.0) GO TO 3
C  22  ANSW(1)=NAME(4)
C  23  ANSW(2)=NAME(5)
C  24  IF(ANSW(2).GT.0.) GO TO 16
C  25  IF(ANSW(2).GT.0.) GO TO 16
C  26  L=ANSW(1)
C  27  GO TO 20
C  28  16  IF(U.NE.0.) GC TO 17
C  29  WRITE(NA,100) ANSW(1),ANSW(2)
C  30  100  FORMAT(' FIRST VALUES OF E,SGI ON KEDAK:E=',E12.5,'SGI=',E12.5)
C  31  F4(I,2)=ANSW(1)
C  32  GC TO 18
C  33  17  F4(I,2)=U
C  34  GO TO 18
C  35  20  CALL LDFNXT(KENNZ,NNAM,NAME,ANSW)
C  36  CALL NDFNXT(KENNZ,NNAM,NAME,NDAT,ACC)
C  37  IF (KENNZ.EQ.0) GO TO 21
C  38  GC TO 22
C  39  21  F4(I,2)=U
C  40  18  CALL DOPW(8HISOT1 ,TYP)
C  41  NAME(2)=TYP
C  42  NAME(3)=TYP
C  43  CALL LDFLOC(KENNZ,NNAM,NAME,ANSW)
C  44  CALL NDFLOC(KENNZ,NNAM,NAME,NDAT,NC0)
C  45  IF(KENNZ.EQ.0) GC TO 3
C  46  ANSW(1)=NAME(4)
C  47  ANSW(2)=NAME(5)
C  48  F4(I,1)=ANSW(1)
C  49  U=F4(I,2)
C  50  A=F4(I,1)
C  51  WRITE(NA,19) U,A
C  52  19  FORMAT(' AT THE END OF REPROB U=',E12.5,'A=',E12.5)
C  53  15  RETURN
C  54  END

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SUBROUTINE ENORG(EU,EO,EI,EF,NACT,KMAX,KEN,NISGI,NISGIP)
C*****SUBROUTINE ESTABLISHES ENERGY-FIELD,CONSISTING OF THE ENERGY
C*****POINTS OF SGIZC (SGI) AND THE ENERGY POINTS OF THE WEIGHTING SPECT
C*****RPM, FOR THE ENERGY REGION OF THE ENERGY-GROUP CALCULATED.
COMMON NAM,ISTRUK,ISPA,AA,LIZ,NANF,NENC,KL

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REAL*8 NAM
DIMENSION EI(NISGI),EF(KEN)
NISGIF=0
EPS=0.0
E1=AMAX1(EF(1),EU)
E2=AMIN1(EF(KEN),EO)
CALL CUTS(E1,E2,EF,KEN,KA,KE,KMAX1)
C*****KA:EF(KA)=POINT OF SPECTRUM EF WITH LOWEST ENERGY, THAT BELONGS TO
C*****THE DESIRED REGION. EF(KE):PCINT CF EF WITH HIGHEST ENERGY, WHICH
C*****BELONGS TO THE DESIRED REGION. KMAX1=NUMBER OF ENERGY PCINTS EF IN
C*****THE REGION.
C WRITE(NA,100) KA,KE,KMAX1
C 100 FCRMAT(' AFTER CUT KA=',I6,'KE=',I6,'KMAX1=',I6)
NISGIF=NACT+KMAX1+2
IF(NISGIF.LE.NISGI) GO TO 1
NISGIP=NISGIF-NISGI
GO TO 10
1 EI(NACT+1)=E1
EI(NACT+2)=E2
NACT2=NACT+2
DO 2 J=1,KMAX1
2 EI(NACT2+J)=EF(KA+J-1)
KMAX=NACT+KMAX1+2
C WRITE(NA,102) (I,EI(I),I=1,KMAX)
C 102 FCRMAT(2(' ',I6,E12.6))
CALL ORD1(KMAX,E1,E2,EI,NISGI,EPS)
C WRITE(NA,101) (KS,EI(KS),KS=1,KMAX)
C 101 FCRMAT(2(' KS=',I6,'EI=',E12.5))
10 RETURN
END

SUBROUTINE ORD1(KMAX,EMIN,FMAX,FELD,NTT,EPS)
DIMENSION FELD(NTT)
C
C ORD1 ORDNET FELD NACH WACHSENDEN WERTEN
C
IF(KMAX.LT.2) GOTO 100
DC 99 K=2,KMAX
M=K-1
IF(FELD(K).GE.FELD(M)) GOTO 59
R=FELD(K)
10 M=M-1
IF(M.EQ.0) GOTO 20
IF(R.LT.FELD(M)) GOTO 10
20 IA=M+1
IE=K-1
J=IE
CC 30 I=IA,IE
FELD(J+1)=FELD(J)
30 J=J-1
FELD(IA)=R
59 CONTINUE

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6C
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8C
9C
100
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14C
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19C
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23C
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250
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28C
290
300
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320
33C
340
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360
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38C
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400
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420
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100 IF(KMAX.EQ.0) GOTO 200
GCTC 300
200 EMIN=0
FMAX=0
GO TO 800
300 KMAXX=KMAX
DC 500 K=2,KMAX
502 IF(K .GT.KMAXX) GO TO 501
M=K-1
IF((FELD(K)-FELD(M))/FELD(K).LE.EPS) GO TO 600
GC TO 500
600 KMAXX=KMAXX-1
KMAXS= MAX0(K,KMAXX)
DC 700 KK=K,KMAXS
700 FELD(KK)=FELD(KK+1)
GC TO 502
500 CONTINUE
501 KMAX=KMAXX
EMIN=FELD(1)
EMAX=FELD(KMAX)
800 CONTINUE
RETURN
END

C*****SUBROUTINE SIMPSI. DATE CF LAST CHANGE 15.11.1976. (LINES 10212
C*****TC 10790)
SUBROUTINE SIMPSI(NUGRE,U,AW,XMJE,A,B,EPS,NMAX),RESINT,N,EZ,SGIZC,
IEF,FI,ENG,NACT,NFE,NE,NA,EP,F1,F2,F3,F4,NEP,NF,KCNT,ERR,INTG)
C*****A,B=LIMITS OF INTEGRATION. NMAX: MAXIMUM NUMBER CF INTEGRATION POIN
C*****TS. FINT: FUNCTION, WHICH IS TO BE INTEGRATED. RESINT: RESULT
C*****OF INTEGRATION. FINT(X,..): X=COORDINATE, OVER WHICH THE INTEGRATION
C*****IS CARRIED OUT.
COMMON NAM,ISTRUK,ISPA,NA,L17,NAF,NFND,KL
REAL*8 NAM
DIMENSION EZ(NACT),SGIZC(NACT),EF(NFE),FI(NFE),ENG(NE),EP(NEP),
F1(NF,NEP),F2(NF,NEP),F3(NF,NEP),F4(NF,NEP)
INTG=0
NINT=0
NMAX=NMAXX
IF(ENG(NUGRE+1).LE.101..AND.A.LE.U*1.0005) NMAX=100
IF(ABS((B-A)/B).LE.1.E-5) GO TO 1C
IF(ABS((B-A)/B).LE.5.E-5) GC TO 5
GC TO 6
5 NMAX=20
6 N=2
SUM=FINT(A,NUGRE,U,AW,XNUE,FZ,SGIZC,EF,FI,ENG,NACT,NFE,NE,NN,FP,
F1,F2,F3,F4,NEP,NF,KCNT)+4.*
2FINT((A+B)*0.5,NUGRE,U,AW,XNUE,EZ,SGIZC,EF,FI,ENG,NACT,NFE,NE,NN,
3EP,F1,F2,F3,F4,NEP,NF,KCNT)
4+FINT(B,NUGRE,U,AW,XNUE,EZ,SGIZC,EF,FI,ENG,NACT,NFE,NE,NA,
5EP,F1,F2,F3,F4,NEP,NF,KCNT)
H=SNGL(D.500*(DBLE(B)-DBLE(A)))

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SUM4=FINT((A+H),NUGRE,U,AW,XNUF,EZ,SGIZC,EF,FI,ENG,NACT,NFE,NE,NN, 290
1EP,F1,F2,F3,F4,NEP,NF,KONT) 300
ERR=1. 310
RFSINT=0. 320
IF(SUM.EQ.0.)GCTC 4 330
1 CONTINUE 340
SLME=SUM 350
N2=N 360
A=2*N 370
H2=H 380
H=0.5*H 390
IF(H/A.LT..5E-6.AND.N.GT.100)NINT=1 400
SUM2=2.*SUM4 410
SLM4=0. 420
HM=A-H 430
DC 2 M=1,N2 440
HM=HM+H2 450
2 SUM4=FINT(HM,NUGRE,U,AW,XMJE,EZ,SGIZC,EF,FI,FNC,NACT,NFE,NE,NN, 460
1EP,F1,F2,F3,F4,NEP,NF,KONT) 470
2+SUM4 480
SLM=-SUM2+4.*SUM4+SUM 490
RESINT=H*SUM/3. 500
ERR=ABS(1.-2.*SUME/SUM) 510
IF(N.GE.NMAX.OR.NINT.EQ.1)GOTO 3 520
IF(N.LT.4.OR.ERR.GT.EPS)GOTO 1 530

GCTC 4 540
3 IF(ERR.LE.EPS)GOTO 4 550
INUGRE=NE-NUGRE 560
INTG=1 570
WRITE(NA,1000)N,NMAX,RESINT,ERR,NN,A,B,INUGRE,H 580
1000 FORMAT(/' **SIMPSI, N=',I6,' NMAX=',I6,' RESINT=',1PE14.6,' ERR= 590
',F14.6/' NN=',I6,' A=',E14.6,' B=',E14.6,' INUGRE=',I4, 600
',H=',E14.6) 610
4 RETURN 620
10 RESINT=FINT(A,NUGRE,U,AW,XNUE,EZ,SGIZC,EF,FI,ENG,NACT,NFE,NE,NN, 630
1EP,F1,F2,F3,F4,NEP,NF,KONT)+FINT(B,NUGRE,U,AW,XNLE,EZ,SGIZC,EF,FI, 640
2ENG,NACT,NFE,NE,NN,EP,F1,F2,F3,F4,NEP,NF,KONT) 650
RESINT=RESINT*(B-A)*0.5 660
GCTC 4 670
END 680

FUNCTION SINPOL(EINT, EFELD,FELC,NFELD) 1C
C*****FUNCTION CALCULATES VALUE OF FELD AT ENERGY FINT BY LINEAR INTERP 20
C*****CLATION 30
C*****OLATION 40
DIMENSION EFELD(NFELD),FELD(NFELD) 50
COMMON NAM,ISTRUK,ISPA,AA,LIZ 60
REAL*8 NAM 70
DC 1 I=1,NFELD 80
IF(EFELD(I).LT.EINT)GO TO 1 90
IF(EFFLD(I).EQ.EINT)GO TO 2 100
IF(EFFLD(I).GT.EINT)GO TO 4 110

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4 IF(I.EQ.1)GO TO 5 120
I1=I 130
GO TO 6 140
2 I1=I 150
GC TO 3 160
1 CONTINUE 170
IF(ABS(EFELD(NFELD)-EINT)/AMAX1(EFELD(NFELD),EINT).LT.1.E-6) 180
1GO TO 8 190
WRITE(NA,101)EFELD(NFELD),EINT 200
101 FORMAT(' INTERPOLATION NOT POSSIBLE,GREATEST VALUE OF FIELD EFFLD 210
1 IS',E14.7,'EINT=',E14.7) 220
SINPOL=0. 230
GC TO 99 240
3 SINPOL=FELD(I1) 250
GC TO 99 260
5 IF(ABS(EFELD(I1)-EINT)/AMAX1(EFELD(I1),EINT).LT.1.E-6)GO TO 10 270
WRITE(NA,100)EFELD(I1),EINT 280
100 FORMAT(' INTERPOLATION NOT POSSIBLE.SMALLEST VALUE OF FIELD EFFLD= 290
1=',E14.7,'EINT=',E14.7) 300
SINPOL=0. 310
GC TO 99 320
6 SINPOL=FIPOLA(EFELD(I1-1),EINT,EFELD(I1),FELD(I1-1),FELD(I1)) 330
C 99 WRITE(NA,102)EINT,SINPOL 340
GC TO 99 350
10 SINPOL=FELD(I) 360
GC TO 99 370
8 SINPOL=FELD(NFELD) 380
C 99 WRITE(NA,102)EINT,SINPOL 390
C 102 FORMAT(' END OF SINPOL EINT=',E14.6,'SINPOL=',E14.6) 400
99 RETURN 410
END 420

FUNCTION FINT(E,NUGRE,U,AW,XNUE,EZ,SGIZC,EF,FI,ENG,NACT,NFE,NF,NN, 10
1EP,F1,F2,F3,F4,NEP,NF,KONT) 20
DIMENSION EZ(NACT),SGIZC(NACT),EF(NFE),FI(NFE),ENG(NE),EP(NEP), 30
1F1(NF,NEP),F2(NF,NFP),F3(NF,NEP),F4(NF,NEP) 40
IF(NF.GT.1)GO TO 1 50
GO TO 2 60
1 W=SINPOL(E,EF,FI,NFE) 70
GC TO 3 80
2 W=PHI(E) 90
3 IF(NN.EQ.2)GC TO 7 100
FFINT=SINPOL(E,EZ,SGIZC,NACT)*W 110
IF(NN.EQ.1)GC TO 4 120
GC TO 5 130
4 FINT=FFINT*PROB(E,NUGRE,U,AW,XNUE,ENG,NF,EP,F1,F2,F3,F4, 140
1NEP,NF,KONT) 150
C WRITE(6,100)FINT,E,NUGRE 160
C 100 FORMAT(' ***FINT=',E12.5,'E=',E12.5,'NUGRE=',I6) 170
GO TO 6 180
5 FINT=FFINT 190
GC TO 6 200

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7 FINT=W
6 RETURN
END

C****FLNCTION PROB. DATE OF LAST CHANGE 15.11.76.(LINES 23970
C****TC 24560)
FLNCTION PROB(E,NUGR,U,A,XNUE,ENG,NE,EP,F1,F2,F3,F4,
INEP,NF,KONT)
C****SUBROUTINE CALCULATES PROBABILITY FOR INELASTIC SCATTERING FROM
C****ENERGY E TO GROUP NUGR. AN EVAPORATION MODEL IS USED. U IS THE
C****TRESHOLD OF THE INELASTIC SCATTERING PROCESS.
C****NUGR=GROUP NUMBER,ENG(NUGR)=LOWER ENERGY LIMIT OF GROUP,
C****ENG(NUGR+1)=UPPER ENERGY LIMIT OF GROUP.
REAL*8 ELD,EUP,EXEM,EINS,SU1,SU2,EMD,WC,EXEL,FXC,
I NAM, EMAX,W,SM
DIMENSION ENG(NE),EP(NEP),F1(NF,NEP),F2(NF,NEP),F3(NF,NEP),
IF4(NF,NEP)
COMMON NAM,ISTRUK,ISPA,NA,LIZ
C XNUE IS THE ADJUSTABLE PARAMETER FOR THE CALCULATION OF THE
C NUCLEAR TEMPERATURE AND IS AN INPUT QUANTITY.
ETHR=E-U
IF(ETHR.LE.ENG(NUGR)) GO TO 1
ELP=AMIN1(ENG(NUGR),ETHR)
ELP=AMIN1(ENG(NUGR+1),ETHR)
IF(KONT.EQ.1) GO TO 3
XN=XNUE*A
THF=THETA(E,XN)
GO TO 2
3 THF=TEMP(E,EP,F3,NEP,NF)*0.000001
IF(THF.EQ.0.) GO TO 1
GO TO 2
1 PROB=0.
GO TO 99
2 THE2=THE**2
FL=ELP/THE*0.000001
EL=EUP/THE*0.000001
EM=EU-EL
ELC=DBLF(EL)
ELD=DBLF(EU)
EMD=DBLF(EM)
EINS=DBLE(1.0)
IF(EM-0.01)600,600,601
C IF (E(H)/THETA-E(H+1)/THETA) LESS OR EQUAL 0.01,(STATEMENT
C NUMBER 600),EXD IS USED TO CALCULATE THE TRANSITION PRORABILITIES,
C OTHERWISE(STATEMENT NUMBER 601) THE DBLBLE PRECISICK EXPONENTIAL
C FUNCTION IS SUFFICIENT.
600 WC=-ELD*FXD(-EMD)-EMD*EXD(-EMD)-EXC(-EMD)-EMD
C EXEL=DEXP(-ELD)
C WD=EXEL*WD
GO TO 602
601 EXEM=DEXP(-EMD)
SU1=EINS+ELD

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210
220
230
10
2C
3C
40
5C
60
7C
80
90
10C
110
120
130
140
15C
160
17C
180
190
20C
210
220
230
240
25C
260
270
280
290
300
310
320
330
340
35C
360
370
380
390
400
410
420
430
440
450
460
470
480

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SL2=FIN5+EUD
SU2=SU2*EXEM
WD=SUL-SU2
6C2 EXEL=DEXP(-ELD)
WC=EXEL*WD
W =WD*DBLF(THF2)
C****WN:PROBABILITY FOR INELASTIC SCATTERING FROM ENERGY E ,INTEGRATED
C****COVER ALL POSSIBLE FINAL ENERGIES.
C****NORMALIZATION OF PROBABILITIES TO 1.
ARG=(E-U)/THE*C.000001
WN=THE2*(1.-EXP(-ARG))*(1.+ARG)
PRCB=SNGL(W)/WN
99 RETURN
END

DOUBLE PRECISION FUNCTION EXC(X)
EXD CALCULATES THE SERIES EXP(X)-1.
REAL*8 X,XN,DNFAK,XN1
N=1
1 XN=X**N/DNFAK(N)
IF(DABS(XN).LE.1.D-50) GO TO 2
N=N+1
GO TO 1
2 IF(N.EQ.1) GO TO 4
N1=N-1
EXD =XN
DO 3 K=1,N1
XN1=XN*DFLOAT(N-K+1)/X
EXD = EXD +XN1
3 XN=XN1
GO TO 5
4 EXC=XN
5 RETURN
END

FUNCTION THETA(E,XN)
C****FLNCTION CALCULATES NUCLEAR TEMPERATURE OF RESIDUAL NUCLEUS IN MEV
THETA=SQRT(E/XN)*0.001
RETURN
END

DOUBLE PRECISION FUNCTION DNFAK(NN)
DNFAK CALCULATES N*(N-1)*(N-2)*.....*(N-(N-1)) FOR THE
SERIES DEVELOPED IN EXC.
REAL*8 N
N=CFLOAT(NN)

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49C
500
510
520
530
540
55C
560
570
580
59C
60C
610
620
1C
2C
30
40
50
60
70
80
90
100
11C
120
130
140
150
16C
170
180
190
10
20
30
40
50
10
20
30
40
50

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1 2 08 1

<pre> DNFAK=N 1 IF(N.LE.(1.DO+1.D-5))RETURN N=N-1.DO DNFAK=DNFAK*N GO TO 1 ENC </pre>	<pre> 60 70 80 90 100 110 </pre>	<pre> FIPOLD=(YA*DX2+YC*DX1)/DX GO TO 2 1 FIPOLD=(YA+YC)/2. 2 RETURN ENC </pre>	<pre> 100 110 120 130 140 </pre>
<pre> C C FUNCTION TEMP(EFS,EP,F3,NEP,AF) COMMON NAM,ISTRUK,ISPA,NA,LIZ,NANF,NEND,KL DIMENSION EP(NEP),F3(NF,NEP) REAL*8 NAM COMMON/APOINT/INEP,INF DO 4 I=1,INEP IF(EP(I)-EFS)1,2,3 1 GO TO 4 3 IF(I.EQ.1) GO TO 9 I1=I GO TO 5 2 TEMP=F3(I,I) GO TO 7 4 CONTINUE TEMP=F3(I,INEP) 8 CONTINUE 8 WRITE (NA,100) EFS,EP(I),EP(NT) C 100 FORMAT(' DIE GEWUENSCHTE ENERGIE EFS=',E16.8,' LIEGT AUSSERHALB C 1 DES VORGEgebenEN ENERGIEBEREICHs', ' E(I)=' ,E16.8, ' EN(T)=' ,E16.8) GO TO 7 9 TEMP=F3(I,I) C 9 TEMP=0. GO TO 8 5 TEMP=(F3(I,I1)-F3(I,I1-1))/(EP(I1)-EP(I1-1))*(EFS-EP(I1-1)) I=F3(I,I1-1) 7 GO TO 6 C 7 WRITE(NA,101) EFS,TEMP C 101 FORMAT(' EFS=' ,E16.8, ' TEMP=' ,E16.8) 6 RETURN ENC </pre>	<pre> 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290 300 310 320 </pre>	<pre> C****SLBROUTINE SCATD.DATE OF LAST CHANGE 14.1C.1976.(LINES 6532 TC C****10210) C CALCULATIONS OF THE INELASTIC SCATTERING PROBABILITIES C SLBROUTINE SCATD(NX,EG,NFE,EF,FI,NE27,WEIN,QUOT,WAHR,VW, 1E,AE,SU,LBA,SGIT,IANF,SGIP,WERT,EZ, 2NISG,NISGP,NAE,NAEP,ISG,ISGP,KINEM,NEA,NAP) REAL*8 NAM,ISOT,NAM4,EC,EU,DIFF,AE,EMIN,EMAX,F,SUM,WAHR, 1WAI,VW,UWA,EH,AB,EZ,FE,FA REAL*8 WITHP,WITH/* WITH /*,WITHC/* WITHOUT*/ DIMENSION AE(NAE),SGIP(ISG,NAE),WERT(ISG), 1EG(NX),EF(NFE),FI(NFE),NN(4),SU(NX),QUOT(NX),WATR(NX), 2LBA(NX),VW(NX),E(NE27),SGIT(ISG), 3ISCT(2),IANF(NAE),EZ(NISG),WEIN(NX,NX) COMMON NAM,ISTRUK,ISPA,NA,LIZ,NANF,NEND,KL DATA ISOT/'BEST ', 'ISOT1'/ WRITE (NA ,9001) 9001 FORMAT(///' PROGRAM ZUR BERECHNUNG INELASTISCHER STREUMATRIZEN' / 1 VCN DISKREten ANREGUNGSNIVEAUS.*/) WRITE(NA,9002) C9002 FORMAT(1H0/' PROBSGIZ'/1X) IF(KINEM.EQ.C)GOTO 20 XM=1.008665 WITHP=WITH GOTO 21 20 XT=0. WITHP=WITHO C 21 WRITE(NA,9003)WITHP C9003 FORMAT(///' CALCULATION ',A8,' KINEMATIC',/' ',32(' - ')) 21 NN(1)=3 AE(1)=NAM AE(2)=ISOT(1) AE(3)=ISOT(2) CALL NDFLOC (I,NN,AE,K,K) IF(I.EQ.0) GO TO 999 A=AE(4) NE=NX C IF NOT CONTAINED IN EG(NX) THE THERMAL GROUP C IS ADDED.THIS RESULTS IN E(NE27). IF(EG(I)-1.E-2)305,301,307 305 WRITE (NA,304) 304 FORMAT(1' ***ERROR 5.01 : THE LOWER BOUNDARY OF THE LOWEST ENERGY' / 2' GROUP HAS TO BE LARGER OR EQUAL TO 1.E-3,WHICH IS THE LOWEST' / 3' ENERGY ON KEDAK FOR ALL DATA TYPES.THIS IS NOT FULFILLED') GC TO 999 </pre>	<pre> 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290 300 310 320 330 340 350 360 370 380 390 400 410 420 430 440 450 460 </pre>
<pre> C C IN THE FOLLOWING FUNCTION FIPOLD(XAD,YA) AND (XCD,YD) ARE THE STARTING POINTS AND (XBD,FIPOLD) IS THE INTERPLATED PCINT. FUNCTION FIPOLD(XAD,XBD,XCD,YA,YC) REAL*8 XAD,XBC,XCC DX1=SNGL(XBD-XAD) DX2=SNGL(XCD-XBD) DX=SNGL(XCD-XAD) IF(DX.LT.1.E-20) GO TO 1 </pre>	<pre> 10 20 30 40 50 60 70 80 90 </pre>		

B 89

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307 NE=NE27
    E(1)=1.0-3
    DO 302 I=2,NE27
302 E(1)=EG(I-1)
    GC TO 303
301 DO 300 I=1,NE
    E(I)=EG(I)
300 CCNTINUE
C   WRITE(NA,9200) (I,E(I),I=1,NE)
C9200 FCRMAT(3(' I=',I6,'E=',E15.9))
C   DETERMINATION OF THE EFFECTIVE INITIAL ENERGY GRUOP CUT OF WHICH
C   INELASTIC SCATTERING OCCURS AND OF THE LAST GROUP UP TO WHICH
C   THE TRANSITION PROBABILITIES ARE REQUIRED
303 NE1=NE-1
    DC 37 IM=1,NE1
37 CUOT(IM)=0.0
    IANF=NE-NANF
    IE=NE-NEND
    KI=2
    KEN=NFE
    IF(NFE.EQ.1) KEN=0
    IA=0
    IC=C
    NAB1=NE27-1
    NAB=NAB1
    NISGP=0
    NISGF=0
    NAEF=0
    NAEF=0
    ISGP=0
    ISGF=0
    JMAT=0
C   WRITE(NA,9010) IC,NISG,NISGF,NISGP,NAE,NAEF,NAEF,ISG,
C   IJMAT
9010 FCRMAT(' IC=',I6,'NISG=',I6,'NISGF=',I6,'NISGP=',I6/'NAE=',I6,
1'NAEF=',I6,'NAEF=',I6,'ISG=',I6,'JMAT=',I6)
    DC 90 I=INF,IE
    CALL DAORG(I,KEN,EZ,E,AE,EF,FI,JMAT,LMAX,NISG,NISGF,NISGP,
*NE27,NAE,NAEF,NAEP,ISG,ISGF,ISGP,IA,NAB,&558)
C   WRITE(NA,9012) IA,NAB,I,NAB1
9012 FORMAT(' IA=',I6,'NAB=',I6,'I=',I6,'NAB1=',I6)
    GC TO 997
558 NEA=0
    NAB=0
    GO TO 999
997 IF(IA.GT.I) GO TO 91
    IF(NISGF.NE.0.OR.NAEF.NE.0.OR.ISGF.NE.0) RETURN
91 IF(NAB.EQ.NAB1) GO TO 9C
    GO TO 92

90 CCNTINUE
C 52 WRITE(NA,9011) IA,NAB
9011 FCRMAT(' IA=',I6,'NAB=',I6)
52 IF(IA.GE.I NF) GOTC 205
    NEA=I NF
    GOTC 206

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850
860
870
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980
990
1000
1010

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205 NEA=IA
    IF(IA.LE.IF) GOTO 206
    WRITE(NA,179)
175 FCRMAT(
1' ***ERROR 5.04 : WITH INCIDENT NEUTRON ENERGIES CUT OF THE' / 1060
2' ENERGY GROUPS REQUESTED IN THE INPUT INELASTIC SCATTERING' / 1070
3' FROM DISCRETE LEVELS CANNOT OCCUR.')
    NEA=0
    NAB=0
    GO TO 999
206 KC=IE-NEA+1
    MZ=C
    CALL DOPW (3HSMTOT ,NAM4)
C 26 WRITE(LIZ) MZ,NAM4
26 CCNTINUE
C IF(EZ(1).LT.E(IA+1)) GOTO 39
C 204 KD=KD-1
39 KZ=KI+1
C WRITE (LIZ) KZ,NAM,KC
C LOOP OVER ALL OUTSCATTERING GROUPS TO BE CONSIDERED
    DC 1 I=NEA,IE
C WRITE(NA,9016) I,NAB,NEA,IE,NFE
9016 FCRMAT(' I=',I6,'NAB=',I6,'NEA=',I6,'IE=',I6,'NFE=',I6)
    CALL AKED(I,E,EZ,SGIP,JMAT,LMAX,SU,QUCT,WERT,AE,
1IA,NAB,IE,IANF,NFE,EF,FI,NE,NX,SGIT,NAE,
2NAEP,ISG,ISGF,IANF,NISG,NISGP)
    IF (LMAX.EQ.0) GO TO 955
    EMIN=EZ(I)
    EMAX=EZ(LMAX)
C WRITE(NA,9050)JMAT,I,SU(I)
C9050 FCRMAT(' AFTER AKED JMAT=',I6,'I=',I6,'SU=',E12.6)
C DO 310 J=1,JMAT
C 310 AE(J)=AE(J)*((A+XM)/A)
    NFI=NE-I
    IF(E(I+1).LE.EZ(1)) GOTO 1
10 GES=0.
    IF(I-NAR)83,85,1002
85 EF=EMAX
    GC TO 89
83 EF=E(I+1)
85 NE1=NE-1
C LOOP OVER ALL INSCATTERING GROUPS
    DO 2 K=1,I
    SUM=0.DO
C LOOP OVER ALL INELASTIC EXCITATION LEVELS OF THE MATERIAL CONSIDER
    DC 3 J=1,JMAT
C WRITE(NA,9014)J,IANF(J),EZ(1),LMAX
C9014 FCRMAT(' J=',I6,'IANF(J)=',I6,'EZ(1)=',G14.6,'LMAX=',I6)
    IF(J.NE.1) GOTO 6
C KMIN=0
    KMIN=IANF(J)-1
    GC TO 8
6 KMIN=IANF(J)-1
C DETERMINATION OF THE LIMITS EU,EO FOR INTEGRATION OVER THE
C CUTSCATTERING GRUOP

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1190
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1550
1560

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8 FE=1.00
FA=1.00
IF(KINEM.EQ.2) GO TO 5
IF (KINEM.EQ.1) GO TO 2C1
GC TO 20C
201 FA=DBLE((A+XM)/A)
GC TO 200
5 EINMIN=(A*A+X*M*A)/(A*A+X*M*X*M)*SNGL(AE(J))
WRITE(NA,9051) J,AE(J),EINMIN
C9C51 FCRMAT(' J=',I6,'AE=',D14.6,'EINMIN=',F14.6)
FE=DBLE((A*A+X*M*X*M)/((A+X*M)*(A+X*M)))
FA=DBLE(A/(A+X*M))
200 IF((E(K)+FA*AE(J)).LT.FE*E(I)) GOTO 9
IF((E(K)+FA*AE(J)).GE.FE*E(I)) GOTO 88
EU=(E(K)+FA*AE(J))/FE
GC TO 44
9 IF((E(K+1)+FA*AE(J)).LT.FE*E(I)) GOTO 3
EU=E(I)
44 IF((E(K+1)+FA*AE(J)).GE.FE*E(I)) GOTO 61
EO=(E(K+1)+FA*AE(J))/FE
GC TO 62
61 EC=EH
C DETERMINATION OF SIGMA AND THE WEIGHTING FUNCTION AT EU,EO
62 KJ=LMAX-IANF(J)+1
C WRITE(NA,9100) I,K,EO,EU
C9100 FORMAT(' I=',I6,'K=',I6,'EO=',D20.6,'EU=',D20.6)
IAB=0
IAF=0
IF1=IAF+1
IB=IAB+1
F11=0.
F12=0.
SGP1=0.
SGP2=0.
IF(KJ.LE.0)GOTO 80
DC 4 IG=1,KJ
KM=KMIN+IG
IF(EZ(KM).GE.EU) GOTO 66
65 IAB=IG
IAF=IG
IF(EZ(KM+1).LT.EO) GOTO 4

IF(EZ(KM+1).GE.EO) GOTO 67
66 IF(IG.NE.1) GOTO 72
SGP1=SGIP(1,J)
CALL TRA(EU,F11,NFE,EF,FI)
IAF=1
IF(EZ(KM).LT.EO) GOTO 4
164 SCP2=SGIP(1,J)
CALL TRA(EO,F12,NFE,EF,FI)
GC TO 80
72 IF(IAB.NE.0) GOTC 70
73 IF(EZ(KM).GE.EO) GOTO 75
76 IAF=IG
GO TO 4
70 IF(EZ(KM).LT.EC) GOTO 74

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1570
1580
1590
1600
1610
1620
163C
1640
1650
1660
1670
168C
1690
170C
1710
1720
173C
1740
175C
1760
1770
178C
1790
180C
1810
1820
1830
1840
1850
1860
1870
1880
1890
190C
1910
1920
193C
1940
1950
1960
1970

1980
1990
2000
2010
202C
2030
2040
2050
2060
207C
2080
209C
2100
2110

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75 IF1=IAF+1
KMF=KMIN+IF1
KMAF=KMIN+IAF
SGF2=FIPOLD(EZ(KMAF),EO,EZ(KMF)),
1SGIP(IAF,J),SGIP(IF1,J))
2120
213C
2140
2150
216C
2170
218C
2190
2200
2210
2220
2230
2240
2250
2260
227C
2280
229C
230C
2310
2320
2330
2340
235C
2360
2370
2380
239C
2400
2410
242C
2430
2440
2450
2460
247C
2480
2490
2500
2510
2520
253C
2540
255C
256C
2570
2580
2590
2600
2610
2620
2630
2640
265C
2660
63 IF(L.NE.IB1) GOTO 49

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48 F1=SGP1*FI1
   DIFF=EZ(KMB1+1)-EU
   GC TO 43
49 IF(L.NE.LIE) GOTO 46
47 F1=F2
   DIFF=E0-EZ(KMAF)
   F2=SGP2*FI2
   GC TO 45
46 F1=F2
   DIFF=EZ(KML+1)-EZ(KML)
43 IF(IAB.EQ.0) GOTO 181
   F2=SGIP(L+1,J)*WERT(KML+1)
   GOTO 45
181 F2=SGIP(L,J)*WERT(KML+1)
45 SUM=SUM+DIFF*(DBLE(F1)+DBLE(F2))/2.DO
C 60 WRITE(NA,9053) L,KML,EZ(KML),EZ(KML+1)
C9053 FORMAT(' L=',I4,'KML=',I4,'EZ(KML)=' ,E12.6,'EZ(KML+1)=' ,E12.6)
60 CONTINUE
C SUMMATION LOOP FOR INTEGRAL CLOSED
2 CONTINUE
C LCCP OVER EXCITATION LEVELS J CLOSED
88 IF(SU(I).EQ.0.0) GCTC 42
51 WAHR(K)=SUM/DBLE(SU(I))
   GC TO 52
42 WAHR(K)=0.DO
52 GES=GES+SNGL(WAHR(K))
C 2 WRITE(NA,9101) I,K,WAHR(K)
C9101 FORMAT(' I=',I6,'K=',I6,'WAHR=' ,E12.6)
2 CONTINUE
C LOOP OVER ALL INSCATTERING GROUPS K CLOSED

1002 GC TO 111
111 QUC=0.
   KE=0
   CC 55 LK=1,I
   LB=I+1-LK
130 IF(GES.EQ.0.0) GOTO 54
53 WAHR(LK)=WAHR(LK)/DBLE(GES)
   GO TO 56
54 WAHR(LK)=0.DO
56 QUC=QUC+SNGL(WAHR(LK))
   VW(LB)=WAHR(LK)
55 CONTINUE
   NZ=1
   CC 170 KV=1,I
   WAHR(KV)=VW(KV)
   AB=0.DO
   IF(WAHR(KV).LE.AB) GOTO 17C
171 NZ=KV
170 CONTINUE
   IF(KE.NE.1) GCTC 136
C CONCERNS ONLY THE SCATTERING PROBABILITIES IN THE DISCRETE REGION
145 CC 137 KO=1,I
   IF(QUC.NE.0.0) GCTC 161
162 UWA=0.DO
   GCTC 163

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2670
2680
2690
2700
271C
272C
273C
274C
275C
276C
277C
278C
279C
280C
281C
282C
283C
284C
285C
286C
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315C
316C
317C
318C
319C
320C
321C
161 UWA=WAHR(KO)/DBLE(QUC)
163 WAHR(KO)=UWA
137 CONTINUE
C ORGANIZATION OF THE OUTPUT ON LISTING IN THE FORM OF MAXIMUM 11
C SCATTERING PROBABILITIES PER LINE STARTING WITH THE OUTSCATTERING
C GROUP OF LOWEST ENERGY(LARGEST GROUP NUMBER ACCORDING TO ABN-SET)
136 DC 126 LN=1,NZ
   LBA(LN)=NEI+LN-1
126 CONTINUE
   GO TO 146
C KI=NZ/11
C KII=KI*11
C IF(N7.NE.KII) GOTO 168
C 167 KII=KI
C GOTO 169
C 168 KII=KI+1
C 169 DC 146 LI=1,KII
C IF(LI.NE.1) GOTO 147
C 148 LIM=1
C GO TO 149
C 147 LIM=(LI-1)*11+1
C IF(LI.EQ.KII) GCTC 150
C 149 IF(KII.LE.1) GOTO 150
C 154 LII=LI*11
C GO TO 151
C 150 LII=NZ
C 151 IF(LIM.GT.LII) GCTC 146
C WRITE(NA,125) (LBA(LM),LM=LIM,LII)
C 125 FORMAT(10X,11(3X,I3,5X))
C IF(LI.NE.1) GOTO 153
C NEI-CUTSCATTERING GROUP ACCORDING TO THE COUNTING IN THE ABN-SET
C I.E. LOWEST GROUP NUMBER CORRESPONDS TO HIGHEST ENERGY BOUNDARIES
C WAHR-PROBABILITY FOR INELASTIC SCATTERING OUT OF GROUP I INTO K
C 152 WRITE(NA,124) NFI,(WAHR(LM),LM=1,LII)
C 124 FORMAT(3X,I2,5X,11(1PE10.3,1X))
C 153 WRITE(NA,129)(WAHR(LM),LM=LIM,LII)
C 129 FORMAT(10X,11(1PE10.3,1X))
146 CONTINUE
   NZ1=NZ+1
   CC 500 K=1,NZ
500 WEIN(I,K)=SNGL(WAHR(K))
C WRITE(LIZ) NZ1,NEI,(WEIN(I,K),K=1,NZ)
C WRITE(NA,9100) NZ1,NEI,I
C9100 FORMAT(' NZ1=',I6,'NEI=' ,I6,'I=' ,I6)
C WRITE(NA,9110) (WEIN(I,K),K=1,NZ)
C9110 FORMAT(1CE12.5)
1 CONTINUE
999 RETURN
   END

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B 92

SUBROUTINE AKED (I, E, EZ, SGIP, JMAT, LMAX, SU, QUOT, WERT, AE,	10	GOTO 316	560
1 IA, NAB, IE, INF, NFE, EF, FI, NE, NX, SGIT, NAE,	20	315 LMAX=LMA	570
2 NAE, ISG, ISGP, IANF, NISG, NISGP)	30	C INTERPOLATION OF THE WEIGHTING FUNCTION AT THE KEDAK ENERGY POINTS	580
REAL*8 NAM, FELC, KFEL, NAM3, NAM3, AE, EMAX, E, EMIN, EZ	40	316 KEN1=KEN-1	590
DIMENSION FELD(6), KFEL(6), NFFL(6), SU(NX), QUOT(NX), E(NE),	50	IF(LMAX.LE.ISG) GO TO 15	600
1 AE(NAE), WERT(ISG), SGIP(ISG, NAE), SGIT(ISG),	60	ISGP=LMAX-ISG+1	610
2 EF(NFE), FI(NFE), IANF(NAE), EZ(NISG)	70	RETURN	620
COMMON NAM, ISTRUK, ISPA, NA, LIZ	80	C 306 IF(KEN.EQ.0) GOTO 156	630
EQUIVALENCE (FELD(1), KFEL(1))	90	15 DC 32 LF=1, LMAX	640
EPST=.001	100	WERT(LF)=0.	650
NISGF=0	110	EA=EZ(LF)	660
NISGP=0	120	CALL TRA(EA, FIS, NFE, EF, FI)	670
NAEF=0	130	32 WERT(LF)=FIS	680
ISGF=0	140	C INTERPOLATION OF SIGMA TCTAL AND THE WEIGHTING FUNCTION AT THE	690
NAEP=0	150	C ENERGY GROUP BOUNDARIES	700
ISGP=0	160	39 II=I	710
ISGP=0	170	NE1=NE-1	720
KEN=NFE	180	C CRITICAL CASES	730
IF(NFE.EQ.1) KEN=0	190	IF(E(IA+1).GT.EZ(1)) GCTC 7	740
CALL DADRG(I, KEN, EZ, E, AE, EF, FI, JMAT, LMA, NISG, NISGF, NISGP,	200	8 IF(II.EQ.1A) GOTO 50	750
1 NE27, NAE, NAEF, NAEP, ISG, ISGF, ISGP, IA, NAB,	210	9 IA=IA+1	760
2 A1000)	220	IF(II-IA) 90, 108, 90	770
C WRITE(NA, 9002) JMAT, LMA	230	7 IF(II-IA) 90, 108, 90	780
9002 FCRMAT('\$\$\$AFTER DACRG JMAT=', I6, ' LMA=', I6)	240	108 IF(E(II).GE.EZ(1)) GCTC 112	790
CALL SIORG(I, EZ, AE, SGIP, SGIT, IANF, JMAT, LMA, NISG,	250	109 LA=1	800
1 ISG, NAE)	260	SGI=0.	810
C WRITE(NA, 9001) JMAT, LMA	270	EA=F(II)	820
C9001 FCRMAT('\$\$\$AFTER SIORG JMAT=', I6, ' LMA=', I6)	280	CALL TRA(EA, FH1, NFE, EF, FI)	830
IF (LMA.EQ.0) GO TO 200	290	GC TO 91	840
GC TO 167	300	112 IF(E(II).EQ.EZ(1)) GCTC 116	850
200 NAB=I-1	310	GC TO 1000	860
LMAX=LMA	320	GC TO 90	870
GC TO 1000	330	116 LA=1	880
167 NE1=NE-1	340	SGI=SGIT(1)	890
180 FCRMAT(350	FH1=WERT(1)	900
1' ***ERROR 5.03 : ONE OF THE BOUNDARIES OF THE ENERGY RANGE, IN' /	360	EA=F(II)	910
2' WHICH INELASTIC SCATTERING IS POSSIBLE : EMAX (- UPPER' /	370	GC TO 91	920
3' ENERGY LIMIT OF THE DISCRETE REGION) OR EMIN (- LAST KEDAK' /	380	90 LA=0	930
4' ENERGY, AT WHICH THE TCTAL INELASTIC SCATTERING CRCS SECTION' /	390	91 SL(II)=J.	940
5' IS STILL EQUAL TO ZERO) IS NOT CONTAINED IN ANY OF THE ENERGY' /	400	SUMM=0.	950
6' GROUPS OF THE GIVEN GRUP STRUCTURE. THAT MEANS THE GIVEN' /	410	LMX1=LMAX-1	960
7' STRUCTURE OF ENERGY GROUPS DOES NOT COVER THE WHOLE ENERGY' /	420	DC 40 LL=1, LMX1	970
8' RANGE')	430	IF(LA.NE.0) GOTO 102	980
C DETERMINATION OF THE ENERGY GRUP IA, IN WHICH EMIN IS LYING, AND	440	101 IF(E(II).LT.EZ(LL)) GCTC 40	990
C CF THE ENERGY GROUP NAB, IN WHICH EMAX IS LYING.	450	118 IF(F(II).GF.EZ(LL+1)) GOTO 40	1000
IA=MAX0(INF, IA)	460	117 LA=LL	1010
NAB=MIN0(IE, NAB)	470	SGI=FI*POL0(FZ(LL), E(II), FZ(LL+1),	1020
IF(EZ(LMA).LT.E(NAB+1)) GOTO 315	480	ISGIT(LL), SGIT(LL+1))	1030
DO 313 L=1, LMA	490	C SGI=SGIT(LL)+(SGIT(LL+1)-SGIT(LL))*(E(II)-EZ(LL))/(EZ(LL+1)-EZ(LL)	1040
LMA=L	500	C 1)	1050
IF(FZ(L).GE.E(NAB+1)) GOTO 314	510	EA=E(II)	1060
313 CCNTINUE	520	CALL TRA(EA, FH1, NFE, EF, FI)	1070
C LMAX - (NUMBER OF KEDAK ENERGIES + 1) BETWEEN EMIN AND THE UPPER	530	102 IF(E(II+1).GT.EZ(LL)) GOTO 122	1080
C ENERGY LIMIT E(NAB+1) OF GRUP NAB	540	GC TO 40	1090
314 LMAX=LMA	550	C THE END GROUP IS THE CASE IN QUESTION	1100

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122 IF(II.NE.NAB) GOTO 107
123 NE1=NE-1
    IF(NAB.NE.NE1) GOTO 107
124 IF(E(NAB+1).LT.EZ(LMAX)) GOTO 107
126 EE=EZ(LMAX)
    LE=LMAX
    SG2=SGIT(LMAX)
    FH12=WERT(LMAX)
    GC TO 100
107 IF(E(II+1).GT.EZ(LL+1)) GO TO 128
    GC TO 127
128 IF(LMX1.GT.LL) GO TO 4C
127 LE=LL+1
    EF=DMIN1(E(II+1),EZ(LMAX))
    SG2=FIPOLD(EZ(LL),EE,EZ(LL+1),
1SGIT(LL),SGIT(LL+1))
C SG2=SGIT(LL)+(SGIT(LL+1)-SGIT(LL))*(F(II+1)-EZ(LL))/(EZ(LL+1)-EZ(L
C LL))
C CALL TRA(EE,FH12,NFE,EF,FI)
    GC TO 100
40 CCNTINUE
C IF(LMAX.GT.0) WRITE(NA,3000) II,E(II+1),EZ(LMAX),LMAX
C3000 FCRMAT(' II=',I10,' E(II+1)=' ,1PD14.6,' EZ(LMAX)=' ,1PD14.6,
C 'LMAX=' ,I6)
    GC TO 41
C CALCULATION OF THE INTEGRAL OVER THE WRIGHTING FUNCTION AND THE
C INTEGRAL OVER SIGMA TOTAL*WEIGHTING FUNCTION BY TRAPEZOIDAL RULE
C 100 WRITE(NA,9101) II,LMAX,LA,LE,E(II),E(II+1)
C9101 FCRMAT(' II=',I6,'LMAX=' ,I6,'LA=' ,I6,'LE=' ,I6,'E=' ,E15.9,'E1=' ,E15
C 1.5)
C WRITE(NA,9102) (SGIT(ISR),EZ(ISR),ISF,ISR=1,LMAX)
C9102 FCRMAT(2(' SGIT=' ,E12.6,'EZ=' ,E15.5,'ISR=' ,I6))
100 LE1=LE-1
    DC 30 IL=LA,LE1
    IF(LA.NE.LE1) GOTO 104
3 IF(E(II).GE.FZ(1)) GOTO 103
44 FU1=SGIT(LA)*WERT(LA)
    FU2=SG2*FH12
    DIF1=EZ(LA)-EA
    DIFF=EE-EZ(LA)
    SLP=DIF1*(WERT(LA)+FH11)/2.+DIFF*(FH12+WERT(LA))/2.
    GOTO 28
103 FU1=SG1*FH11
    FU2=SG2*FH12
    DIFF=EE-EA
    SLP=DIFF*(FH12+FH11)/2.
    GO TO 28
104 IF(IL.NE.LA) GOTO 19
5 IF(E(II).GE.EZ(1)) GOTO 34
6 FU1=SGIT(LA)*WERT(LA)
    DIF1=EZ(LA)-EA
    DIFF=EZ(LA+1)-EZ(LA)
    SLP=DIF1*(WERT(LA)+FH11)/2.+DIFF*(WERT(LA+1)+WERT(LA))/2.
    GOTO 35
34 FU1=SG1*FH11

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111C
1120
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114C
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119C
1200
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128C
129C
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138C
1390
1400
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143C
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1460
1470
148C
149C
1500
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1600
161C
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DIFF=EZ(LA+1)-EA
SUP=DIFF*(WERT(LA+1)+FH11)/2.
GC TO 35
15 IF(IL.NE.LE1) GOTO 26
27 FU1=FU2
    DIFF=EE-EZ(LE1)
    SUP=DIFF*(FH12+WERT(LE1))/2.
    FU2=SG2*FH12
    GO TO 28
26 FU1=FU2
    DIFF=EZ(IL+1)-EZ(IL)
    SUP=DIFF*(WERT(IL+1)+WERT(IL))/2.
35 FU2=SGIT(IL+1)*WERT(IL+1)
28 SLM=SUMM+DIFF*(FU1+FU2)/2.
    SL(II)=SU(II)+SUP
30 CCNTINUE
41 IF(SU(II).EQ.0.) GOTO 31
C 29 CLCT(II)=SUMM/SU(II)
29 CLCT(II)=SUMM
    GC TO 50
31 CLCT(II)=0.
C 50 WRITE(NA,9100) II,QUOT(II),SUMM,SU(II)
C9100 FCRMAT(' II=',I6,'QUCT=' ,E12.6,'SUMM=' ,E12.6,'SU=' ,E12.6)
50 CONTINUE
1000 RETURN
END

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166C
1670
168C
1690
1700
171C
1720
1730
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176C
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180C
181C
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186C
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188C
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190C
1910

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SUBROUTINE TRA(EFI,FIS,NF,EF,FI)
DIMENSION EF(NF),FI(NF)
KEN=NF
IF(NF.EQ.1)KEN=0
KLA=0
IF(KEN.NE.0)GOTO 2
1 FIS=PHI(EFI)
GOTO 3
2 CC 105 KI=1,KEN
    IF(EF(KI).GE.EFI)GOTO 114
113 KUA=KI
    GOTO 105
114 KAB=KUA+1
    GOTO 106
105 CCNTINUE
106 FIS=FIPOLA(EF(KUA),EFI,EF(KAB),FI(KUA),FI(KAB))
3 RETURN
END

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1C
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3C
4C
5C
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7C
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110
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140
15C
160
17C
18C

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C*****SLBRoutine NDRoad DATE OF LAST CHANGE 14.10.1976.(LINES 10792
C*****12660)
SLBRoutine NDREAC(I,EZ,E,AE,XLEVEL,J,KMAX,NENRE,NISG,
INTSGF,NI SGP,NE27,NAE,NAEF,NAEP,NETMAX,IL,IB,IP,*)
C*****SUBROUTINE READS ENERGY SCALE OF EXCITATION CROSS-SECTIONS,
C*****HIGH COVER ENERGY GROUP I, WITH LOWER ENERGY LIMIT E(I) AND
C*****UPPER ENERGY LIMIT E(I+1).
DIMENSION EZ(NISG),AE(NAE),E(NE27),FELD(6),KFEL(6),NFEL(6)
REAL*8 NAM,NAM2,NAM3,KFEL,FELD,XLEVEL,AE,E,EZ,EN,XLEV
COMMON NAM,ISTRUK,ISPA,NA,LIZ
EQUIVALENCE (FELD(1),KFEL(1))
CALL DOPW(8HBEST ,NAM2)
CALL DOPW(8HSGIZ ,NAM3)
KFEL(1)=NAM
KFEL(2)=NAM2
170 FCRMAT(' FELD(5)=' ,G16.8)
KFEL(3)=NAM3
NFEL(1)=4
FFLD(4)=XLEVEL
ISN=0
K=1
KK=0
IF(J.NE.0) GO TO 9
NETMAX=1
KMAX=0
C*****FINDING EXCITATION CROSS-SECTION TABLE WITH EXCITATION ENERGY
C*****GREATER THAN FELD(4).
9 NANRE=0
NENRE=0
CALL NDFLOC(N,NFEL,FELD,NDAT,NCO)
IF(N.EQ.1) GO TO 2
C*****NANRE=0 (NENRE=0): FIRST (LAST) ENERGY POINT BELONGING TO GROUP
C*****I HAS NOT YET BEEN FOUND. NANRE=1 (NENRE=1) : FIRST (LAST)
C*****ENERGY POINT BELONGING TO I HAS BEEN FOUND.
C*****NENRE=2: ALL EXCITATION CROSS-SECTIONS INFLUENCING GROUP I
C*****HAVE BEEN READ.
CALL NDFLOC(N,NFEL,FELD,NDAT,NCO)
IF(N.EQ.0) GO TO 30
GO TO 2
30 CCNTINUE
GO TO 3
C 3 WRITE(NA,110) NAM,NAM3,FELD(4)
C 110 FCRMAT(' FOR THE ISOTOPE',A8,' THE DATA TYPE',A8,' IS NOT AVAILABLE
C IFOR EXCITATION ENERGIES ABOVE',G16.8,'CN KEDAK')
3 IF (J.EQ.0) GO TO 1000
IL=1
GO TO 57
C*****IL=1 MEANS : LAST EXCITATION LEVEL OF THE KEDAK LIBRARY
C*****HAS BEEN REACHED.
2 J=J+1
IF(J.LE.NAE) GO TO 22
J=1
NAEF=NAEF+1
22 AE(J)=FELD(4)
XLEV=AE(J)

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IF(AE(J).GT.E(I+1)) GO TO 55
GO TO 6
55 NENRE=2
J=J-1
IF(J.EQ.0) IB=1
GO TO 57
C*****FINDING AT THE BEGINNING OF THE TABLE OF EXCITATION CROSS-SECTIONS
C*****LAST ENERGY POINT EN WITH CROSS-SECTION VALUE EQUAL TO ZERO.
6 IF(FELD(6).NE.0.) GO TO 11
EN=FELD(5)
CALL NDFNXT(N,NFEL,FELD,NDAT,NCO)
IF(N.EC.1) GO TO 6
WRITE(NA,112) J,AE(J)
112 FCRMAT(' *** WARNING 5.20 : FOR LEVEL J= ',I6,'AE(J) = ',E12.6,'
111 EXCITATION CROSS SECTIONS ARE EQUAL TO ZERO.')
J=J-1
NENRE=2
GO TO 57
C*****CHECK WHETHER EN BELONGS TO THE ENERGY SCALE NEEDED FOR ENERGY
C*****GROUP I
11 CONTINUE
IF(EN.GE.E(I).AND.EN.LT.E(I+1)) GO TO 19
IF(FELD(5).GE.E(I).AND.FELD(5).LT.E(I+1)) GO TO 18
IF(EN.LT.E(I)) GO TO 19
IF(EN.GT.E(I+1)) GO TO 40
C*****FOLLOWING CONDITION, THAT LEADS TO STATEMENT NUMBER 18. (EN OR
C*****FELD(5) BETWEEN LOWER AND UPPER LIMIT OF GROUP I)
18 KK=KMAX+K
IF(KK.LE.NISG) GO TO 24
NISGF=NISGF+1
KK=1
24 CCNTINUE
EZ(KK)=EN
K=K+1
KK=KMAX+K
IF(KK.LE.NISG) GO TO 50
NISGF=NISGF+1
KK=1
50 CCNTINUE
EZ(KK)=FELD(5)
NANRE=1
GO TO 42
C*****FOLLOWING CONDITION , THAT LEADS TO STATEMENT NUMBER 19 ( EN IS
C*****LESS THAN THE LOWER LIMIT OF GROUP I)
19 IS=1
EN=FELD(5)
GO TO 42
C*****FOLLOWING CONDITION, THAT LEADS TO STATEMENT NUMBER 40 ( EN IS
C*****GREATER THAN UPPER LIMIT OF GROUP I)
40 NENRE=2
IF (J.EQ.1) IB=1
C*****IB=1 : LOWEST ENERGY POINT OF FIRST INELASTIC CROSS-SECTION
C*****IS GREATER THAN THE UPPER ENERGY LIMIT OF GROUP I
GO TO 57
C*****FINDING FURTHER ENERGY POINTS OF CROSS-SECTION TABLE

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B 95


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42 CONTINUE
CALL NDFNXT(N,NFEL,FELC,NOAT,NCO)
IF(N.EQ.0) GO TO 51
IF(FELD(5).GE.E(I).AND.FELD(5).LE.E(I+1)) GO TO 43
IF(FELD(5).LT.E(I)) GO TO 47
IF(FELD(5).GT.E(I+1)) GO TO 48
C****FOLLOWING CONDITION LEADING TO STATEMENT NUMBER 43.(FELD(5)
C****WITHIN ENERGY LIMITS OF GROUP I)
43 K=K+1
KK=KMAX+K
IF(KK.LE.NISG) GO TO 44
NISGF=NISGF+1
KK=1
44 IF(NANRE.EQ.0) GC TC 45
EZ(KK)=FELD(5)
GC TO 42
45 NANRE=1
K=MAXO((K-1),1)
KK=KMAX+K
EZ(KK)=ENN
K=K+1
KK=KMAX+K
IF(KK.LE.NISG) GO TO 46
NISGF=NISGF+1
KK=1
46 EZ(KK)=FELD(5)
GC TO 42
C****FOLLOWING CONDITION,LEADING TO STATEMENT NUMBER 47(FELD(5)
C****IS LESS THAN THE LOWER ENERGY OF GROUP I)
47 ISN=1
EAN=FELD(5)
K=MAXO((K-1),0)
GC TO 42
C****FOLLOWING CONDITION,THAT LEADS TO STATEMENT NUMBER 48(FELD(5)
C****IS LARGER THAN THE UPPER ENERGY OF GROUP I)
48 K=K+1
KK=KMAX+K
IF(K.EQ.1.AND.ISN.EQ.1.AND.NANRE.EQ.0) GO TO 70
GC TO 71
70 NANRE=1
EZ(KK)=ENN
K=K+1
KK=KMAX+K
71 IF(KK.LE.NISG) GO TO 49
NISGF=NISGF+1
KK=1
49 EZ(KK)=FELD(5)
C****LAST ENERGY OF CROSS-SECTION TABLE ,CORRESPONDING TO EXCITATION
C****ENERGY FELC(4),THAT INFLUENCES ENERGY GROUP I, HAS BEEN READ.
51 IF(XLEV.LT.FELC(4))
I1H=1
IF(NISGF.NE.0) GO TO 52
C IF(NAEF.NE.0) GC TO 53
GC TO 54
52 NISGF=NISGF+NISG

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NISGP=NISGF-NISG
GC TO 57
C 53 NAEP=(NAEF-1)*NAE+J+4
C GC TO 57
1000 WRITE(NA,111) J,FELC(4)
111 FORMAT(' J=',I6,' FELD=',G16.8)
RETURN 1
54 XLEVFL=FELD(4)
IF (NENRE.EQ.2) GO TO 57
KMAX1=KMAX
KMAX=KK
62 IF(EZ(KMAX-1).EQ.E(I+1)) GO TO 56
GC TO 59
56 KMAX=KMAX-1
59 IF(EZ(KMAX1+2).EQ.E(I)) GO TO 60
GC TO 58
60 KMAX11=KMAX1+1
KMAX=KMAX-1
CC 61 IO=KMAX11,KMAX
61 EZ(IO)=EZ(IO+1)
58 CCNT INUE
NETMAX=MAXO(NETMAX,K)
57 RETURN
END
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172C
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SUBROUTINE DAORG(I,KEN,EZ,E,AE,EF,FI,J,KMAX,NISG,NISGF,NISGP
1,NE27,NAE,NAEF,NAEP,ISG,ISGF,ISGP,IA,NAB,*
2)
C****SUBROUTINE CONSTRUCTS ENERGY FIELD EZ,CONSISTING OF ALL ENERGIES
C****CONTAINED IN THE CROSS-SECTIONS TABLES OF THE EXCITATION
C****CROSS-SECTIONS,BELONGING TO DIFFERENT EXCITATION ENERGIES.
DIMENSION EZ(NISG),AE(NAE),E(NE27),EF(KEN),FI(KEN)
REAL*8 EZ,AE,E,NAM,XLEVEL,E1,E2
COMMON NAM,ISTRUK,ISPA,NA,LIZ
C****IH=1:LAST ENERGY POINT ,FOR WHICH SGIZ ARE STORED FOR
C****LEVEL AE(J) HAS BEEN READ.IH=0:LAST ENERGY POINT,FOR
C****WHICH VALUES OF SGIZ ARE STORED FOR LEVEL AE(J) HAS
C****NOT YET BEEN READ.IH=0,IF LAST ENERGY POINT FOR SGIZ
C****OF HIGHEST EXCITATION LEVEL HAS BEEN READ.
NABL=0
IR=0
IL=0
IF=0
J=C
EPS=0.0
EPSI=0.001
C EPSI=1.
KMAX=0
KMAXC=0
XLEVEL=0.00
1 CALL NDFNXT(I,EZ,E,AE,XLEVEL,J,KMAX,NENRE,NISG,NISGF,NISGP,NE27,
INAE,NAEF,NAEP,NETMAX,IL,IR,IH,& 1000)
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C      IF(NAEF.NE.0) GO TO 10
      KMAXC=MAX0(KMAXC,KMAX)
      IF(IL.EQ.1.AND.KMAXC.EQ.0) GO TO 26
      IF(IL.EQ.1) GC TC 24
      IF(IB.EQ.1) GO TO 23
C****IA=0 MEANS : CROSS-SECTIONS OF TYPE SGIZ ARE AVAILABLE FOR THE
C****LCWFST ENERGY REQUIRED BY INPUT. IA.NE.0 : CROSS-SECTIONS ARE
C****AVAILABLE STARTING FROM GROUP IA.
      IF(NISGF.NE.0.AND.J.NE.1) GC TC 10
      IF(J.EQ.1.AND.NENRE.NE.2) GO TO 3
      IF(NENRE.EQ.2) GO TO 11
      CALL ORDREN(KMAX,EMIN,EMAX,EZ,NISG,EPS)
      3  IF (IH.EQ.0)
      1XLEVEL=XLEVEL*(1.DO*1.D-5)
      IH=0
      GC TO 1
      11 CONTINUE
C****ACCING THE ENERGY POINTS OF THE WEIGHTING FUNCTION.
      25 IF(KEN.EQ.0) GO TO 12
      E1=DMAX1(EZ(I),E(I))
      E2=DMIN1(EZ(KMAX),E(I+1))
      CALL CUTS(SNGL(E1),SNGL(E2),FF,KEN,KA,KE,KMAX)
      DC 13 K=KA,KE
      KK=KMAX+K-KA+1
      IF(KK.LE.NISG) GO TO 13
      NISGF=KK
      KK=1
      13 EZ(KK)=EF(K)
      IF(NISGF.NE.0) GC TC 15
      GO TO 16
      15 NISGP=NISGF-NISG
      RETURN
      16 KMAX=KMAX+KMAX1
      20 CALL ORDREN(KMAX,EMIN,EMAX,EZ,NISG,EPS)
      IF (NABL.EQ.1) GO TO 27
      GC TC 28
      27 DO 29 IS=1,KMAX
      ISS=IS
      IF (EZ(IS).LE.E2) GO TO 29
      IF (EZ(IS).GT.E2) GO TO 30
      29 CCNTINUE
      GO TO 28
      30 KMAX=MAX0(1,ISS-1)
C      WRITE(NA,1010) (IS,EZ(IS),IS=1,KMAX)
C1010 FORMAT(2(' IS=',I6,'EZ=',E12.6))
      28 IF(KMAX.LE.ISG) GO TO 17
      ISGF=MAX0(KMAX,NETMAX)
      ISGP=ISGF-ISG
      17 IF(NISG.LT.(KMAX+NETMAX)) GC TC 18
      GO TO 21
      18 NISGF=KMAX+NETMAX
      NISGP=NISGF-NISG
      21 IF(NAEF.NE.0) NAEP=NAEF
      GC TC 10
1CCC IA=C

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820

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      NAB=0
      RETURN 1
C*****WEIGHTING FUNCTION GIVEN AS AN ANALYTICAL FUNCTION.
      12 CALL SPECTI(KMAX,EZ,NISG,NISGF,NISGP,EPSI,EPS)
C      WRITE(NA,105) NISG,NISGF,NISGP
      105 FCRMAT(' NISG=',I6,'NISGF=',I6,'NISGP=',I6)
      IF(NISGF.NE.0) GO TO 19
      GC TC 20
      19 NISG=NISG+NISGP
      GC TC 10
C      24 WRITE(NA,107) IL,J,XLEVEL
C      107 FORMAT(' IL=',I6,'J=',I6,'LAST EXCITATION LEVEL=',G14.6)
      24 NABL=1
      IF (EZ(KMAX).LT.E(I+1).AND.EZ(KMAX).GE.E(I)) NAB=I
      IF(EZ(KMAX).EQ.E(I)) NAB=I-1
C      WRITE(NA,108) NAB
C      108 FCRMAT(' LAST ENERGY PCINT OF SGIZ LIFS WITHIN GROUP NAB=',I6)
      GO TO 25
C      23 WRITE(NA,106) IB,I,E(I+1)
C      106 FORMAT(' IB=',I6,'ALL ENERGY PCINTS OF THE FIRST INELASTIC LEVEL
C      1LIE ABOVE THE UPPER GROUP LIMIT FO GROUP I.'/' I=',I6,
C      2'E(I+1)=',G14.6)
      23 CCNTINUE
      26 IA=I+1
C      WRITE(NA,109) I,IA
C      109 FCRMAT(' NO CNTRIBUTION TO DISCRETE INELASTIC LEVELS
C      IIA GROUP I=',I6,'IA IS SET EQUAL TO IA=',I6)
      10 RETURN
      ENC

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SUBROUTINE SPECTI(KMAX,EZ,NISG,NISGF,NISGP,EPSI,EPS)
DIMENSION EZ(NISG)
COMMON NAM,ISTRUK,ISPA,NA,LIZ
REAL*8 NAM,EZ
NA=6
IO=1
KMAX1=KMAX-1
4 DO 1 I=IO,KMAX1
EI=SNGL((EZ(I)+EZ(I+1)))*0.5
PHIE=PHI(EI)
E1=SNGL(EZ(I))
E2=SNGL(EZ(I+1))
PHI1=PHI(E1)
PHI2=PHI(E2)
PHI=PIPOLA(E1,EI,E2,PHI1,PHI2)
ERR=ABS((PHI1-PHI)/PHIE)
IF(ERR.LT.EPSI) GC TC 1
IS=I
GC TC 2
1 ISS=I
GC TO 5
2 KMAX=KMAX+1

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IF (KMAX.LE.NISG) GO TO 3
NISGF=NISGF+10
NISGP=NISGP+10
KMAX=NISG
IC=IS
KMAX1=KMAX-1
GC TO 6
3 EZ(KMAX)=DBLE(EI)
CALL ORDNEK(KMAX,EMIN,EMAX,EZ,NISG,EPS)
IC=IS
KMAX1=KMAX-1
GC TO 4
5 CCNTINUE
6 RETURN
END

SUBROUTINE ORDNEK(KMAX,EMIN,EMAX,FELC,ATT,EPS)
DIMENSION FELC(NTT)
REAL*8 FELD

C
C CROEN ORDNET FELD NACH WACHSENDEN WERTEN
C
IF(KMAX.LT.2) GOTO 100
DO 99 K=2,KMAX
M=K-1
IF(FELD(K).GE.FELD(M)) GOTO 99
R=FELD(K)
10 M=M-1
IF(M.EQ.0) GOTO 20
IF(R.LT.FELD(M)) GOTO 1C
20 IA=M+1
IE=K-1
J=IE
DO 30 I=IA,IE
FELD(J+1)=FELD(J)
30 J=J-1
FELD(IA)=R
99 CCNTINUE
100 IF(KMAX.EQ.0) GOTO 200
GOTO 300
200 EMIN=0
EMAX=0
GC TO 800
300 KMAXX=KMAX
DO 500 K=2,KMAX
502 IF(K .GT.KMAXX) GO TO 501
M=K-1
IF(SNGL(DABS((FELD(K)-FELD(M))/FELD(K))).LE.EPS) GO TO 60C
GC TO 500
60C KMAXX=KMAXX-1
KMAXS= MAX0(K,KMAXX)
DC 700 KK=K,KMAXS

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700 FELC(KK)=FELD(KK+1)
GO TO 502
500 CCNTINUE
501 KMAX=KMAXX
EMIN=FELD(1)
EMAX=FELD(KMAX)
800 CONTINUE
RETURN
END

C
SUBROUTINE CUTS CUTS ARRAY FELD AT ENERGIES
UGG - LOWER VALUE,CGG - UPPER VALUE
SUBROUTINE CUTS( UGG,OGG,FELD,NFE,KA,KE,KMAX1)
DIMENSION FELC(NFE)
WRITE(6,101) UGG,OGG
C
C 101 FORMAT(' UGG=',E12.6,' CGG=',E12.6)
KA=1
KE=NFE
LC=AMAX1(UGG,FELD(1))
OG=AMIN1(OGG,FELD(NFE))
CC 1 K=1,NFE
IF(FELD(K).LT.UG) GO TO 1
KA=K
IF(FELD(K).GT.UG) KA=MAX0((K-1),1)
GC TO 2
1 CCNTINUE
KMAX1=0
GC TO 7
2 KMAX1=NFE-KA+1
K=NFE
DC 4 I=1,NFE
IF(FELD(K).LT.OG) GO TO 5
K=K-1
4 CONTINUE
GC TO 7
5 KE=K+1
KC=NFE-KE
KMAX1=KMAX1-KC
RETURN
7 WRITE(6,100) UG,OG,FELD(1),FELD(NFE)
100 FORMAT(' CUTS : UG=',E12.6,' CG=',E12.6,' FELD(1)=' ,E12.6,
*' FELD(NFE)=' ,E12.6)
RETURN
END

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SCINN=0.0
CALL NDFLOC(N,NFEL,FELD,NDAT,NCO)
IF(N.EQ.1) GO TO 2
CALL NDFLOC(N,NFEL,FELD,NDAT,NCO)
IF(N.EQ.0) GO TO 30
GC TO 2
30 CONTINUE
GC TO 3
C 3 WRITE(NA,110) NAM,NAM3,FELD(4)
C 110 FORMAT(' FOR THE ISOTOPE',A8,'THE DATA TYPE',A8,'IS NOT AVAIL=
C 11ABLE FOR EXCITATION ENERGIES ABOVE',G16.8,'ON KEDAK')
3 IF(J.EQ.0) GO TO 1000
IL=1
GC TO 57
C*****IL=1 MEANS : LAST EXCITATION LEVEL OF THE KEDAK LIBRARY
C*****HAS BEEN REACHED.
2 J=J+1
AE(J)=FELD(4)
XLFV=AE(J)
IF(AE(J).GT.EZ(KMAX)) GO TO 55
GC TO 6
55 NENRE=2
IF(J.EQ.1) IB=1
C*****IB=1 MEANS : THRESHOLD FOR INELASTIC SCATTERING LIES ABOVE
C*****THE UPPER ENERGY LIMIT OF ENERGY FIELD EZ(1) EZ(KMAX).
GC TO 57
C*****FINDING AT THE BEGINNING OF THE TABLE OF EXCITATION CROSS
C*****SECTIONS HIGHEST ENERGY POINT EN WITH CROSS-SECTION VALUE
C*****EQUAL TO ZERO.
6 CONTINUE
IF(FELD(6).NE.0.) GO TO 11
EN=FELD(5)
SCIN=FELD(6)
CALL NDFNXT(N,NFEL,FELD,NDAT,NCO)
IF(N.EQ.1) GO TO 6
GC TO 54
C*****CHECK, WHETHER EN BELONGS TO ENERGY SCALE NEEDED FOR THE
C*****ENERGY REGION EZ(1).....EZ(KMAX)
11 CONTINUE
IF(EN.GE.EZ(1).AND.EN.LT.EZ(KMAX)) GO TO 16
IF(FELD(5).GE.EZ(1).AND.FELD(5).LT.EZ(KMAX)) GO TO 18
IF(EN.LT.EZ(1)) GO TO 15
IF(EN.GT.EZ(KMAX)) GO TO 40
C*****FOLLOWING CONDITION , THAT LEADS TO STATEMENT NUMBER 18.
C*****[EN OR FELD(5) BETWEEN LOWER AND UPPER LIMIT OF FIELD EZ].
18 CONTINUE
KK=KMAX1+K
EZ(KK)=EN
SGIT(K)=SGIN
K=K+1
KK=KMAX1+K
EZ(KK)=FELD(5)
SGIT(K)=FELD(6)
NANRE=1
GO TO 42

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750
760

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C*****FOLLOWING CONDITION, THAT LEADS TO STATEMENT NUMBER 19 (EN IS
C*****LESS THAN THE LOWER LIMIT OF ENERGY FIELD EZ).
19 EN=FELD(5)
SGINN=FELD(6)
GO TO 42
C*****FOLLOWING CONDITION , THAT LEADS TO STATEMENT NUMBER 40
C*****[EN IS GREATER THAN EZ(KMAX)]
40 NENRE=2
IF(J.EQ.1) IB=1
GC TO 57
C*****FINDING FURTHER ENERGY POINTS OF CROSS-SECTION TABLE
42 CONTINUE
CALL NDFNXT(N,NFEL,FELD,NDAT,NCO)
IF(N.EQ.0) GO TO 54
IF(FELD(5).GE.EZ(1).AND.FELD(5).LE.EZ(KMAX)) GO TO 43
IF (FELD(5).LT.EZ(1)) GC TO 47
IF (FELD(5).GT.EZ(KMAX)) GO TO 48
C***** FOLLOWING CONDITION LEADING TO STATEMENT NUMBER 43(FELD(5)
C*****WITHIN ENERGY LIMITS OF FIELD EZ)
43 CONTINUE
K=K+1
KK=KMAX1+K
IF(NANRE.EQ.0) GO TO 45
EZ(KK)=FELD(5)
SGIT(K)=FELD(6)
GO TO 42
45 NANRE=1
K=MAX0((K-1),1)
KK=KMAX1+K
EZ(KK)=EN
SGIT(K)=SGINN
K=K+1
KK=KMAX1+K
EZ(KK)=FELD(5)
SGIT(K)=FELD(6)
GO TO 42
C*****FOLLOWING CONDITION, THAT LEADS TO STATEMENT NUMBER 47. (FELD(5)
C*****IS LESS THAN THE LOWER ENERGY LIMIT OF FIELD EZ)
47 EN=FELD(5)
SGIN=FELD(6)
K=MAX0((K-1),0)
GC TO 42
C*****FOLLOWING CONDITION, THAT LEADS TO STATEMENT NUMBER 48. (FELD(5)
C*****IS LARGER THAN THE UPPER ENERGY OF FIELD EZ)
48 CONTINUE
K=K+1
KK=KMAX1+K
EZ(KK)=FELD(5)
SGIT(K)=FELD(6)
C*****LAST ENERGY OF CROSS-SECTION TABLE, BELONGING TO EXCITATION
C*****ENERGY FELD(4), THAT INFLUENCES ENERGY FIELD EZ(1).....EZ(KMAX)
C*****HAS BEEN READ
GO TO 54
1000 WRITE(NA,111) J,FELD(4)
111 FORMAT(' J=',I6,'FELD=',G16.8)

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770
780
790
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810
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830
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870
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1010
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1190
1200
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1220
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1270
1280
1290
1300
1310

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1 B 100 1

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RETURN 1
54 IF(XLEV.LT.FELD(4)) IH=1
XLEVEL=FELD(4)
IF(NENRE.EQ.2) GO TO 57
C*****CUTTING ENDS OF ENERGY FIELD,IF EZ(I) OR EZ(KMAX) ARE CONTAINED
C*****IN EZ(KMAX2).....EZ(KMAX1).
KMAX2=KMAX1
KMAX1=KK
C IF(EZ(KMAX1-1).EQ.EZ(KMAX)) GO TO 56
C GO TO 59
C 56 KMAX1=KMAX1-1
C 55 IF(EZ(KMAX2+2).EQ.EZ(I)) GO TO 60
C GO TO 58
C 60 KMAX21=KMAX2+1
C KMAX1=KMAX1-1
C DO 61 IO=KMAX21,KMAX1
C 61 EZ(IO)=EZ(IO+1)
58 KMAX22=KMAX2+1
57 NET=KMAX1-KMAX2
RETURN
END

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1320
132C
1340
1350
1360
1370
1380
139C
140C
1410
142C
1430
1440
145C
1460
1470
1480
1490
150C
1510
1520

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C XINPOL PERFORMS LINEAR INTERPOLATION OF THE EXCITATION
C CROSS-SECTIONS OF EACH LEVEL IN THE ENERGY FIELD EZ.
C SGIT - VALUES READ FROM KEDAK,SGP - INTERPOLATED VALUES.
C SLBROUTINE XINPOLIEZ,SGIT,SGP,NISG,NETACT,KMAX,KANF,KEND)
REAL*8 NAM,EZ
DIMENSION EZ(NISG),SGIT(NETACT),SGP(KMAX)
COMMON NAM,ISTRUK,ISPA,NA,LIZ
C WRITE(6,100)((J,EZ(KMAX+J),SGIT(J)),J=1,NETACT)
C 100 FORMAT(2(' J=',I6,'EK=',G16.8,'SK=',G16.8))
DC 1 I=1,KMAX
DC 2 J=1,NETACT
JA=J
IF(EZ(KMAX+J).LT.EZ(I)) GO TO 2
IF(EZ(KMAX+J).EQ.EZ(I)) GO TO 7
IF(EZ(KMAX+J).GT.FZ(I).AND.J.EQ.1) GO TO 3
SGP(I)=FIPOLD(EZ(KMAX+J-1),EZ(I),FZ(KMAX+J),
ISGIT(J-1),SGIT(J))
C SGP(I)=SGIT(J-1)+SNGL((EZ(I)-EZ(KMAX+J-1))/(EZ(KMAX+J)-EZ(KMAX+J-1
1)))*(SGIT(J)-SGIT(J-1))
C GO TO 1
2 CONTINUE
3 SGP(I)=0.
C GO TO 1
7 SGP(I)=SGIT(JA)
1 CONTINUE
KANF=1
KEND=KMAX
DO 4 K=1,KMAX
IF(SGP(K).EQ.0.) GO TO 5
IF(K.EQ.1) GO TO 4

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IF(SGP(K-1).EQ.0.)KANF=K-1
GO TO 4
5 IF(K.EQ.KANF) GO TO 6
IF(K.LT.KMAX.AND.KEND.GT.K) KEND=K
GO TO 4
6 KANF=K+1
4 CONTINUE
IF(KANF.GT.KMAX) KANF=KMAX
C WRITE(NA,121) KANF,KEND
C 121 FORMAT(' KANF=',I6,'KEND=',I6)
KMAXX=ISG-KANF+1
DC 9 I=1,KMAX
9 SGP(I)=SGP(KANF+I-1)
C 120 FORMAT(3(' I=',I6,'EZ=',G14.8,'SGP=',G14.8))
C DC 8 I=1,KMAXX
C 8 SGIT(I)=SGP(I)
RETURN
END

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310
32C
330
340
350
360
370
380
390
400
410
42C
43C
440
45C
460
470
480

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SLBROUTINE FLUMMI(A,B,EA,EB,E,EN,SGN,ECO,SCO,V,W,F,AR,FU,ABN,INT,
1 GR,FEKOE,EG,R,RSP,ESP,SPEK,SGNC,FEKC,ELSIG,
2 ELTOT,ET,ST,MAT,CAT,ALA,NLE,ISEL,NMAX,NX,NE27,
3 NSPEK,LSPEK,MAZ,ATK,KT,NTTT,ATTP,ICCS,ICOSP,
4 NECU,NECUP,ISM,ISMP,ISD,ISDP,ISCO,ISCP,ISEC,
5 ISECP,KIM,NS,NK,AR,GE,SG,SGTCT)
C
C
C*****
C
C FLUMMI
C
C*****
C*****ELASTISCHE STREUMATRIX BIS ZUR 5. ORDNUNG*****
C*****UND TOTALE GRUPPENQUERSCHNITTE MIT MOMENTABHAENIGER WICHTUNG
C
REAL*8 STOFF,MAT
DIMENSION A(ISM),B(ISM),EA(ISM),EB(ISM),E(ISM),
1 EN(ISD),SGN(ISD),ECO(ISD),SCO(ISD),V(ISD),W(ISD),F(ISD),
2 AR(ICOS),FU(ICOS),
3 ABN(NE27),INT(NE27),GR(NE27),FEKOE(NE27),
4 EG(NX),R(NX),RSP(6,NX),
5 ESP(NSPEK),SPEK(LSPEK),
6 NST(6),LEG(6),MAZ(2),
7 SGNC(ICOS,ISM),FEKO(ISM,NECU),ELSIG(6,NFCU,NX),
8 ELTOT(2,NX),
9 MAT(KT),DAT(KT),
A ET(NTTT),ST(NTTT),
B GE(ISD),SG(ISD),SGTOT(6,NX)
COMMON STOFF,ISTRUK,ISPA,NOUT,KPR,IM,IL,KL

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1C
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80
90
100
110
120
130
14C
150
160
170
180
19C
200
210
220
230
240
250
26C
27C
280
29C
300
310
32C
330

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C          DATA NST/81,81,161,161,321,321/          340
C          NST(L)= ANZAHL DER AEQUIDISTANTEN STREUKOSINUSSTUETZPUNKTE DER 350
C          SGNC IM L-SYSTEM FUER DAS (L-1)-TE MOMENT 360
C          DATA LEG/2,1,3,4,5,6/                   370
C          LEG = REIHENFOLGE BEI DER MOMENTENBERECHNUNG 380
C                                                    390
C          WRITE (NOUT ,9000)                          400
C          9000 FORMAT(1H0/1H0/' PROGRAMM KEANZIFFER 6') 410
C          WRITE (NOUT ,9001)                          420
C          9001 FORMAT(' PROGRAMM ZUR BERECHNUNG ELASTISCHER STREUMATRIZEN') 430
C          CALL FSPIE                                  440
C                                                    450
C*****SETZEN INTERNER KONSTANTEN*****              460
C          ISM = ANZAHL DER ENERGIESTUETZPUNKTE PRO MAKROGRUPPE IM GROBNETZ 470
C          ISD = MAXIMALE ANZAHL DER ENRGIESTUETZPUNKTE PRO MAKROGRUPPE 480
C          IM FEINNETZ                                490
C          NK = ANZAHL VON GRUNDPUNKTEN IM UEBERSTREUBEREICH 500
C          NR = MAXIMALZAHL VON GRUNDPUNKTEN IM NICHT-UEBERSTREUBEREICH 510
C          NS = MAXIMALE FEINGRUPPENZAHL PRO GROBGRUPPE 520
C          PM = 1                                      530
C          PM = ANTEIL VON MUEL BEI DER KORREKTUR DES 1. MOMENTES 540
C          NECU = MAXIMALE STREUBREITE                550
C          NMAX = MAXIMALER LEGENDRE-APPROXIMATIONSFAD 560
C          NCUT = UNIT-NUMMER DER AUSGABE-CATEGI 570
C          ICOS = ANZAHL DER AEQUIDISTANTEN STREUKOSINUSSTUETZPUNKTE DER VON 580
C          KNDF GELESENEN DIFFERENTIELLEN STREUQUERSCHNITTE (SGNC) 590
C          NF = 10                                     600
C          NF = SPEICHEREINHEIT FUER ENERGIECTIFF. LEGENDRE-KOEFF. 610
C                                                    620
C          630
C*****INITIALISIERUNG INTERNER GROSSEN*****        640
C          NCT = 1                                     650
C          KIM = 0                                     660
C          NEN = 0                                     670
C          ITA = 0                                     680
C          ISC=1                                       690
C          NSTIS = NST(6)                               700
C          NLEB = NECU                                  710
C          CD = 2./(ICOS-1)                             720
C          NGS=0                                       730
C          NECUP=0                                      740
C          ISCP=0                                       750
C          ISMP=0                                       760
C          ICOSP=0                                      770
C          ISCO=0                                       780
C          ISECP=0                                      790
C          NITP=0                                       800
C          KSPE=1                                       810
C                                                    820
C*****LESEN DES ATOMGEWICHTES*****                830
C          CALL LOOKO(XMAT,MASSE,COM,&ICO1)             840
C          ALFA = ((XMAT-1.)/(XMAT+1.))**2            850
C                                                    860
C          870
C*****UMSORTIEREN DER GRUPPENGRENZEN*****          880
C          KSPE=NSPEK
C          IF(NSPEK.GT.1) GO TO 305                    890
C          KSPE=0                                       900
C          KSPEK=0                                       910
C          305 CC 302 I=1,NX                               920
C          II=NX-I+1                                       930
C          302 ABN(I)=EG(II)                               940
C
C          IF(ABN(NX)-1.E-3)301,303,304                950
C          301 WRITE(NOUT,350)                          960
C          350 FORMAT(/' ***ERROR 6.8 : THE SMALLEST GROUP BOUNDARY MUST BE GREA 970
C          IFTER THAN OR EQUAL TO 1.E-3')              980
C          GC TO 8000                                    990
C          304 NEGR=NEZ7                                  1000
C          ABN(NEGR)=AMAX1(1.E-3, .99*ABN(NX))         1010
C          GO TO 4                                       1020
C          303 NEGR=NX                                  1030
C                                                    1040
C*****BESTIMMUNG DER GRUPPENLETHARGIEN*****        1050
C          4 NGR = NEGR-1                                  1060
C          ALFA = AMAX1(ALFA,ABN(NEGR)/ABN(1))         1070
C          ALLN = ALOG(ALFA)                             1080
C          CA = ABN(1)/ABN(2)                            1090
C          DO 5 I = 1,NGR                                 1100
C          R(I)=ALOG(ABN(I)/ABN(I+1))                   1110
C                                                    1120
C*****LESEN DER SGNC-ENERGIEN UND BESTIMMUNG DER STREUBREITE***** 1130
C          IF(MASSE.EQ.1) GOTO 6                          1140
C          CALL LOOK3(NEN,EB,ISC,NGR,ABN,ISM,ISMP,GR,NEGF,ISEL,ISGNC) 1150
C          IF(ISGNC.EQ.1) GO TO 8000                    1160
C          CALL LOOK2(I,EB,ICOS,ICOSP,AR,ISM,SGNC)      1170
C          ES = EB(1)                                    1180
C          GCTO 7                                         1190
C          6 ES = ABN(1)                                  1200
C          I = 100*ALOG10(ABN(1)/ABN(NEGR))            1210
C          NK = MAXO(I,NK)                               1220
C          7 NUE=2                                       1230
C          DO 10 I = 2,NGR                               1240
C          AM = ALFA*ABN(I)                              1250
C          IF = I+1                                       1260
C          DO 9 II = IP,NEGR                             1270
C          IF(ABN(II).LE.AM) GOTO 10                    1280
C          9 CCNTINUE                                    1290
C          II = NEGR                                     1300
C          10 NUE = MAXO(NUE,II-I+1)                    1310
C          IF(NUE.LE.NUEB) GCTO 8                       1320
C          NECUP=NUE-NUEB                                1330
C          8 NLEB = NUE                                   1340
C          ISCO=NUEB*ISC-ISCO                             1350
C          IF(ISCO.LT.0) ISCCP=0                         1360
C          ISECP=ISD-ISEC                                1370
C          IF(ISECP.LT.0) ISECP=0                       1380
C          IF(ISMP+ICOSP+NECUP+ISCCP+ISECP.GT.0) RETURN 1390
C                                                    1400
C          C*****BESTIMMUNG DER MAKROGRUPPENEINTEILUNG***** 1410
C          12 KIM = MINO(NGR-IP,NUEB-1)                1420
C          IM = IM+KIM                                    1430

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CALL MAKRO(ALFA,ALLN,ISC,IL,IM,NGR,ABN,R,ISD,ISM,ISCP,NS,NK,NR,
- NEN,NECU,NUEB,V,W,F,ELTOT,INTT,INT,NEGR,KSPE,NSPEK,
- ESP,NTK,KT,MAT,NTTT,NTTP,NF,ISEL,ISGT)
IF(ISGT.EQ.1) GO TO 8000
IF(ISDP+NTTP.GT.0) RETURN
C
13 NEK = NEN
IF(NEN.EQ.0) GOTO 16
IF(EB(NEN).GE.ABN(IL)) GOTO 16
WRITE(ROUT,913) STOFF,EB(NEN)
STOP
16 CONTINUE
C
C***** P A K R O G R U P P E N R E C H N U N G *****
C
IR = 1
20 NANF = INT(IR)+1
IF(IR.EQ.1) NANF = NANF-1
NEND = INT(IR+1)
NEN = NEK
ISCT = 1
C
C***** BESTIMMUNG DES EINSTREUINTERVALLES*****
EANF = ABN(NENC+1)
22 EEND=ABN(NANF)
IF(MASSE.GT.1) GOTO 28
NEN = 1
EA(1) = ABN(IL)
28 IF(MASSE.EQ.1) GOTO 62
DC 60 NE = 1,NEN
60 EA(NE) = EB(NE)
62 CONTINUE
C
C***** MAKROSKOPISCHER TOTALER QUERSCHNITT FUER FEINSTRUKTURWICHTUNG*****
NIT=1
IF(NTK.EQ.1) CALL MIXSGT(KT,MAT,DAT,NTTT,NTTP,NTT,ET,ST,EANF,EEND,
IISGT)
IF(ISGT.EQ.1) GO TO 8000
IF(NTTP.GT.0) RETURN
C
C***** EINORDNEN DES AUSSTREUINTERVALLES UND LESEN DER SGNC*****
IF(EA(1).GE.EEND) GOTC 88
CC 64 NE = 1,NEN
NI = NE
IF(EA(NE).GE.EANF) GOTC 66
64 CONTINUE
66 DC 68 NE = 1,NEN
NC = NEN-NE+1
IF(EA(NC).LE.EEND) GOTC 70
68 CONTINUE
C
70 IF(NI.EQ.1) GOTO 78
NC=MINO(NO+2,NEN)
NI=MAXO(NI-2,1)

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NEN = NO-NI+1
CC 74 NE = NI,NO
74 A(NE) = EA(NE)
CC 76 NE = 1,NEN
76 EA(NE) = A(NE+NI-1)
CALL LOOK2(NEN,EA,ICOS,ICOSP,AR,ISM,SGNC)
IF(ICOSP.NE.0) RETURN
IF(EA(NEN).GE.EEND) GOTO 100
NEN = NEN+1
EA(NEN) = EEND
DO 77 IP = 1,ICOS
77 SGNC(IP,NEN) = SGNC(IP,NEN-1)
GOTO 100
C
78 NEN=MINO(NO+2,NEN)
CALL LOOK2(NEN,EA,ICOS,ICOSP,AR,ISM,SGNC)
IF(ICOSP.NE.0) RETURN
IF(FS.LE.EANF) GO TO 100
CC 84 NE = 1,NEN
NA = NEN-NE+1
NU = NEN-NE+2
EA(NU) = EA(NA)
DC 84 IP = 1,ICOS
84 SGNC(IP,NU) = SGNC(IP,NA)
EA(1) = EANF
NEN = NEN+1
CC 86 IP = 1,ICOS
86 SGNC(IP,1) = C.7957747E-01
GOTO 100
C
C*****KOSINUS UND ENERGIEN BEI ISCTROPIE IM CM-SYSTEM*****
88 CC 90 IP = 1,ICOS
90 AR(IP) = (IP-1)*CD-1.
NEN = 0
CALL PUNK(NGR,NEGR,ABN,NANF,NEND,NEN,ALFA,NK,NR,
- ISM,ISMP,ISN,E,R,ALLN)
IF(ISMP.GT.0) RETURN
ISCT = 0
GOTO 115
C
C*****TRANSFORMATION DER SGNC*****
100 A1 = ABS(AR(1)+1.)
A2 = ABS(AR(ICOS)-1.)
IF(A1.LT.1.E-5.AND.A2.LT.1.E-5) GOTC 102
101 WRITE(ROUT,920) (AR(IP),IP=1,ICOS)
GOTO 8000
102 CC 103 IP = 2,ICOS
IF(AR(IP).LE.AR(IP-1)) GO TC 101
103 CONTINUE
CALL TRAFD(ICCS,NEN,ISM,SGNC,XMAT,ALFA,AR)
C
C*****ENERGIEINTERPLATION DER SGNC*****
CALL PUNK(NGR,NEGR,ABN,NANF,NEND,NEN,ALFA,NK,NF,
- ISM,ISMP,ISN,E,R,ALLN)
IF(ISMP.GT.0) RETURN

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CALL PUSUM(ISM,NEN,EA,ISN,E,V)
NU=0
NC=0
104 IF(F(NU+1).GE.EANF) GO TO 106
NL=NU+1
GO TO 104
106 IF(E(ISN-NO).LE.EENC) GO TO 108
NC=NO+1
GO TO 106
108 ISK=ISN-NU-NO
DO 111 IP = 1,ICOS
CC 110 NE = 1,NEN
110 B(NE) = SGNC(IP,NE)
CALL IPDLA(NEN,EA,B,ISN,E,A,F)
DO 111 NE=1,ISK
NC=NE+NU
IF(E(NO).LE.EE) A(NO)=A(1)
111 SGNC(IP,NE)=A(NO)
DO 113 NE=1,ISK
113 E(NE)=E(NE+NU)
ISK = ISK
C
C*****ENERGIEDIFFERENTIELLE LEGENDRE-KOEFFIZIENTEN *****
115 CALL LECAL (MASSE,XMAT,ALFA,ISOT,LEG,NLE,NANF,NEND,NUEB,IL,IM,
1 NEGR,ABN,ICOS,AR,ISN,E,SGNC,NST,NSTIS,ISM,ISD,NECU,
2 ITA,NF,GR,FEKOE,FU,A,ECC,SCO,V,W,F,FEK)
C
C*****LISEN DER SGT, SGN UND MUEL*****
IF(IABS(ISEL).EQ.1.AND.ISOT.EQ.0) GOTO 120
CALL LCOK1(ISC,M,ECC,SCC,EANF,EEND,1,ISGT)
IF(ISGT.EQ.1) GO TO 8000
AM = ECO(M)
IF(M.LT.ISD) GOTO 117
116 ISDP = ISD*(ALOG(EEND/AM)/ALOG(AM/EANF))
RETURN
117 IF(MASSE.GT.1.OR.EANF.GT.10.) GOTO 119
DO 118 J = 1,M
IF(ECO(J).GT.10.) GOTO 119
118 SCO(J) = .6667
119 CALL LCOK1(ISC,K,EN,SGN,EANF,EENC,0,ISGT)
IF(ISGT.EQ.1) GO TO 8000
IF(NGT.EQ.0) GOTO 130
CALL LCOK1(ISD,NGG,GE,SG,EANF,EENC,2,ISGT)
IF(ISGT.EQ.1) GO TO 8000
AM = GE(NGG)
IF(NGG.GE.ISD) GOTO 116
GOTO 130
C
120 IF(NGT.EQ.0) GOTO 122
NGG = 2
GE(1) = EANF
GE(2) = EEND
SG(1) = 1.
SG(2) = 1.
122 K = 2

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EN(1) = EANF
EN(2) = EEND
SGN(1) = 1.
SGN(2) = 1.
M=2
ECC(1)=EANF
ECC(2)=EEND
SCO(1)=COM
SCC(2)=CCM
IF(NGS.EQ.0) NGS=NANF
C
C*****MULTIGRUPPEN-ENERGIEINTEGRATION*****
130 CALL GRUJIN (MASSE,XMAT,ALFA,COM,ISOT,PM,LEG,NLE,NANF,NEND,NUEB,
1 IL,IM,NGR,NEGR,ABN,ISN,E,K,EN,SGN,M,ECC,SCO,NTT,ET,
2 ST,MAZ,KSPE,KSPEK,FSP,SPEK,NSFEK,LSPEK,ISM,ISC,
3 NECU,ISCO,ISEC,NF,F,A,GR,SGNC,FEKO,V,W,I,STT,RSP,
4 ELSIG,NGT,NGG,GE,SG,SGTCT)
C
C*****ALSGABE VON INFORMATIKEN*****
1 IF(ISEL.LT.0) CALL INFORM(ALFA,NEGR,ABN,R,IL,IM,INTT,INT,
1 NST,NSTIS,TR,I,STT,K,NTK,NTT,NCUT)
C
IF(IR+1.GE.INTT) GOTO 290
IR = IR+1
GOTO 20
C
C*****MULTIGRUPPENKONSTANTEN*****
290 CALL MUKON(ELSIG,ELTOT,NLE,NECU,NUEB,IL,IM,NGR,MASSE)
C
C*****AUSDRUCKEN DER ERGEBNISSE*****
IM = IM-KIM
300 CALL PRINT(ELSIG,ELTOT,ALA,NLE,NFCU,NUEB,ISEL,NGF,KSPE,MAZ,NTK,
- KIM,NGT,SGTOT,RSP,MASSE,NGS)
GO TO 8000
C
1001 WRITE (NOUT,1002) STOFF
8000 KL = KL+1
RETURN
C
909 FORMAT(LH0)
913 FORMAT(//' ***ERROR 6.1 : FOR ',A8,' SCATTERING MATRICES CANNOT B
1E CALCULATED*/16X'FOR ENERGIES ABOVE ',IPEIC.3,' EV FOR LACK OF SGA
2C ON KEDAK')
920 FORMAT(//' ***ERROR 6.8 : THE FOLLOWING SGNC-COSINE-MESH FOUND C
-N KEDAK CANNOT BE USED'//(10F12.3))
1002 FORMAT(//' ***ERROR 6.7 : FOR ',A8,' SCATTERING MATRICES CANNOT B
1E CALCULATED FOR*/16X,'LACK OF ISOT1 (ATOMIC WEIGHT) ON KEDAK')
C
END

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SUBROUTINE SUM(M,A,S)
C
C*****SUMMATION*****
C
REAL*8 SP,SN
DIMENSION A(M)
C
IF(M.LE.2) GOTO 13
C*****SORTIEREN*****
N = 1
IA = 2
KK = 0
1 K = 0
DO 2 I = IA,M,2
IB = I-1
IF(A(IB).LE.A(I)) GOTO 2
B = A(I)
A(I) = A(IB)
A(IB) = B
K = 1
2 CONTINUE
N = -N
IA = IA-N
IF(K.EQ.1) GOTO 1
IF(KK.EQ.1) GOTO 3
KK = 1
GOTO 1
C
C*****SUMMIEREN*****
3 SF = 0.
SA = 0.
IF(A(1).GE.0.) GOTO 8
IF(A(M).LE.0.) GOTO 10
DO 4 I = 2,M
IF((A(I-1).LE.0.).AND.(A(I).GE.0.)) GOTO 5
4 CONTINUE
5 IA = I
IB = I-1
DO 6 I = IA,M
6 SF = SP+DBLE(A(I))
DO 7 I = 1,IB
7 SN = SN+DBLE(A(IA-I))
GOTO 12
8 DO 9 I = 1,M
9 SF = SP+DBLE(A(I))
GOTO 12
10 MP = M+1
DO 11 I = 1,M
11 SN = SN+DBLE(A(MP-I))
12 S = SNGL(SN+SP)
RETURN
13 S = A(1)
IF(M.EQ.2) S = S+A(2)
RETURN
C
END

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SUBROUTINE IPCLA(M,A,B,N,X,Y,T)
C
C KUBISCH-QUADRATISCH-LINEARE INTERPOLATION
C UNTER VERMEIDUNG ZUSAEZTLICHER EXREMWERTE
C
DIMENSION A(M),B(M),T(M),X(N),Y(N)
C
C TANGENTEN
T(1) = (B(2)-B(1))/(A(2)-A(1))
T(M) = (B(M)-B(M-1))/(A(M)-A(M-1))
MA = M-1
DO 2 J = 2,MA
JF = J+1
JM = J-1
T(J) = 0.
IF(B(JP).GT.B(J).AND.B(J).GT.B(JM))
-T(J) = (B(JP)-B(JM))/(A(JP)-A(JM))
IF(B(JP).LT.B(J).AND.B(J).LT.B(JM))
-T(J) = (B(JP)-B(JM))/(A(JP)-A(JM))
2 CCNTINUE
C
C INTERPOLATION
Y(1) = B(1)
Y(N) = B(M)
NM = N-1
J = 1
DO 16 I = 2,NM
4 IF(X(I)-A(J)) 6,8,10
6 S = X(I)-A(K)
Y(I) = A0+(A1+(A2+A?S)*S)*S
GOTO 16
8 Y(I) = B(J)
GOTO 16
10 K = J
J = J+1
L = A(J)-A(K)
V = B(J)-B(K)
R = V-T(K)*J
W = U*(T(J)-T(K))
A0 = B(K)
A1 = T(K)
A2 = (3*R-W)/(U*L)
A3 = (W-2*R)/(U*U)
IF(T(K).EQ.0..AND.T(J).EQ.0.) GOTO 4
IF(ABS(A3).LT.1.E-30) GOTO 4
XW = -A2/(3*A3)
IF(XW.LE.0..OR.XW.GE.U) GOTO 4
A3 = 0.
IF(T(J).EQ.0.) GOTO 12
IF(T(K).EQ.0.) GOTO 14
A2 = R/(U*U)

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T(J) = 2*V/U-T(K)
IF(ABS(A2).LT.1.E-30) GOTO 4
XW = -A1/(2*A2)
IF(XW.LE.0..OR.XW.GE.U) GOTO 4
A1 = V/U
A2 = 0.
T(J) = A1
GOTO 4
12 A1 = 2*V/U
A2 = -V/(U*U)
GOTO 4
14 A1 = 0.
A2 = V/(U*U)
GOTO 4
16 CCNTINUE
RETURN
C
ENC

SUBROUTINE PUSUM(ISO,KA,A,KE,E,B)
C
C*****STUETZPUNKTMENGEN VEREINIGEN*****
C
DIMENSION A(ISO),E(ISO),B(ISO)
C
CC 2 K = 1,KE
2 B(K) = E(K)
C
J=1
I=1
K=1
3 IF(J.GT.ISD) GOTO 18
IF(K.GT.KA) GOTO 10
IF(I.GT.KE) GOTO 14
IF(A(K)-B(I)) 4,5,6
4 E(J) = A(K)
J = J+1
K = K+1
GOTO 3
5 E(J) = A(K)
J = J+1
I = I+1
K = K+1
GOTO 3
6 E(J) = B(I)
J = J+1
I = I+1
GOTO 3
10 IF(I.GT.KE) GOTO 18
DC 12 K=I,KE
E(J)=B(K)
J = J+1

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IF(J.GT.ISD) GOTO 18
12 CCNTINUE
GOTO 18
14 DC 16 I=K,KA
E(J)=A(I)
J = J+1
IF(J.GT.ISD) GOTO 18
16 CCNTINUE
18 KE=J-1
RETURN
C
END

SUBROUTINE MAKRO(ALFA,ALLN,ISO,IL,IM,NGR,ABN,R,ISD,ISM,ISDP,NS,NK,
- NR,NEN,NECU,NUEB,V,W,F,LST,INT,NEGR,
- KSPE,NSPEK,ESP,NTK,KT,MAT,NTTI,NTTP,NF,ISEL,ISGT)
C
C*****BESTIMMUNG EINER DEN QUERSCHNITTS- UND SPEKTRUMSSTUETZSTELLEN UND
C DER ANZAHL DER GRUNDPUNKTE ANGEPAASSTEN MAKROGRUPPEN-EINTEILUNG
C
REAL*8 STOFF,MAT,STM
REAL URAN/'U 23'/
DIMENSION ABN(NEGR),R(NGR),INT(NEGR),LST(2,NGF),V(ISO),W(ISO),
- F(ISO),ESP(NSPEK),MAT(KT)
COMMON STOFF,ISTRUK,ISPA,NCUT
C
C*****ANZAHL DER SGT-STUETZSTELLEN (MISCHUNG) PRC GRUPPE *****
CC 2 N = IL,IM
2 LST(1,N) = 0
IF(NTK.GT.1) GOTO 46
IF(NTK.EQ.0) GOTO 24
DC 4 K = 1,KT
A = MAT(K)
IF(A.NE.URAN) GOTO 4
STM = MAT(K)
MAT(K) = MAT(1)
MAT(1) = STM
4 CCNTINUE
STM = STOFF
EA = ABN(IM+1)
EF = ABN(IL)
6 STOFF = MAT(1)
CALL LOOK1(ISO,K,V,W,EA,EE,2,ISGT)
IF(ISGT.EQ.1) RETURN
V(1) = EA
IF(KT.EQ.1) GOTO 10
DO 8 MM = 2,KT
STOFF = MAT(MM)
CALL LOOK1(ISO,I,F,W,EA,V(K),2,ISGT)
IF(ISGT.EQ.1) RETURN
F(1) = EA
CALL PUSUM(ISO,I,F,K,V,W)

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- B 106 -

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8 CCNTINUE
10 NN = IM-IL+1
   K1 = 1
   DC 16 N = 1,NN
   I = IM-N+1
   A = ABN(I)
   DC 12 MM = K1,K
   IF(V(MM).GE.A) GOTO 14

12 CONTINUE
   PP = K+1
14 LST(1,I) = LST(1,I)+MM-K1
   K1 = MM
   IF(K1.GT.K) GOTO 18
16 CONTINUE
18 IF(K.LT.ISD) GOTO 20
   EA = V(K)
   GOTO 6
20 STOFF = STM
   IF(ISEL.LT.0) WRITE(NDOUT,110)
   DC 22 N = IL,IM
   LST(1,N) = LST(1,N)+3
   IF(ISEL.LT.0) WRITE(NDOUT,102) N,LST(1,N)
22 NTP = MAXO(NTP,LST(1,N)-NTTI)
24 CCNTINUE

C
C*****ANZAHL SGN-,MUEL-,SGT- UND MAKROWICHTUNGSSPEKTRUM-STUETZSTELLEN
C
   PRO GRUPPE
   IMM = IM
   IF(IABS(ISEL).EQ.1) IMM = MINO(IM,ISC-1)
   DC 26 N = IL,IM
26 LST(2,N) = 2
   IF(IMM.LT.IL) GOTO 44
   EA = ABN(IMM+1)
   EE = ABN(IL)
28 CALL LOOKI(ISO,K,V,W,EA,EE,0,ISGT)
   IF(ISGT.EQ.1) RETURN
   V(1) = EA
   CALL LOOKI(ISO,I,F,W,EA,V(K),1,ISGT)
   IF(ISGT.EQ.1) RETURN
   F(1) = EA
   CALL PUSUM(ISO,K,V,I,F,W)
   CALL LOOKI(ISC,K,V,W,EA,F(1),2,ISGT)
   IF(ISGT.EQ.1) RETURN
   V(1) = EA
   CALL PUSUM(ISO,I,F,K,V,W)
   NN = IMM-IL+1
   K1 = 1
   DO 34 N = 1,NN
   I = IMM-N+1
   A = ABN(I)
   DO 30 MM = K1,K
   IF(V(MM).GE.A) GOTO 32
30 CCNTINUE
   MM = K
32 LST(2,I) = LST(2,I)+MM-K1

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   K1 = MM+1
   IF(K1.GT.K) GOTO 36
34 CCNTINUE
36 IF(K.LT.ISD) GOTO 38
   EA = V(K)
   GOTO 28
38 IF(ISEL.LT.0) WRITE(NCUT,100)
   ISDP = 0
   DC 42 N = IL,IMM
   LST(2,N) = LST(2,N)-2
   IF(ISFL.LT.0.AND.LST(2,N).NE.0) WRITE(NCUT,102) N,LST(2,N)
   IF(KSPE.EQ.0) GOTO 42
   A = ABN(N+1)
   B = ABN(N)
   DC 40 MM = 1,NSPEK
   IF(A.LT.ESP(MM).AND.ESP(MM).LT.8) LST(2,N) = LST(2,N)+1
40 CCNTINUE
42 ISDP = MAXO(ISCP,ISM+LST(2,N)-ISD)

C
44 IF(NTTP+ISDP.EQ.0) GOTO 48
   NTK = IABS(NTK)+2
   WRITE(NF) ((LST(N,K),K=IL,IM),N=1,2)
   REWIND NF
   RETURN
46 READ(NF) ((LST(N,K),K=IL,IM),N=1,2)
   NTK = NTK-2
   REWIND NF

C
C*****MAKROGRUPPENEINTEILUNG*****
48 IT = ISO
   ID = ISD-ISM
   INT(1) = IL-1
   IR = 2
50 II = INT(IR-1)+1
   Iw = 0
   IS = 0
   JS = 0
   DC 52 I = II,IM
   Iw = Iw+LST(1,I)
   IS = IS+LST(2,I)
   J = NK+NR
   A = -R(I)/ALLN
   IF(A.LT.1.) J = A*NK
   JS = JS+J
   IF(IS.GE.ID.OR.JS.GE.ISM-NEN.OR.1+1-II.GT.NS.OR.IW.GT.NTTI)GOTO 56
   IF(I.NE.IT) GOTO 52
   IF(I.EQ.IM.OR.I.EQ.II) GOTO 52
   IT = 0
   GOTO 56
52 CCNTINUE
   INT(IR) = IM
54 INT(1) = IL
   INTT = IR
   IE = IR-1
   GOTO 58

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56 INT(IR) = MAX0(I,I-1) 1500
   IF(INT(IR).EQ.IM) GOTO 54 1510
   IR = IR+1 1520
   GOTO 50 1530
C 1540
C*****SCHREIBEN DER MAKROGRUPPENEINTEILUNG***** 1550

58 IF(ISEL.GT.0) RETURN 156C
   WRITE(NOUT,94) 1570
   DO 60 I = 1,IE 1580
   IP = INT(I)+1 1590
   IF(I.EQ.1) IP = IP-1 1600
60 WRITE(NOUT,96) I,IP,INT(I+1) 1610
C 1620
   RETURN 1630
C 1640
94 FORMAT(///11X,'M A K R C G R U P P E N'///) 1650
56 FORMAT(1H0,2X,12,'. MAKRCGRUPPE',5X,13,'. BIS ',13,'. FEINGRUPPE') 166C
100 FORMAT(///5X,'STUETZSTELLEN FUER SGN, MUEL, SGT LND MAKRC SPEKTRUM' 1670
-//10X,'GRUPPE',11X,'ANZAHL'//) 168C
102 FORMAT(9X,16,11X,16) 1690
110 FORMAT(///5X,'STUETZSTELLEN FUER SGT (MISCHUNG FEINSTRUKTURWICHTUN 1700
-G)'//10X,'GRUPPE',11X,'ANZAHL'//) 1710
C 1720
   END 1730

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SUBROUTINE MIXSGT(KT,MAT,DAT,NTT,NTP,NT,ET,ST,EA,FE,ISGT) 10
C 20
C*****TCTALER QUERSCHNITT EINER MISCHUNG***** 30
C 40
REAL*8 MAT(KT),A(5),STCFF 50
DIMENSION DAT(KT),ET(NTT),ST(NTT),NW(4),NAD(2) 60
COMMON STOFF,ISTRUK,ISPA,NOUT 70
DATA NW(1),A(2),A(3) /3,'BEST ', 'SGT '/ 80
C 90
ISGT=0 100
DO 10 K = 1,KT 110
C = DAT(K) 120
A(1) = MAT(K) 130
NU = 0 140
CALL NDFLOC(KP,NW,A,NAD,KC) 150
IF(KP.NE.1) GOTO 12 16C
E = A(4) 170
S = A(5) 180
IF(E-EA) 6,4,14 19C
4 CALL ADD(K,NTT,NTP,NT,ET,ST,NU,D,E,S,EV,SV,EW,SW,EA,EE) 200
IF(NTP.GT.0) RETURN 21C
6 EV = E 220
SV = S 230
CALL NDFNXT(KP,NW,A,NAD,KC) 240
IF(KP.EQ.1) GOTO 7 250
E = FE 26C
S = SV 27C

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GOTO 8 280
7 E = A(4) 290
S = A(5) 300
IF(E-EA) 6,4,8 310
8 CALL ADD(K,NTT,NTP,NT,ET,ST,NU,D,E,S,EV,SV,EW,SW,EA,EE) 32C
IF(NTP.GT.0) RETURN 330
IF(E.LT.EE) GOTO 6 340
1C CONTINUE 35C
RETURN 360
C 370
12 WRITE(NOUT,20) MAT(K) 380
ISGT=1 390
RETURN 40C
14 WRITE(NOUT,22) MAT(K),EA 410
ISGT=1 420
RETURN 430
C 440
2C FORMAT(///' ***ERROR 6.5 : FOR ',A8,' IN THE FINE-STRUCTURE MIXTUR 450
1E NO SGT '/16X,'ARE ON KEDAK') 460
22 FORMAT(///' ***ERROR 6.6 : FOR ',A8,' IN THE FINE-STRUCTURE MIXTUR 47C
1E NO SGT '/16X,'ARE ON KEDAK FOR ENERGIES BELOW',1PE10.3,' EV') 480
C 490
   END 500

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SUBROUTINE ADD(K,NTT,NTP,NT,ET,ST,NU,C,E,S,EV,SV,EW,SW,EA,EE) 1C
C 20
C DIMENSION ET(NTT),ST(NTT) 30
C 40
C*****ERSTES MATERIAL***** 50
IF(K.GT.1) GOTO 1C 6C
IF(NU.GT.0) GOTO 6 70
IF(E.GT.EA) GOTO 2 80
ET(1) = E 90
ST(1) = S*D 100
GOTO 4 11C
2 T = (S-SV)/(E-EV) 120
ET(1) = EA 13C
ST(1) = D*(S+T*(EA-E)) 140
4 NU = 1 150

NT = 1 160
IF(E.LT.EE) RETURN 170
ET(2) = EE 180
ST(2) = D*(S+T*(EE-E)) 19C
NL = 2 200
NT = 2 210
RETURN 22C
6 NU = NU+1 230
NT = NT+1 24C
IF(NT.GT.NTT) GOTO 22 250
IF(E.LT.EE) GOTO 8 260
ET(NU) = EE 27C
ST(NU) = ST(NU-1) 280

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RETURN
8 ET(NU) = E
ST(NU) = S*D
RETURN
C
C*****WEITERE MATERIALIEN*****
10 IF(NU.GT.0) GOTO 12
EW = ET(1)
SW = ST(1)
IF(E.GT.EA) GOTO 12
ST(1) = ST(1)+D*S
EV = E
SV = S
NU = 1
RETURN
12 T = (S-SV)/(E-EV)
NP = NU+1
DO 14 I = NP,NT
IF(ET(I).GT.E) GOTO 16
Z = SV+T*(ET(I)-EV)
EW = ET(I)
SW = ST(I)
14 ST(I) = ST(I)+D*Z
RETURN
16 IF(E.EQ.ET(I-1)) GOTO 20
Z = SW+(ST(I)-SW)/(ET(I)-EW)*(E-EW)
IF(NT+1.EQ.NTT) GOTO 22
DO 18 J = I,NT
JJ = NT+I-J
ET(JJ+1) = ET(JJ)
18 ST(JJ+1) = ST(JJ)
NT = NT+1
ET(I) = E
ST(I) = Z+D*S
NL = I
EV = E
SV = S
RETURN
20 NU = I-1
EV = E
SV = S
RETURN
C
22 NTP = 1000
RETURN
C
END

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SUBROUTINE TRAFO(IC,NE,ISM,S,XM,AL,A)
C
C*****TRANSFORMATION DER SGAC INS L-SYSTEM*****
C
DIMENSION A(IC),S(IC,ISM)
C
XMP = XM-1
XMP = XM+1
CM = XM*XM
DO 2 I = 1,IC
V = SQRT(0.5*(1.+AL+(1.-AL)*A(I)))
A(I) = 0.5*(XMP*V-XMP/V)
B = SQRT(A(I)*A(I)+CM-1.)
F = (A(I)+B)*(A(I)+B)/(XM*B)
DO 2 N = 1,NE
2 S(I,N) = S(I,N)*F
C
RETURN
C
END

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SUBROUTINE PUNK(NGR,NEGR,ABN,NA,NE,NEN,ALFA,NK,NR,ISM,
IIMP,ISA,F,R,ALLN)
C
C*****GRUNDPUNKTE INTERVALLWEISE LOGARITHMISCH AEQUICISTANT*****
C
REAL*8 C,ED,EX,EP
DIMENSION ABN(NEGR),E(ISM),R(NGR)
C
JJ = 0
DO 2 N = NA,NE
J = NK+NR
AR = -R(N)/ALLN
IF(AB.LT.1.) J = AB*NK+1
2 JJ = JJ+J
JJ = JJ+NA-NE+1
IIMP = MAX(0,JJ+NEN-ISM)
IF(IIMP.GT.0) RETURN
C
E(1) = ABN(NE+1)
J = 2
DO 10 NN = NA,NE
N = NA+NE-NN
AB = -R(N)/ALLN
FX = DBLE(1./(NK-1))
IF(AB.LT.1.) EX = DBLE(1./(AB*NK))
EC = DBLE(E(J-1))
AB = ABN(N)
A = AMIN1(AB,ABN(N+1)/ALFA)
4 D = DBLE(A/ABN(N+1))
C = D**EX
6 EP = ED*D

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E(J) = SNGL(EP)
IF(E(J).GT.A) GOTO 8
EC = EP
J = J+1
GOTO 6
8 E(J-1) = A
IF(A.GE.AB) GOTC 7
EC = DBLE((AB/A)**(1./NR))
IF(ED.GE.D) C = EC
EC = DBLE(A)
11 EP = ED*D
E(J) = SNGL(EP)
IF(E(J).GT.AB) GOTO 9
ED = EP
J = J+1
GOTO 11
9 E(J-1) = AB
7 FM = .99999*E(J-1)
IF(J.LE.2) GOTC 10
IF(E(J-2).GE.EM) GOTC 10
E(J) = E(J-1)
E(J-1) = EM
J = J+1
10 CCNTINUE
ISN = J-1
ISMP = MAXO(0,ISN-ISM)
RETURN
C
END

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SUBROUTINE LOGKO(XMAT,MASSE,COM,*)
C
C*****LESEN DES ATOMGEWICHTS *****
C
REAL*8 STOFF,F(6),ST
INTEGER*2 U/'H','V
DIMENSION NWCRT(4),NACAT(2)
COMMON STOFF,ISTRUK,ISPA,NCUT
EQUIVALENCE(ST,V)
DATA F(2),F(3) /'BEST ','ISOT1'/
C
NWORT(1) = 3
F(1) = STOFF
CALL NDFLOC(KP,NWORT,F,NACAT,KC)
IF(KP.NE.1) GO TO 1
F(4) = F(4)/1.008665
XMAT = F(4)
CCM = 2/(3*F(4))
MASSE = XMAT
IF(XMAT-MASSE.GT.0.5) MASSE = MASSE+1
RETURN
C

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1 ST=STOFF
IF(U.NE.V) RETURN 1
WRITE(NOUT,2)
2 FORMAT/' WARNING NDF. 3 MAY BE IGNORED IN THE CASE OF HYDROGEN'/
XMAT=1.
MASSE=1
CCM=0.6666667
RETURN
END

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SUBROUTINE LOCK1(ISC,K,E,SGN,EO,EE,NT,ISGT)
C
C*****LESEN DER SGN, MUEL UND SGT VON KEDAK *****
C
REAL*8 STOFF,A(5),B(3)
DIMENSION E(ISC),SGN(ISC),NWORT(4),NACAT(2)
COMMON STOFF,ISTRUK,ISPA,NCUT
FG(XA,XB,XC,YA,YC) = YA*(YC-YA)/(XC-XA)*(XB-XA)
DATA A(2),B /'BEST ','SGN ','MUEL ','SGT '/
C
ISGT=0
A(3) = B(NT+1)
1 NWCRT(1) = 3
A(1) = STOFF
CALL NDFLOC(KP,NWORT,A,NACAT,KC)
IF(KP.NE.1) GOTC 15
K = 1
F(1) = A(4)
SGN(1) = A(5)
IF(E(1)-EO) 5,4,3
3 WRITE(NOUT,40) STOFF,EO,A(3)
ISCT=1
RETURN
4 K = K+1
5 CALL NDFNXT(KP,NWORT,A,NACAT,KC)
IF(KP.NE.1) GOTC 14
IF(K.GT.1) GOTC 11
IF(A(4)-EO) 8,9,10
8 E(1) = A(4)
SGN(1) = A(5)
GOTO 5
9 E(1) = A(4)
SGN(1) = A(5)
GOTO 4
10 K = 2
11 E(K) = A(4)
IF(K.EQ.ISO) RETURN
SGN(K) = A(5)
IF(E(K)-EE) 4,16,12
12 Y = FG(E(K-1),EE,E(K),SGN(K-1),SGN(K))
E(K) = EE
SGN(K) = Y

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- B 110 -

GCTO 16	43C	IF(KP.EQ.1) GOTO 3	280
14 E(K) = EE	440	IF(IP.GT.ICOS) GO TO 4	290
SGN(K) = SGN(K-1)	450	ICCS = IP-1-ICOS	300
WRITE(NOUT,42) A(3),STOFF,E(K-1),A(3),E(K-1)	460	WRITE(NOUT,44) STOFF,ICOS,EA(NE)	310
16 IF(E(1).EQ.E0) RETURN	470	RETURN	320
Y = FG(E(1),EC,E(2),SGN(1),SGN(2))	480	4 CONTINUE	330
E(1) = E0	490	RETURN	340
SGN(1) = Y	500		350
RETURN	510		360
15 WRITE(NOUT,41) STOFF,E0,A(3)	520	44 FORMAT(// ' ***WARNING 6.3 : FOR ',A8,' THE SGNC COSINE MESH HAS M	370
ISGT=1	530	LOPE'/18X,' THAN ',I3,' MESHPOINTS AT',IPE10.3,' EV')	380
RETURN	540	END	390
	55C		
40 FORMAT(// ' ***ERROR 6.2 : FOR ',A8,' SCATTERING MATRICES CANNOT B	560		
1E CALCULATED'/16X'FOR ENERGIES BELOW',IPE10.3,' EV FOR LACK OF ',	570		
2AE,' ON KEDAK')	580		
41 FORMAT(// ' ***ERROR 6.9 : FOR ',A8,' SCATTERING MATRICES CANNOT B	590		
1E CALCULATED'/16X'FOR ENERGIES BELOW',IPE10.3,' EV FOR LACK OF ',	60C		
2AE,' ON KEDAK')	610		
42 FORMAT(// ' ***WARNING 6.1 : THE ',A8,' FOR ',A8,' AT ENERGIES AB	62C		
IOVF',IPE10.3,' EV'/18X,' ARE SET EQUAL TO THE ',A8,' AT',E10.3,' E	630		
2V'//)	640		
	65C		
END	660		
		SLBRoutine LOCK3(NE,EA,ISC,NGR,ABN,ISM,ISMP,LST,NEGR,ISEL,ISGNC)	1C
			20
		C*****LESEN DER SGNC-ENERGIEN VOM KERNDATENBAND*****	30
			40
		REAL*8 STOFF,F(6)	5C
		DIMENSION EA(ISM),ABN(NEGR),LST(NEGR),NWORT(4),NADAT(2)	60
		COMMON STOFF,ISTRUK,ISPA,NOUT	70
		DATA F(2),F(3) /'BEST ', 'SGNC '/	8C
			90
		ISGNC=0	1CC
		2 NWORT(1) = 4	110
		F(1) = STOFF	12C
		F(4) = 0.	130
		NE = 1	140
		4 CALL NDFLOC(KP,NWORT,F,NADAT,KC)	150
		IF(KP.EQ.1) GO TO 5	160
		CALL NDFLOC(KP,NWORT,F,NADAT,KC)	17C
		IF(KP.EQ.1) GO TO 5	180
		IF(NE-1)13,13,6	190
		5 EA(NE)=F(4)	20C
		F(4) = F(4)+F(4)*(1.E-06)	210
		IF(EA(NE).LT.1.) GO TO 4	22C
		NE = NE+1	230
		IF(NE.LE.ISM) GOTO 4	240
		ISMP=5)	25C
		RETURN	260
		6 WRITE(NOUT,62)	270
		IF(EA(1).GE.ABN(1)) GO TO 12	280
			290
		C*****ANZAHL DER SGNC IN DER N-TEN GRUPPE*****	30C
		NE=NE-1	310
		CC 10 N = 1,NGR	32C
		LST(N) = 0	330
		CC 8 M = 1,NE	340
		IF((ABN(N+1).LE.EA(M)).AND.(EA(M).LT.ABN(N))) LST(N) = LST(N)+1	35C
		8 CCNT INUE	360
		10 CONTINUE	370
		IF(ISEL.GT.0) GO TO 11	380
		WRITE(NOUT,52)	390


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DO 7 N=1,NGR
7 WRITE(NOUT,54) N,LST(N)
C
C*****ANISOTROPIE-SCHWELLE*****
11 DC 14 N = 1,NGR
    NN = NGR-N+1
    IF(LST(NN),NE,0) GOTO 16
14 CCNTINUE
16 ISO = NN+1
    RETURN
C
12 IF(ISEL.GT.0) GO TO 15
    WRITE(NOUT,52)
    WRITE(NOUT,58)
15 EA(1) = ABN(1)
    ISC=1
    RETURN
C
13 WRITE(NOUT,60) STOFF
    ISGNC=1
    RETURN
C
52 FCFMAT(///10X,'STUETZSTELLEN FUER SGNC'//
- 10X,'GRUPPE',11X,'ANZAHL'//)
54 FCFMAT(9X,16,11X,16)
58 FCFMAT(5X,'ENERGIEBEREICH LIEGT IM BEREICH ISOTROPER STREUUNG')
60 FCFMAT(///'***ERROR 6.4 : FOR ',A8,' SCATTERING MATRICES CANNOT B
IE CALCULATED'/16X'FOR LACK OF SGNC ON KEDAK')
62 FCFMAT(///'***MESSAGE 6.1 : WARNING NOF. 2 MAY BE IGNORED')
C
END
C
SUBROUTINE LECAL(MASSE,XMAT,ALFA,ISOT,LEG,NLE,NANF,NENC,NUEB,IL,
1 IM,NEGR,ABN,ICOS,AR,ISN,E,SGNC,NST,NSTIS,ISM,ISD,
2 NECU,ITA,NF,GR,FEKOE,FU,EW,A,F,V,W,F,FEKO)
C
C*****BERECHNUNG DER ENERGIEDIFFERENTIELLEN LEGENDRE-KOEFFIZIENTEN*****
C
DIMENSION NST(6),LEG(6),AR(ICOS),FU(ICOS),ABN(NEGR),GR(NEGR),
1 FEKOE(NEGR),A(ISD),H(ISC),E(ISM),EW(ISM),V(ISC),W(ISD),
2 F(ISD),SGNC(ICOS,ISM),FEKO(ISM,NECU)
C
EP = 0.8
XP = XMAT+1
XP = XMAT-1
IF(MASSE.EQ.1) XM = 0.
NP = NUEB-1
IA = NANF
IC = MINO(NEGR,NEND+NUEB)
IB = IC-1
IF(ITA.EQ.0.AND.ISOT.EQ.0)
1CALL LEGINT(NLE,NSTIS,XMAT,ITA)

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REWIND NF
C
C*****ENERGIEDIFF. LEGENDRE-KOEFF. (L-1)-TER ORDNUNG*****
N = 0
L = 1
GOTO 2
1 N=N+1
L=LEG(N)
2 IF(ISOT.EQ.0) GOTO 3
NSB = NSTIS
NSA = NST(L)
CALL LEGPOL(NSA,H,NLE)
C
3 DC 28 J = 1,ISN
C
C*****GRENZEN FUER WINKEL INTEGRATION*****
GRM = 0.
EL = AMAX1(ABN(IM+1),ALFA*E(J))
DC 8 I = 1A,IC
IF(EL.LT.ABN(I)) GOTO 6
GR(I) = -1.
GOTO 8
6 IF(E(J).GT.ABN(I)) GOTO 7
GR(I) = 1.
GOTO 8
7 G = SQRT(ABN(I)/E(J))
GR(I) = 0.5*(XP*G-XM/G)
GRA = ABS(GR(I))
IF((GRA.LT.1.).AND.(GRM.LT.GRA)) GRM = GRA
8 CCNTINUE
IF(ISOT.EQ.0) GOTC 11
C
C*****MOMENTE BEI ANISOTROPIE IM SP-SYSTEM*****
IF(GRM.LT.EP) NSB = NST(L)
IF(NSA.EQ.NSB) GOTO 9
NSA = NSB
CALL LEGPOL(NSA,H,NLE)
9 DO 10 IP = 1,ICOS
10 FL(IP) = SGNC(IP,J)
CALL IPOLA(ICOS,AR,FU,NSA,H,A,F)
CALL LEGANS(L,NSA,A,IA,IB,NEGR,GR,FEKOE,V,W)
NSB = NSTIS
GOTO 12
C
C*****MOMENTE BEI ISOTROPIE IM SP-SYSTEM*****
11 CALL LEGIST(L,NSTIS,IA,IB,NEGR,GR,FEKOE)
C
C*****VORBEREITUNG ZUM ABSPEICHERN*****
12 II = 1
DC 22 I = 1A,IB
IF(ABN(I+1).GT.E(J)) GOTO 22
FEKO(J,II) = 6.283185*FEKOE(I)
II = II+1
IF(II.GE.NUEB) GOTC 27
22 CCNTINUE

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DO 26 I = 1, NM
26 FEKO(J, I) = 0.
27 FEKO(J, NUEB) = 6.283185*FEKCE(NEGR)
C
28 CCNTINUE
C
C*****NORMIERUNG FUER ZWISCHENPUNKTE*****
IF(N.GT.0) GOTO 30
CC 29 J = 1, ISN
29 EW(J) = FEKO(J, NUEB)
GOTO 1
30 CC 31 J = 1, ISN
DO 31 I = 1, NUEB
31 FEKO(J, I) = FEKO(J, I)/EW(J)
C
C*****SPEICHERN DER ENERGIEDIFF. LEGENDRE-KOEFF. (L-1)-TER ORDNUNG*****
DO 32 I = 1, NUEB
32 WRITE(NF) (FEKO(J, I), J = 1, ISN)
IF(N.LT.NLE+1) GOTO 1
C
RFIND NF
C
RETURN
C
END

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SUBROUTINE LEGPOL(NST, A, N, NSTIS)
C
C*****BERECHNUNG VON LEGENDRE-POLYNOME*****
REAL*8 X(321), F(6, 321), D
DIMENSION A(NSTIS)
COMMON /INTEG/ X, F, D
C
NSM = NST-1
NA = -100000
NC = 320/NSM*625
CC 6 I = 1, NST
X(I) = DFLOAT(NA)*1.0-05
A(I) = SNGL(X(I))
E NA = NA*ND
E = ND*1.E-05
C
IF(N.GT.0) GOTO 2
CC 1 I = 1, NST
1 F(1, I) = 1.
RETURN
C
2 IF(N.GT.1) GOTO 4
CC 3 I = 1, NST
F(1, I) = 1.
3 F(2, I) = X(I)

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RETURN
C
4 NP = N-1
DO 5 I = 1, NST
F(1, I) = 1.
F(2, I) = X(I)
CC 5 J = 1, NM
5 F(J+2, I) = ((2*J+1)*X(I)*F(J+1, I) - J*F(J, I))/(J+1)
C
RETURN
C
END

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SUBROUTINE LEGINT(N, NAK, XMAT, ITA)
C
C*****BERECHNUNG VON LEGENDRE-INTEGRAL*****
REAL*8 H(321), GRAL(6, 321), F(6), A, B, C, D, DE, G, P, F0, F1, F2, F3, F4, F5,
I X, Y
COMMON /INTEG/ H, GRAL, D
C
ITA = 1
NST = 321
C
NA = -100000
CC 1 K = 1, NST
H(K) = DFLOAT(NA)*1.0-05
1 NA = NA+625
D = 0.00625
C
IF(XMAT.GT.1.5) GOTO 4
C*****WASSERSTOFF*****
CC 2 K = 1, 160
DC 2 L = 1, 6
2 GRAL(L, K) = 0.
DC 3 K = 161, 321
A = H(K)*H(K)
B = A*H(K)
GRAL(1, K) = 2*A
GRAL(2, K) = 4*B/3
GRAL(3, K) = 0.5*A*(3*A-2)
GRAL(4, K) = 2*B*(A-1)
GRAL(5, K) = A*(35*(A-1)*(A-2./7)-1)/12
GRAL(6, K) = 4.5*B*(A-1)*(A-5./9)
3 CCNTINUE
GOTO 12
C
C*****NICHT-WASSERSTOFFE*****
4 A = DBLE(XMAT)
DO 5 L = 1, 6
5 GRAL(L, 1) = 0
IF(XMAT.GT.30.) GOTO 8

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C = 0.5*DSQRT((A+1)*(A-1))
F(1) = C
DC 6 L = 2,5
6 F(L) = F(L-1)*C
P = A-1./A
Y = DSQRT((A-1)/(A+1))
C
DC 7 K = 2,NST
X = (H(K)+DSQRT((H(K)+1)*(H(K)-1)+A*A))/(2*C)
DE = X-Y
FC = 0.5*G(2,X,Y)
F1 = F(1)*(G(3,X,Y)/3-1)
F2 = F(2)*(0.25*G(4,X,Y)-G(2,X,Y)+DLGG(X/Y)/DE)
F3 = F(3)*(0.2*G(5,X,Y)-G(3,X,Y)+3-1./(X*Y))
F4 = F(4)*(G(6,X,Y)/6-G(4,X,Y)+3*G(2,X,Y)-4*DLGG(X/Y)/DE
1 +0.5/(X*Y)*G(2,1./X,1./Y))
F5 = F(5)*(G(7,X,Y)/7-G(5,X,Y)+10*G(3,X,Y)/3-1C+5./(X*Y)
1 -G(3,1./X,1./Y)/(3*X*Y))
GRAL(1,K) = P*F0*DE
GRAL(2,K) = P*F1*DE
GRAL(3,K) = P*0.5*(3*F2-F0)*DE
GRAL(4,K) = P*0.5*(5*F3-3*F1)*DE
GRAL(5,K) = P*0.125*(35*F4-30*F2+3*F0)*DE
GRAL(6,K) = P*0.125*(63*F5-70*F3+15*F1)*DE
7 CCNTINUE
ECTO 11
C
8 B = 1./(A*A)
C = B*B
DC 10 K = 2,NST
X = H(K)
Y = -1.
DC 9 L = 1,6
9 F(L) = -0.125*(5*G(L+4,X,Y)/(L+4)-6*G(L+2,X,Y)/(L+2)+G(L,X,Y)/L)*C
1 +0.5*(3*G(L+2,X,Y)/(L+2)-G(L,X,Y)/L)*B
2 +2*G(L+1,X,Y)/(A*(L+1))+G(L,X,Y)/L
DE = X-Y
GRAL(1,K) = F(1)*DE
GRAL(2,K) = F(2)*DE
GRAL(3,K) = 0.5*(3*F(3)-F(1))*DE
GRAL(4,K) = 0.5*(5*F(4)-3*F(2))*DE
GRAL(5,K) = 0.125*(35*F(5)-30*F(3)+3*F(1))*DE
GRAL(6,K) = 0.125*(63*F(6)-70*F(4)+15*F(2))*DE
10 CONTINUE
C
11 GRAL(1,NST) = 2.
GRAL(2,NST) = 4/(3*A)
GRAL(4,NST) = 0.
GRAL(6,NST) = 0.
C
C*****REDUKTION VON NST AUF NAK *****
12 NP = N+1
13 IF(NAK.EQ.NST) RETURN
K1 = (NST-1)/(NAK-1)
KK = K1+1

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DO 15 K = 2,NAK
H(K) = H(KK)
DC 14 L = 1,NP
14 GRAL(L,K) = GRAL(L,KK)
15 KK = KK+K1
D = 2./(NAK-1)
C
RETURN
C
ENC
FUNCTION G(N,X,Y)
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- B 114 -

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SUBROUTINE LEGIST(L,NST,IA,IB,NEGR,GR,E)
C*****BERECHNUNG VON PARTIELLEN LEGENDRE-KOEFFIZIENTEN BEI ISOTROPIE IM
C*****SP-SYSTEM*****
C
REAL*8 X(321),GRAL(6,321),D,A,B
DIMENSION GR(NEGR),E(NEGR)
COMMON /INTEG/ X,GRAL,D
C
DC 7 I=IA,IB
GO = 1.
GL = -1.
IKO = NST
IKU = 1
IF(GR(I+1).GE.1.) GOTO 5
IF(GR(I).LE.-1.) GOTO 5
IF(GR(I).GE.1.) GOTO 2
GO = GR(I)
XIKO = 1.+0.5*(NST-1)*(GO+1.)
IKO = XIKO
IF(FLOAT(IKO).LT.XIKO) IKO = IKO+1
2 IF(GR(I+1).LE.-1.) GOTO 3
GU = GR(I+1)
XIKU = 1.+0.5*(NST-1)*(GU+1.)
IKU = XIKU
IF(FLOAT(IKU).LT.XIKU) IKU = IKU+1
3 A = GRAL(L,IKO)
IF(GC.LT.X(IKC)) A = A+(GO-X(IKC))/D*(GRAL(L,IKO)-GRAL(L,IKO-1))
B = GRAL(L,IKU)
IF(GU.LT.X(IKU)) B = B+(GU-X(IKU))/D*(GRAL(L,IKU)-GRAL(L,IKU-1))
4 F(I) = (A-B)*0.7957747E-01
GOTO 7
5 E(I) = 0.
7 CONTINUE
E(NEGR) = GRAL(L,NST)*C.7957747E-C1
C
RETURN
C
END

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SUBROUTINE LEGANS(L,NST,F,IA,IB,NEGR,GR,E,POLY,A)
C*****BERECHNUNG VON PARTIELLEN LEGENDRE-KOEFFIZIENTEN BEI ANISOTROPIE
C*****IM SP-SYSTEM*****
C
REAL*8 X(321),PCL(6,321),C,B
DIMENSION F(NST),GR(NEGR),E(NEGR),POLY(NST),A(NST)
COMMON /INTEG/ X,PCL,D
C
C*****BESTIMMUNG DER ZU INTEGRIERENDEN FUNKTION*****
DC 2 J = 1,NST
B = DBLE(F(J))

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2 PCL(J) = B*PCL(L,J)
C
C*****SUCHEN DER GRENZINDICES MIT KORREKTURINTERVALLEN*****
ES = 0
I = IA-1
3 I = I+1
IF((GR(I+1).GE.1.).CR.(GR(I).LF.-1.)) GOTO 18
IF(GR(I).LT.1.) GOTO 4
II = I
GOTO 18
4 GC = GR(I)
GL = AMAX1(-1.,GR(I+1))
XIKO = 1.+0.5*(NST-1)*(1.+GO)-0.001
AC = XIKO
XIKU = 1.+0.5*(NST-1)*(1.+GU)+0.001
NU = XIKU
IF(FLOAT(NU).LT.XIKC) AC = AC+1
NUO = NU-NU
IF((NUO/2*2).NE.NUO) NO = NO-1
DL = GU-X(NU)
DC = GO-X(NO)
IF(ABS(DU).LT.1.E-2C) DU = 0
IF(ABS(DO).LT.1.E-2D) DO = 0
C
C*****SIMPSON-INTEGRATION FUER UBERSTREUUNG UND TOTALES MOMENT*****
5 NO1 = NO-2
NC2 = NO-1
NL1 = NU+2
NU2 = NU+1
IF(NO1.GE.NU1) GOTO 7
E(I) = (POLY(NU)+POLY(NC))*D/2.
IF(NO2.LT.NU2) GOTO 19
DC 6 J = NU2,NC2
6 E(I) = E(I)+D*POLY(J)
GOTO 19
7 DO 12 J = NU2,NO2,2
JJ = (J-NU2+2)/2
12 A(JJ) = POLY(J)
CALL SUM(JJ,A,SA)
DC 15 J = NU1,NC1,2
JJ = (J-NU1+2)/2
15 A(JJ) = POLY(J)
CALL SUM(JJ,A,SO)
SE = POLY(NO)+POLY(NU)
E(I) = (4*SA+2*SC+SE)*C/3
C
C*****RANDKORREKTUR DES SIMPSON-INTEGRALS*****
IF(I.EQ.NEGR) GOTO 2C
TU = (POLY(NU2)-POLY(NU))/D
TC = (POLY(NC)-POLY(NC2))/D
E(I) = (POLY(NO)+0.5*DO*TC)*DO-(POLY(NU)+0.5*DL*TC)*DU+E(I)
GOTO 19
18 E(I) = 0.
19 ES = ES+E(I)
IF(I.LT.IB) GOTO 3

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C
C*****INTEGRATIONSBEREICH FUER DAS TOTALE MOMENT*****
  NU = 1
  NC = NST
  I=NEGR
  GOTO 5
C
C*****G,G-STREUUNG *****
  20 E(II) = E(NEGR)-ES
  RETURN
C
  END
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  760
  770
  780
  790

  SUBROUTINE GRUPIN(MASSE,XMAT,ALFA,COM,ISCT,PM,LEG,NLE,NANF,NEND,
  1 NUEB,IL,IM,NGR,NEGR,ABN,ISN,EH,K,H,F,M,G,EN,
  2 NTT,ET,ST,MAZ,KSPE,KSPEK,ESP,SPEK,NSPEK,LSPEK,
  3 ISM,ISD,NECU,ISCC,ISEC,NF,E,EG,GR,WA,U,V,W,ISTT,
  4 RSP,ELSIG,NGT,NGG,EG,SG,SGTOT)
C
C*****GEWICHTETE MULTIGRUPPEN-ENERGIEINTEGRATION*****
  REAL*8 DXY
  DIMENSION LEG(6),ABN(NEGR),RSP(6,NGR),ESP(NSPEK),SPEK(LSPEK),
  1 EH(ISM),EW(ISM),H(ISD),F(ISD),G(ISD),EN(ISD),V(ISD),
  2 W(ISD),E(ISD),WA(ISCO),L(ISEC),ET(NTT),ST(NTT),GR(NGR),
  3 MAZ(2),ELSIG(6,NECU,NGR),EG(ISC),SG(ISD),SGTOT(6,NGR)
C
  NF = NLE+1
  XP = XMAT+1
  XM = XMAT-1
  GW = -1.
  IF(MASSE.EQ.1) GW = 0.
  IF(MASSE.EQ.1) XM = 0.
  NM = NUEB-1
C
C*****VEREINIGUNG DER ENERGIESTUFTZPUNKTMENGEN*****
  JI = 0
  JF = 0
  IF(KSPE.EQ.0) GOTO 3
  XX = EH(1)
  XY = EH(ISN)
  DO 1 J = 1,KSPEK
  IF(JI.EQ.0.AND.XX.LE.ESP(J)) JI = J
  IF(XY.LE.ESP(J)) JP = J-JI
  IF(JP.GT.0) GOTO 3
  1 CCNTINUE
  3 DO 2 J = 1,ISN
  2 E(J) = EH(J)
  ISTT = ISN
  CALL PUSUM(ISD,K,H,ISTT,F,V)
  IF(KSPE*JI*JP.NE.0) CALL PUSUM(ISD,JP,ESP(JI),ISTT,E,V)
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C*****INTERPOLATION DER TOTALEN ELASTISCHEN QUERSCHNITTE*****
  CALL IPOLIN(K,H,F,ISTT,E,W,U)
C
C*****INTERPOLATION DER TOTALEN QUERSCHNITTE*****
  IF(NGT.EQ.0) GOTO 7
  CALL IPOLIN(NGG,EG,SG,ISTT,E,F,U)
  NCG = ISTT
  DC 5 J = 1,NGG
  E(J) = E(J)
  5 SG(J) = F(J)
C
C*****INTERPOLATION DER MITTLEREN STRECKKOSINUS*****
  7 CALL IPOLIN(M,G,EN,ISTT,E,V,U)
C
  8 DC 66 N = 1,NP
  L = LFG(N)
C*****LESEN UND INTERPOLATION DER NORMIERTEN ENERGIEDIFF. LEGENDRE-KOEFF
  DO 11 I = 1,NUEB
  JI = (I-1)*ISTT
  READ(NF) (EW(J),J = 1,ISN)
  IF(ISTT.EQ.0.AND.I.EQ.NUEB) GOTO 9
  CALL IPOLIN(ISN,EH,EW,ISTT,E,WA(I+JI),U)
  GOTO 11
  9 XY = EW(ISN)
  DC 10 J = 1,ISTT
  10 WA(J+JI) = XY
  11 CCNTINUE
C
C*****MUEL-ANGEPASSTE ENERGIEDIFF. LEGENDRE-KOEFF. *****
  DC 44 J = 1,ISTT
  DXY = 0.
  JP = J+NM*ISTT
  IF(L.NE.2) GOTO 27
  V(J) = PM*(V(J)-WA(JP))
  IF(ABS(V(J)).LT.1.E-7) V(J) = 0.
  27 DC 12 NN = NANF,NEND
  IF((ABN(NN+1).LE.E(J)).AND.(F(J).LE.ABN(NA))) GOTO 14
  12 CCNTINUE
  NN = NEND
  14 EL = AMAX1(ABN(IM+1),ALFA*E(J))
  DC 42 I = 1,NUEB
  JI = J+(I-1)*ISTT
  NI = MINO(IM,NN+I-1)
  P = 0.
  EU = GW
  IF(EL.GE.ABN(NI+1)) GOTO 16
  GU = SQRT(ABN(NI+1)/E(J))
  GU = 0.5*(XP*GU-XM/GU)
  16 GO = 1.
  IF(I.EQ.1) GOTO 18
  LI = MINO(IM+1,NA+I-1)
  GO = GW
  IF(EL.GE.ABN(LI)) GOTO 18
  GO = SQRT(ABN(LI)/E(J))
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GC = 0.5*(XP*GO-XM/GO)
18 IF(GU.LT.GO) GOTO 20
P = 0.
GCTO 36
20 IF(GO-GU.LT.2.) GOTO 22
P = 0.
IF(L.EQ.2) P = 1.
GCTO 36
22 C2 = GO*GO
U2 = GU*GU
C3 = O2*GO
U3 = U2*GU
IF(MASSE.EQ.1) GOTO 13
GCTO(24,26,28,30,32,34),L
13 GOTO(15,17,19,21,23,25),L
15 P = 12*(O3-O2)
P = P-12*(U3-U2)
GCTO 36
17 P = O3*(9*GO-8)
P = P-U3*(9*GU-8)
GCTO 36
19 P = .6*O2*(12*O3-10*(O2+GO-1))
P = P-.6*U2*(12*U3-10*(U2+GU-1))
GCTO 36
21 P = 1.5*O3*(10*O3-8*O2-9*GO+8)
P = P-1.5*U3*(10*U3-8*U2-9*GU+8)
GOTO 36
23 P = .5*O2*(O2*(45*O3-35*O2-54*GO+45)+9*GO-9)
P = P-.5*U2*(U2*(45*U3-35*U2-54*GU+45)+9*GU-9)
GOTO 36
25 P = .1875*O3*(O2*(189*C3-144*O2-280*GO+224)+90*GO-80)
P = P-.1875*U3*(U2*(189*U3-144*U2-280*GU+224)+90*GU-80)
GCTO 36
24 P = 0.75*(O2-U2)
GOTO 36
26 P = 0.5*(O3-U3)
GCTO 36
28 P = 0.1875*(O2*(3*O2-2)-U2*(3*U2-2))
GOTO 36
30 P = 0.75*(O3*(O2-1)-U3*(U2-1))
GCTO 36
32 P = 0.03125*(O2*((O2-1)*(35*O2-10)-1)-U2*((U2-1)*(35*U2-10)-1))
GCTO 36
34 P = 0.1875*(O3*(O2-1)*(9*O2-5)-U3*(U2-1)*(9*U2-5))
36 IF(ABS(P).LT.1.E-16) P = 0.
IF(EL.LT.ABN(NI+1).AND.I.LT.NUEB) GCTO 40
WA(JI) = WA(JP)-SNGL(DXY)
IF(I.EQ.NUEB) GOTC 42
IA = I+1
DC 38 II = IA,NUEB
38 WA(J+(I-1)*ISTT) = 0.
WA(JI) = WA(JI)+P*V(J)
GCTO 44
40 DXY = DXY+DBLE(WA(JI))
42 WA(JI) = WA(JI)+P*V(J)

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44 CONTINUE
C
C*****AUSSORTIEREN ZUR GEWICHTETEN INTEGRATION*****
DO 64 NR = 1,NUEB
NI = (NR-1)*ISTT
JA = 1
CO 58 NT = NANF,NEND
NN = NANF+NEND-NT
C
C NN-TE GRUPPE = AUSSTREUGRUPPE
C (NN+NR-1)-TE GRUPPE = EINSTREUGRUPPE
AP = ABN(NN)
DC 46 J = JA,ISTT
IF(E(J).GT.AM) GOTC 48
JI = J-JA+1
EN(JI) = E(J)
46 F(JI) = WA(J+NI)*W(J)
J = ISTT+1
48 IKK = J-JA
JA = J-1
IF(NN+NR-1.GT.IM) GOTO 58
IF(IKK.GE.3) GOTO 52
IKK = 2
FN(2) = AM
F(2) = F(1)
GOTO 56
52 EN(IKK) = AM
T = (F(IKK-2)-F(IKK-1))/(EN(IKK-2)-EN(IKK-1))
F(IKK) = F(IKK-1)+T*(AM-EN(IKK-1))
C
C*****SPEKTRUMSGEWICHTETE ENERGIEINTEGRATION*****
56 CALL SPRAL(KSPE,KSPEK,MAZ,ESP,SPEK,NTT,ET,ST,L,IKK,FN,F,G,
1 ELSIG(L,NR,NN),NSPEK,LSPEK,NLE)
58 CCNTINUE
64 CCNTINUE
66 CCNTINUE
C
C*****ACRMTERUNG*****
JA = 1
DC 70 NT = NANF,NEND
NN = NANF+NEND-NT
AP = ABN(NN)
DC 67 J = JA,ISTT
IF(E(J).GT.AM) GOTO 68
I = J-JA+1
EN(I) = E(J)
67 F(I) = 1.
J = ISTT+1
68 IKK = J-JA
JA = J-1
EN(IKK) = AM
F(IKK) = 1.
DC 70 L = 1,AP
CALL SPRAL(KSPE,KSPEK,MAZ,ESP,SPEK,NTT,ET,ST,L,IKK,EN,F,G,
1 RSP(L,NN),NSPEK,LSPEK,NLE)
II = MINC(NUEB,IM-NN+1)

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      DC 69 I = 1, II
      69 ELSIG(L,I,NN) = ELSIG(L,I,NN)/RSP(L,NN)
      70 CCNTINUE
C
C***** 1-GEWICHTETE TOTALE QUERSCHNITTE *****
      IF(NGT.EQ.0) RETURN
      JA = 2
      DC 82 NT = NANF,NEND
      NN = NANF+NEND-NT
      AM = ABN(NN)
      CD 72 J = JA,NGG
      IF(EG(J).GT.AM) GOTO 74
      I = J-JA+2
      E(I) = EG(J)
      72 F(I) = SG(J)
      J = NGG+1
      74 IKK = J-JA+1
      T = (SG(JA)-SG(JA-1))/(EG(JA)-EG(JA-1))
      E(I) = ABN(NN+1)
      F(I) = SG(JA-1)+T*(E(I)-EG(JA-1))
      IF(IKK.GT.1) GOTO 76
      E(2) = AM
      F(2) = SG(JA-1)+T*(E(2)-EG(JA-1))
      IKK = 2
      GOTO 78
      76 IF(J.EQ.NGG+1) GOTO 78
      T = (SG(J)-SG(J-1))/(EG(J)-EG(J-1))
      F(IKK) = F(IKK)+T*(AM-EG(J-1))
      E(IKK) = AM
      78 DC 80 L = 1,NP
      CALL SPRAL(KSPE,KSPEK,MAZ,ESP,SPEK,NTT,ET,ST,L,IKK,F,F,G,VAL,
      1 NSPEK,LSPEK,NLE)
      80 SGTOT(L,NN) = VAL/RSP(L,NN)
      82 JA = J
C
      RETURN
C
      END

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C***** INTERPOLATION *****
      Y(I) = B(I)
      Y(N) = B(M)
      I = 1
      DO 14 J = 2,NM
      8 IF(A(I+1)-X(J)) 9,10,11
      9 I = I+1
      GOTO 8
      10 Y(J) = B(I+1)
      GOTO 14
      11 Y(J) = B(I)+HR(I)*(X(J)-A(I))
      14 CCNTINUE
C
      RETURN
C
      END

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      SUBROUTINE SPRAL(KS,NS,MZ,E,S,NTT,ET,ST,L,IKK,EN,H,G,VAL,AP,NL,
      1NLE)
C
C***** GEWICHTETE INTEGRATION
      REAL*8 W,WER
      DIMENSION E(NP),S(NL),EN(IKK),G(IKK),H(IKK),ET(NTT),ST(NTT),MZ(2)
C
      WW(D1,D2,D3,S1,S2,S3) = (S1*D2*D3+C1*S2*D3+D1*C2*S3)/3.+S1*S2*S3
C
C***** MAKROSPEKTRUM 1/E
      IF(KS.NE.0) GOTO 16
      DO 2 I = 1,IKK
      2 G(I) = PHI(EN(I))
      GOTO 24
C
C***** MAKROSPEKTRUM AUS PUNKTWEISER EINGABE
      16 NN = 2
      DC 22 I = 1,IKK
      DC 18 N = NN,NS
      M = N
      IF(MZ(1).NE.0) M = M+(L-1)*NL/(NLE+1)
      IF(E(N)-EN(I)) 18,19,20
      18 CCNTINUE
      N = NS
      19 G(I) = S(M)
      NN = N
      GOTO 22
      20 G(I) = S(M-1)+(S(M)-S(M-1))/(E(N)-E(N-1))*(E(I)-F(N-1))
      IF(N.GT.2) NN = N-1
      22 CCNTINUE
C
C***** INTERVALLINTEGRALE OHNE MIKROGEWICHTUNG
      24 WER = 0.
      IF(NTT.GT.1) GOTO 28

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      IK = IKK-1
      DO 26 I = 1,IK
      C1 = H(I+1)-H(I)
      S1 = H(I+1)+H(I)
      D2 = G(I+1)-G(I)

      S2 = G(I+1)+G(I)
      CF = EN(I+1)-EN(I)
26  WER = WER+(D1*D2/3.+S1*S2)*DE
      VAL = .25*WER
      RETURN
C
C***** INTERVALL INTEGRALE MIT MIKROWICHTUNG
28 DC 27 M = 2,NTT
      IF(ET(M)-EN(I)) 27,27,29
27 CONTINUE
      M = NTT
29 IK = IKK-1
      DC 54 I = 1,IK
      N = M
      IF(I.GT.1) GOTO 32
      STE = ST(N)+(EN(I)-ET(N))*(ST(N)-ST(N-1))/(ET(N)-ET(N-1))
      IF(NTT.EQ.2) GOTO 35
      DC 30 N = 2,NTT
      IF(ET(N)-EN(I)) 30,30,32
30 CONTINUE
      N = NTT
32 DO 34 M = N,NTT
      IF(ET(M)-EN(I+1)) 34,35,35
34 CONTINUE
      M = NTT
35 STA = STE
      STE = ST(M)+(EN(I+1)-ET(M))*(ST(M-1)-ST(M))/(ET(M-1)-ET(M))
      DE = EN(I+1)-EN(I)
      TH = (H(I+1)-t(I))/DE
      AH = H(I)-TH*EN(I)
      TG = (G(I+1)-G(I))/DE
      AG = G(I)-TG*EN(I)
      IF(MZ(2).EQ.0) GOTO 36
      IF(L.GT.2) GOTO 48
      GOTO(36,42),L
C***** 0. MOMENT
36 IF(M.GT.N) GOTO 38
      D1 = H(I+1)-H(I)
      S1 = H(I+1)+H(I)
      D2 = G(I+1)-G(I)
      S2 = G(I+1)+G(I)
      U = 1./STA
      V = 1./STE
      C3 = V-U
      S3 = V+U
      W = WW(D1,D2,D3,S1,S2,S3)*DE
      GOTO 54
28 U = H(I)
      V = TH*ET(N)+AH
      D1 = V-U

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      S1 = V+U
      U = G(I)
      V = TG*ET(N)+AG
      C2 = V-U
      S2 = V+U
      U = 1./STA
      V = 1./ST(N)
      C3 = V-U
      S3 = V+U
      CE = ET(N)-EN(I)
      W = WW(D1,D2,D3,S1,S2,S3)*DE
      MM = M-1
      U = TH*ET(M)+AH
      V = H(I+1)
      C1 = V-U
      S1 = V+U
      U = TG*ET(M)+AG
      V = G(I+1)
      D2 = V-U
      S2 = V+U
      U = 1./ST(MM)
      V = 1./STE
      C3 = V-U
      S3 = V+U
      CF = EN(I+1)-ET(MM)
      W = WW(D1,D2,D3,S1,S2,S3)*DE
      IF(N.EQ.MM) GOTO 54
      MM = M-2
      VH = TH*ET(N)+AH
      VG = TG*ET(N)+AG
      VS = 1./ST(N)
      DO 40 J = N,MM
      JP = J+1
      LH = VH
      UG = VG
      US = VS
      VH = TH*ET(JP)+AH
      VG = TG*ET(JP)+AG
      VS = 1./ST(JP)
      D1 = VH-UH
      S1 = VH+UH
      D2 = VG-UG
      S2 = VG+UG
      D3 = VS-US
      S3 = VS+US
      DE = ET(JP)-ET(J)
40 W = WW(D1,D2,D3,S1,S2,S3)*DE
      GOTO 54
C***** 1. MOMENT
42 IF(M.GT.N) GOTO 44
      C1 = H(I+1)-H(I)
      S1 = H(I+1)+H(I)
      C2 = G(I+1)-G(I)
      S2 = G(I+1)+G(I)
      U = 1./(STA*STA)

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V = 1./ (STF*STF)
C3 = V-I
S2 = V+U
W = WW(D1,D2,D3,S1,S2,S3)*DE
GOTO 54
44 U = H(I)
V = TH*ET(N)+AH
D1 = V-U
S1 = V+U
L = G(I)
V = TG*ET(N)+AG
D2 = V-U
S2 = V+U
U = 1./ (STA*STA)
V = 1./ (ST(N)*ST(N))
E3 = V-U
S3 = V+U
DE = ET(N)-EN(I)
W = WW(D1,D2,D3,S1,S2,S3)*DE
MM = M-1
U = TH*ET(MM)+AH
V = H(I+1)
D1 = V-U
S1 = V+U
U = TG*ET(MM)+AG
V = G(I+1)
C2 = V-U
S2 = V+U
U = 1./ (ST(MM)*ST(MM))
V = 1./ (STE*STE)
D3 = V-U
S3 = V+U
DE = FN(I+1)-ET(MM)
W = W+WW(D1,D2,D3,S1,S2,S3)*DE
IF(N.EQ.MM) GOTO 54
MM = M-2
VH = TH*ET(N)+AH
VG = TG*ET(N)+AG
VS = 1./ (ST(N)*ST(N))
DC 46 J = N,MM
JP = J+1
LH = VH
UG = VG
LS = VS
VH = TH*ET(JP)+AH
VG = TG*ET(JP)+AG
VS = 1./ (ST(N)*ST(N))
C1 = VH-UH
S1 = VH+UH
D2 = VG-UG
S2 = VG+UG
D2 = VS-US
S3 = VS+US
DE = ET(JP)-ET(J)
46 W = W+WW(D1,D2,D3,S1,S2,S3)*DE

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GOTO 54
C***** 2. UND HOEHERE MOMENTE
48 IF(M.GT.N) GOTO 50
D1 = H(I+1)-H(I)
S1 = H(I+1)+H(I)
C2 = G(I+1)-G(I)
S2 = G(I+1)+G(I)
U = 1./STA**L
V = 1./STE**L
C3 = V-U
S3 = V+U
W = WW(D1,D2,D3,S1,S2,S3)*DE
GOTO 54
50 U = H(I)
V = TH*ET(N)+AH
C1 = V-U
S1 = V+U
U = G(I)
V = TG*ET(N)+AG
C2 = V-U
S2 = V+U
U = 1./STA**L
V = 1./ST(N)**L
D3 = V-U
S3 = V+U
DE = ET(N)-EN(I)
W = WW(D1,D2,D3,S1,S2,S3)*DE
MM = M-1
U = TH*ET(MM)+AH
V = H(I+1)
D1 = V-U
S1 = V+U
U = TG*ET(MM)+AG
V = G(I+1)
C2 = V-U
S2 = V+U
U = 1./ST(MM)**L
V = 1./STE**L
D3 = V-U
S3 = V+U
DE = EN(I+1)-ET(MM)
W = W+WW(D1,D2,D3,S1,S2,S3)*DE
IF(N.EQ.MM) GOTO 54
MM = M-2
VH = TH*ET(N)+AH
VG = TG*ET(N)+AG
VS = 1./ST(N)**L
DC 52 J = N,MM
JP = J+1
LH = VH
UG = VG
LS = VS
VH = TH*ET(JP)+AH
VG = TG*ET(JP)+AG
VS = 1./ST(JP)**L

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D1 = VH-UH'
S1 = VH+UH
D2 = VG-UG
S2 = VG+UG
D3 = VS-US
S3 = VS+US
DE = ET(JP)-ET(J)
52 W = W+WW(D1,D2,D3,S1,S2,S3)*DE
54 WER = WER+W
VAL = .125*WER
C
RETURN
C
ENC

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SUBROUTINE MUKON(ELSIG,ELTOT,NLE,NECU,NUEB,IL,IP,NGR,MASSE) 10
C*****MULTIGRUPPENKONSTANTEN***** 20
C 30
C DIMENSION ELSIG(6,NECU,NGR),ELTOT(2,NGR) 40
C 50
C NP = NLE+1 60
C*****TOTALER STREUQUERSCHNITT***** 70
C 80
C DO 14 NN = IL,IP 90
C STO = C. 100
C DO 12 NS = 1,NUEB 110
C NT = NS+NN-1 120
C STO = STO+ELSIG(1,NS,NN) 130
C IF(NT.EQ.IM) GOTO 14 140
C 12 CONTINUE 150
C 14 ELTOT(1,NN) = STO 160
C *****NORMIERUNG AUF DEN TOTALEN STREUQUERSCHNITT***** 170
C 180
C 22 DO 26 L = 1,NP 190
C DO 26 NN=IL,IP 200
C DO 24 I = 1,NUEB 210
C NT=I+NN-1 220
C FLSIG(L,I,NN) = ELSIG(L,I,NN)/ELTOT(1,NN) 230
C IF(NT.EQ.IM) GO TO 26 240
C 24 CONTINUE 250
C 26 CONTINUE 260
C *****MITTLERER STREUKOSINUS***** 270
C 280
C 15 DO 20 NN = IL,IP 290
C STO = C. 300
C DO 18 NS = 1,NUEB 310
C NT = NS+NN-1 320
C STO = STO+ELSIG(2,NS,NN) 330
C IF(NT.EQ.IM) GOTO 20 340
C 18 CONTINUE 350
C 20 ELTOT(2,NN) = STO 360
C 37C

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C*****ABSCHNEIDEN (NULLSETZEN) VON GROESSEN KLEINER 1.E-6 ***** 380
IF(MASSE.EQ.1) RETURN 390
DO 40 L = 1,NP 400
CC 40 NN=IL,IP 410
DC 38 I = 1,NUEB 420
NT=I+NN-1 430
ELSIG(L,I,NN) = AINT(ELSIG(L,I,NN)*1.E+5)*1.E-5 440
IF(NT.EQ.IM) GO TO 40 450
38 CCNTINUE 460
40 CCNTINUE 470
C RETURN 480
C 490
C 500
C 510

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SUBROUTINE PRINT(ELSIG,ELTOT,NLA,NLE,NECU,NUEB,ISEL,NGR,KSPFK, 10
- MAZ,NTK,KIM,NCT,SGTOT,RSP,MASSE,NGS) 20
C 30
C*****SUBROUTINE ZUM AUSDRUCKEN DER STREUMATRIX,DER STREUKOSINUSMATRIX** 40
C 50
C REAL*8 STOFF,MMM 60
C DIMENSION ELSIG(6,NECU,NGR),ELTOT(2,NGR),MAZ(2),SGTOT(6,NGR), 70
- RSP(6,NGR) 80
C COMMON STOFF,ISTRUK,ISPA,NOUT,KPR,NEND,NANF 90
C NP = NLE+1 100
C 110
C 120
C*****AUSDRUCKEN DER STREUMATRIZEN***** 130
C 140
C DO 3 L = 1,NP 150
C LP = L-1 160
C WRITE(NOUT,21) LM,LM,STOFF 170
C IF(IABS(ISEL).EQ.1) WRITE(NOUT,28) NGS 180
C I1 = NANF 190
C I2 = I1+MINO(9,NEND-I1) 200
C WRITE(NOUT,24) (I,I = I1,I2) 210
C WRITE(NOUT,19) 220
C DO 2 I = 1,NUEB 230
C I3=MINO(I2,NEND+KIM-I+1) 240
C IF(I3.LT.I1) GO TO 2 250
C WRITE(NOUT,22) (ELSIG(L,I,NN),NN=I1,I3) 260
C 2 CCNTINUE 270
C WRITE(NOUT,20) 280
C IF(I2.GE.NEND) GOTO 3 290
C I1 = I2+1 300
C GOTO 1 310
C 3 CCNTINUE 320
C WRITE(NOUT,52) 330
C *****INFORMATIONEN UEBER DIE WICHTUNG***** 340
C 350
C IF(KSPEK.GT.0.AND.MAZ(1).EQ.0)WRITE(NOUT,32) 360
C IF(KSPEK.GT.0.AND.MAZ(1).EQ.1)WRITE(NOUT,34) ALF 370

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IF(KSPEK.EQ.0.AND.MAZ(1).EQ.0)WRITE(NOUT,36)
IF(KSPEK.EQ.0.AND.MAZ(1).EQ.1)WRITE(NOUT,38)
WRITE(NOUT,40)
IF(NTK.EQ.1.AND.MAZ(2).EQ.0)WRITE(NOUT,42)
IF(NTK.EQ.1.AND.MAZ(2).EQ.1)WRITE(NOUT,44) NLE
IF(NTK.EQ.0) WRITE(NOUT,46)
WRITE(NOUT,47)
C
C*****AUSDRUCKEN DER TOTALEN ELAST. QUERSCHNITTE UND STREUKOSINUS
WRITE(NOUT,27) STOFF
IF(MASSE.EQ.1) WRITE(NOUT,29)
IF(IABS(ISEL).EQ.1) WRITE(NOUT,28) NGS
I1 = NANF
9 I2 = I1+MINO(9,NEND-I1)
WRITE(NOUT,24) (I,I = I1,I2)
WRITE(NOUT,19)
DC 10 I = 1,2
10 WRITE(NOUT,25) (ELTOT(I,NN),NN = I1,I2)
WRITE(NOUT,20)
IF(I2.GE.NEND) GOTO 11
I1 = I2+1
GOTO 9
11 WRITE(NOUT,54)
C
C*****AUSDRUCKEN DER TOTALEN QUERSCHNITTE*****
IF(NGT.EQ.0) GOTO 15
WRITE(NOUT,48) STOFF
IF(IABS(ISEL).EQ.1) WRITE(NOUT,28) NGS
I1 = NANF
12 I2 = I1+MINO(9,NEND-I1)
WRITE(NOUT,24) (I,I = I1,I2)
WRITE(NOUT,19)
DC 13 L = 1,NP
13 WRITE(NOUT,25) (SGTOT(L,NN),NN=I1,I2)
WRITE(NOUT,20)
IF(I2.GE.NEND) GOTO 14
I1 = I2+1
GOTO 12
14 WRITE(NOUT,50)
C
C*****AUSDRUCKEN DER NORMIERUNGSINTEGRAL*****
15 WRITE(NOUT,66) NLE
I1 = NANF
16 I2 = I1+MINO(9,NEND-I1)
WRITE(NOUT,24) (I,I = I1,I2)
WRITE(NOUT,19)
DC 17 L = 1,NP
17 WRITE(NOUT,25) (RSP(L,NN),NN=I1,I2)
WRITE(NOUT,20)
IF(I2.GE.NEND) GOTO 23
I1 = I2+1
GOTO 16
23 WRITE(NOUT,68)
C
C*****RESERVIEREN DER RESULTATE*****

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CALL DOPW(8HF LUM ,MMM)
I=C
WRITE (KPR) I,MMM
I1=NANF
I2=NEND
I=4
L=NLE-NLA+1
NA=I2-I1+1
WRITE (KPR) I,STOFF,NA,L
I=3+L
CC 31 NN=I1,I2
WRITE (KPR) I,NN,ELTOT(I,NN),ELTOT(I2,NA),(SGTOT(K,NN),K=1,L)
31 CCNTINUE
DC 33 L = 1,NP
LM=L-1
DC 33 NN=I1,I2
LL=MINO(NUER,I2+KIM-NA+1)
I=LL+2
WRITE (KPR) I,LM,NA,(ELSIG(L,K,NN),K=1,LL)
33 CCNTINUE
C
RETURN
C
19 FCFMAT(IH)
20 FORMAT(IH0)
21 FCFMAT(IH0//29X,'SGNC',I1,8X,'ELASTISCHE STRELMATRIX ',I1,'. ORDN
IUNG FUER ',A8//)
22 FORMAT(1X,10E13.5)
24 FCFMAT(1X,1)(I6,'.GRUPPE')
25 FORMAT(1X,1P10E13.5)
27 FCFMAT(IH0//20X,'TOTALE ELASTISCHE GRUPPENSTREUQUERSCHNITTE SGN UN
ID GRUPPENSTREUKOSINUS MUFL FUER ',A8//)
28 FORMAT(42X,'SGN(E) = SGT(E) = 1 GESETZT AB GRUPPE',I4//)
29 FCFMAT(20X,'** REI WASSERSTOFF WIRD UNTERFALB 10 FV DIE STREUUNG I
1M SCHWERPUNKTSYSTEM ISOTROP ANGENOMMEN'/20X,'** UND FS WIRD DER MI
3TTLERE STREUKOSINUS IM LABCRSYSTEM GLEICH 0.6667GESETZT **'//)
30 FORMAT(///42X,'M A K R C W I C H T U N G F //)
32 FORMAT(42X,'ALLE MOMENTE WIE DAS 0. MOMENT MIT DEM'//
1 42X,'EINGELESENEN PUNKTSPEKTRUM F(E,1)')
34 FORMAT(42X,'DAS L-TE MOMENT MIT DEM (L+1)-TEN EINGE-'//
1 42X,'LESENEN PUNKTSPEKTRUM F(E,L+1), L = 0,1,...,I2)
36 FORMAT(42X,'ALLE MOMENTE WIE DAS 0. MOMENT MIT'//
1 42X,'F(E,1) (STANDARD F(E,1) = 1/E)')
38 FORMAT(42X,'DAS L-TE MOMENT MIT F(E,1)'/
1 42X,'(STANDARD F(E,1) = 1/E)')
40 FCFMAT(///42X,'M I K R C W I C H T U N G FS (FFINSTRUKTUR)')
42 FORMAT(42X,'ALLE MOMENTE WIE DAS 0. MOMENT MIT FS(E,L)=1/SGT(E)'/
1 42X,'SGT(E)=TOTALER QUERSCHNITT DER EINGELESENEN MISCHEUNG')
44 FORMAT(42X,'DAS L-TE MOMENT MIT FS(E,L+1), L = 0,1,...,I2/'
1 42X,'(STANDARD FS(E,L)=1/SGT(E))*L')
46 FORMAT(42X,'ALLE MOMENTE MIT FS(E,1) = 1/'
1 42X,'(KEINE FEINSTRUKTURWICHTUNG)')
47 FORMAT(///42X,'G E S A M T W I C H T U N G F * FS')
48 FCFMAT(IH0//44X,'TOTALE GRUPPENQUERSCHNITTE SGT FUER ',A8//)

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B 122 -

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50 FORMAT(//29X,'ERLAEUTERUNG'/29X,'G-TE GRUPPE, L-TE ZFILE: TOTALER 1480
-QUERSCHNITT DER G-TEN GRUPPE,'/29X,'GEWICHTET WIE DAS (L-1)-TE MOM 1490
-ENT DER STREUMATRIX') 1500
52 FORMAT(//29X,'ERLAEUTERUNG'/29X,'L-TE CRDUNG, G-TE GRUPPE, I-TE Z 1510
LEILE: MATRIXELEMENT L-TER GRDUNG'/29X,'FUER STREUUNG AUS DER G-TE 1520
2N GRUPPE IN DIE (G+I-1)-TE GRUPPE, BEZOGEN'/29X,'AUF DEN TCTALEN E 1530
3LASTISCHEN QUERSCHNITT (TOTALES C.MOMENT) DER '/29X,'G-TEN GRUPPE') 1540
54 FCRMAT(//29X,'ERLAEUTERUNG'/29X,'G-TE GRUPPE, 1. ZEILE: TOTALER EL 1550
1ASTISCHER QUERSCHNITT DER G-TEN'/29X,'GRUPPE'/29X,'G-TE GRUPPE, 2. 1560
2 ZEILE: MITTLERER STREUKOSINUS DER G-TEN GRUPPE') 1570
66 FORMAT(////42X,'NORMIERUNGSINTEGRALE BIS ZUM',I3,'. MOMENT'//) 1580
68 FCRMAT(//29X,'ERLAEUTERUNG'/29X,'G-TE GRUPPE, L-TE ZEILE: (L-1)-TE 1590
-S MOMENT DES WICHTUNGSSPEKTRUMS'/29X,'INTEGRIFERT UEBER DIE G-TE GR 1600
-UPPE') 1610
C END 1620
1630

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SUBROUTINE INFORM(ALFA,NEGR,ABN,R,IL,IM,INTT,INT,NST,NSTIS, 10
1 IR,ISTT,K,NTK,NTT,NOUT) 20
C *****INFORMATIONEN***** 30
C DIMENSION ABN(NEGR),R(NEGR),INT(NEGR),NST(6),NA(6),NB(6) 40
C IF(IR.GT.1) GOTO 6 50
WRITE(NOUT,919) 60
WRITE(NOUT,935) ALFA 70
CC 5 I = 1,6 80
NA(I) = I-1 90
NB(I) = NSTIS 100
WRITE(NOUT,936) (NA(I),I = 1,6),(NB(I),I = 1,6), 110
1 NST(I),I = 1,6) 120
6 IF(IR+1.LT.INTT) GOTO 7 130
WRITE(NOUT,932) 140
CC 4 I = IL,IM 150
4 WRITE(NOUT,933) I,ABN(I),ABN(I+1),R(I) 160
WRITE(NOUT,934) 170
7 I1 = INT(IR+1)+1 180
I2 = INT(IR)+1 190
IF(IR.EQ.1) I2 = I2-1 200
WRITE(NOUT,909) 210
EFIN = AMAX1(ALFA*ABN(I1),ABN(IM+1)) 220
WRITE(NOUT,920) IR,IR,ABN(I1),ABN(I2) 230
WRITE(NOUT,921) IR,EFIN,ABN(I2) 240
WRITE(NOUT,922) IR,ISTT 250
WRITE(NOUT,925) K 260
IF(NTK.EQ.1) WRITE(NOUT,126) NTT 270
RETURN 280
C 290
909 FCRMAT(1H0) 300
919 FCRMAT(1H0//24X,'I N F C R M A T I O N E N'//) 310
920 FCRMAT(1H0,I2,'. AUSSTREUINTERVALL = ',I2,'. MAXRCGRUPPE', 5X,E10. 320
4) 330

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14,' EV', ' - ',E10.4,' EV') 360
921 FORMAT(1H0,I2,'. EINSTREUINTERVALL',23X,E10.4,' EV', ' - ',E10.4, 370
1' EV') 380
922 FORMAT(1H0,'ZAHL DER ENERGIESTUETZPUNKTE IM ',I2,'. AUSSTREUINTERV 390
ALL',18X,I4) 400
925 FCRMAT(1H0,'ZAHL DER GELESENEN SCN IM AUSSTREUINTERVALL',28X,I4) 410
932 FORMAT(////16X,'F E I N G R U P P E N E I N T F I L U N G'//) 420
933 FCRMAT(1X,I3,'.GRUPPE',1X,1PE10.3,' EV -',1PE10.3,' EV',1X,'DU = 430
-',E9.2) 440
934 FCRMAT(////18X,'CU = LETHARGIFDIFFERENZ') 450
925 FCRMAT(1H0,'ALFA = ',F8.5) 460
936 FCRMAT(1H0,'WINKELSTUETZSTELLEN'//12X,'MOMENT',5X,6(3X,I3)/12X,'IS 470
1CTROPIE',3X,6(3X,I3)/12X,'ANISOTROPIE',1X,6(3X,I3)) 480
126 FCRMAT(1H0,'ZAHL DER SGT FUER FEINSTRUKTURWICHTUNG IM AUSSTREUINTE 490
IRVALL',11X,I5) 500
C ENC 510
520

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C BESTIMMUNG DER I/V - WERTE 10
C SUBROUTINE EDV (NE,ENG,NSP,E,F,EPS,V,NEF,ST,FI,IW) 20
REAL*8 MAT,MMM 30
DIMENSION ENG(NE),F(NSP),F(NSP),V(NE),ST(NEF),FI(NEF) 40
COMMON MAT,ISTRUK,ISPA,NOUTP,JA,NANF,NEND,KL 50
DATA MMM/'S1/V' '/' 60
WRITE(NOUTP,1) 70
1 FCRMAT(1H0/1H0/' EDV - A PROGRAM FOR THE CALCULATION OF THE I/V AV 80
IFRAGE GROUP VALUES'//) 90
IW=0 100
JF=0 110
C=7.229286F-7 120
L=NF-1 130
IF(NSP.GT.1) GC TO 9 140
150
C WICHTUNGSFUNKTION F(E) IST ALS FUNCTION GEGEBEN 160
C 170
NN=1 180
LI=L 190
36 DO 2 II=NN,LI 200
K=10 210
ER1=ENG(II) 220
ER2=FNG(II+1) 230
4 M=1 240
ST(M)=ER1 250
CC 3 J=1,K 260
M=M+1 270
IF(M.LE.NEF) GO TO 31 280
NEF=K+1 290
IW=1 300
CC TO 30 310
31 ST(M)=ER1*FLOAT(J)*(ER2-ER1)/FLOAT(K) 320
3 CONTINUE 330
340

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- B 123 -

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Z1=0.
XN1=0.
N=1
7 F11=PHI(ST(1))
DC 5 J=1,K
F12=PHI(ST(J+1))
Z1=Z1+0.5*(F11*C/SQRT(ST(J))+F12*C/SQRT(ST(J+1)))*(ST(J+1)-ST(J))
XN1=XN1+0.5*(F11+F12)*(ST(J+1)-ST(J))
5 F11=F12
IF(N.EQ.2) GC TC 6
Z2=Z1
XN2=XN1
Z1=0.
XN1=0.
A=2
GC TO 7
6 ABWZ=ABS(Z2-Z1)/Z1
ABWN=ABS(XN2-XN1)/XN1
IF(ABWZ.LE.EPS.AND.ABWN.LE.EPS) GC TC 8
K=K+K
GC TO 4
8 V(I+1)=Z1/XN1
2 CCNTINUE
IF(JF.EQ.1) GC TO 37
V(1)=0.8862269*C/SQRT(0.0253)
GO TO 26
C
C
C
WICHTUNGSFUNKTION IST PUNKTWEISE GEGEBEN
9 DC 10 I=1,L
JF=0
ST(1)=ENG(I)
DO 16 J=1,NSP
IF(E(J).LT.ST(1)) GO TO 16
IF(E(J).EQ.ST(1)) GO TO 17
IF(J.EQ.1) GO TO 38
F1(1)=F(J-1)+(F(J)-F(J-1))/(E(J)-E(J-1))*(ST(1)-E(J-1))
GO TO 18
16 CCNTINUE
38 JF=1
NA=I
LI=I
GC TO 36
37 J=NE-I
WRITE (NOUTP,25) J
35 FORMAT(1H0/' ***WARNING : IN ENERGYGROUP ',I5,' THE 1/V VALUE IS C
1ALCULATED WITH THE FUNCTION PHI(E)*/14X,
1'BECAUSE NO POINT OF SPECTRUM IS GIVEN IN THIS GROUP'/)
GC TO 10
17 F1(1)=F(J)
18 A=J-1
M=1
DC 11 J=N,NSP
IF(E(J).LT.ENG(I)) GC TC 11
IF(E(J).LE.ENG(I+1)) GC TO 12

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GO TO 13
12 M=M+1
IF(M.LE.NEF) GO TO 32
NEF=NSP
Iw=1
GO TO 30
32 ST(M)=E(J)
FI(M)=F(J)
GO TO 11
13 A=J-1
GO TO 14
11 CCNTINUE
GC TO 38
14 IF(ST(M).EQ.ENG(I+1)) GO TO 15
M=M+1
IF(M.LE.NEF) GC TO 33
NEF=NEF+1
Iw=1
GC TO 30
33 ST(M)=ENG(I+1)
FI(M)=F(J-1)+(F(J)-F(J-1))/(E(J)-E(J-1))*(ST(M)-E(J-1))
15 Z1=0.
XN1=0
K=1
23 MM=M-1
DC 19 J=1,MM
Z1=Z1+(C/SQRT(ST(J))*FI(J)+C/SQRT(ST(J+1))*FI(J+1))*(ST(J+1)-
IST(J))
19 XN1=XN1+(FI(J)+FI(J+1))*(ST(J+1)-ST(J))
IF(K.EQ.2) GC TO 20
25 Z2=Z1
XN2=XN1
Z1=0.
XN1=0.
K=2
IF(2*MM-1.LE.NEF) GC TC 34
NEF=M
Iw=1
GC TO 30
34 CC 21 J=1,M
MM=M-J
ST(MM*2+1)=ST(MM+1)
21 FI(MM*2+1)=FI(MM+1)
M=2*MM-1
DO 22 J=2,M,2
ST(J)=0.5*(ST(J-1)+ST(J+1))
22 FI(J)=0.5*(FI(J-1)+FI(J+1))
GO TO 23
20 ABWZ=ABS(Z2-Z1)/Z1
ABWN=ABS(XN2-XN1)/XN1
IF(ABWZ.LE.EPS.AND.ABWN.LE.EPS) GO TO 24
GC TO 25
24 V(I+1)=Z1/XN1
10 CCNTINUE
V(1)=0.8862269*C/SQRT(0.0253)

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C		1450	9000	FORMAT(1H0/1HC/' PROGRAMM KEANZIFFER 7')	110
C	AUSGABE DER ERGEBNISSE	1460		WRITE (NOUTP,9001)	120
C		1470	9001	FCRMT(' PROGRAMM ZUR BERECHNUNG DES SPALTSPEKTRUMS')	130
	26 I=0	1480		IF(ENG(NE).LT.10.E6) GO TO 35	140
	WRITE(JA)I,MMM	1490		Z=ENG(NF)	150
	WRITE (NOUTP,27)	1500		ENG(NF)=20.E6	160
	27 FORMAT(/' GRUPPE',7X,'1/V')	1510		WRITE(NOUTP,36)	170
	L=NE	1520	36	FCRMT(/' IN THIS MODULE THE HIGHEST ENERGY GRUOP BOUNCARY IS SET	180
	WRITE (JA) L,(V(I),I=1,L)	1530		IEQUAL TO 20.E6 EV')	190
	CC 28 I=1,L	1540	35	N=1	200
	K=L-I+1	1550		I=0	210
	28 WRITE (NOUTP,29)I,V(K)	1560		L=NE-NANF	220
	29 FCRMT(15,E17.8)	1570		IGRUP=NE-NEND	230
	KL=KL+1	1580		CALL DOPW (8HBEST ,NFEST(2))	240
	30 RETURN	1590		CALL DOPW (8HCHICR ,NFEST(3))	250
	END	1600		CALL DOPW (8HSPALT ,MMM)	260
				NSATZ(1)=3	270
				NFEST(1)=MAT	280
	SLBRoutine CHIIN(E1,E2,TETA,X2)	10		CALL NDFLOC (NSUCH,NSATZ,FEST,NUDAT,NC)	290
	WPI=1.772454	20		IF(NSUCH)6,6,7	300
	XX1=E1/TETA	30	6	IF(MAT.NE.MNAME) GC TC 19	310
	XX2=E2/TETA	40		TETA=9.9999999E-40	320
	XR1=SQRT(XX1)	50		E=9.9999999E-40	330
	XR2=SQRT(XX2)	60		GO TO 20	340
	IF(XX1.LT.1.0E-03.AND.XX2.LT.1.0E-03) GO TO 3	70	19	CALL DOPW (8HSEDF ,NFEST(2))	350
	IF(XX1.LT.1.317.AND.XX2.LT.1.317) GO TO 1	80		NSATZ(1)=4	360
	ERFSUM=ERFC(XR1)-ERFC(XR2)	90		FFEST(4)=C.	370
	GO TO 2	100		IT=0	380
	1 ERFSUM=ERF(XR2)-ERF(XR1)	110	45	CALL NDFLOC (NSUCH,NSATZ,FEST,NUDAT,NC)	390
	2 EXPSUM=XR2*EXP(-XX2)-XR1*EXP(-XX1)	120		IF(NSUCH)38,38,16	400
	X2=ERFSUM-EXPSUM*2.0/WPI	130	38	CALL NDFLOC (NSUCH,NSATZ,FEST,NUDAT,NC)	410
	GO TO 4	140		IF(NSUCH)15,15,16	420
	3 S1=(XR2*XX2-XR1*XX1)*2.C/3.C	150	15	WRITE (NOUTP,8) FEST(1)	430
	S2=(XR2*XX2**2-XR1*XX1**2)*2.0/5.0	160		8 FCRMT(' FUER DAS MATERIAL',A9,' GIBT ES KEIN SPALTSPEKTRUM')	440
	S3=(XR2*XX2**3-XR1*XX1**3)*2.0/7.0	170		GO TO 5	450
	S4=(XR2*XX2**4-XR1*XX1**4)*2.0/9.0	180	7	E=FEST(4)	460
	X2=(-S4+S3-S2+S1)*2.0/WPI	190		B=FEST(6)	470
	4 RETURN	200		C=FFEST(7)	480
	END	210		T=1./B	490
				EF= C/(4.*B*B)	500
	SLBRoutine SPALT(NE,ENG,X)	10		EW=DSQRT(EF/T)	510
		20		DC 9 K=L,IGRUP	520
	BERECHNUNG DES SPALTSPEKTRUMS	30		EG=DSQRT(ENG(K)/T)	530
	REAL*8 MAT,FEST(10),NFEST(10),MMM,MNAME	40		EG1=DSQRT(ENG(K+1)/T)	540
	REAL*8 E,B,C,T,EF,EW,EG,EG1,XG,XG1,YG,YG1,XG2,XG12,YG12	50		XG=EG1-EW	550
	DIMENSION ENG(NF),NADAT(2),NSATZ(4),X(NE)	60		XG1=EG-EW	560
	COMMON MAT,I STRUK,I SPA,NOUTP,JA,NANF,NEND,KL	70		YG=EG1+Ew	570
	EQUIVALENCE(FEST(1),NFEST(1))	80		YG1=EG+EW	580
	DATA MNAME/' /	90		XG2=XG*XG	590
	WRITE (NOUTP,9000)	100		YG2=YG*YG	600
				XG12=XG1*XG1	610
				YG12=YG1*YG1	620
				X(K)=0.2820947917738/EW*(DEXP(-XG12)-DEXP(-XG2)-DEXP(-YG12)	630
				1+DEXP(-YG2))-0.5*(DFRF(XG1)-DERF(XG)+CFRF(YG1)-CFRF(YG))	640
			5	CONTINUE	650

- B 125 -

IF(N.EQ.2) GO TO 10	660	WRITE (JA) NNN,(X(IJ),IJ=L,IGRUP)	1210
N=2	670	WRITE (NOUTP,30)	1220
IJ=0	680	30 FORMAT(//' MAXWELL SPEKTRUM')	1230
WRITE (JA) IJ,MMM	690	WRITE (NOUTP,31) MAT,E,TETA,K,J	1240
10 IJ=6	700	21 FORMAT(IHO,A9,' EINFALLENERGIE =',E16.8,' TETA =',E16.8,	1250
K=NE-L	710	1' VON GRUPPE',I3,' BIS',I3)	1260
J=NE-IGRUP	720	WRITE (NOUTP,14) I	1270
WRITE (JA) IJ,MAT,E,K,J	730	WRITE (NOUTP,13) (X(IJ),IJ=L,IGRUP)	1280
NNN=IGRUP+1-L	740	5 KL=KL+1	1290
WRITE (JA) NNN,(X(IJ),IJ=L,IGRUP)	750	ENG(NE)=Z	1300
WRITE (NOUTP,29)	760	RETURN	1310
25 FCRMAT(//' WATT - CRANBERG SPEKTRUM')	770	END	1320
WRITE (NOUTP,12) MAT,E,K,J	780		
12 FCRMAT(IHO,A9,' EINFALLENERGIE =',E16.8,' VCN GRUPPE',I3,' BIS'	790		
1, I3)	800		
WRITE(NOUTP,14) I	810		
14 FCRMAT(' CHI ',I1)	820		
I=I+1	830		
WRITE (NOUTP,13) (X(IJ),IJ=L,IGRUP)	840		
13 FORMAT(IH,7E16.8/(IX,7E16.8))	850		
CALL NDFNXT(NSUCH,NSATZ,FEST,NUDAT,NC)	860		
IF(NSUCH) 5,5,7	870		
16 F=FEST(5)*1.0001	880		
G=FEST(6)*1.0001	890		
IF(IT.EQ.0) E=FEST(4)	900		
IF(IFIX(F).EQ.2.AND. IFIX(G).EQ.1) GO TO 17	910		
CALL NDFNXT (NSUCH,NSATZ,FEST,NUDAT,NC)	920		
IF (NSUCH)39,35,16	930		
39 IF(FEST(4).GT.E) GO TO 38	940		
WRITE (NOUTP,37) FEST(1)	950		
37 FCRMAT(' MATERIAL ',A10,' : DIE BEDINGLNGEN ZUR BERECHNUNG EINES S	960		
IPALTSPEKTRUMS (K=2, P=1) SINCE NICHT ERRECHT')	970		
GO TO 5	980		
17 IF(FEST(4)-1.6505)22,22,23	990		
23 IF(IT.EQ.0) GO TO 22	1000		
TETA2=FEST(7)	1010		
TETA=TETA1+(TETA2-TETA1)/(FEST(4)-E)*(1.6505-E)	1020		
E=1.6505	1030		
GO TO 20	1040		
22 TETA1=FEST(7)	1050		
E=FEST(4)	1060		
IT=1	1070		
IF(E-1.6505)21,18,18	1080		
21 FEST(4)=FEST(4)*1.0001	1090		
GO TO 45	1100		
18 TETA=TETA1	1110		
20 CC 28 K=L,IGRUP	1120		
28 CALL CHINM (ENG(K),ENG(K+1),TETA,X(K))	1130		
IJ=0	1140		
WRITE (JA) IJ,MMM	1150		
IJ=6	1160		
K=NE-L	1170		
J=NE-IGRUP	1180		
WRITE (JA) IJ,MAT,E,K,J	1190		
NNN=IGRUP+1-L	1200		

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SUBROUTINE REMO(NG,ABN,NSP,F,E,FRR,NLA,NLE,NGRE,NFG,NFI,NJM,NUJM,
IISEL,IWORK,WORK,L)
C
C SUBROUTINE MODIFIED BY BROEDERS,INR JUNE,1975
C
C CONTROL VARIABLES IN THE FIRST 36 WORDS OF THE WORKING FIELD
C WORD MEANING
C 1 ADDRESS OF ENERGY POINTS OF ANGULAR DISTRIBUTION (FA)
C 2 ADDRESS OF ANGLE MESH POINTS OF ANGULAR DISTRIBUTION (XL)
C 3 ADDRESS OF ANGULAR DISTRIBUTIONS (SGNC)
C 4 IG NUMBER OF THE ACTUALLY CALCULATED GROUP
C
-----EXTENSION BY BROEDERS-----
C
C THE LENGTH OF THE WORKING AREAS OF WORD (5-7) IS ENLARGED
C IN CPDR TO CALCULATE FROM KEDAK-DATA WITH DIFFERENT ENERGY-POINTS
C FOR DIFFERENT DATA-TYPES.
C NOW THE LENGTH OF THESE ARRAYS IS 3*MAX OF WORD 36
C 5 ADDRESS OF ELASTIC SCATTERING OR TOTAL CROSS-SECTIONS (SGN)
C 6 ADDRESS OF AVERAGE COSINES (AMU)
C 7 ADDRESS OF ENERGIE MESH POINTS FOR CROSS-SECTIONS (FS)
C
-----
C 8 ISEL (SEE INPUT DESC.) OR E THE ACTUAL ENERGY
C 9 ADDRESS OF AN ACTUAL ANGULAR DISTRIBUTION (SG)
C 10 ADDRESS OF AUX. ARRAY IN WAHRS FOR ROMBERG INTEGRATION (TF)
C 11 ADDRESS OF AUX. ARRAY IN LMI FOR ROMBERG INTEGRATION (PER)
C 12 ADDRESS OF RESULT STORAGE (SP)
C 13 ADDRESS OF A BUFFER STORAGE (BUF)
C 14 NG NUMBER OF GROUPS
C 15 NSP NUMBER OF SPECTRUM POINTS
C 16 NLA THE LOWEST LEGENDRE MOMENT
C 17 NLE THE HIGHEST LEGENDRE MOMENT
C 18 IMAX MAXIMUM GROUPCHANGE+1
C 19 NJM+1 (SEE INPUT DESC.)
C 20 NUJM (SEE INPUT DESC.)
C 21 ICOS NUMBER OF MESHPOINTS OF ANGULAR DISTRIBUTION
C 22 ADDRESS OF ACTUALLY FREE PLACE FOR RESULTS
C 23 KJ CONTROL NUMBER FOR ANISOTROPIE
C 24 NJ CONTROL NUMBER IN ANGLE INTEGRATION
C 25 NDAT NUMBER OF CROSS-SECTION POINTS IN AN ENERGY INTERVAL
C 26 NIV NUMBER OF ANGULAR DISTRIBUTION
C 27 ERR ERROR FOR ROMBERG INTEGRATION
C 28 AM ATOMIC MASS
C 29 QM=((AM+1)/(AM-1))**2
C 30 XM=(AM+1)**2/2/AM
C 31 QM=ALOG(QM)
C 32 Q=-0.1
C 34 ADDRESS OF A WORKING FIELD FOR ANGLE INTEGRATION
C
-----EXTENSION BY BROEDERS-----
C
C 33 FIRST FREE WORD IN IWORK. FOR THIS VERSION ENLARGED TO 37.
C 35 ADDRESS OF DOUBLE PRECISION ARRAY FOR COARSE-GROUP-WISE

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C
C 36 ENERGY-INTERVAL-BOUNDARIES.
C NMAX, THE MAXIMUM NUMBER OF DATAPOINTS PRO COARSE ENERGY GROUP
C FOR ONE OF THE FOLLOWING DATA-TYPES
C SGT,SGN OR MUEL.
C
-----
C
C DIMENSION IWORK(1),WORK(1),KDAT(3)
C REAL*8 FNEV(4)
C RFAL*8 NHID/'H HI'/'
C REAL*8 REM/'REMO'/'
C DATA NZKBY/2048/
C REAL*8 MATN
C DIMENSION ABN(1),F(1),F(1),NFG(1),NFI(1)
C COMMON MATN,IQQ(2),NOUT,LI,M1,M2,KLL
C EQUIVALENCE(N7,N8)
C EQUIVALENCE(N3,N4)
C DATA FNEV/'SGNC ','SGT ','SGN ','MUEL'/'
C KLL=KLL+1
C WRITE (NOUT ,9000)
9000 FORMAT(1H0/1H0/' PROGRAMM KFNNZIFFER 9')
C WRITE (NOUT ,9001)
9001 FORMAT(' PROGRAMM ZUR BERECHNUNG DER ELASTISCHEN STREUMATRIZEN FUE
IR DIE REMO-KORREKTUR'/)
C DO 1 I=1,L
1 IWORK(I)=0
C IWORK(33)=37
C MC=IWORK(33)+2+2*NJM
C MP=MO+NG+1
C TF(MM-(MM/2)+2,EG,0)MP=MM+1
C IWORK(34)=MM
C IWORK(8)=ISEL
C IWORK(14)=NG
C IWORK(15)=NSP
C IWORK(16)=NLA
C IWORK(17)=NLE
C IWORK(19)=NJM+1
C IWORK(20)=NUJM
C WORK(27)=ERR
C WORK(32)=-0.1
C DO 30 I=1,NG
C I1=NG-I+1
30 WORK(MO+I1-1)=ABN(I)
C WCRK(MO+NG)=0.
C CALL MASSIN(WORK,WORK(MO))
C IMAX=IWORK(18)
C MP=MM+(NLE+1)*IMAX*2
C IWORK(35)=MM
C NFI=MFI(M2)
C NFGM=NFG(M2)
C DO 31 I=M2,M1
C IG=M1+M2-I
C NFI=MAXO(NFI(IG),NFI(M))
C NFGM=MAXO(NFG(IG),NFG(M))
31 NC=IWORK(35)+2*(NFI*MNFGM+1)
C IWORK(1)=NO

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IF (MATN.EQ.NHID)GOTO 3	1120	IF (KDAT (J), LT. NDAT) KDAT (J) =NDAT	1670
CALL NIVNUM (MATN, FNEV (1), NIV, WORK (MO+M2-1), WORK (MO+M1), FNW,	1130	GOTO 6	1680
1.63, 63, 63)	1140	WRITE (NOUT, 71) MATN, FNEV (J+1)	1690
NIV=NIV+2	1150	71 FORMAT (' ***ERROR 9.5 : FOR ', A8, ' THERE IS NO ', A8)	1700
GOTO 4	1160	6 CCAT INUE	1710
3 NIV=0	1170	NMAX=MAXO (KDAT (1), KDAT (2), KDAT (3)) *3	1720
ICOS=0	1180	IWORK (36) =NMAX/3	1730
N2=NO	1190	NTCT=KDAT (1) +KCAT (2) +KDAT (3)	1740
N2=NO	1200	N5=N4+2*NMAX	1750
N4=NO	1210	N6=N5+2*NMAX	1760
IS=M2-1	1220	IMAX=IWORK (18)	1770
LMA=NO	1230	7 N7=N6+NMAX	1780
WRITE (NOUT, 74) MATN, FNEV (1)	1240	N9=N8+ICOS	1790
74 FORMAT (///' FOR MATERIAL', A10, ', TYPE', A10, ' NO KEDAK-DATA HAS B	1250	N10=N9+IMAX*VUJM*(VLE+1)	1800
FEN USED.')	1260	N11=IMAX(NLE+1)+N10	1810
4 IWCRC (26) =NIV	1270	N11=N11+1+IMAX	1820
N1=NO+NIV	1280	IWORK (6) =N5	1830
IWORK (2) =N1	1290	IWORK (7) =N6	1840
IF (NIV.EQ.0)GOTO 5	1300	IWORK (9) =N8	1850
NW=1	1310	IWORK (10) =N9	1860
CALL DATNUM (MATN, FNEV (1), ICOS, NW, 1.0, -1.0, 63, 63, 63)	1320	IWORK (11) =N10	1870
LM=N1+ICOS	1330	IWORK (12) =N11	1880
IF (LM.GT.L)GOTO 20	1340	NZM=1	1890
IF (FNW.GE.WORK (MO+M2-1))GOTO 3	1350	DO 9 I=M2, M1	1900
IS=IC SOP (FNW, WORK (MO))	1360	NZ=NFG (I) *NFI (I)	1910
IF (FNW.EQ.WORK (MO+IS-1)) IS=IS-1	1370	NZM=MAXO (NZM, NZ)	1920
N2=N1+ICOS*2	1380	9 CONTINUE	1930
N3=N2+ICOS*NIV	1390	IZV=IMAX*(NLE+1)	1940
L1=N3+NIV	1400	IZV=MAXO (4, IZV)	1950
L2=L1+ICOS	1410	IWORK (13) =N11+NZM*IZV	1960
LH=L2+ICOS*NIV	1420	JJ=2+IMAX*NZM	1970
LMA=LM	1430	JJ=MAXO (JJ, NTOT)	1980
IF (M1.LT.IS) IS=M1	1440	LM=IWORK (13) +JJ	1990
IF (LM.GT.L)GOTO 20	1450	20 CONTINUE	2000
CALL KEDLEC (MATN, FNEV (1), NIV, WORK (NO), IWORK (N3), WORK (MO+M2-1),	1460	LREST=L-MAXO (LM, LMA)	2010
IWORK (NO+IS),	1470	LRESTA=4*ABS (LREST) /NZKBY*2	2020
IWORK (N1), WORK (L1), WORK (L2), WORK (N2), 1.0, -1.0, 63, 63, 63)	1480	IF (LREST.GE.0)GOTO 21	2030
IWCRC (26) =NIV	1490	LRESTA=LRESTA+2	2040
WRITE (NOUT, 73) MATN, FNEV (1), NIV, ICOS, IS	1500	WRITE (NOUT, 70) LM, L, LRFSTA	2050
73 FORMAT (///' FOR MATERIAL', A10, ', TYPE', A10, ' THERE ARE', I6,	1510	70 FORMAT (' ***ERROR 9.1 : REGION.G TOO SMALL', /	2060
*' ANGULAR DISTRIBUTIONS WITH', I6, ' ANGLE POINTS RETRIEVED FOR TH	1520	*' *** REQUIRED NUMBER OF WORDS', I10, /	2070
*IS TASK.', /' THE LOWEST CALCULATED ENERGY GROUP NUMBER WITH SGNC I	1530	*' *** AVAILABLE NUMBER OF WORDS', I9, /	2080
*S', I3, ', ')	1540	*' *** PLEASE INCREASE REGION.G WITH AT LEAST', I10, ' K BYTES.')	2090
5 CONTINUE	1550	RETURN	2100
IWORK (21) =ICOS	1560	21 WRITE (NOUT, 72) LRESTA	2110
IWORK (3) =N2	1570	72 FORMAT (///' IN MODULE 9', I10, ' K BYTES OF REGION.G NOT USED.', //	2120
IWORK (5) =N4	1580	*/)	2130
KCAT (1) =1	1590	NG=0	2140
KDAT (2) =1	1600	WRITE (LI) NQ, REM	2150
KCAT (3) =1	1610	NQ=4	2160
DO 6 I=M2, M1	1620	N11=NLE-NLA+1	2170
IGR=MO+I-1	1630	WRITE (LI) NQ, MATN, NG, N11	2180
DC 6 J=1, 3	1640	CALL REMP (WORK (MO), NFG, NFI, F, F, WORK, IWORK, IS)	2190
CALL DATNUM (MATN, FNEV (J+1), NDAT, NW, WORK (IGR), WCRK (IGR+1),	1650	RETURN	2200
1.610, 610, 610)	1660	END	2210

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SUBROUTINE ENERG(NFG,NFI,EM,EP,E)
C
C SUBROUTINE ADDED BY BROEDERS,INR   JUNE,1975
C
REAL*8 E(1),DE,CDE,ER1,ER2,EF1,EF2,EDE1
IP=0
DE=DBLOG(DBLE(EP/EM))/DFLOAT(NFG)
EDE1=DEXP(DE)
ER1=DBLE(EM)
DC 2 I=1,NFG
ER2=ER1*EDE1
CDE=(ER2-ER1)/DFLOAT(NFI)
EF1=ER1
DO 1 J=1,NFI
EF2=EF1*DEXP(CDE)
EF2=EF1+CDE
E(IP+1)=EF1
IP=IP+1
1 EF1=EF2
2 ER1=ER2
E(IP+1)=ER2
RETURN
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SUBROUTINE KEDAT(NAMIZ,NAMTYP,NW,NWI,FNW,NDAT,FA,FF,EP,EM,*,*,*)
C
C SUBROUTINE MODIFIED BY BROEDERS,INR   JUNE,1975
C
REAL*8 FM(6),NAMIZ,NAMTYP,NGAC,NGIZ,NISO
DIMENSION EA(1),IEA(1),FA(1),FF(1),FAW(1),FFW(1),NWORT(4),NDT(2)
COMMON MATN(4),NCUT
DATA FM(2)/'BEST'/'',KERST/0/ ,NGAC/'SGNC'/'',NGIZ/'SGIZ'/'
1,'TSC'/'ISOT1'/'
KK=1
IF(NAMTYP.EQ.NGAC.OR.NAMTYP.EQ.NGIZ)KK=2
GOTO 1
ENTRY DATNUM(NAMIZ,NAMTYP,NDAT,NW,EP,EM,*,*,*)
KK=3
IF(NAMTYP.EQ.NGAC.OR.NAMTYP.EQ.NGIZ)KK=4
GOTO 1
ENTRY KEDLEC(NAMIZ,NAMTYP,NWI,EA,IEA,EPW,EMW,FA,FF,FAW,FFW,EP,EM,
1,*,*,*)
KK=5
NW=0
GOTO 1
ENTRY NIVNUM(NAMIZ,NAMTYP,NWI,EPW,EMW,FFR,*,*,*)
NW=0
KK=6
1 CONTINUE
IF(KERST.NE.0)GOTO 20
L=1
KERST=1

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20 FM(1)=NAMIZ
FM(3)=NAMTYP
GOTO (2,3,2,3,3,3),KK
2 CONTINUE
NWORT(1)=3
LL=0
CALL NDFLOC(NT,NWORT,FM,N1,N2)
IF(NT.EQ.0)RETURN 1
NCAT=1
IF(FM(4+LL).LE.EM)GOTO 21
IF(KK.EQ.3)GOTO 40
FA(1)=EM
FF(1)=FM(5+LL)
40 CONTINUE
NCAT=2
21 CONTINUE
IF(KK.EQ.3)GOTO 8
FA(NDAT)=FM(4+LL)
FF(NDAT)=FM(5+LL)
8 NDAT=NDAT+1
CALL NDFNXT(NT,NWORT,FM,N1,N2)
IF(NT.EQ.0)GOTO 5
IF(FM(4+LL).LE.EM)NDAT=1
IF(KK.EQ.3)GOTO 41
FA(NDAT)=FM(4+LL)
FF(NDAT)=FM(5+LL)
41 CONTINUE
IF(FM(4+LL).GE.EP)GOTO 30
GOTO 8
30 CONTINUE
IF(KK.EQ.1.ANC.NAMTYP.NE.NISO.ANC.NAMTYP.NE.NGIZ)GO TO 52
GO TO 93
52 CALL AUSGL(NDAT,EM,EP,FA,FF)
93 IF(FF.EQ.0)RETURN
IF(KK.EQ.1.OR.KK.EQ.3)RETURN
GOTO 10
9 CONTINUE
IF(KK.EQ.3)GOTO 42
IF(NAMTYP.NE.NISO.AND.NAMTYP.NE.NGIZ)
*WRITE(NOUT,100)FM(1),FM(3),FA(NDAT-1),FF(NDAT-1)
100 FORMAT(/' ***WARNING 9.4 MATERIAL',A10,' TYPE',A10,/
*' ***LAST ENERGY POINT ON KEDAK IS',1PE14.6,
*' EV WITH THE CROSS-SECTION VALUE',1PE14.6,' BAFR.*/
*' *** EXTRAPOLATION IS CARRIED OUT WITH THE CONSTANT VALLE OF THE
*CRSS-SECTION. ')
FA(NDAT)=EP
FF(NDAT)=FF(NDAT-1)
IF(NAMTYP.EQ.NGIZ)FF(NDAT)=0.
42 CONTINUE
GOTO 30
3 CONTINUE
NWORT(1)=4
LL=1
NWI=0
FM(4)=1.0

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23 CALL NDFLOC(NT,NWORT,FM,N1,N2)
CALL NDFLOC(NT,NWORT,FM,N1,N2)
IF(NT.EQ.0.AND.NW1.EQ.0)RETURN 1
IF(NT.EQ.0)GOTO 18
IF(KK.EQ.6.AND.NW1.EQ.0)EFR=FM(4)
NW1=NW1+1
IF(NW.EQ.0.AND.FM(4).GE.EMW)GOTO 24
IF(NW.EQ.NW1)GOTO 24
FM(4)=(1+1.E-6)*FM(4)
GOTO 23
24 CCNTINUE
IF(KK.GE.7)GOTO 26
IF(KK.GE.5)GOTO 25
FNW=FM(4)
KK=KK-1
GOTO 22
25 NW=NW1-1
IF(EMW.EQ.FM(4))NW=NW1
LZ=0
IF(NW.EQ.0)LZ=1
IF(NW.EQ.0)NW=1
NPA=0
KK=KK+2
GOTO 3
26 FAW=FM(4)
IF(KK.EQ.7)GOTO 22
IF(FM(4).GE.EPW)RETURN
FM(4)=(1+1.E-6)*FM(4)

NW=NW+1
GOTO 23
10 IF(LZ.NE.0)GOTO 88
CC 90 I=1,NDAT
FAW(I)=FA(I)
90 FFW(I)=FF(I)
IEA(I)=NDAT
EA(I)=EMW
LZ=2
NPA=NDAT
88 CONTINUE
CC 91 I=1,NDAT
FAW(I+NPN)=FA(I)
91 FFW(I+NPN)=FF(I)
EA(LZ)=FNW
IEA(LZ)=NDAT
NPA=NPN+NDAT
LZ=LZ+1
IF(FNW.GE.EPW)GOTO 89
NW=NW+1
FM(4)=(1+1.E-6)*FNW
GOTO 23
18 FNW=EPW
IF(KK.EQ.7)GOTO 88
NW1=NW1+1
RETURN
89 NW1=LZ-1

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94 RETURN
END
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C SLBROUTINE LINTNT(N,X1,Y1,M,X2,Y2)
C SLBROUTINE ADDED BY BRCEDERS, INR JUNE, 1975
C
COMMON MATN(4),NOUT
DIMENSION X1(N),Y1(N),X2(M),Y2(M)
JN=1
JA=1
DO 3 I=1,M
NN=1
IF(X2(I).GE.X1(1))GOTO 4
Y2(I)=Y1(1)
GOTO 5
4 NN=N
IF(X2(I).LE.X1(N))GOTO 6
Y2(I)=Y1(N)
5 WRITE(NOUT,100)X2(I),X1(1),X1(N),Y2(I)
GOTO 9
6 CCNTINUE
CC 1 J=JA,N
JA=J
IF(X2(I).LE.X1(J))GOTO 2
1 CCNTINUE
2 IF(X1(JN).EQ.X1(JN-1))GOTO 7
Y2(I)=FIPOL(X1(JN-1),X2(I),X1(JN),Y1(JN-1),Y1(JA))
GOTO 8
7 NA=JN
9 Y2(I)=Y1(NN)
8 CCNTINUE
JA=MAXC(1,(JN-2))
3 CCNTINUE
10 RETURN
100 FORMAT(/' ***WARNING 9.6 INTERPOLATION ERROR.' /
*' ***DESIRED ENERGY',1PE14.6,' NOT IN RANGE (' ,1PE14.6,' ',
*1PE14.6,') . CONSTANT BOUNDARY VALUE',1PE14.6,' TAKEN.' /
*' ***PROBABLY PROGRAM-ERROR.')
END

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C SLBROUTINE AUSGL(NDAT,EM,EP,FA,FF)
C SUBROUTINE ADDED BY BRCEDERS, INR JUNE, 1975
C
COMMON MATN(4),NOUT
DATA EPS/1.E-6/
DIMENSION FA(1),FF(1)
CC 1 I=1,2

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2   PTL=XX                               60
   RETURN                                70
3   PTL=0.5*(3*(XX**2)-1.0)              80
   RETURN                                90
4   PTL=0.5*(5*(XX**3)-3*XX)            100
   RETURN                                110
5   PTL=0.125*(35*(XX**4)-30*(XX**2)+3) 120
   RETURN                                130
6   PTL=0.125*(63*(XX**5)-7*(XX**3)+15*XX) 140
   RETURN                                150
   END                                    160

SUBROUTINE ZWIN(KL,EP,EM,ES,J2,J1)      10
DIMENSION ES(KL)                       20
J1=KL                                    30
J2=1                                     40
KL1=KL-1                                50
DO 1 I=1,KL1                             60
  IF(ES(I).EQ.ES(I+1))GOTO 1             70
  IF(EP.GE.ES(I).AND.EP.LT.ES(I+1))GCTC 2 80
GCTO 1                                    90
2   J1=I+1                                100
   GOTO 11                                110
1   CCATINUE                              120
11  CCATINUE                              130
   DO 12 I=2,KL                          140
   IF(ES(I).EQ.ES(I+1).AND.I.LT.KL)GOTO 12 150
   IF(EM.LE.ES(I).AND.EM.GT.ES(I-1))GCTO 13 160
GCTO 12                                    170
13  J2=I-1                                180
   GCTO 14                                190
12  CCATINUE                              200
14  CCATINUE                              210
   RETURN                                220
   END                                    230

FUNCTION FIPOL(XA,XB,XC,YA,YC)          10
C                                         20
C FUNCTION ADDED BY BROEDERS,INR JUNE,1975 30
C                                         40
   DX=XC-XA                              50
   IF(DX.NE.0.)GCTO 1                    60
   FIPOL=0.5*(YA+YC)                     70
   GCTO 2                                 80
1   CONTINUE                              90
   DX1=XB-XA                             100
   DX2=XC-XB                             110
   FIPOL=(YA*DX2+YC*DX1)/DX              120
2   RETURN                                130
   FNC                                    140

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SUBROUTINE IPOL(M,A,B,X,Y,T)            10
C                                         20
C SUBROUTINE IPOLA BY H. WIESE,INR      30
C                                         40
C MODIFIED BY BROEDERS,INR JUNE,1975   50
C                                         60
C                                         70
C KUBISCH-GUADRATISCH-LINEARE INTERPOLATION 80
C FINE ERZEUGUNG ZUSAETZLICHER EXTREMWERTE 90
C                                         100
DIMENSION A(M),B(M),T(M)                110
DATA AA1/0./,AAH/0./,AAM/0./,BB1/0./,BBH/0./,BBM/0./ 120
NF=M/2                                    130
C                                         140
IF(BB1.NE.B(1).OR.BBH.NE.B(NF).OR.BBM.NE.B(M))GCTO 20 150
IF(AA1.NE.A(1).OR.AAH.NE.A(NH).OR.AAM.NE.A(M))GCTO 20 160
GCTO 21                                    170
C                                         180
C TANGENTEN                               190
20  CCATINUE                              200
   T(1) = (B(2)-B(1))/(A(2)-A(1))        210
   T(M) = (B(M)-B(M-1))/(A(M)-A(M-1))    220
   MN = M-1                               230
   DO 2 J = 2,MN                          240
   JP = J+1                                250
   JM = J-1                                260
   T(J) = 0.                               270
   IF(B(JP).GT.B(J).AND.B(J).GT.B(JM))    280
   -T(J) = (B(JP)-B(JM))/(A(JP)-A(JM))    290
   IF(B(JP).LT.B(J).AND.B(J).LT.B(JM))    300
   -T(J) = (B(JP)-B(JM))/(A(JP)-A(JM))    310
2   CCATINUE                              320
   AA1=A(1)                                330
   AAH=A(NH)                                340
   AAM=A(M)                                350
   EE1=B(1)                                360
   BBH=B(NH)                                370
   BBM=B(M)                                380
21  CCATINUE                              390
C                                         400
C INTERPOLATION                           410
   J = 1                                    420
4   IF(X -A(J)) 6,B,10                     430
6   S = X -A(K)                             440
   Y = A0+(A1+(A2+A3*S)*S)*S              450
   GCTC 16                                  460
8   Y = B(J)                                470
   GCTO 16                                  480
10  K = J                                    490
   J = J+1                                  500
   U = A(J)-A(K)                           510

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V = B(J)-B(K)
R = V-T(K)*U
h = U*(T(J)-T(K))
A0 = B(K)
A1 = T(K)
A2 = (3*R-W)/(U*L)
A3 = (W-2*R)/(U*U)
IF(T(K).EQ.0..AND.T(J).EQ.0.) GOTO 4
IF(ABS(A3).LT.1.E-30) GOTO 4
XW = -A2/(3*A3)
IF(XW.LE.0..OR.XW.GE.U) GOTO 4
A3 = 0.
IF(T(J).EQ.0.) GOTO 12
IF(T(K).EQ.0.) GOTO 14
A2 = R/(U*U)
T(J) = 2*V/U-T(K)
IF(ABS(A2).LT.1.E-30) GOTO 4
XW = -A1/(2*A2)
IF(XW.LE.0..OR.XW.GE.U) GOTO 4
A1 = V/U
A2 = 0.
T(J) = A1
GOTO 4
12 A1 = 2*V/U
A2 = -V/(U*U)
GOTO 4
14 A1 = 0.
A2 = V/(U*U)
GOTO 4
16 CONTINUE
RETURN
END

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SUBROUTINE MASSIN(WORK,ABN)
C
C SUBROUTINE MODIFIED BY BROEDERS,INR JUNE,1975
C
REAL*8 MATN
REAL*8 HID
DIMENSION WORK(1),ABN(1),A(6),AC(13)
COMMON MATN,IS(2),NCUT,LI,IR(2)
DATA A/0.57735,0.774596,0.33598,0.86114,0.53847,0.90618/
DATA HID/'H HI'/
IF(MATN.EQ.HID)GOTO 40
CALL KEDDAT(MATN,'ISOT1 ',C,NW1,FNW,NDAT,FA,FF,3CO,0,1,C,
1,40,440,440)
AME=FA(2)
GOTO 41
40 CONTINUE
AME=1.008665

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41 CONTINUE
AME=AME/1.008665
CC 10 I=1,6
XA=A(I)**2-1
AC(I+6)=(XA-A(I)*SQRT(XA+AME**2))/AME
10 AC(I)=(XA+A(I)*SQRT(XA+AME**2))/AME
AC(13)=-1/AME
XM=(AME+1)**2/2/AME
IF(AME.EQ.1.)GOTO 1
CM=(AME+1.)/(AME-1.))**2
GOTO 2
1 CM=2.E8
2 CONTINUE
CMX=ALOG(QM)
WCRK(28)=AME
WORK(29)=QM
WCRK(30)=XM
WORK(31)=QMX
CALL TRDMES(AC)
I1=IR(1)
I2=IR(2)
IMAX=2
DO 11 I=I2,I1
E=ABN(I+1)/QM
IM=IC SOP(E,ABN(I))
IF(IM.GT.IMAX)IMAX=IM
11 CONTINUE
CALL IWIN(18,IMAX,WORK)
RETURN
END

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B 133 -

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SUBROUTINE INTFN(E,SG,SGNC,EA,ICCS)
C
C SUBROUTINE MODIFIED BY BROEDERS,INR JUNE,1975
C
DIMENSION SG(1),SGNC(1),EA(1)
NE=0
3 NE=NE+1
IF(E.GT.EA(NE)+EA(NF)*1.0E-4)GOTO 3
IF(NE.EQ.1)GOTO 5
DO 4 I=1,ICCS
4 SG(I)=FIPOL(EA(NE-1),E,FA(NE),SGNC(1,NE-1),SGNC(1,NF))
RETURN
5 DO 6 I=1,ICCS
SG(I)=0.5
6 CONTINUE
RETURN
END

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FUNCTION FXINT(EP,EM,SGN,ES,FLUX,EFLUX,NSP,NDAT)
C
C FUNCTION MODIFIED BY BROEDERS, INR JUNE, 1975
C
C DIMENSION FLUX(1),EFLUX(1)
C DIMENSION SGN(1),FS(1)
C CALL ZWIN(NDAT,EP,EM,ES,J2,J1)
C Y=0.
C
C SAVE BOUNDARY VALUES
C
C SGN1=SGN(J1)
C SGN2=SGN(J2)
C ES1=ES(J1)
C ES2=ES(J2)
C SGN(J1)=FIPOL(ES(J1),EP,ES(J1-1),SGN(J1),SGN(J1-1))
C SGN(J2)=FIPOL(ES(J2),EM,ES(J2+1),SGN(J2),SGN(J2+1))
C ES(J1)=EP
C ES(J2)=EM
C J11=J1-1
C IF(NSP.EQ.1)GOTO 1
C CALL ZWIN(NSP,EP,EM,EFLUX,JF2,JF1)
C FF1=FIPOL(EFLUX(JF2),EM,EFLUX(JF2+1),FLUX(JF2),FLUX(JF2+1))
C GOTO 2
1 FF1=PHI(EM)
2 CONTINUE
C IF(J2.GT.J11)GOTO 17
C DC 16 I=J2,J11
C CX=ES(I+1)-ES(I)
C IF(NSP.EQ.1)GOTO 3
C CALL ZWIN(NSP,ES(I+1),ES(I+1),EFLUX,ISG,ISF)
C FF2=FIPOL(EFLUX(ISG),ES(I+1),EFLUX(ISG+1),FLUX(ISG),FLUX(ISG+1))
C GOTO 4
3 CONTINUE
C FF2=PHI(ES(I+1))
4 Y=Y+DX*(SGN(I)*FF1+SGN(I+1)*FF2)
C FF1=FF2
16 CONTINUE
C FXINT=Y*0.5
C
C RESTORE BOUNDARY VALUES
C
C 17 ES(J1)=ES1
C ES(J2)=ES2
C SGN(J1)=SGN1
C SGN(J2)=SGN2
C RETURN
C
C END

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SUBROUTINE SMCRN(PI,N,IM,WORK)
C
C DIMENSION PI(N,IM),WORK(1)
C C=WORK(32)
C JM=1
C IF(Q.GT.0)JM=IMN(26,WORK)
C AS=0
C DO 1 I=JM,IM
1 AS=PI(I,I)+AS
C IF(AS.EQ.0)RETURN
C DO 2 I=JM,IM
C CC 2 J=1,N
2 PI(J,I)=PI(J,I)/AS
C RETURN
C
C END

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SUBROUTINE SEARCH(NFI,NFI,WORK,IWORK,FLUX,EFLUX,ENERG)
C
C SUBROUTINE MODIFIED BY BROEDERS, INR JUNE, 1975
C
C DIMENSION WORK(1),IWORK(1),FLUX(1),EFLUX(1),SGS(4)
C REAL*8 MATN,ENERG(1)
C COMMON MATN,MAY(2),NOUT,LI
C DATA SGS/'SGT ','SGN ','MUEL','FLUX'/
C NDAT=IWORK(25)
C N9=IWORK(13)
C DC 3 I=1,NDAT
3 WORK(N9+I-1)=1.0
C N4=IWORK(7)
C NZ=NFG*NFI
C N11=IWORK(12)
C I4=N11+3*NZ
C IG=IWORK(4)
C NSP=IWORK(15)
C DC 20 I=1,NFG
C IF=(I-1)*NFI+1
C E1=SNGL(ENERG(IP))
C E2=SNGL(ENERG(IP+NFI))
C FF=FXINT(E2,E1,IWORK(N9),WORK(N4),FLUX,EFLUX,NSP,NDAT)
C DO 21 J=1,NFI
C IF=NFI*(I-1)+J
C EM=SNGL(ENERG(IP))
C EP=SNGL(ENERG(IP+1))
C WCRK(IW)=FXINT(EP,EM,WCRK(N9),WORK(N4),FLUX,EFLUX,NSP,NDAT)/FF
C IW=IW+1
21 CONTINUE
20 CONTINUE
C IWORK(22)=N11
C NC=4*NZ+3
C J=4*NZ
C WRITE(LI)NQ,IG,NFG,NFI,(WORK(N11+I-1),I=1,J)
C WRITE(NOUT,70)IG,NZ,MATN
C NZ1=NZ+1

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B 134

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WRITE(NOUT,73)
WRITE(NOUT,74)(ENERG(I),I=1,NZ1)
DC 1 M=1,4
WRITE(NOUT,71)SGS(M)
Ih=N1+(M-1)*NZ-1
1 WRITE(NOUT,72)(WORK(IW+I),I=1,NZ)
70 FCRMAT(/ '_GROUP=' ,I3,' NUMBER OF FINE INTERVALS=' ,I5,
1' MATERIAL' ,2X,A8)
71 FORMAT('OTHE VALUES OF ' ,A4)
72 FCRMAT(' ' ,1P10E12.4)
73 FORMAT('OTHE INTERVAL-BOUNDARIES ARE' ,/)
74 FCRMAT(' ' ,1P6C20.10)
75 FORMAT('1')
RETURN
END

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SUBROUTINE REMF(ABN,IGR,NFI,FLUX,EFLUX,WORK,IWORK,IS)
C
C SUBROUTINE MODIFIED BY BRCEDERS,INR JUNF,1975
C
DIMENSION ABN(1),IGR(1),NFI(1),FLUX(1),EFLUX(1),WORK(1),IWORK(1)
REAL*8 MATN
REAL*8 FNEV(4)
COMMON MATN,IZ(2),NOUT,LI,IL,IM
DATA FNEV/SGN,'SGT','SGN','MUEL',/,FPS/0.15/,FRMTOL/0.5/
REAL*8 WITHP,WITH/'WITH','WITHO','WITHOUT'/
NC=IWORK(1)
N2=IWORK(3)
N4=IWORK(5)
N5=IWORK(6)
N6=IWORK(7)
NENERG=IWORK(35)
NMAX=IWORK(36)
NESGT=N4+NMAX*3
NFSGN=NFSGT+NMAX
NEMUE=NE SGN+NMAX
NWSGT=N5+3*NMAX
NWSGN=NWSGT+NMAX
NWMUE=NWSGN+NMAX
NE=IWORK(26)
NLA=IWORK(16)
NLE=IWORK(17)
N11=IWORK(12)
IMAX=IWORK(18)
AP=WORK(28)
DO 10 IG1=IM,IL
IREAD=0
IG=IM+IL-IG1
WRITE(NOUT,93) IG
CALL ENERGI(IGR(IG),NFI(IG),ABN(IG+1),ABN(IG),WORK(NENERG))
IWORK(4)=IG
IF(IG-IS)20,20,21
20 CONTINUE
WITHP=WITH
IWORK(23)=1
CALL ZWTN(INE,ABN(IG),ABN(IG+1),WORK(NO),JW2,JW1)

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CALL NORM(JW2,JW1,WORK(N2),WORK)
GOTO 22
21 IWORK(23)=0
WITHP=WITHO
22 CONTINUE
WRITE(NOUT,95)WITHP
IWORK(22)=N11
JN=2
CALL KEDDAT(MATN,FNEV(JN),NW,NW1,FNW,NDATT,
*WORK(NESGT),WORK(NWSGT),
IABN(IG),ABN(IG+1),E2,E3,E4)
JN=3
CALL KEDDAT(MATN,FNEV(JN),NW,NW1,FNW,NDATS,
$WORK(NESGN),WORK(NWSGN),
IABN(IG),ABN(IG+1),E2,E3,E4)
JN=4
CALL KEDDAT(MATN,FNEV(JN),NW,NW1,FNW,NDATM,
*WORK(NEMUE),WORK(NWMUE),
IABN(IG),ABN(IG+1),E5,E3,E4)
IF(IWORK(23),NE,0)GOTO 24
AMUI=2./3./AM
ERMAX=0.
DO 23 I=1,NDATM
ERM=ABS(WORK(NWMUE-I+I)-AMUI)/AMUI
IF(ERM>LE,EP)GOTO 23
WRITE(NOUT,96)FNEV(4),FNEV(1),WORK(NEMUE-I+I),
*AMUI,ERM,EP
ERMAX=AMAX1(ERMAX,ERM)
23 CONTINUE
IF(ERMAX,LE,ERM TOL)GOTO 24
WRITE(NOUT,97)ERMAX,ERM TOL
GOTO 10
24 CONTINUE
DC 30 I=1,NDATS
WORK(N6+I-1)=WORK(NESGN+I-1)
DC 31 I=1,NDATM
WORK(N6+NDATS+I-1)=WORK(NEMUE+I-1)
DC 32 I=1,NDATT
WORK(N6+NDATS+NDATM+I-1)=WORK(NESGT+I-1)
NDAT=NDATS+NDATM+NDATT
CALL CRONI(NDAT,WORK(N6))
WRITE(NOUT,92)MATN,ABN(IG+1),ABN(IG),FNEV(2),NDATT,FNEV(3),NDATS,
*FNEV(4),NDATM,NDAT
IWORK(25)=NDAT
CALL LININT(NDATT,WORK(NESGT),WORK(NWSGT),NDAT,WORK(N6),WORK(N4))
CALL SINT(IGR(IG),NFI(IG),FLUX,EFLUX,WORK,N4,N6,WORK(NENFRG))
CALL LININT(NDATS,WORK(NFSGN),WORK(NWSGN),NDAT,WORK(N6),WORK(N4))
CALL LININT(NDATM,WORK(NEMUE),WORK(NWMUE),NDAT,WORK(N6),WORK(N5))
7 CONTINUE
N4=-N4
CALL SINT(IGR(IG),NFI(IG),FLUX,EFLUX,WORK,N4,N6,WORK(NENERG))
IF(IREAD,EQ,1)GOTO 6
CALL LININT(NDATM,WORK(NEMUE),WORK(NWMUE),NDAT,WORK(N6),WORK(N5))
8 CONTINUE
CALL SEARCH(IGR(IG),NFI(IG),WORK,IWORK,FLUX,EFLUX,WORK(NENERG))
CALL ISOFAL(ABN(IG),IGR(IG),NFI(IG),FLUX,EFLUX,WORK,WORK(NENERG))
WRITE(NOUT,94)
DC 16 IQ=NLA,NLE
16 CALL SUCHM(IGR(IG),NFI(IG),WORK,IWORK,IQ,ABN)
GOTO 10
5 ASYGN 7 TO NNN
IREAD=1
GOTO 9

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6 ASSIGN 8 TO NNN 1030
9 W=2.0/3.0/AM 1040
DC 15 J=1,NDAT 1050
15 WORK(N5+J-1)=W 1060
GCTC NNN,(7,8) 1070
10 CONTINUE 1080
RETURN 1090
2 WRITE(NDOUT,80)MATN 1100
RETURN 1110
3 WRITE(NDOUT,90)MATN,FNEV(JN) 1120
RETURN 1130
4 WRITE(NDOUT,91)MATN,FNEV(JN) 1140
RETURN 1150
80 FORMAT(' ***ERROR 9.2 : MATERIAL ',A8,' IS NOT FOUND') 1160
90 FORMAT(' ***ERROR 9.3 MATERIAL ',A8,' TYP ',A8, 1170
1' ARE NOT FOUND') 1180
91 FORMAT(' ***ERROR 9.4 MATERIAL ',A8,' TYP ',A8, 1190
1' ARE NOT FOUND IN LST') 1200
92 FORMAT(/' NUMBER OF ENERGY POINTS RETRIEVED FOR MATERIAL',A10, 1210
*' IN THE ENERGY-RANGE',IPE14.6,' ',IPE14.6,' EVs',/ 1220
*3(/' ',A10,0PI10),/ 'TOTAL NUMBER OF DIFFERENT POINTS',I10) 1230
93 FORMAT(' CALCULATION FOR GROUP',I4,/' ',25('**')) 1240
94 FORMAT('1') 1250
95 FORMAT(/' FOR THIS ENERGY GROUP CALCULATION',A10,' ANGULAR DISTRIB 1260
*UTIONS,') 1270
96 FORMAT(' ***WARNING 9.5 : DISCREPANCY FOR',A10,' WITHOUT',A10,' ', 1280
*/ ' *** : E=',IPE14.6,' MUENL=',E14.6,' 2/(3A)=', 1290
*E14.6,' ERM=',E14.6,' G.T.',E14.6) 1300
97 FORMAT(' ***ERROR 9.7 : MAXIMUM DISCREPANCY IN MUENL(SEE WARNING 9. 1310
*5)=' ,IPE14.6,' G.T.',E14.6,/' 1320
*' : NO CALCULATION FOR THIS GROUP.') 1330
ENC 1340
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SUBROUTINE NORM(J2,J1,SC,WORK) 10
COMMON A(4),NCUT 20
REAL*8 ANINT 30
DIMENS(ON SC(1),WORK(1) 40
NN=IWO(33,WORK) 50
NJM=IWO(19,WORK) 60
NPL=IWO(17,WORK) 70
NEA=IWO(1,WORK) 80
KJJ=1 90
KJJT=1 100
N5=IWO(2,WORK) 110
ICCS=IWO(21,WORK) 120
BL=WORK(N5) 130
BU=WORK(N5+ICCS-1) 140
NJ=0 150
CALL IWIN(24,NJ,WORK) 160
DC 1 I=J2,J1 170
IW=(I-1)*ICOS 180
ASG=ANINT(BU,EL,1,SC(IW+1),WORK(N5),0.0,ICOS,WORK,WORK(NN),NJM) 190
NJ=IWO(24,WORK) 200
IF(NJ.LT.(NJM-1))GO TO 3 210
KJJ=2 220
NJM1=NJM-1 230
WRITE(NDOUT,100)I,WORK(NEA-1+I),NJM1,ASG 240
3 CONTINUE 250
KJJT=MAX0(KJJT,KJJ) 260
NJ=0 270

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CALL IWIN(24,NJ,WORK) 280
DC 2 J=1,ICOS 290
2 SC(IW+J)=SC(IW+J)/ASG 300
1 CONTINUE 310
CALL IWIN(23,KJJT,WORK) 320
RETURN 330
100 FORMAT( 340
** ***WARNING 9.8 : FOR ANGLE DISTR. NR.',I3,' AT THE ENERGY', 350
*1PE11.3,' INTEGRATION PROBLEMS OCCUR WITH NJM=',I3,' INTEGRAL=', 360
*E11.3,/' ***',I4X,'THE ANGLE MESH-POINTS FROM AN INT WILL BE REPLACE 370
*D BY THE KEDAK-VALUES. INCREASING OF NJM MAY AVOID THIS POSSIBLY.' 380
*) 390
END 400

SUBROUTINE SINT(NG,NI,FLUX,EFLUX,WORK,N,N4,ENERG) 10
C 20
C SUBROUTINE MODIFIED BY BROEDERS,INR JUNE,1975 30
C 40
REAL*8 ENERG(1) 50
DIMENSION FLUX(1),EFLUX(1),WORK(1) 60
N2=IWO(5,WORK) 70
N3=IWO(6,WORK) 80
N7=IWO(22,WORK) 90
N9=IWO(13,WORK) 100
NSP=IWO(15,WORK) 110
NDAT=IWO(25,WORK) 120
IC=1 130
L=N 140
N=IABS(N) 150
N2=IABS(N2) 160
N7=NI*NG 170
DC 3 I=1,NDAT 180
IF(L.LT.0)WORK(N3+I-1)=WORK(N3+I-1)*WORK(N2+I-1) 190
3 WORK(N9+I-1)=1.0 200
Iw=N7 210
DC 1 IP=1,NZ 220
EP=SNGL(ENERG(IP)) 230
EP=SNGL(ENERG(IP+1)) 240
WORK(IW)=FXINT(EP,EM,WORK(N),WORK(N4),FLUX,EFLUX,NSP,NDAT) 250
FF=FXINT(EP,EM,WORK(N9),WORK(N4),FLUX,EFLUX,NSP,NDAT) 260
IF(L.GT.0)GOTO 4 270
WORK(IW+NZ)=FXINT(EP,FM,WORK(N3),WORK(N4),FLUX,EFLUX,NSP,NDAT) 280
I/WORK(IW) 290
4 WORK(IW)=WORK(IW)/FF 300
IW=IW+1 310
1 CONTINUE 320
IF(L.LT.0)IW=IW+NZ 330
CALL IWIN(22,IW,WORK) 340
RETURN 350
END 360

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C      SLBROUTINE ISOFAL(ABN,IGR2,NF11,FLUX,EFLUX,WORK,ENERG)
C      SUBROUTINE MODIFIED BY BRCEDEBS,INR   JUNE,1975
C
      REAL*8 ENERG(1)
      DIMENSION ABN(1),FLUX(1),EFLUX(1),WORK(1)
      IC=1
      NS=IWO(10,WORK)
      QQ=WORK(32)
      IC=IG
      IGI=IWO(4,WORK)
      IF(QQ.GT.0)CALL EGRENZ(ABN(1),ABN,IC,IV,WORK)
      IFI=IGI+IG-1
      CALL IWIM(4,IFI,WORK)
      NM1=IWO(17,WORK)+1
      NJM=IWO(19,WORK)
      NUJM=IWO(20,WORK)
      AME=WORK(28)
      IMAX=IWO(18,WORK)
      IX=IWO(11,WORK)
      N7=IWO(22,WORK)
      NZ=IGR2*NF11
      IG1=IG+1
      DO 15 IP=1,NZ
      EP=SNGL(ENERG(IP))
      EP=SNGL(ENERG(IP+1))
      FNV=0.
      IF(QQ.GT.0.)FNV=CQ*AME/(AMF-1.)
      NU=NM1*IMAX
      DC 9I=1,NU
9      WORK(N7+I-1)=0.0
      IF(EP.LE.FNV)GOTO 7
      IF(QQ.LE.0)GOTO 6
      IF(EM.LE.FNV)EM=FNV
6      CALL WAHRS(EP,EM,IMAX,WORK(N7),ABN(IC),NM1,NUJM,FLUX,EFLUX,
      IWORK(N9),WORK,WORK(IX))
      CALL SMORN(WORK(N7),NM1,IMAX,WORK)
7      CONTINUE
      N7=N7+NM1*IMAX
15  CONTINUE
      CALL IWIM(22,N7,WORK)
      RETURN
      END
      SUBROUTINE WAHRS(EP,EM,IMAX,PI,ABN,NM1,NUJM,FLUX,EFLUX,TE,WCRK,EZ)
      DIMENSION FLUX(1),EFLUX(1),WORK(1)
      DIMENSION TE(NM1,IMAX,NUJM)
      DIMENSION ABN(IMAX),PI(NM1,IMAX)
      DIMENSION EZ(1)
      COMMON MATN(4),NOUT
      CP=WCRK(29)
      NJM=IWO(19,WORK)-1

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      NN=IWO(34,WORK)
      IC=1
      AM=WORK(28)
      Q=WORK(32)
      KL=IWO(25,WORK)
      N2=IWO(5,WORK)
      KJ=IWO(23,WORK)
      N3=IWO(6,WORK)
      N4=IWO(7,WORK)
      N10=IWO(11,WORK)
      NIC=N10+1+IMAX
      EZ(1)=EM
      IJ=1
      JM=1
      E=EM/QM
      IMAX1=IC SOP(E,ABN)
      IF(E.EQ.ABN(IMAX1))IMAX1=IMAX1-1
      IF(Q.GT.0)CALL EGRENZ(EM,ABN,IK,IMAX1,WORK)
      IMAX1=IMAX1+1
      IC=IWO(4,WORK)
      NG=IWO(14,WORK)
      IT=NG-IG
      IT=MINO(IMAX,IT)
      IF(Q.GT.0)GOTO 45
      DC 42 I=1,IT
      EPI=QM*ABN(IT-I+2)
      IF(EPI.GE.EP.OR.EP1.LE.EM)GOTO 42
      IJ=IJ+1
      EZ(IJ)=EPI
42  CONTINUE
45  CONTINUE
      DC 44 LJ=1,IJ
      EZ(IJ+1)=EP
      IMAX1=IMAX1-1
      CALL ZWIN(KL,EZ(LJ+1),EZ(LJ),WORK(N4),J2,J1)
      J11=J1-1
      EM1=EZ(LJ)
      DO 44 IK=J2,J11
      EPI=WORK(N4+IK)
      IF(IK.EQ.J11)EPI=EZ(LJ+1)
      CALL LMI(EPI,EM1,WORK(N4+IK),WORK(N4+IK-1),WORK(N2+IK),
      WCRK(N2+IK-1),WORK(N3+IK),WCRK(N3+IK-1),IMAX1,ABN,TE,NM1,NUJ,NUJM,
      2FLUX,EFLUX,WORK,WORK(NIC),IMAX,WORK(NN))
      IF(Q.GT.0)JM=IWO(26,WORK)
      IF(IMAX1.GT.1.OR.KJ.GT.0)GOTO 3
      IF(NM1.LT.3)GOTO 3
      TE(3,JM,NUJ)=TE(1,JM,NUJ)/AM/AM/5
      IF(NM1.LT.5)GOTO 3
      TE(5,JM,NUJ)=-TE(1,JM,NUJ)/AM/AM/AM/AM/63
3      CONTINUE
      NJ=IWO(24,WORK)
      IF(NJ.GT.0)WRITE(NOUT,70)EPI,EM1,NJM,WORK(27)
70  FORMAT(' ***WARNING 9.2 : NO CONVERGENCE FOR RC*BERG ANGLE INTEGRA
      *T ION IN THE RANGE',IP2E12.4,' EV. NJM=',I3,' ERR=',IPE12.4)
      NJ=0

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CALL IWIN(24,NJ,WORK)
EM1=EP1
DC 43 J=JM,IMAX1
DC 43 K=1,NM1
43 PI(K,J)=PI(K,J)+TE(K,J,NUJ)
44 CCNTINUE
RETURN
ENC

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```

SUBROUTINE LMI(EP,EM,E1,E2,SG1,SG2,AMU1,AMU2, IMAX,ABN,TE,
1AM1,MUJ,NUJM,FLUX,EFLUX,WORK,PER, IMAM,PL)

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C SUBROUTINE MODIFIED BY BROEDERS,INR JUNE,1975
C

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REAL*8 PLK,PL(NM1,IMAM)
REAL*8 ANINT
DIMENSION ABN(IMAX),WORK(1)
DIMENSION EFLUX(1),FLUX(1)
DIMENSION PER(NM1,IMAM),TE(NM1,IMAM,NUJM)
COMMON MATN(4),NOUT
EQUIVALENCE(JM,JM1)
NJM=IWO(19,WORK)
AM=WORK(28)
CP=WORK(29)
KJ=IWO(23,WORK)
XM=WORK(30)
Q=WORK(32)
NSP=IWO(15,WORK)
ERR=WORK(27)
NLA=IWO(16,WORK)
NLE=IWO(17,WORK)
JM=1
IF(Q.GT.0)FNW=Q/AM/(AM+1.)
IF(Q.GT.0)CALL EGRENZ(EP,ABN,JM,II,WORK)
ICOS=IWO(21,WORK)
NNE=IWO(26,WORK)
N1=IWO(3,WORK)
N5=IWO(2,WORK)
NR=IWO(33,WORK)
NE=IWO(9,WORK)
NG=IWO(14,WORK)
N6=IWO(4,WORK)
NL1=1
NL2=NLE+1
IF(NSP.GT.1)CALL ZWIN(NSP,EP,EM,EFLUX,JF2,JF1)
IF(Q.GT.0)GOTO 9
NC=IWO(1,WORK)
IF(KJ.EQ.0)GOTO 9
CALL ZWIN(NNE,EP,EM,WORK(N0),JW2,JW1)
JW=JW2+N0-1
Iw=(JW2-1)*ICOS+NI
9 CONTINUE
DC 31 I=1,NM1
DC 31 J=1,IMAX

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67C
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5C
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15C
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20C
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220
230
240
25C
260
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30C
310
320
33C
340
35C
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370
380
390
40C
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42C
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450

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PER(I,J)=1.0
PL(I,J)=0
21 CONTINUE
EU =EP-EM
M1=1
NUJ=0
M2=1
ANS=1.0
SE=1
ISEL=IWO(8,WORK)
JZZ=0
41 NUI=2**NUJ+1
DX=DU/(NUI-1)
DC 21 I=M1,NU1,M2
E=EM+(I-1)*DX
IF(Q.GT.0)WORK(8)=E
IF(ISEL.EQ.1)SE=FIPOL(E1,E,E2,SG1,SG2)
ASE=FIPOL(E1,E,E2,AMU1,AMU2)
AZ=(ASE-2.0/3.0/AM)*3/(1.0-3.0/5.0/(AM**2))
IF(NSP.GT.1)GOTO 2
FF=PHI(E)
GOTO 3
2 DO 22 J=JF2,JF1
ISG=J-1
IF(EFLUX(J),GT.E)GOTO 23
22 CCNTINUE
23 CCNTINUE
FF=FIPOL(EFLUX(ISG),E,EFLUX(ISG+1),FLUX(ISG),FLUX(ISG+1))
3 CCNTINUE
ANS=0.0
BU=1.0
J=JM-1
IF(KJ.EQ.0)GOTO 62
CALL INTEN(E,WORK(N8),WORK(TW),WORK(JW),ICOS)
BL=-1.0
ANS=ANINT(BU,BL,2,WORK(N8),WORK(N5),AZ,ICOS,WORK,WORK(NR),NJM)
ANS=ASE-ANS
62 J=J+1
BL=-1.0
IF(J.GE.NG-N6+1)GOTO 30
IF(IMAX.EQ.1)GOTO 30
BL=RCM(E,ABN(J+1),WORK)
IF(BL.LE.-1.0)BL=-1.0
30 CCNTINUE
DC 8 K=NL1,NL2
IF(PER(K,J).LT.ERR)GOTO 8
IF(BL.EQ.BU)GOTO 4
IF(BL.LT.BU)GOTO 6
JZZ=1
BL1=BL
BU1=BU
BL=BU
BU=BL1
6 CCNTINUE
IF(BL.GE.1)GOTO 4
PLK=ANINT(BU,BL,K,WORK(N8),WORK(N5),AZ,ICOS,WORK,WORK(NR),NJM)
IF(ANS.NE.0)PLK=PLK+AKCR(BU,BL,K,AM)*ANS

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82C
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850
860
87C
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89C
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94C
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97C
980
99C
1000
101C
102C

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IF(K.GT.1.OR.PLK.GE.0.)GOTO 5
WRITE(NOUT,1000)E,BL,BU,PLK,ANS
1000 FORMAT(' ***ERROR 9.8 : NEGATIVE RESULT OF ANIAT FOR L=0. ',
*/      ' ***      : E= ',
*1PE14.6, ' BL= ',E14.6, ' BU= ',E14.6, ' PLK= ',E14.6, ' ANS= ',E14.6,
*/      ' ***      : PLK=0. TAKEN. ')
4 PLK=0.0
5 CONTINUE
IF(JZZ.EQ.0)GOTO 66
JZZ=0
BL=BL1
BL=BU1
66 CONTINUE
PLK=PLK*FF
IF(I.EQ.1)PL(K,J)=0.5*PLK*D*X*SE
IF(I.EQ.NU1)PL(K,J)=PL(K,J)+0.5*PLK*D*X*SE
IF(I.EQ.1.OR.I.EQ.NU1)GOTO 8
PL(K,J)=PL(K,J)+PLK*D*X*SE
8 CONTINUE
BU=BL
IF(BU.EQ.-1.0)GOTO 20
GOTO 62
20 CONTINUE
21 CONTINUE
IF(NU1.GT.2)GOTO 27
DO 50 J=JM,IMAX
DC 50 K=NL1,NL2
TE(K,J,1)=PL(K,J)
50 PL(K,J)=0
NUJ=NUJ+1
M1=2
M2=2
IF(IMAX.GT.JM.OR.KJ.GT.0)GOTO 41
IF(NL2.LT.3)GOTO 41
DO 25 J=3,NL2
PER(J,JM)=0.
IF(J.NE.5)ITE(J,JM,1)=0.
25 CONTINUE
GOTO 41
27 LX=0
DO 26 J=JM,IMAX
DC 7 K=NL1,NL2
IF(PER(K,J).LT.ERR)TE(K,J,NUJ+1)=TE(K,J,NUJ)
IF(PER(K,J).LT.ERR)GOTO 7
AJ=0.5*TE(K,J,1)+PL(K,J)
AL=TE(K,J,NUJ)
ZC=1
DO 52 IB=1,NUJ
ZC=4*ZC
AF=(ZC*AJ-TE(K,J,IB))/(ZC-1)
TE(K,J,IB)=AJ
52 AJ=AP
TE(K,J,NUJ+1)=AP
PER(K,J)=ABS(AP)
IF(ABS(AP).GT.1.E-10)PER(K,J)=ABS((AP-AL)/AP)
IF(PER(K,J).GT.ERR)LX=1

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PL(K,J)=0
7 CONTINUE
26 CONTINUE
NLJ=NUJ-1
IF(NUJ.GE.NUJM.AND.LX.EQ.1)GOTO 100
IF(LX.EQ.1)GOTO 41
IF(Q.GT.0)CALL IWIN(26,JM,WORK)
CALL IWIN(8,ISEL,WORK)
RETURN
100 CONTINUE
IF(Q.GT.0)CALL IWIN(26,JM,WORK)
WRITE(NOUT,71)EP,EM,NUJM,ERR
DO 10 J=JM,IMAX
DO 10 K=1,NM
IF(PER(K,J).LE.ERR)GOTO 10
WRITE(NOUT,70)K,J,TE(K,J,NUJ),PER(K,J)
IF(ABS((EP-EM)/EM).LT.1.E-7)TE(K,J,NUJ)=0.
10 CONTINUE
70 FORMAT(10X,'SCATTERING MATRIX_',2I4,3X,1PE12.4,' ERROR ',
1PE12.4)
71 FORMAT(' ***WARNING 9.3 : NO CONVERGENCE FOR ROMBERG ENERGY INTEGR
*ATION IN THE RANGE ',1P2E12.4,' EV. NUJM=',I3,' ERR=',1PE12.4)
CALL IWIN(8,ISEL,WORK)
RETURN
END
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FUNCTION IWO(L,IWORK)
DIMENSION IWORK(1)
IWC=IWORK(L)
RETURN
END
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SUBROUTINE IWIN(L,N,IWORK)
DIMENSION IWORK(1)
IWRK(L)=N
RETURN
END
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SUBROUTINE SUCHM(NFC,NFI,IWORK,WORK,MOM,ABN)
DIMENSION ABN(1)
DIMENSION WORK(1),IWORK(1)
REAL*8 MATN
COMMON MATN,MAY(2),NOUT,LI,IL,IMI
IG=IWORK(4)
Q=WCRK(32)
MK=2
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IK=IG
IF(Q.LT.O)GOTO 15
CALL EGRENZ(ABN(IG),ABN,IK,IV,WORK)
AM=WORK(28)
FNW=Q*AM/(AM-1.)
EF=AMAX1(FNW,ABN(IG+1))
CALL EGRENZ(EF,ABN,I,IV,WORK)
**=4
15 CONTINUE
N9=IWORK(13)
N11=IWORK(12)
NLE=IWORK(17)
I#=IWORK(18)
IW=N11
NZ=NFG*NFI
DC 11 J=1,NZ
DO 12 K=1,IM
L=(K-1)*NZ+MK+N9
LL=IW+(K-1)*(NLE+1)+MCM
WCRK(L+J)=WORK(LL)
12 CCNTINUE
11 IW=IW+(NLE+1)*IM
I#CRK(N9)=I#*NZ+MK
L=IWORK(N9)+N9
I#CRK(N9+1)=MCM
IWORK(N9+2)=IG
IF(Q.LT.O)GOTO 5
I#CRK(N9+3)=IK
IWORK(N9+4)=IV
5 CCNTINUE
WRITE(L1)(WORK(I),I=N9,L)
NGR=IWORK(14)
WRITE(NOUT,70)MCM,MATN,IG
DC 2 I=1,IM
IZ=IK+I-1
IF(IZ.GT.NGR)RETURN
WRITE(NOUT,71)IG,IZ
IW=N9+MK+(I-1)*NZ
2 WRITE(NOUT,72)(WORK(IW+J),J=1,NZ)
70 FORMAT(/, ELASTIC SCATTERING MATRIX SGNC',I1,' FOR ',A8,
1' GROUP=',I4)
71 FCRMAT(' FROM GROUP ',I4,' TC GROUP ',I4)
72 FORMAT(' ',IP10E12.4)
RETURN
END

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SUBROUTINE AMESH(B1,B2,Z,J2,AX,NL)
DIMENSION Z(6),ZA(6),ZF(6)
DIMENSION A(13),AC(1)
DATA NW/10/
GCTO (1,2,3,4,5,6),NL
1 NX=1

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J1=0
J2=1
Z(1)=B1
RETURN
2 N=1
Z(1)=A(13)
GCTO 7
3 N=2
Z(1)=A(7)
Z(2)=A(1)
GCTO 7
4 N=3
Z(1)=A(8)
Z(2)=A(13)
Z(3)=A(2)
GCTO 7
5 N=4
Z(1)=A(10)
Z(2)=A(9)
Z(3)=A(3)
Z(4)=A(4)
GCTO 7
6 Z(1)=A(12)
Z(2)=A(11)
Z(3)=A(13)
Z(4)=A(5)
Z(5)=A(6)
N=5
7 CONTINUE
IF(AC(13).GT.-1+1.0/NW)GOTO 11
M=N
N=N/2
IF(N.EQ.O)GOTO 1
DC 12 I=1,N
12 Z(I)=Z(M-N+I)
11 CCNTINUE
J1=N
J2=1
ZA(J2)=Z(J2)-(Z(J2)+1)/NW
ZF(J1)=Z(J1)+(1-Z(J1))/NW
IF(J1.EQ.1)GOTO 9
J11=J1-1
DC 8 I=J2,J11
SW=Z(I+1)-Z(I)
SW=SW/NW
ZA(I+1)=Z(I+1)-SW
ZF(I)=Z(I)+SW
8 CCNTINUE
9 CCNTINUE
DO 10 I=1,N
IF(ZA(I).LE.B2)J2=J2+1
IF(ZF(I).GE.B1)J1=J1-1
10 CCNTINUE
NX=J1-J2+2
Z(J1+1)=B1

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RETURN
ENTRY IRDMES(AC)
CO 20 I=1,13
20 A(I)=AC(I)
RETURN
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DOUBLE PRECISION FUNCTION ANG(XX,GAM)
REAL*8 XX,GAM
ANG =(XX+GAM)/DSQRT(GAM**2+2*XX*GAM+1.0)
RETURN
END

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DOUBLE PRECISION FUNCTION ANINT(BU,BL,K,SG,XL,AZ,ICOS,WORK,T,NJM)
REAL*8 YA,YB
REAL*8 MATN
REAL*8 T(NJM)
REAL*8 ANG,XX,GAM
REAL*8 XA,XB,XA1,YA1,AJ,AI,AK,AL,AP,AXX
REAL*8 PTL
DIMENSION SG(1),XL(1),Z(7),WORK(1)
COMMON MAT(4),NOUT
EQUIVALENCE(MATN,MAT(1))
C DATA NHD/'H H1'/
C ANG(XX)=(XX+GAM)/DSQRT(GAM**2+2*XX*GAM+1.0)
ERR=WORK(27)
AM=WORK(28)
GAM=1/AM
Q=WORK(32)
IF(Q.LT.0)GOTO 56
EI=WORK(8)
56 GAM=GAM*SQRT(EI/(EI-(AM+1)/AM*Q))
CONTINUE
IF(AM.LT.1.1)CALL HICR(BU,BL,K,AXX,850)
IF(AM.LT.1.1)GOTO 50
XP=WORK(30)
KJ=IWO(23,WORK)
CALL AMESH(BU,BL,Z,L2,NX,K)
NU=1
XA=BL
YA=ANG(XA,GAM)
YA=PTL(K,YA)
YA=YA*WINK(XL,SG,KJ,ICOS,AZ,XA)
AXX=0
IL=1
18 CCNTINUE
XA1=XA
XP=Z(IL+L2-1)
IF(KJ.NE.2)GOTO 20

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CO 21 I=1, ICOS
J=I
IF(XL(I).GT.XA+ERR.AND.XL(I).LT.XB-ERR)GOTO 22
21 CCNTINUE
GOTO 20
22 XB=XL(J)
IL=IL-1
20 CCNTINUE
YB=ANG(XB,GAM)
IF(YB.EQ.0.AND.(K-2*(K/2)).EQ.0)GOTO 57
YB=PTL(K,YB)
GCTC 58
57 YB=0.0
58 CCNTINUE
YB=YB*WINK(XL,SG,KJ,ICOS,AZ,XB)
NJ=0
AJ=0.5*(YA+YB)*(XB-XA)
XA1=XA
YA1=YA
T(I)=AJ
10 NJ=NJ+1
XA=XA1
YA=YA1
AI=AJ
NP=2**NJ+1
EM=(XB-XA)/(NP-1)
AJ=0.5*AI
CC 40 IZ=2,NP,2
XA=XA+DM
YA=ANG(XA,GAM)
YA=PTL(K,YA)
YA=YA*WINK(XL,SG,KJ,ICOS,AZ,XA)
XA=XA+DM
40 AJ=AJ+YA*DM
AK=AJ
AL=T(NJ)
ZC=1
CO 51 IB=1,NJ
ZC=ZC*4
AP=(ZC*AK-T(IB))/(ZC-1)
T(IB)=AK
51 AK=AP
T(NJ+1)=AP
EPS=(AP-AL)/AP
EPS=10.0*EPS
IF(NJ.GE.NJM-1.AND.ABS(EPS).GT.ERR)GCTC 28
IF(ABS(EPS).GT.ERR)GOTO 10
GCTC 29
28 CCNTINUE
NJM1=NJM-1
WRITE(NOUT,70)BL,BU,NJM1,ERR,EPS,KJ
70 FCRMAT(' ***WARNING 9.7 : NO CONVERG. FOR ROMBERG ANGLE INTEGR. IN
* THE RANGE',IP2E10.2,'. NJM=',I2,' ERR=',E10.2,' EPS=',E10.2,
* ' KJ=',I2)
CALL IWIN(24,NJ,WCRK)

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B 141

29	CCONTINUE	920	RETURN 1	90
	AXX=AXX+T(NJ+1)	930	A=2.0/3.0*(X2**3-X1**3)	100
	XA=XB	940	RETURN 1	110
	YA=YB	950	A=3.0/4.0*(X2**4-X1**4)-0.5*(X2**2-X1**2)	120
	IL=IL+1	960	RETURN 1	130
	IF(IL.LE.NX)GOTO 18	970	A=0.5*(X2**5-X2**3-X1**5+X1**3)	140
50	CCONTINUE	980	RETURN 1	150
	ANINT=AXX	990	A=0.125*(35.0/6.0*(X2**6-X1**6)-7.5*(X2**4-X1**4)+1.5*(X2**2-	160
	RETURN	1000	X1**2))	170
	END	1010	RETURN 1	180
			A=0.125*(9*(X2**7-X1**7)-14*(X2**5-X1**5)+5.*(X2**3-X1**3))	190
			RETURN 1	200
			END	210
	FUNCTION WINK(XL,SG,KJ,ICOS,AZ,AM)	10		
C		20		
C	FUNCTION MODIFIED BY BROEDERS, INR JUNE,1975	30		
C		40	FUNCTION AKJR(B14,BL4,K,AM4)	10
	DIMENSION XL(1),SG(1)	50	IMPLICIT REAL*8 (A-H,O-Z)	20
	DATA ICOMA/20/	60	REAL*4 B14,BL4,AM4,AKOR	30
	COMMON M(4),NOUT	70	Q0(X)=0.75*X*X	40
	IF(KJ.NE.0)GOTO 1	80	Q1(X)=0.5*(X**3)	50
C	WINK=0.5*(1.+AZ*AM)	90	Q2(X)=3./16.*X*X*(3*X*X-2)	60
	WINK= (1.+AZ*AM)	100	Q3(X)=0.75*(X**3)*(X*X-1)	70
	GOTO 10	110	Q4(X)=1./32.*((X*X-1.)*(35.*X*X-10)-1)*X*X	80
	1 CONTINUE	120	Q5(X)=3./16.*(X**3)*(X*X-1.)*(9*X*X-5)	90
	IF(AM.LT.XL(1).OR.AM.GT.XL(ICOS))GOTO 2	130	B1=DBLE(B14)	100
	IF(ICOS.GT.ICOMA)GOTO 3	140	BL=DBLE(BL4)	110
	CALL IPOL(ICOS,XL,SG,AM,WINK,XL(ICOS+1))	150	A=DBLE(AM4)	120
	GOTO 10	160	GAM=1./AM	130
	3 CONTINUE	170	IF(GAM.LT.0.99)GOTO 7	140
	CC 4 I=2,ICOS	180	A1=DSQRT((B1+1.)/2)	150
	I=I+1	190	A2=DSQRT((BL+1.)/2.)	160
	IF(AM.LE.XL(I))GOTO 5	200	GOTO 8	170
	4 CONTINUE	210	7 CONTINUE	180
	WINK=FIPOL(XL(I-1),AM,XL(I),SG(I-1),SG(I))	220	A1=ANG(B1,GAM)	190
	GOTO 10	230	A2=ANG(BL,GAM)	200
	2 CONTINUE	240	CONTINUE	210
	WRITE(NOUT,100)AM,XL(1),XL(ICOS)	250	GOTO(1,2,3,4,5,6),K	220
	10 RETURN	260	1 AKOR8=Q0(A1)-Q0(A2)	230
100	FORMAT(' ***WARNING 9.1, THE ANGLE',1PE14.6,' IS NOT IN THE RANG	270	GCTC 90	240
	'E',E14.6,' ,',E14.6,' .')	280	2 AKOR8=Q1(A1)-Q1(A2)	250
	END	290	GOTO 90	260
			3 AKOR8=Q2(A1)-Q2(A2)	270
			GOTO 90	280
			4 AKOR8=Q3(A1)-Q3(A2)	290
			GOTO 90	300
			5 AKOR8=Q4(A1)-Q4(A2)	310
			GCTC 90	320
			6 AKOR8=Q5(A1)-Q5(A2)	330
			90 AKOR8=SNGL(AKOR8)	340
			RETURN	350
			END	360
	SLBRoutine HIDR(BU,BL,K,A,*)	10		
	REAL*8 A,X1,X2,B1,B2	20		
	B1=BU	30		
	B2=BL	40		
	X2=DSQRT(0.5*(1.0+B1))	50		
	X1=DSQRT(0.5*(1.0+B2))	60		
	GOTO(1,2,3,4,5,6),K	70		
1	A=X2**2-X1**2	80		

- B 142 -

SLBRoutine EGRENZ(E,ABA,IK,IV,WORK)	10	807 WRITE(NOUT,808) MAT	490
RETURN	20	808 FORMAT(1H0/' ***WARNING 10. 1 : THE GROUP CROSS SECTION SGC CAN NO	500
END	20	1T BE CALCULATED FOR ',A9/' BECAUSE THE REACTION TYPES SGF AND SGA	510
		ZARE NOT SPECIFIED IN THE INPUT')	520
		GC TO 801	530
		822 LAR=C	540
		CC 821 JJ=1,NTY	550
		IF(TYP(JJ).EQ.C) GO TO 801	560
C BERECHNUNG DES QUERSCHNITTS IN DER THERMISCHEN GRUPPE	10	821 CCNTINUE	570
	20	GC TO 807	580
	30	801 I=0	590
SUBROUTINE THERM (NE,NTY,TYP)	40	WRITE (LIZ)I,A	600
REAL*8 MAT,TYP(NTY),FEST(5),A,B,C,D,P,F,G,H,Z,X,O,Q,U,SGNCO,PRSGI	50	FEST(1)=MAT	610
I,R	60	IC=0	620
INTEGER*2 IHC(2),IMP(2)	70	CC 26 I=1,NTY	630
DIMENSION N(4),E(2),S(2)	80	IF(TYP(I).EQ.U) GO TO 27	640
COMMON MAT,I STRUK,I SPA,NOUT,LIZ,NAF,NEND,KL	90	26 CCNTINUE	650
EQUIVALENCE(IHC(1),HM)	100	GC TO 22	660
DATA IMP/'PU','U'/'	110	27 LL=0	670
WRITE (NOUT ,9000)	120	SGT=0.	680
9000 FORMAT(1H0/1H0/' PROGRAMM KENNZIFFER 10')	130	IC=1	690
WRITE (NOUT ,9001)	140	DO 20 I=1,NTY	700
9001 FORMAT (' PROGRAMM ZUR BERECHNUNG DER THERMISCHEN QUERSCHNITTE '/')	150	IF(TYP(I).EQ.X) GO TO 21	710
N(I)=3	160	IF(TYP(I).EQ.C) GO TO 21	720
CALL DOPW (8HBEST ,FEST(2))	170	IF(TYP(I).EQ.O) GO TO 21	730
CALL DOPW (8HTHERM ,A)	180	IF(TYP(I).NE.C) GO TO 20	740
CALL DOPW (8HSGF ,B)	190	21 LL=LL+1	750
CALL DOPW (8HSGA ,C)	200	IF(LL-4)20,22,22	760
CALL DOPW (8HSGC ,D)	210	20 CCNTINUE	770
CALL DOPW (8HALPHA ,P)	220	IF(LL-4)23,22,22	780
CALL DOPW (8HETA ,F)	230	23 WRITE(NOUT,25) MAT	790
CALL DOPW (8HNUE ,G)	240	25 FORMAT(1H0/' ***WARNING 10. 5 : THE GROUP CROSS SECTION SGT CAN NO	800
CALL DOPW (8HSGG ,H)	250	1T BE CALCULATED FOR ',A9/' BECAUSE THE REACTION TYPES SGN, SGA, SG	810
CALL DOPW (8HMUEL ,Z)	260	2I AND SG2N ARE NOT SPECIFIED IN THE INPUT')	820
CALL DOPW (8HSGN ,X)	270	22 DO 1 I=1,NTY	830
CALL DOPW (8HSGI ,O)	280	IF(TYP(I).EQ.U) GO TO 1	840
CALL DOPW (8HSG2N ,Q)	290	KSJK=0	850
CALL DOPW (8HSGT ,U)	300	IF(TYP(I).NE.P.AND.TYP(I).NE.F) GC TO 871	860
CALL DOPW (8HCHI ,R)	310	IF(LAR.EQ.O) GO TO 875	870
CALL DOPW (8HSGNCO ,SGNCO)	320	KSJK=1	880
CALL DOPW (8HPROBSGI ,PRSGI)	330	FEST(3)=H	890
FM=MAT	340	GC TO 872	900
IAR=0	350	875 WRITE(NOUT,876) MAT,TYP(I)	910
ISGT=0	360	876 FORMAT(1H0/' ***WARNING 10. 2 : THE GROUP CROSS SECTION FOR ',2A8,	920
IE=0	370	1' CAN NOT BE CALCULATED BECAUSE THE VALUE OF SGF IS ZERO')	930
SC=0.	380	GO TO 1	940
LL=0	390	874 KSJK=2	950
IF(IHC(1).EQ.IMP(1)) GO TO 802	400	FEST(3)=B	960
IF(IHC(1).NE.IMP(2)) GC TO 822	410	GC TO 872	970
802 LAR=1	420	879 KSJK=3	980
CC 803 JJ=1,NTY	430	FEST(3)=G	990
IF(TYP(JJ).EQ.C) GO TO 805	440	GC TO 872	1000
IF(TYP(JJ).NE.B) GO TO 803	450	871 FEST(3)=TYP(I)	1010
805 LL=LL+1	460	872 CALL NDFLOC (J,N,FEST,K,K)	1020
IF(LL-2)803,801,803	470	IF(J)2,2,3	1030
803 CCNTINUE	480		
IF(LL-2)807,801,807			

