

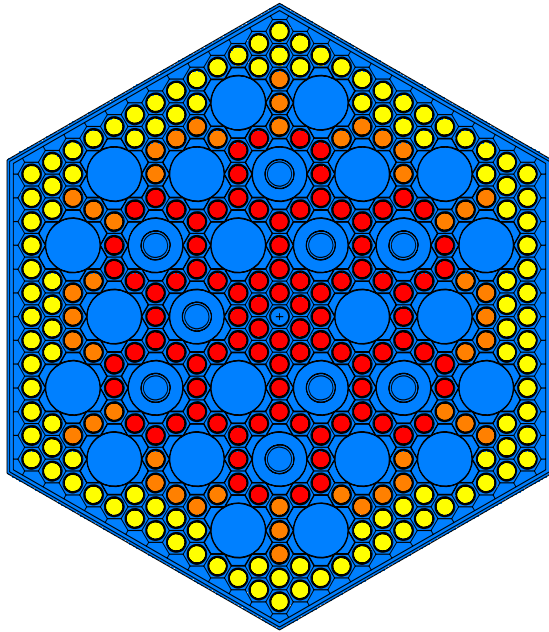
## **Validation of coupled neutron physics and thermal-hydraulic analysis for a high performance light water reactor (HPLWR)**

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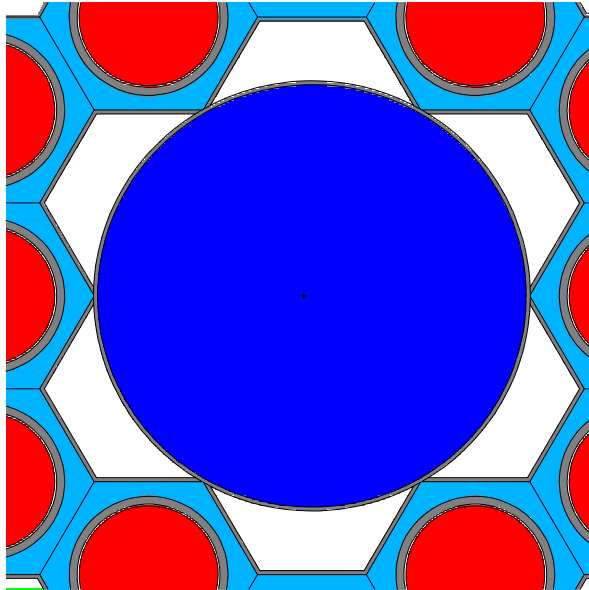
### ***Outline of presentation:***

- **Validation of neutron physics calculation tools and development of simplified fuel assembly models for neutron physics calculations**
- **Improvement and modeling of the thermal-hydraulic code RELAP5**
- **Coupling of the neutron physics and thermal-hydraulic codes and first results of coupled calculations**
- **Outlook**

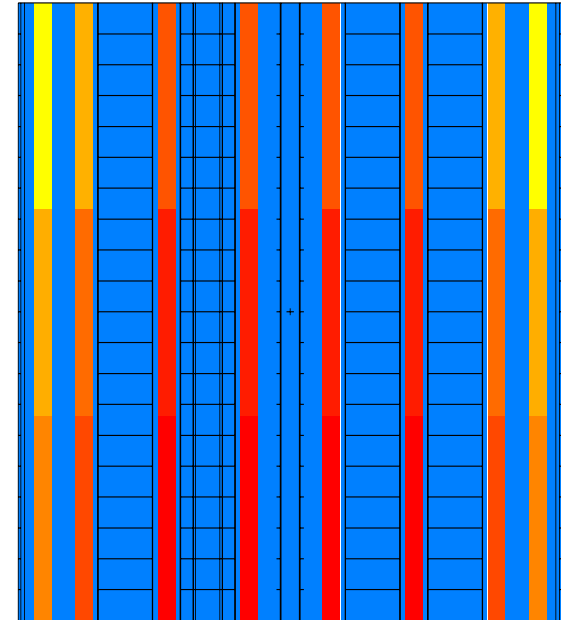
*Part of the work was funded in the 5. Framework Program of the European Community, contract number FIKI-CT-2000-00033.*



*Horizontal cross section*



*Close look to the water rod*



*Vertical cross section  
(not in scale)*

## Details of reference HPLWR fuel assembly design

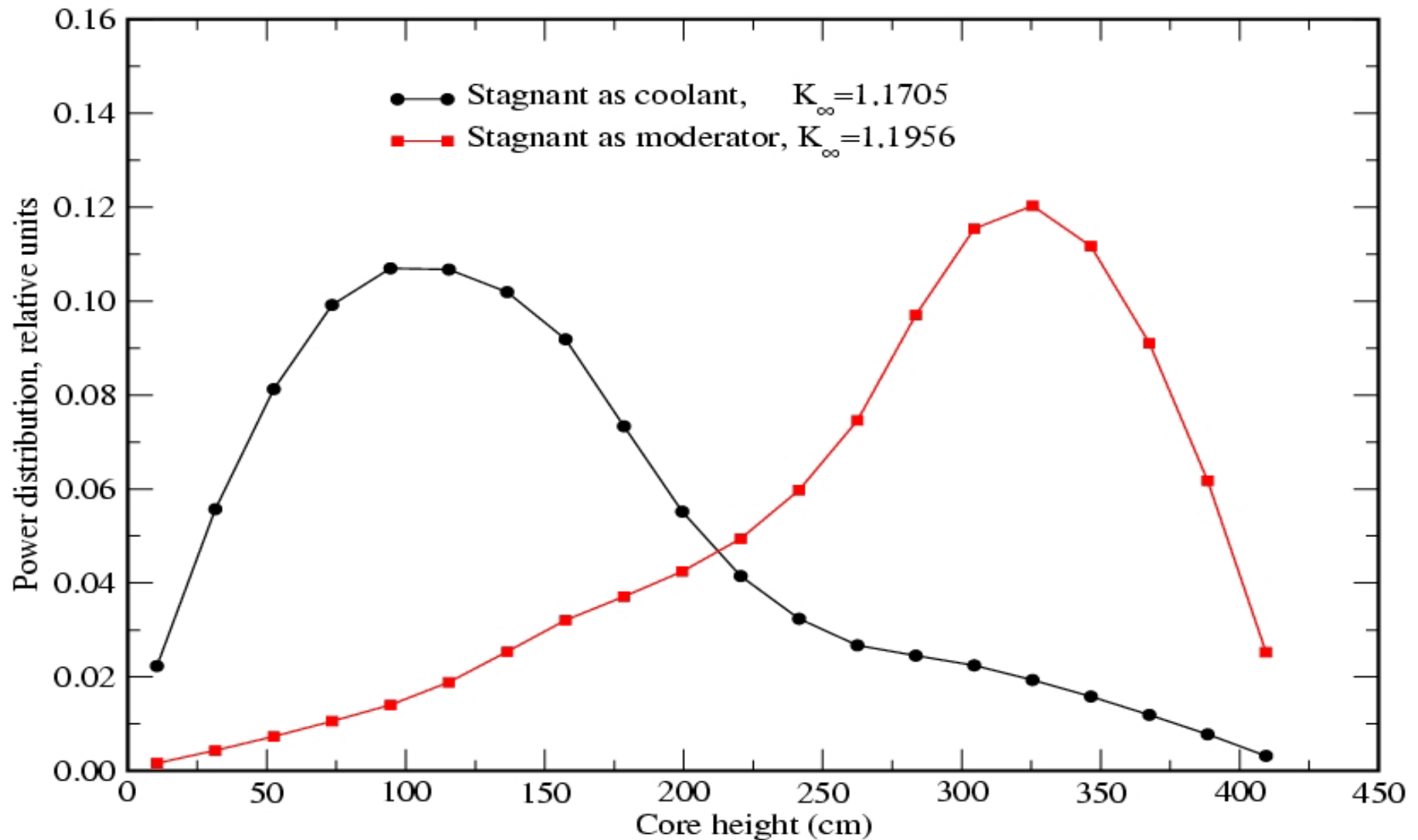
## **Development and validation of MCNP models at FZK**

- **MCNP models based on HPLWR reference design of EC project**
- **VTT 30<sup>0</sup> symmetry layout for 2-d slice model for comparisons**
- **First automatized input generation for 2-d slice model: FZK-S**
- **Second more compact 2-d model could be extended to 3-d: FZK-T**
- **Slightly modified FZK-T model for same modeling as VTT of guide tubes in moderator rods; FZK-Tmod**
- **Table of  $K_{\infty}$  results on separate slide**

Description	$K_{\infty}$
VTT geometry ( $30^0$ )	$1.1730 \pm 0.0006$
FZK-S model ( $360^0$ )	$1.1783 \pm 0.0005$
FZK-T model ( $360^0$ )	$1.1790 \pm 0.0010$
FZK-T-mod <sup>a</sup>	$1.1737 \pm 0.0006$

<sup>a</sup> same guide tube modelling as VTT

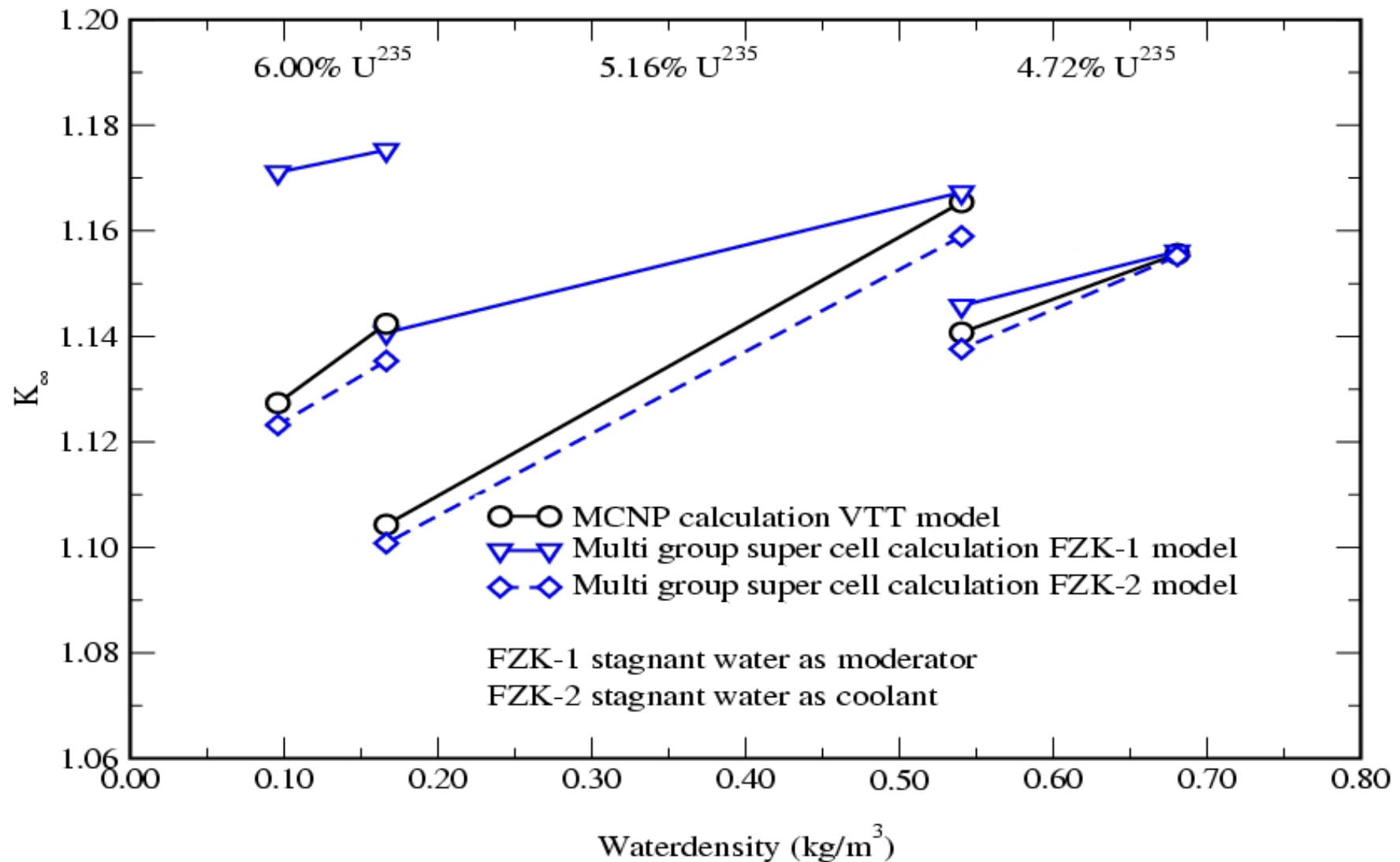
MCNP4C results based on temperature dependant libraries from VTT for different geometry models for HPLWR benchmark case 3



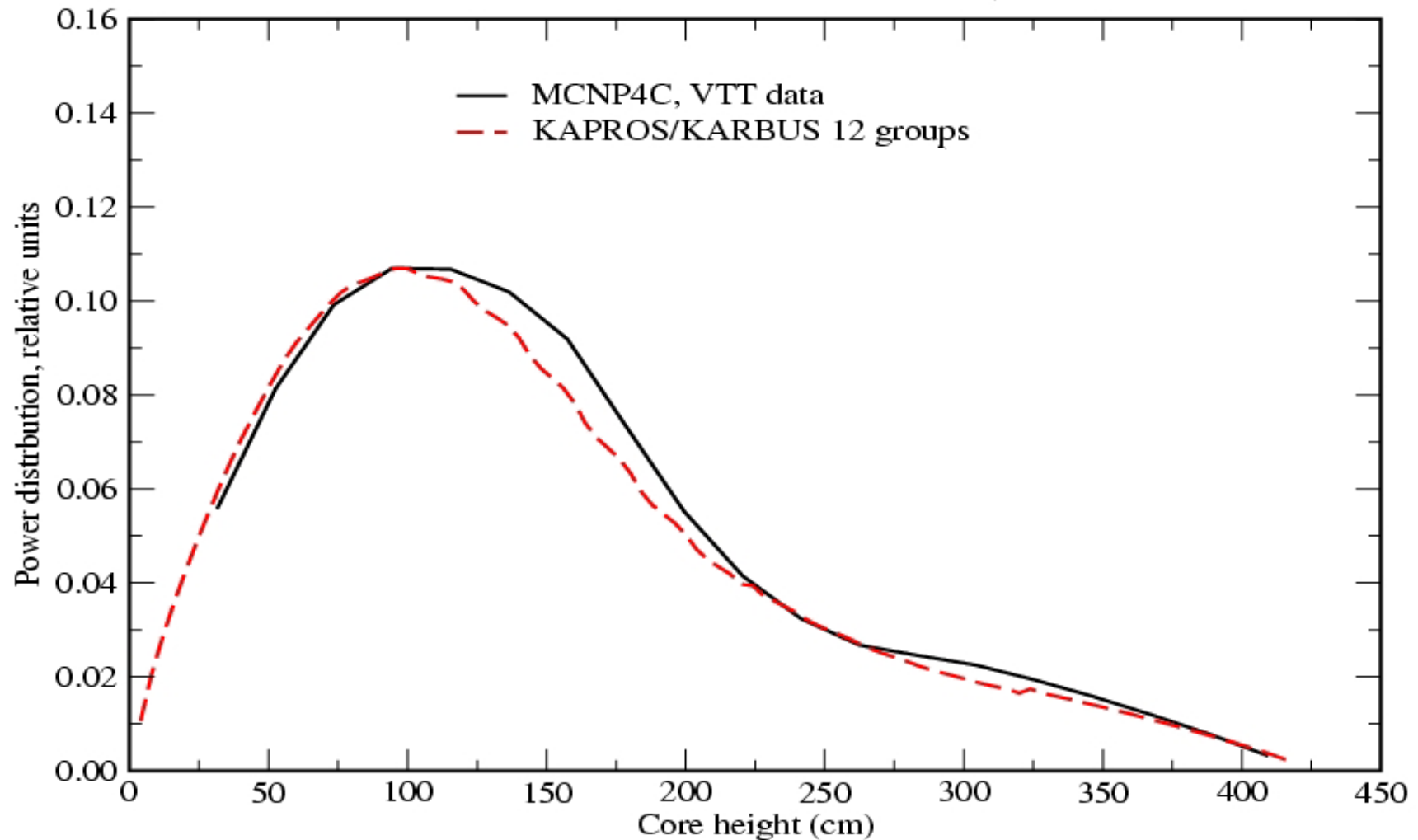
Comparison of MCNP results for axial power distributions for different treatment of stagnant water

## **Development of a cylinderized supercell FA model for HPLWR**

- **Supercell based on moderator rod surrounded by wrapper zone and equivalent fuel zone (FA structures smeared in fuel zone)**
- **Fuel zone cross sections from unit cell calculations**
- **Water characteristics in wrapper zone have large impact on reactivity results for 2-d supercell slice calculations**
- **3-D supercell calculations with 3 axial mean fuel enrichments show strong sensitivity to wrapper treatment; confirmation with MCNP calculations for axial power distributions**
- **Good agreement of axial power distributions of supercell multi-group and MCNP calculations for same densities and temperatures**



Comparison of  $K_{\infty}$  values for HPLWR fuel assembly slices from super-cell calculations with Monte Carlo results



**Comparison of axial power distributions in a HPLWR fuel assembly from deterministic and Monte Carlo calculations for the same material compositions and temperatures**

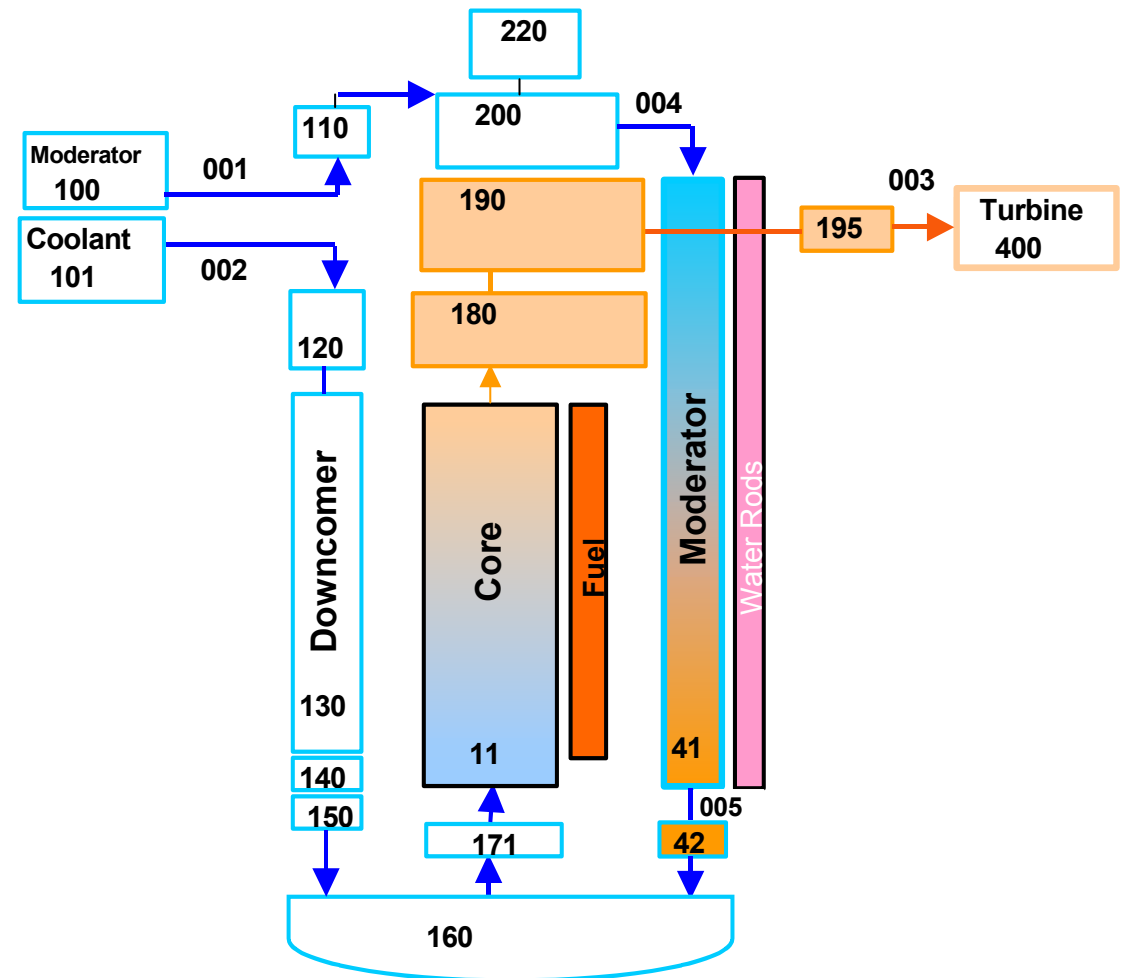


## **RELAP5-Appropriateness for HPLWR**

- **RELAP5-capability to simulate NPP operating at thermodynamically supercritical conditions checked (steady state conditions)**
  - Physical models (e.g. heat transfer, thermo-physical properties of steam, etc.)
  - Numeric (e.g. interpolation scheme around critical point)
- **RELAP5-Capability to different kind of transients checked:**
  - Operational transients
  - Accidents
- **Original RELAP5/MOD3.2.2 poorly predicted steady state conditions**
- **Performed code extensions (in cooperation with ISL)**
  - Refinement of interpolation point for the pressure and temperature around and above the critical point
  - Modification of two phase flow definitions for single phase supercritical water e.g. void fraction
- **Present status (RELAP5/MOD3.3):**
  - Good prediction of steady state conditions
  - Simulation of transients with depressurisation ( $P > P_{crit}$ ) possible
  - Simulation of LB-LOCA need further improvements and code validation
    - Modification of the interpolation scheme for the prediction of steam properties
    - Overall qualification of heat transfer correlations for wall/supercritical water, critical flow, etc.

## Simplified Model of the HPLWR-Plant

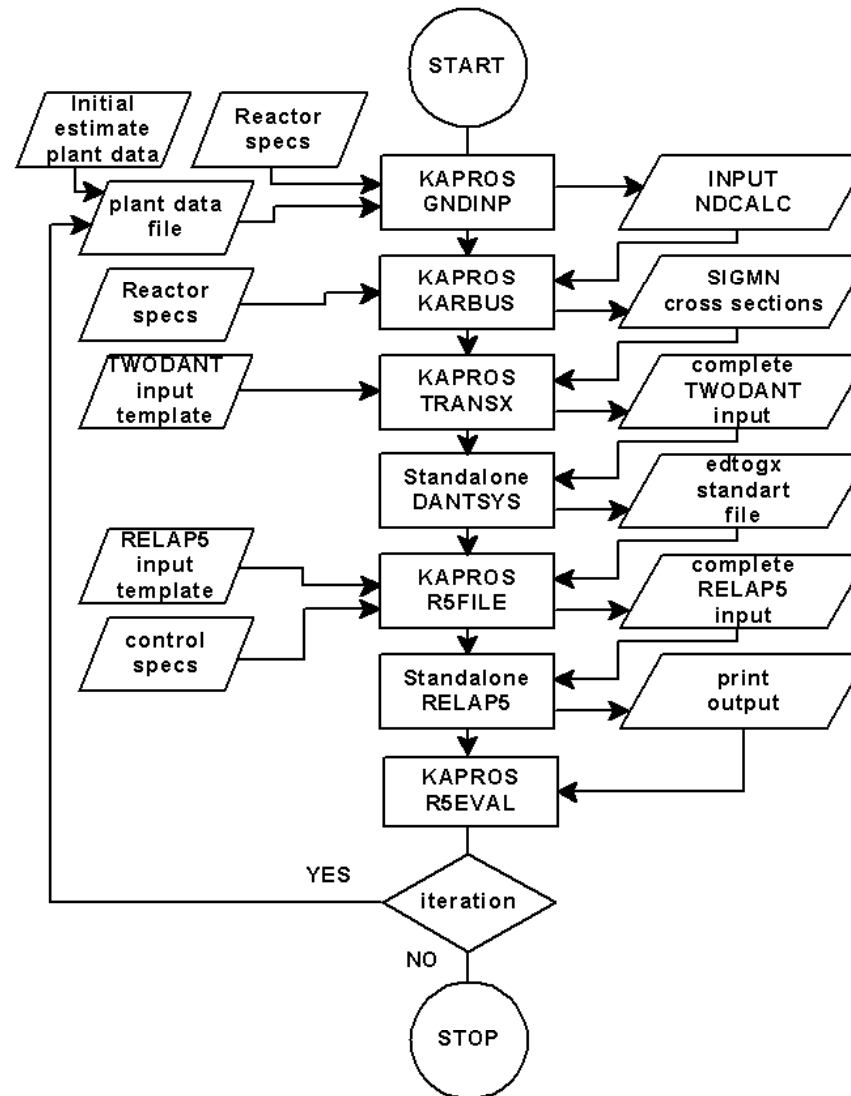
- **Direct cycle plant model**
  - Detail representation of the reactor pressure vessel (RPV)
  - Simplify representation of feed-water and steam lines
  - Two main flow stream within RPV: coolant and moderator
- **Core model**
  - Average fluid channel
  - Average heat structure
- **Moderator model**
  - One average fluid channel
  - One average heat structure



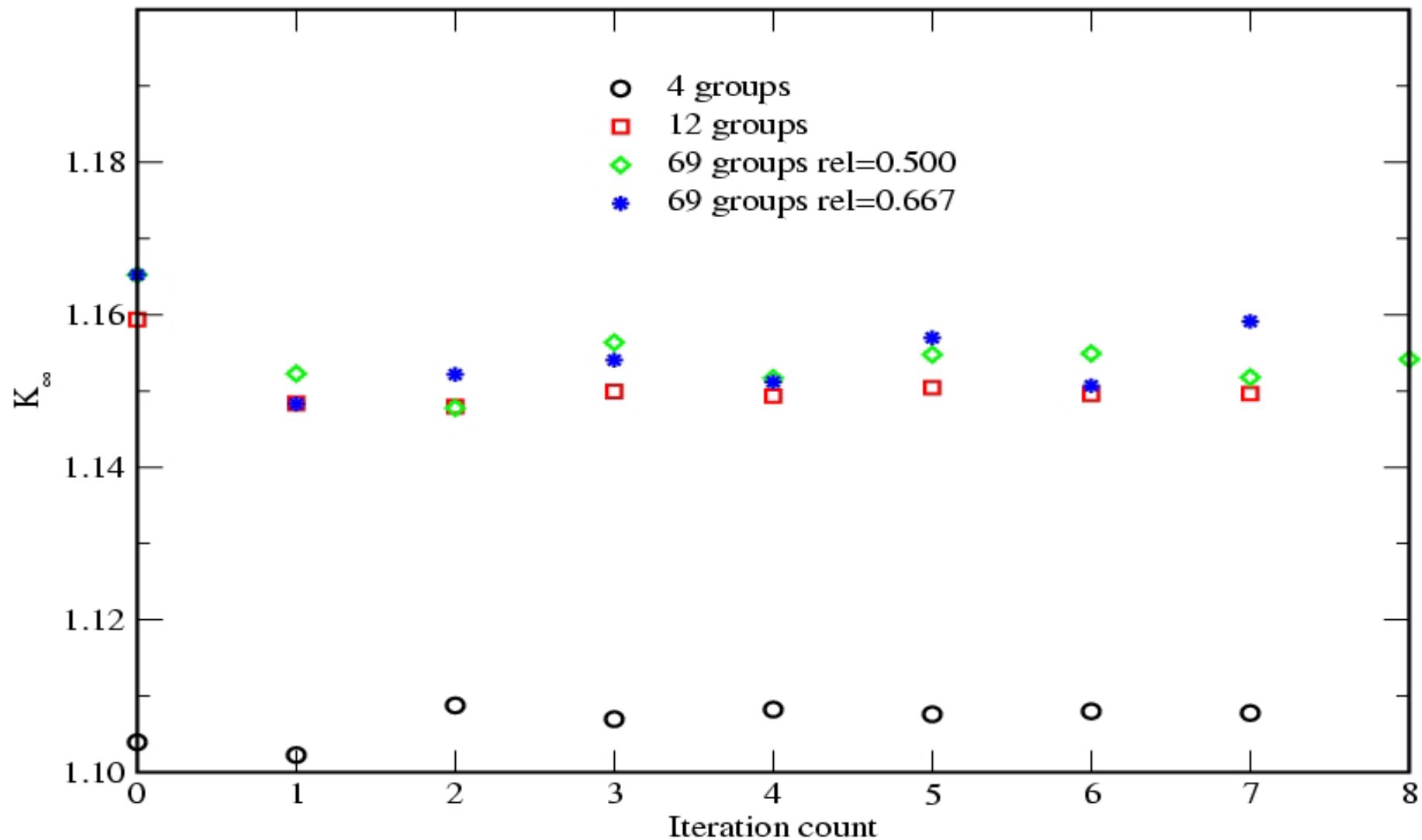
## **Current coupling of neutron physics and thermal-hydraulic codes**

- **Neutron physics code: KAPROS/KARBUS modular system developed at FZK with large efforts since mid-seventies:**
  - **Cross section generation with procedures developed and validated for Tight Lattice Light Water Reactor investigations**
  - **Supercell (R-Z) calculations with loosely to KAPROS coupled TWODANT transport code**
- **Thermal-hydraulic code: RELAP5 version improved at FZK for HPLWR investigations**
  - **Integral plant simulation**
  - **One channel core representation**

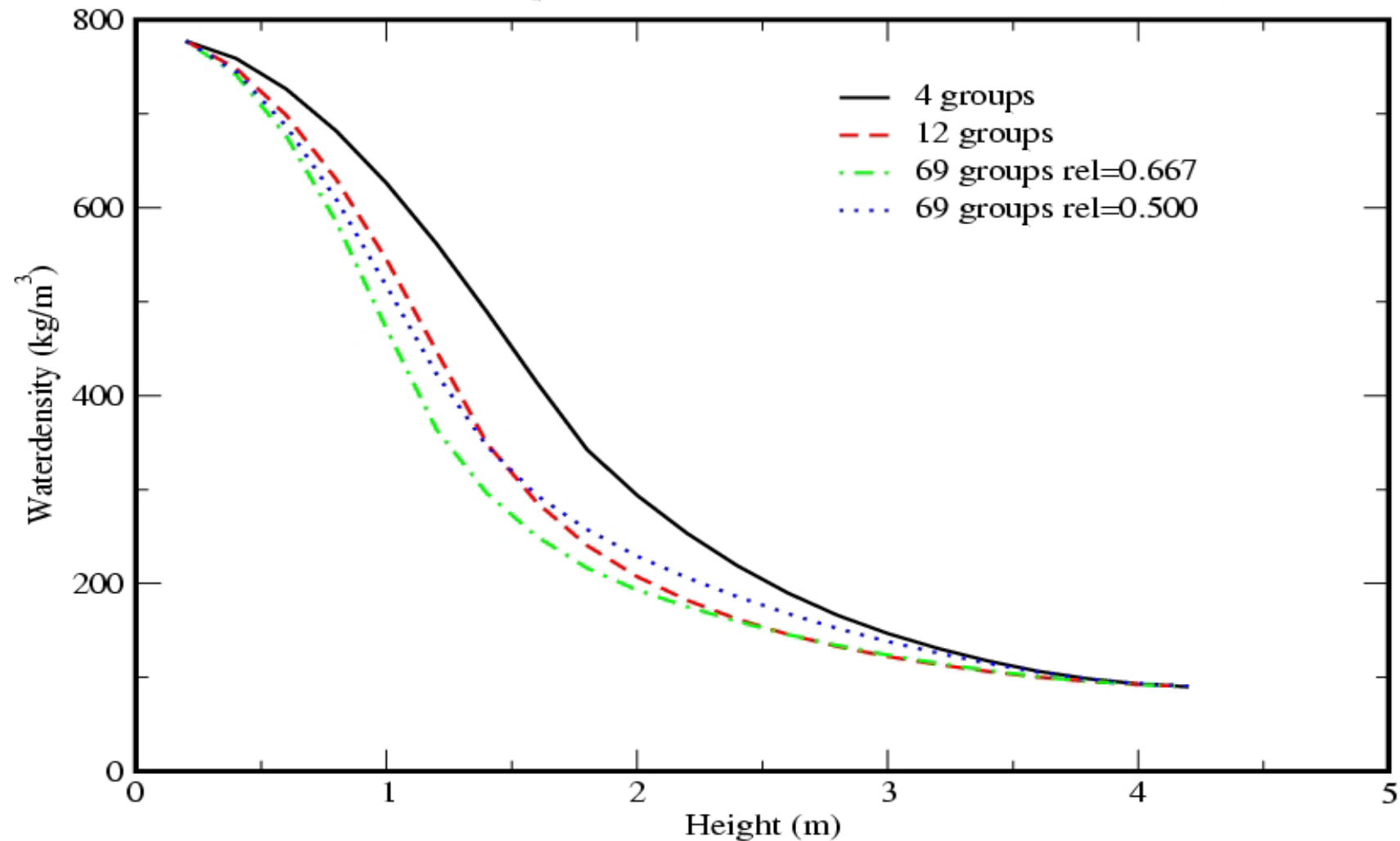
# Forschungszentrum Karlsruhe in der Helmholtz-Gemeinschaft



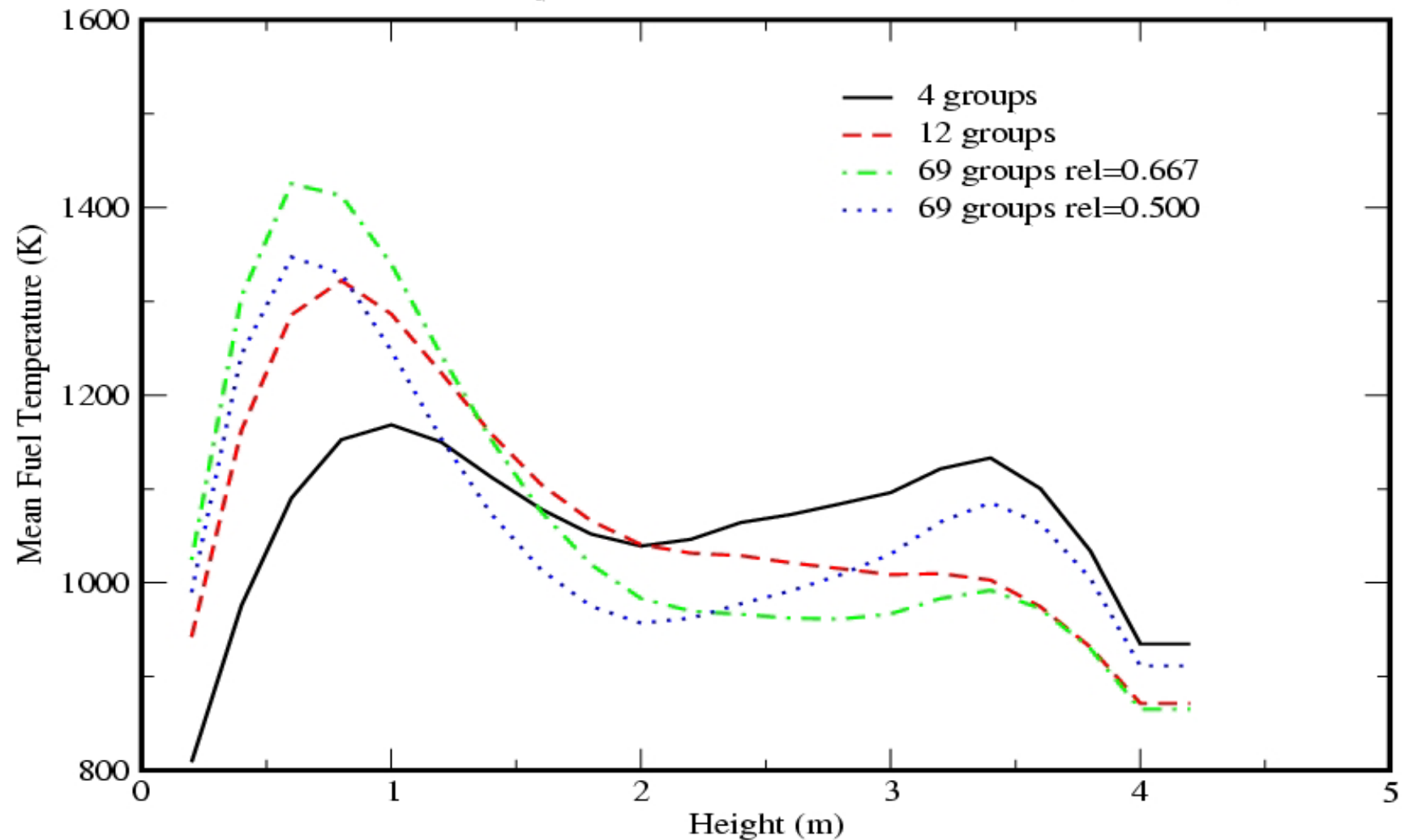
Procedure R5PROC for KARBUS / RELAP5 Coupling



Reactivity changes during iteration steps for coupled RELAP5/KARBUS calculations



Axial distributions of the water density after 8 iterations of coupled RELAP5/KARBUS system



Axial distributions of the mean fuel temperature after 8 iterations of coupled RELAP5/KARBUS system

*Outlook*

- The existing coupling within the KAPROS system easily may be modified to use other thermal-hydraulics fuel assembly codes
- Extension of the RELAP5 application to more core channels is possible but needs also the implementation of a new core model for the neutron physics calculation, including adequate cross section generation
- Determination of reactivity coefficients and burn-up effects needs full core calculations
- The complexity of the neutron physics and thermal-hydraulics calculations should be comparable with respect to geometrical approximations and CPU-times if possible